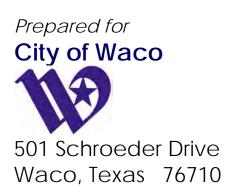
City of Waco Landfill
McLennan and Limestone Counties
TCEQ Permit No. MSW-2400
Parts III and IV, Volume 2 of 4

Administratively Complete



Prepared by:

SCS ENGINEERS

SCS Project No. 16216088.00 | Revision 0 – May 2020 and June 2020

1901 Central Drive, Suite 550 Bedford, Texas 76021 817.571.2288 City of Waco Landfill

VOLUME 2 OF 4

McLennan and Limestone Counties

TCEQ Permit No. MSW -2400

MSW Landfill Permit Application, Parts III and IV Table of Contents



SCS Engineers

TBPE Reg. # F-3407

TCEQ Core Data Form (TCEQ-10400)(Update)

TCEQ Part I Form for New Permit for a MSW Facility (TCEQ-0650)

Checklist for MSW Permits, Registrations, and Amendments (Parts III/IV only)

Part III Site Development Plan Narrative

Attachment 1 Site Layout Plans

Attachment 2 Fill Cross Sections

Attachment 3 Landfill Completion Plan

Attachment 4 Geology and Groundwater Report

VOLUME 3 OF 4

Attachment 5 Geotechnical/Stability Analysis
Attachment 6A Surface Water Drainage Plan

Attachment 6B Floodplain Evaluation

Attachment 6C Groundwater Protection Plan

VOLUME 4 OF 4

Attachment 7 Groundwater Sampling and Analysis Plan

Attachment 8 Closure and Post-Closure Care Cost Estimates

Attachment 9 Final Closure and Post-Closure Care Plan

Attachment 10 Soil and Liner Quality Control Plan

Attachment 11 Landfill Gas Management Plan

Attachment 12 Leachate and Contaminated Water Management Plan

Part IV Site Operating Plan



TCEQ Core Data Form

TCEQ Use Only

For detailed instructions regarding completion of this form, please read the Core Data Form Instructions or call 512-239-5175.

SECTION I: General Informatio	U							
	Reason for Submission (If other is checked please describe in space provided.)							
New Permit, Registration or Authorization (Core Data Form should be submitted with the program application.)								
	Renewal (Core Data Form should be submitted with the renewal form) Other Update to Sections II and III Information							
2. Customer Reference Number (if issu	ed) Fo	llow this link to	search	3. Regu	ulated Entity Referenc	e Number (if is	ssued)	
CN 600131940		r CN or RN nun entral Regi		RN	110471307			
SECTION II: Customer Informa	tion	cittai ixegi	<u> </u>					
4. General Customer Information	5. Effective Date f	for Customer I	nformatio	n Update	es (mm/dd/yyyy)			
New Customer Change in Legal Name (Verifiable with the Texas Secretary of State or Texas Comptroller of Public Accounts)								
The Customer Name submitted	d here may be up	odated auto	matical	lly base	ed on what is cur	rent and ac	tive with the	
Texas Secretary of State (SOS)	or Texas Comp	troller of P	ublic Ad	ccount	s (CPA).			
6. Customer Legal Name (If an individua	l, print last name first: ε	e.g.: Doe, John)		If new	Customer, enter previo	ous Customer b	<u>elow:</u>	
7. TX SOS/CPA Filing Number 8. TX State Tax ID (11 digits) 9. Federal Tax ID (9 digits) 10. DUNS Number (if applicable)								
11. Type of Customer: Corpora	tion	Individ	dual		Partnership: Genera	al Limited		
Government: X City County Federal	State Other	Sole F	Proprietors	ship	Other:			
12. Number of Employees			<u> </u>	13. Inc	dependently Owned a	nd Operated?		
0-20 21-100 101-250		501 and high		∐ Y∈				
14. Customer Role (Proposed or Actual)					ease check one of the fo	ollowing:		
Occupational Licensee Oper	rator onsible Party		& Operato ry Cleanu		ant Other:			
15 Mailian								
15. Mailing Address:								
City		State	Z	IP		ZIP + 4		
16. Country Mailing Information (if outside	e USA)	•	17. E-N	1ail Addre	ess (if applicable)	·		
				d@wad	cotx.gov			
18. Telephone Number	19. [Extension or C	ode		20. Fax Number	(if applicable)		
() -					() -			
SECTION III: Regulated Entity I	nformation							
21. General Regulated Entity Information	n (If `New Regulated	d Entity" is sele	cted belo	w this for	rm should be accompa	anied by a peri	mit application)	
<u> </u>	e to Regulated Entity		•		ted Entity Information			
The Regulated Entity Name so of organizational endings such	•	•	n order	to mee	t TCEQ Agency I	Data Standa	irds (removal	
22. Regulated Entity Name (Enter name			s taking pla	ice.)				

TCEQ-10400 (04/15) Page 1of 2

23. Street Address of the Regulated Entity:					4	
(No PO Boxes)	City	State		ZIP		ZIP + 4
24. County	,	0.0.0				1.20
	Enter Physical Lo	cation Description	n if no street	address is	provided.	
25. Description to Physical Location:						
26. Nearest City					State	Nearest ZIP Code
27. Latitude (N) In Decima	al:		28. Loi	ngitude (W) In Decimal:	
Degrees	Minutes S	Seconds	Degrees		Minutes	Seconds
29. Primary SIC Code (4 digi	ts) 30. Secondary SIC C	Code (4 digits)	31. Primary (5 or 6 digits)	y NAICS C		econdary NAICS Code 6 digits)
			100			
33. What is the Primary Bus	siness of this entity? (Do not	repeat the SIC or NA	CS description.)			
	201 Cohrander Drive					
34. Mailing	301 Schroeder Drive					
Address:	Tayar.		_			
	City Waco	State	TX	ZIP	76710	ZIP+4
35. E-Mail Address:	charlesd@wacotx.go				100 E 11 11	
36. Telepho	ne Number	37. Extens	ion or Code		38. Fax Numb	er (if applicable)
	•				()	
39. TCEQ Programs and ID Num Form instructions for additional guid	bers Check all Programs and write in lance.	n the permits/registra	tion numbers tha	t will be affect	ted by the updates subm	nitted on this form. See the Core Da
☐ Dam Safety	□ Districts	☐ Edwards /	Aquifer	Emis	sions Inventory Air	Industrial Hazardous Was
	☐ New Source Review Air	OSSF		Petrol	eum Storage Tank	☐ PWS
To Be Assigned						
Sludge	Storm Water	Title V Air		☐ Tire	S	☐ Used Oil
				1		
☐ Voluntary Cleanup	☐ Waste Water	Wastewate	er Agriculture	☐ Wat	er Rights	Other:
SECTION IV: Preparer	Information		1	1		
40. Name: Ryan R. Kuntz, F	0.0000000000000000000000000000000000000			11 Title:	Vice President	
1.7		AA Fau Niverk				
42. Telephone Number	43. Ext./Code	44. Fax Numb	2	1 1 2 2 X 1 X 1 X 1 X X	ail Address	
(817)358-6117	10: 1	(817)57	1 - 2188	RKuntz(c	scsengineers.com	
	ed Signature rtify, to the best of my knowledge ne entity specified in Section II, F					
Company: City of Waco	and the same and section (1)	/046/2-24/3/27 at 18		Job Title:	City Manager	AV. V. 10310, 8 21.
Name(In Print): Wiley Stem III				Phone:	(254)750]-564	5
Signature: Cule				Date:	05/21/20	

Facility Name: City of Waco Landfill Permittee/Registrant Name: City of Waco

MSW Authorization #:2400 Initial Submittal Date: 8/7/2018

Revision Date: 6/15/2020



Texas Commission on Environmental Quality Part I Form for New Permit/Registration and Amendment Applications for an MSW Facility

1.	Reason for Submittal				
	☐ Initial Submittal		ncy (NOD) Response		
2.	Authorization Type				
	□ Permit	Registration			
3.	Application Type				
	⊠ New	☐ Major Amendme	ent		
	☐ Major Amendment (Limited Scope)				
4.	Application Fees				
	☐ Pay by Check ☐ Online Payment				
	If paid online, e-Pay Confirmat	ion Number: 582EA	000311862		
_	Annliestien UDI				
5.	Application URL				
	Is the application submitted fo Yes No	r Type I Arid Exempt	(AE) and/or Type IV AE facility?		
		evisions to that applic			
6	Application Publishing				
<u> </u>		a Natica			
	Party Responsible for Publishin		⊠ Caracultant		
	Applicant Aç	gent in Service	○ Consultant		
	Contact Name: Ryan R. Kunt	z, P.E.	Title: Vice President /Project		
	Director				

Facility Name: City of Waco Landfill Initial Submittal Date: 8/7/2018 MSW Authorization #: 2400 Revision Date: 6/15/2020 7. Alternative Language Notice Is an alternative language notice required for this application? (For determination refer to Alternative Language Checklist on the Public Notice Verification Form TCEQ-20244-Waste) ☐ Yes \bowtie No 8. Public Place Location of Application Name of the Public Place: Waco-McLennan County Central Library Physical Address: 1717 Austin Avenue City: Waco County: McLennan State: TX Zip Code: 76701 (Area code) Telephone Number: 254.750.5941 9. Consolidated Permit Processing Is this submittal part of a consolidated permit processing request, in accordance with 30 TAC Chapter 33? ☐ Yes \boxtimes No ■ Not Applicable If "Yes", state the other TCEQ program authorizations requested: 10. Confidential Documents Does the application contain confidential documents? ☐ Yes \boxtimes No If "Yes", cross-reference the confidential documents throughout the application and submit as a separate attachment in a binder clearly marked "CONFIDENTIAL." 11. Permits and Construction Approvals Not Permit or Approval Received Pending **Applicable** Hazardous Waste Management Program under the П П \boxtimes Texas Solid Waste Disposal Act Underground Injection Control Program under the \boxtimes Texas Injection Well Act National Pollutant Discharge Elimination System Program under the Clean Water Act and Waste \bowtie Discharge Program under Texas Water Code, Chapter 26 Prevention of Significant Deterioration Program under the Federal Clean Air Act (FCAA). \boxtimes Nonattainment Program under the FCAA National Emission Standards for Hazardous Air

Research and Sanctuaries Act

Pollutants Preconstruction Approval under the FCAA
Ocean Dumping Permits under the Marine Protection

 \boxtimes

 \boxtimes

Permit or Approval	Received	Pending	Not Applicable		
Dredge or Fill Permits under the CWA					
Licenses under the Texas Radiation Control Act			\boxtimes		
Other (describe)					
Other (describe)					
Other (describe)					
Other (describe)					
12. General Facility Information					
Facility Name: City of Waco Landfill					
Contact Name: Charles Dowdell	Title	e: Directo	r of Solid		
Waste					
MSW Authorization No. (if available): 2400					
Regulated Entity Reference No. (if issued)*: RN11	0471307				
Physical or Street Address (if available): 4730 T K	Parkway				
City: Axtell County: McLennan & Limestone S	State: TX Zi	p Code: 7 6	6624		
(Area Code) Telephone Number: (254) 750-1601					
Latitude (Degrees, Minutes Seconds): N 31° 42' C	5.31"				
Longitude (Degrees, Minutes Seconds): W 96° 55	52.07"				
Benchmark Elevation (above mean sea level):	ft.				
Provide a description of the location of the facility with respect to known or easily identifiable landmarks: approximately 0.4 mile south of the intersection of TK Parkway and State Highway 31 in McLennan County					
Detail access routes from the nearest United States or state highway to the facility: approximately 0.4 mile south of the intersection of TK Parkway and State Highway 31 in McLennan County					
*If this number has not been issued for the facility, complete a TCEQ Core Data Form (TCEQ-10400) and submit it with this application. List the Facility as the Regulated Entity.					
13. Facility Type(s)					

5 51 , ,			
⊠ Type I □ Type I AE	☐ Type IV ☐ Type IV AE	☐ Type V ☐ Type VI	
14. Activities Cond	ucted at the Facility		
☐ Storage	☐ Processing	□ Disposal	

15. Facility Waste Management Uni	t(s)
∠ Landfill Unit(s)	☐ Incinerator(s)
☐ Class 1 Landfill Unit(s)	☐ Autoclave(s)
☐ Process Tank(s)	Refrigeration Unit(s)
☐ Storage Tank(s)	☐ Mobile Processing Unit(s)
☐ Tipping Floor	☐ Type VI Demonstration Unit
☐ Storage Area	☐ Compost Pile(s) and/or Vessel(s)
☐ Container(s)	☐ Other (Specify)
☐ Roll-off Boxes	☐ Other (Specify)
Surface Impoundment	Other (Specify)

16. Description of Proposed Facility or Changes to Existing Facility

Provide a brief description of the proposed activities if application is for a new facility, or the proposed changes to an existing facility or permit conditions if the application is for an amendment.

Proposed Type I Municipal Solid Waste Landfill located on 502.5 acres of land in McLennan and Limestone Counties, designed in accordance with Title 30, Texas Administrative Code, Chapter 330. The primary purpose of this landfill is to serve as a replacement for the current City of Waco landfill (MSW Permit No. 948A). The landfill will provide disposal capacity for residences, businesses, and industries primarily in the communities of McLennan and Limestone Counties and other nearby counties. The landfill will provide disposal of household waste, yard waste, commercial waste, Class 2/3 non-hazardous industrial wastes, C/D waste, and special wastes authroized by TCEQ. Includes submittal of Parts III and IV of the permit application.

Site Operator (Permittee/Registrant) Name: City of Waco Customer Reference No. (if issued)*: CN600131940 Contact Name: Charles Dowdell Title: Director of Solid Waste Mailing Address: 501 Schroeder Drive City: Waco County: McLennan State: TX Zip Code: 76710 (Area Code) Telephone Number: (254) 750-1601 Email Address: charlesd@wacotx.gov TX Secretary of State (SOS) Filing Number: *If the Site Operator (Permittee/Registrant) does not have this number, complete a TCEQ Core Data Form (TCEQ-10400) and submit it with this application. List the Site Operator (Permittee/Registrant) as the Customer.

	Operator Name ¹ : same as Permittee							
	Customer Reference No. (if issued)*:							
	Contact Name:		Tit	le:				
	Mailing Address:							
	City: Coun	ty:	State:	Zip	Code:			
	(Area Code) Telepho	one Numbe	r:					
	Email Address:							
	TX SOS Filing Numb	er:						
		t have this nu	mber, comple	te a TCEQ Co		· Operator (Permittee/Registrant)". rm (TCEQ-10400) and submit it		
	Consultant Name	(if applica	ble): SCS	Engineer	s, TBPE	Registration No. F-3407		
	Texas Board of Prof	essional En	gineers Firr	n Registrat	tion Num	nber:		
	Contact Name: Ryan R. Kuntz, P.E. Title: Vice Pres., Pr. Director							
	Mailing Address: 19	901 Centra	al Drive, S	uite 550				
	City: Bedford Cou	unty: Tarra	ant State:	TX Zip C	ode: 76	021		
	(Area Code) Telepho	one Numbe	r: 817.35	8.6117				
	E-Mail Address: rk i	untz@scse	ngineers.d	com				
	Agent in Service N	Name (req	uired only	for out-o	f-state)	:		
	Mailing Address:							
	City: Coun	ty:	State:	Zip	Code:			
	(Area Code) Telepho	one Numbe	r:					
	E-Mail Address:							
18	. Facility Supervis	or's Licens	se					
	Select the Type of License that the Solid Waste Facility Supervisor, as defined in 30 TAC Chapter 30, Occupational Licenses and Registrations, will obtain prior to commencing facility operations.							
	☐ Class B							
10	Overnous bis Chair	o of the F	acilit.					
19	. Ownership Statu	is of the Fa	acility					
	☐ Corporation		nited Partne	•	_	eral Government		
			y Governm		_	er Government		
	☐ Sole Proprietorsh	·	unty Gover		∐ Milit			
	General Partners	ship Sta	ate Governr	nent	∐ Othe	er (Specify):		

Facility Name: City of Waco Landfill

MSW Authorization #: 2400

Initial Submittal Date: 8/7/2018

Revision Date: 6/15/2020

Does the Site Operator (Permittee/Registrant) own all the facility units and all the facility property?

☑ Yes ☐ No

If "No", provide the information requested below for any additional ownership.

Owner Name:

Street or P.O. Box:

City: County: State: Zip Code:

(Area Code) Telephone Number:

Email Address (optional):

20. Other Governmental Entities Information

Texas Department of Transportation District: Waco

District Engineer's Name: **Stanley Swiatek, P.E.**Street Address or P.O. Box: **100 S. Loop Drive**

City: Waco County: McLennan State: TX Zip Code: 76704-2858

(Area Code) Telephone Number: (254) 867-2700

E-Mail Address (optional):

The Local Governmental Authority Responsible for Road Maintenance (if applicable): N.A.

Contact Person's Name:

Street Address or P.O. Box:

City: County: State: Zip Code:

(Area Code) Telephone Number:

E-Mail Address (optional):

City Mayor Information

City Mayor's Name: **Kyle Deaver** Office Address: **300 Austin Ave**

City: Waco County: McLennan State: TX Zip Code: 76702

(Area Code) Telephone Number: **(254) 750-5750**E-Mail Address (optional): **kyle.deaver@wcotx.gov**

City Health Authority: Waco-McLennan County Public Health District

Contact Person's Name: **Dr. Brenda Gray, Director**Street Address or P.O. Box: **225 W. Waco Drive**

City: Waco County: McLennan State: TX Zip Code: 76707

(Area Code) Telephone Number: (254) 750-5450

E-Mail Address (optional):

Facility Name: City of Waco Landfill

MSW Authorization #: 2400

Initial Submittal Date: 8/7/2018

Revision Date: 6/15/2020

County Judge Information

County Judge's Name: Scott M. Felton

Street Address or P.O. Box: **501 Washington Ave, Room 214**City: **Waco** County: **McLennan** State: **TX** Zip Code: **76701**

(Area Code) Telephone Number: (254) 757-5049

E-Mail Address (optional):

County Health Authority: Waco-McLennan County Public Health District

Contact Person's Name: E. Farley Verner, M.D.

Street Address or P.O. Box: **7030 New Sanger Road, Suite 202**City: **Waco** County: **McLennan** State: **TX** Zip Code: **76712**

(Area Code) Telephone Number: **(254) 855-9790**E-Mail Address (optional): **farleyverner@gmail.com**

State Representative Information

District Number: 12

State Representative's Name: Kyle Kacal

District Office Address: 3000 Briarcrest Dr., Ste 203

City: Bryan County: Brazos State: TX Zip Code: 77802

(Area Code) Telephone Number: 979-774-7276

E-Mail Address (optional):

State Senator Information

District Number: 22

State Senator's Name: **The Honorable Brian Birdwell** District Office Address: **900 Austin Ave, Suite 500**

City: Waco County: McLennan State: TX Zip Code: 76701

(Area Code) Telephone Number: (254) 772-6225

E-Mail Address (optional):

Council of Government (COG) Name: Heart of Texas

COG Representative's Name: Falen Bohannon

COG Representative's Title: Solid Waste Program Manager

Street Address or P.O. Box: 1514 S. New Road

City: Waco County: McLennan State: TX Zip Code: 76711

(Area Code) Telephone Number: (254)292-1800

E-Mail Address (optional): Falen.Bohannon@hot.cog.tx.us

Facility Name: City of Waco Landfill

MSW Authorization #: 2400

Initial Submittal Date: 8/7/2018

Revision Date: 6/15/2020

County Judge Information

County Judge's Name: Limestone County Judge: Honorable Richard Duncan

Street Address or P.O. Box: 200 W. State ST., Ste 101

City: Groesbeck County: Limestone State: TX Zip Code: 76642

(Area Code) Telephone Number: 254-729-3810

E-Mail Address (optional):

County Health Authority: Limestone Medical Center

Contact Person's Name: Dr. Jeffrey Rettig

Street Address or P.O. Box: 204 W. Trinity Street

City: Groesbeck County: Limestone State: TX Zip Code: 76642

(Area Code) Telephone Number: 254-729-3740

E-Mail Address (optional):

State Representative Information

District Number: 12

State Representative's Name: Kyle Kacal

District Office Address: 3000 Briarcrest Dr., Ste 203

City: Bryan County: Brazos State: TX Zip Code: 77802

(Area Code) Telephone Number: 979-774-7276

E-Mail Address (optional):

State Senator Information

District Number: 5

State Senator's Name: Charles Schwertner

District Office Address: 3000 Briarcrest Drive, Suite 202

City: Bryan County: Brazos State: TX Zip Code: 77802

(Area Code) Telephone Number: 979-776-0222

E-Mail Address (optional):

Council of Government (COG) Name: Heart of Texas

COG Representative's Name: Falen Bohannon

COG Representative's Title: Solid Waste Program Manager

Street Address or P.O. Box: 1514 S. New Road

City: Waco County: McLennan State: TX Zip Code: 76711

(Area Code) Telephone Number: (254)292-1800

E-Mail Address (optional): Falen.Bohannon@hot.cog.tx.us

River Basin Authority Name: Brazos River Authority						
Contact Person's Name: Phil Ford						
Watershed Sub-Basin Name:						
Street Address or P.O. Box: 4600 Cobbs Drive						
City: Waco County: McLennan State: TX Zip Code: 76710						
(Area Code) Telephone Number: (888) 922-6272						
E-Mail Address (optional):						
Coastal Management Program						
Is the facility within the Coastal Management Program boundary?						
☐ Yes No						
U.S. Army Corps of Engineers						
The facility is located in the following District of the U.S. Army Corps of Engineers:						
☐ Albuquerque, NM ☐ Galveston, TX						
Local Government Jurisdiction						
Within City Limits of:						
Within Extraterritorial Jurisdiction of:						
Is the facility located in an area in which the governing body of the municipality or county has prohibited the storage, processing or disposal of municipal or industrial solid waste?						
☐ Yes						
(If "Yes", provide a copy of the ordinance or order as an attachment):						

Facility Name: City of Waco Landfill MSW Authorization #: 2400

Initial Submittal Date: 8/7/2018

Revision Date: 6/15/2020

Signature Page

(Site Operator (Permittee/Registrant)'s Authorized Signatory) certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowling violations. Signature: Date: €-16-3.0 **TO BE COMPLETED BY THE OPERATOR IF THE APPLICATION IS SIGNED BY AN AUTHORIZED REPRESENTATIVE FOR THE OPERATOR I, hereby designate (Print or Type Representative Name) as my representative and hereby authorize said representative to sign any application, submit additional information as may be requested by the Commission; and/or appear for me at any hearing or before the Texas Commission on Environmental Quality in conjunction with this request for a Texas Water Code or Texas Solid Waste Disposal Act permit. I further understand that I am responsible for the contents of this application, for oral statements given by my authorized representative in support of the application, and for compliance with the terms and conditions of any permit which might be issued based upon this application. Printed or Typed Name of Operator or Principal Executive Officer Signature SUBSCRIBED AND SWORN to before me by the said Wiley Sylem TITO On this Light day of Light		I, Wiley Stem III	City Manager,				
my direction or Supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware there are significant penalties for submitting false information, including the possibility of fine and Imprisonment for knowing violations. Signature: Date: 6-16-20 TO BE COMPLETED BY THE OPERATOR IF THE APPLICATION IS SIGNED BY AN AUTHORIZED REPRESENTATIVE FOR THE OPERATOR I, hereby designate (Print or Type Representative Name) as my representative and hereby authorize said representative to sign any application, submit additional information as may be requested by the Commission; and/or appear for me at any hearing or before the Texas Commission on Environmental Quality in conjunction with this request for a Texas Water Code or Texas Solid Waste Disposal Act permit. I further understand that I am responsible for the contents of this application, for oral statements given by my authorized representative in support of the application, and for compliance with the terms and conditions of any permit which might be issued based upon this application. Printed or Typed Name of Operator or Principal Executive Officer Signature SUBSCRIBED AND SWORN to before me by the said Wileu Sylem TIL On this Light day of Light d		(Site Operator (Permittee/Registrant)'s Authorized Signatory)	(Title)				
REPRESENTATIVE FOR THE OPERATOR I,		personnel properly gather and evaluate the information submitte the person or persons who manage the system, or those persons gathering the information, the information submitted is, to the be belief, true, accurate, and complete. I am aware there are signif submitting false information, including the possibility of fine and inviolations.	d to assure that qualified d. Based on my inquiry of directly responsible for est of my knowledge and icant penalties for imprisonment for knowing				
(Print or Type Operator Name) (Print or Type Representative Name) as my representative and hereby authorize said representative to sign any application, submit additional information as may be requested by the Commission; and/or appear for me at any hearing or before the Texas Commission on Environmental Quality in conjunction with this request for a Texas Water Code or Texas Solid Waste Disposal Act permit. I further understand that I am responsible for the contents of this application, for oral statements given by my authorized representative in support of the application, and for compliance with the terms and conditions of any permit which might be issued based upon this application. Printed or Typed Name of Operator or Principal Executive Officer Signature SUBSCRIBED AND SWORN to before me by the said Wiley Stem TT On this Was day of Wash, 2022 My commission expires on the 3/3 day of Mash, 2022 Notary Public in and for Notary Public, State of Texas Comm. Expires 03-31-2022	A'	TO BE COMPLETED BY THE OPERATOR IF THE APPLICATION IS STREPRESENTATIVE FOR THE OPERATOR	IGNED BY AN AUTHORIZED				
submit additional information as may be requested by the Commission; and/or appear for me at any hearing or before the Texas Commission on Environmental Quality in conjunction with this request for a Texas Water Code or Texas Solid Waste Disposal Act permit. I further understand that I am responsible for the contents of this application, for oral statements given by my authorized representative in support of the application, and for compliance with the terms and conditions of any permit which might be issued based upon this application. Printed or Typed Name of Operator or Principal Executive Officer Signature SUBSCRIBED AND SWORN to before me by the said Wiley Sylem TII On this 14th day of 14th day of 15th day of March, 2022 My commission expires on the 31st day of March, 2022 Notary Public in and for Notary Public. State of Texas Comm. Expires 03-31-2022		I,, hereby designate (Print or Type Operator Name) (Print or Type Repre	esentative Name)				
Signature SUBSCRIBED AND SWORN to before me by the said Wiley Stem III On this		submit additional information as may be requested by the Commission; and/or appear for me at any hearing or before the Texas Commission on Environmental Quality in conjunction with this request for a Texas Water Code or Texas Solid Waste Disposal Act permit. I further understand that I am responsible for the contents of this application, for oral statements given by my authorized representative in support of the application, and for compliance with the terms and conditions of any permit which might be issued based upon					
SUBSCRIBED AND SWORN to before me by the said Wiley Stem TT On this		Printed or Typed Name of Operator or Principal Executive Officer					
On this		Signature					
Notary Public In and for Notary Public, State of Texas Comm. Expires 03-31-2022		On this 10th day of June, 2020	em III				
		Makennan County, Texas	Notary Public, State of Texas Comm. Expires 03-31-2022				

Facility Name: City of Waco Landfill Initial Submittal Date: 8/7/2018

MSW Authorization #: 2400 Revision Date: 6/15/2020

Part I Attachments

(See Instructions for P.E. seal requirements.)

Required Attachments	Attachment No.
Supplementary Technical Report	X
Property Legal Description	X
Property Metes and Bounds Description	X
Facility Legal Description	X
Facility Metes and Bounds Description	X
Metes and Bounds Drawings	X
On-Site Easements Drawing	X
Land Ownership Map	X
Land Ownership List	X
Electronic List or Mailing Labels	X
Texas Department of Transportation (TxDOT) County Map	X
General Location Map	X
General Topographic Map	X
Verification of Legal Status	X
Property Owner Affidavit	X
Evidence of Competency	X
Additional Attachments as Applicable- Select all those apply and ac	dd as necessary
□ TCEQ Core Data Form(s)	X
Signatory Authority Delegation	X
☐ Fee Payment Receipt	X
☐ Confidential Documents	
☐ Waste Storage, Processing and Disposal Ordinances	
☐ Final Plat Record of Property	
☐ Certificate of Fact (Certificate of Incorporation)	
Assumed Name Certificate	

CHECKLIST FOR MSW PERMITS, REGISTRATIONS, AND AMENDMENTS (PARTS III/IV ONLY)

Administrative and Technical Review Checklist for Municipipal Solid Waste (MSW) Permits, Registrations and Amendments

This checklist is designed to provide guidance for the Municipal Solid Waste (MSW) rules found in Title 30 Texas Administrative Code (30 TAC) Chapter 330, for Type I, IV and V registration, permit, and permit amendment applications. Areas of the checklist that are shaded in gray are for information purposes only.

Please fill out application information before selecting and filling out a checklist.

	Applicant Information					
First name:	Charles					
Applicant Title:	Director of Solid Wast	te	Prefix:			
Company:	City of Waco					
Street Address:	501 Schroeder Drive					
City:	Waco	State: Texas	Zipcode:	76701		
	Co	onsultant Information				
First name:	Ryan	Last name:	Kuntz			
Consultant Title:	Vice President		Prefix:			
Consultant Firm:	SCS Engineers					
Consultant Address:	1901 Central Drive, S	uite 550				
City:	Bedford	State: Texas	Zipcode:	76021		
	Ap	plication Information				
Facility Name:	City of Waco Landfill					
Application Date	May	13 2020				
CN:	600131940		MSW ID: 2400			
RN:	110471307	Authorization Type:	Permit			
County:	McLennan	Application Type:	New Permit	i		

Disclaimer: This checklist is intended for use as a reference in the application process and will not be considered a substitute for required application materials. Rules referenced have been paraphrased or reworded to facilitate this process. Any conflict or questions regarding rule interpretation should be directed to TCEQ for determination, and disputes will be resolved in favor of the exact language of rules, statutes or federal requirements. Should any dispute occur in an administrative proceeding, the applicant will bear the burden of proof of compliance with any and all applicable TCEQ and federal statutes, rules, or policies and procedures. This checklist is subject to discovery in administrative and civil legal proceedings and should not be considered confidential from the public.

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
266	Part III	Describe facility access control features	Required	330.63(b)(1)	Yes	Drawings 1.1 and 1.5		General Facility Design
267	Part III	Submit a process design for the facility [that includes items 330.63(b)(2)(A) through 330.63(b)(2)(I)]	Required	330.63(b)(2)	Yes	Drawings 1.1 and 1.5		General Facility Design
268	Part III	storage, processing, and disposal sequences for such type of waste and/or feedstock/recyclable. Submit a schematic view drawing(s) showing	Required	330.63(b)(2)(A)	No		Not Applicable	General Facility Design
269	Part III	phases for collection, separation and processing/disposal of each type of waste and/or feedstock/recyclable material	Required	330.63(b)(2)(B)	Yes	Drawing 1.2		General Facility Design
270	Part III	Provide ventilation & odor control measures for each unit	Required	330.63(b)(2)(C)	No		Not Applicable	General Facility Design
271	Part III	Provide construction details of storage, processing units & components, dimensions, capacity, materials used, etc.	Required	330.63(b)(2)(D)	No		Not Applicable	General Facility Design
272	Part III	Provide performance data for all storage and processing units and ancillary equipment	Required	330.63(b)(2)(D)	No		Not Applicable	General Facility Design
281	Part III	Provide adequate floor drains and/or sumps	Required	330.63(b)(3)(D)	No		Not Applicable	General Facility Design
282	Part III	Describe proper disposal of liquids resulting from waste processing, cleaning, and washing and provide for the treatment of waste water	Required	330.63(b)(4)	No		Not Applicable	General Facility Design
283	Part III	Describe how facility will be designed to protect endangered species	Required	330.63(b)(5)	Yes	Part I/II, Section 12, Paragraph 2, and see coordination letters to TPWD and USFWS in Appendix I/IIA.		General Facility Design
284	Part III	Acknowledge that the facility design complies with the requirements of 30 TAC 330.303(a) - (b)	Acknowledgement	330.63(c)	Yes	Attachment 6A, Section 1		Surface Water Drainage Report
285	Part III	Submit a surface water and drainage report that is in accordance with 30 TAC, Chapter 330, Subchapter G	Required	330.63(c)	Yes	Attachment 6A		Surface Water Drainage Report
286	Part III	Demonstrate that existing or permitted drainage patterns will not be adversely altered	Required	330.305(a)	Yes	Attachment 6A, Section 5.4		Surface Water Drainage Report
287	Part III	Provide a design of the run-on control system to prevent 25 yr. storm run-on to active face	Required	330.305(b)	Yes	Attachment 12, Section 2.3, Paragraph 1; Appendix 12C and Drawing 12C.1		Surface Water Drainage Report
288	Part III	Provide a design for run-off management system to, at a minimum, collect & control run-off at the active face from a 24 hr. 25 yr. storm event	Required	330.305(c)	Yes	Attachment 12, Section 4 and Drawing 6A.2		Surface Water Drainage Report
289	Part III	Provide erosion control of top dome & external embankment side slope surfaces during life and post-closure care of facility	Required	330.305(d)	Yes	Attachment 6A, Section 6		Surface Water Drainage Report
290	Part III	Demonstrate estimated peak velocities for top surfaces and external embankment slopes to be less than the permissible non-erodible velocities under similar conditions	Required	330.305(d)(1)	Yes	Attachment 6A, Section 6.4 and 6.5, Appendix 6A.E		Surface Water Drainage Report
291	Part III	Provide a design for top surfaces and external embankment slopes to minimize erosion and not exceed the permissible soil loss	Required	330.305(d)(2)	Yes	Drawings 6A.3, 6A-E1, 6A-E2, 6A-E3, 6A-E4, and 6A-E5		Surface Water Drainage Report

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
292	Part III	Provide a design for drainage features, sizing and grading to prevent erosion, long term, low maintenance geotechnical stability to the final cover	Required	330.305(e)	Yes	Attachment 6A, Section 2.2.2, and Drawings 6A-12 and 6A-13		Surface Water Drainage Report
293	Part III	Describe maintenance and repair procedures of the collection, drainage, and/or storage units	Required	330.305(e)(1)	Yes	Attachment 6A, Section 6.7		Surface Water Drainage Report
294	Part III	Provide interim erosion controls for phased development	Required	330.305(e)(2)	Yes	Attachment 6A, Section 6.1		Surface Water Drainage Report
295	Part III	Provide drainage calculations using Rational Method for areas 200 acres or less	Required	330.305(f)(1)	Yes	Attachment 6A, Section 2.2.2.1, Appendix 6A-E		Surface Water Drainage Report
296	Part III	Provide drainage calculations using w/ HEC Modeling Systems or equivalent for areas > 200 acres	Required	330.305(f)(2)	Yes	Attachment 6A, Section 2.1, Appendix 6A-A		Surface Water Drainage Report
297	Part III	Acknowledge that handling, storage, treatment, & disposal of contaminated surface or groundwater should be per 330.207	Acknowledgement	330.305(g)	Yes	Attachment 6A, Section 6.2.3, last bullet; Attachment 15, Sections 4 & 5		Surface Water Drainage Report
298	Part III	Provide designs for contaminated water storage units	Required	330.305(g)	Yes	Attachment 6A, Section 6.2.3, last bullet; Attachment 12, Sections 4		Surface Water Drainage Report
299	Part III	Provide drainage area drawing(s) & calculations	Required	330.63(c)(1)(A)	Yes	Drawings 6A.1A, 6A.1B, and 6A.2		Surface Water Drainage Report
300	Part III	Submit drainage area designs to include cross- sections for drainage facilities within the facility area	Required	330.63(c)(1)(B)	Yes	Drawings 6A.3, 6A.4, 6A.5, 6A.6, 6A.7, and 6A.8		Surface Water Drainage Report
301	Part III	Submit drainage area designs to include ditch grades	Required	330.63(c)(1)(B)	Yes	Drawings 6A.4, 6A.5, 6A.6, 6A.7, and 6A.8		Surface Water Drainage Report
302	Part III	Submit drainage area designs to include water flow rates, elevations, velocities, and flow line elevations	Required	330.63(c)(1)(B)	Yes	Appendix 6A-E		Surface Water Drainage Report
303	Part III	Submit calculations verifying drainage patterns will not be adversely altered	Required	330.63(c)(1)(C)	Yes	Attachment 6A, Section 5.4, and Appendix 6A-D		Surface Water Drainage Report
304	Part III	Submit and identify hydrologic method & calculations used to estimate peak flow rates and run-off volumes	Required	330.63(c)(1)(D)	Yes	Attachment 6A, Section 2.1		Surface Water Drainage Report
305	Part III	Submit and identify the 25-year rainfall intensity used for facility design including the source of the data	Required	330.63(c)(1)(D)(i)	Yes	Attachment 6A, Section 2.1.1.3, Appendix 6A-A		Surface Water Drainage Report
306	Part III	Submit and identify the 25-year rainfall intensity used for facility design including all other data used in conjunction with the selected hydrologic method. Their sources should be documented and described	Required	330.63(c)(1)(D)(i)	Yes	Appendix 6A-A		Surface Water Drainage Report
307	Part III	Submit and identify hydraulic calculations and designs for sizing the necessary collection, drainage, and/or detention facilities	Required	330.63(c)(1)(D)(ii)	Yes	Appendix 6A-A (basins) Appendix 6A-E (swales, downchutes,channels)		Surface Water Drainage Report
308	Part III	Submit a discussion and analyses to demonstrate that existing drainage patterns will not be adversely altered as a result of the proposed landfill development	Required	330.63(c)(1)(D)(iii)	Yes	Attachment 6A, Section 5, Appendix 6A-D		Surface Water Drainage Report
309	Part III	Submit structural designs of the collection, drainage, and/or storage facilities	Required	330.63(c)(1)(D)(iv)	Yes	Attachment 6A, Section 6.2.2 & 6.2.3, Drawings 6A.9, 6A.10, 6A.11, 6A.12, 6A.13, 6A.14		Surface Water Drainage Report

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
310	Part III	Provide the location for the facility to identify whether the site is located within a 100-year floodplain. Indicate the 100-year floodplain on the drawing listed in paragraph 330.63(c)(1)(A) of this subsection	Required	330.63(c)(2)(A)	Yes	Attachment 6B and Drawing 6B.1		Surface Water Drainage Report
311	Part III	Provide the source of all data for flood plain determination. The boundaries of the proposed landfill facility should be shown on the floodplain map	Required	330.63(c)(2)(B)	Yes	Attachment 6B, Section 2		Surface Water Drainage Report
312	Part III	Provide (if the site is located within the 100-year floodplain) information detailing the specific flooding levels. If the Preliminary Plan approval is not required under Chapter 301 of this title and Section 16.236 of Texas Water Code you may indicate that the checklist items relevant to Chapter 301 are not applicable.	Required	330.63(c)(2)(C)	No		Not Applicable	Surface Water Drainage Report
313	Part III	The facility shall be protected from flooding by suitable levees constructed to provide protection from a 100-year frequency flood and in accordance with the rules of the commission relating to levee improvement districts and approval of plans for reclamation projects or the rules of the county or city having jurisdiction under Texas Water Code, §16.236, as implemented by Chapter 301, Subchapter C of this title (relating to Approval of Levees and Other Improvements)	Informational	330.307(a)				Surface Water Drainage Report
314	Part III	Provide maps, plats, drawings, computations and narratives of landfill levees; the applicant should submit a detailed map	Required if Requested	301.33(a)(1)	No		Not Applicable	Surface Water Drainage Report
315	Part III	Provide the name and course of the river, stream, or other watercourse, which is associated with or would be affected by the proposed project	Required if Requested	301.33(a)(2)	No		Not Applicable	Surface Water Drainage Report
316	Part III	Provide the location & ownership of existing levees, channels, dams, etc. that may be affected	Required if Requested	301.33(a)(3)	No		Not Applicable	Surface Water Drainage Report
317	Part III	Provide the location and ownership, including current mailing address of owners, and location, shown by map, of all properties lying within any proposed protected area	Required if Requested	301.33(a)(4)(A)	No		Not Applicable	Surface Water Drainage Report
318	Part III	Provide a list of potentially affected property owners for notice adjacent to the proposed works or which may be affected by the project's alteration of the flood flows of the stream	Required if Requested	301.33(a)(4)(B)	No		Not Applicable	Surface Water Drainage Report
319	Part III	Provide a project design based on a statistical 100-year flood as a minimum. Flood level data available from state or federal agencies or other sources shall be provided for consideration in the selection of design flood frequency and elevation	Required if Requested	301.33(b)(1)	No		Not Applicable	Surface Water Drainage Report

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
320	Part III	Provide plans to demonstrate the effects the proposed project will impose on existing flood conditions. This shall be illustrated by floodwater surface-elevation profiles and design-flood delineations of the floodplain with and without the project in place	Required if Requested	301.33(b)(2)	No		Not Applicable	Surface Water Drainage Report
321	Part III	Provide additional flood water surface-elevation profiles and design-flood delineations of the floodplain with the project in place and with a comparable levee or landfill on the opposite site of the stream if such do not exist	Required if Requested	301.33(b)(3)	No		Not Applicable	Surface Water Drainage Report
322	Part III	Submit plans for levees that include structural integrity	Required if Requested	301.34(1)	No		Not Applicable	Surface Water Drainage Report
323	Part III	Submit plans that show compatibility with existing hydraulic conditions.	Required if Requested	301.34(2)	No		Not Applicable	Surface Water Drainage Report
324	Part III	Submit a design that any proposed levee or other improvement will not increase flooding or divert waters in such a way that any person's life or property will be endangered or subjected to significantly increased flooding	Required if Requested	301.34(3)	No		Not Applicable	Surface Water Drainage Report
325	Part III	The rights of third parties affected by a proposed levee or other improvement must be considered	Informational	301.34(4)				Surface Water Drainage Report
326	Part III	The commission and the executive director shall assure that, as far as possible, levees or other improvements shall be designed with primary consideration to the topographic and hydrographic conditions, and in such a manner that each division of a project shall be a complete, united project forming a coordinate part of an ultimately finished series of projects, so constituted that the successful operation of each united project shall coordinate with the successful operation of other projects within the same hydraulic influence	Informational	301.34(5)				Surface Water Drainage Report
327	Part III	Provide a minimum freeboard of three feet above the 100-year design flood hydraulic gradient where levees furnish protection for urbanized or developing areas	Required if Requested	301.34(6)	No		Not Applicable	Surface Water Drainage Report
328	Part III	levees must not significantly restrict the flow of a 100-year frequency flood nor significantly reduce the temporary water storage capacity of the 100-year floodplain	Informational	330.307(b)(2)				Surface Water Drainage Report
329	Part III	The executive director may request any additional pertinent information from the applicant	Required if Requested	301.35	No		Not Applicable	Surface Water Drainage Report
330	Part III	Submit plans with PE design, signed & sealed	Required if Requested	301.36	No		Not Applicable	Surface Water Drainage Report
331	Part III	Submit, if constructed in a floodplain, the Preliminary Plan approval (along with the submitted application) from the governmental entity with jurisdiction under Texas Water Code, §16.236, as implemented by Chapter 301	Required if Requested	330.63(c)(2)(D)(i)	No		Not Applicable	Surface Water Drainage Report

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
337	Part III	Provide a design to control and contain spills and contaminated water from leaving the facility. Unenclosed containment areas shall also account for precipitation from a 25-year, 24- hour rainfall event	Required	330.63(d)(1)(B)	No		Not Applicable	Waste Management Unit Design
338	Part III	Provide the maximum amount of time processed and unprocessed waste are to remain on site	Required	330.63(d)(1)(C)	No		Not Applicable	Waste Management Unit Design
339	Part III	Submit an estimate of the amount and planned method for testing and final disposal of incinerator ash, and an estimate of the volume and method of treatment for process water	Required	330.63(d)(2)	No		Not Applicable	Waste Management Unit Design
340	Part III	Provide design specifications; including a plan view and a cross-section for surface impoundments	Required	330.63(d)(3)(A)	No		Not Applicable	Waste Management Unit Design
341	Part III	Provide a design that maintains the minimum freeboard and the basis of the design to prevent overtopping from a 25-year, 24-hour rainfall event	Required	330.63(d)(3)(B)	No		Not Applicable	Waste Management Unit Design
342	Part III	Provide a liner quality control plan for surface impoundments per 30 TAC 330.339	Required	330.63(d)(3)(C)	No		Not Applicable	Waste Management Unit Design
343	Part III	Provide all-weather operation during wet weather. Include interior access road locations and the type of surfacing on a facility plan. Provide control to minimize the tracking of mud onto the public road	Required	330.63(d)(4)(A)	Yes	Part III, Section 3.2		Waste Management Unit Design
344	Part III	Provide the landfill method proposed (e.g., moving-face cell trench, area fill, etc.)	Required	330.63(d)(4)(B)	Yes	Part III, Section 3.1		Waste Management Unit Design
345	Part III	Provide the elevation of deepest excavation, maximum elevation of waste, and maximum elevation of final cover	Required	330.63(d)(4)(C)	Yes	Part III, Section 3.1		Waste Management Unit Design
346	Part III	Provide a calculation for the estimated rate of solid waste deposition and operating life of the landfill unit	Required	330.63(d)(4)(D)	Yes	Part III, Section 2.2 and Appendix IIIA		Waste Management Unit Design
347	Part III	Provide cross-sections showing the top of the levee, top of the proposed fill, and top of the wastes	Required	330.63(d)(4)(E)	Yes	Part III, Section 3.1 and Attachment 2		Waste Management Unit Design
348	Part III	Provide sufficient number of cross-section w/ inset key map showing maximum elevation of proposed fill, existing ground, bottom of the excavations, and side slopes of trenches and fill areas	Required	330.63(d)(4)(E)	Yes	Attachment 2, Drawings 2.2, 2.3, 2.4		Waste Management Unit Design
349	Part III	Provide sufficient number of cross-section w/ inset key map gas vents or wells, groundwater monitoring wells, initial and static levels of any groundwater encountered	Required	330.63(d)(4)(E)	Yes	Attachment 4, Drawings 4C.2, 4C.3, 4C.4, 4C.5, 4C.6, 4C.7		Waste Management Unit Design
350	Part III	Provide sufficient number of cross-section w/ inset key map showing the top of the levee, top of the proposed fill, top of the wastes, maximum elevation of proposed fill, existing ground, bottom of the excavations, side slopes of trenches and fill areas, gas vents or wells, groundwater monitoring wells, initial and static levels of any groundwater encountered	Required	330.63(d)(4)(E)	Yes	Attachment 2, Drawings 2.2, 2.3, 2.4; and Attachment 4, Drawings 4C.2, 4C.3, 4C.4, 4C.5, 4C.6, 4C.7		Waste Management Unit Design

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
351	Part III	Provide cross-sections so as to accurately depict the existing and proposed depths of all fill areas within the site. The fill cross-sections shall go through or very near the soil borings in order to show boring logs on the profile.	Required	330.63(d)(4)(E)	Yes	Attachment 2, Drawings 2.2, 2.3, 2.4		Waste Management Unit Design
352	Part III	Provide cross-sections to depict construction and design details of proposed compacted perimeter or toe berms and aerial-fill waste disposal areas	Required	330.63(d)(4)(F)	Yes	Attachment 2, Drawings 2.2, 2.3, 2.4, and Drawings 6A.4, 6A.5, 6A.6, 6A.7, and 6A.8		Waste Management Unit Design
353	Part III	Submit a Liner Quality Control Plan, prepared by a PE to include construction methods, engineering practices & the installation & testing of geomembrane (if used)	Required	330.63(d)(4)(G)	Yes	Attachment 10		Waste Management Unit Design
354	Part III	Submit a liner design for Type I units constructed that ensures that the concentration values listed in Table 1 (Figure: 30 TAC§330.331(a)(1)) will not be exceeded in the uppermost aquifer at the point of compliance	Required	330.331(a)(1)	Yes	Part III, Section 3.5.2		Waste Management Unit Design
355	Part III	Submit a liner design constructed with a composite liner, and a leachate collection system that is designed and constructed to maintain less than a 30-centimeter depth of leachate over the liner	Required	330.331(a)(2)	Yes	Part III, Section 3.5.2 and 3.5.3		Waste Management Unit Design
356	Part III	Submit a liner design that considers the hydrogeologic characteristics of the facility and surrounding land	Required	330.331(c)	Yes	Part III, Section 3.5.2		Waste Management Unit Design
357	Part III	Submit a liner design that considers the climatic factors of the area	Required	330.331(c)	Yes	Part III, Section 3.5.2		Waste Management Unit Design
358	Part III	Submit for a liner design that considers the volume and physical and chemical characteristics of the leachate	Required	330.331(c)	Yes	Part III, Section 3.5.2		Waste Management Unit Design
359	Part III	Submit for a liner design that considers the quantity, quality, and direction of flow of groundwater	Required	330.331(c)	Yes	Part III, Section 3.5.2		Waste Management Unit Design
363	Part III	Submit for a liner design that considers the public health, safety, and welfare effects; and	Required	330.331(c)	Yes	Part III, Section 3.5.2		Waste Management Unit Design
364	Part III	Submit for a liner design that considers the practicable capability of the owner or operator.	Required	330.331(c)	Yes	Part III, Section 3.5.2		Waste Management Unit Design
365	Part III	Submit a design for a liner system that includes at least four feet of in-situ soil between the deposited waste and groundwater. This in-situ soil liner must meet all the physical properties for a constructed liner as detailed in §330.339(c)(5) of this title (relating to Liner Quality Control Plan)	Required	330.331(d)(1)	No		Not Applicable	Waste Management Unit Design

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
366	Part III	Submit a design for a liner system that includes at least a three-foot thick re-compacted clay liner between the deposited waste and groundwater. The constructed liner must meet all the criteria detailed in §330.339	Required	330.331(d)(2)	No		Not Applicable	Waste Management Unit Design
367	Part III	Submit a design for a liner system that includes an alternative liner system, in accordance with §330.335 of this title (relating to Alternative Liner Design).	Required if Requested	330.331(d)(3)	No		Not Applicable	Waste Management Unit Design
368	Part III	Landfill units that accept Class 1 industrial solid wastes, other than asbestos-containing material, must provide dedicated cells that meet the requirements prescribed under 30 TAC 330.331(e) through (e)(2)(C)	Informational	330.331(e)			Not Applicable	Waste Management Unit Design
369	Part III	Demonstrate location compliance for a new landfill cell or an aerial expansion of an existing landfill cell as prescribed under 335.584(b)(1) and (2) relating to Location Restrictions.	Required if Requested	330.331(e)(3)	No		Not Applicable	Waste Management Unit Design
370	Part III	Provide a design for a leachate-collection and associated leachate-removal systems to be constructed of materials that are chemically resistant to the leachate expected to be generated	Required	330.333	Yes	Part III, Section 3.5.3, and Attachment 12, Section 3.4, and Appendix 12D		Waste Management Unit Design
371	Part III	Provide a design for a leachate-collection and associated leachate-removal systems to be constructed of sufficient strength and thickness to prevent collapse under the pressures exerted by overlying wastes, waste cover materials, and by any equipment used at the landfill	Required	330.333	Yes	Part III, Section 3.5.3, and Attachment 12, Section 3.3, and Appendix 12B		Waste Management Unit Design
372	Part III	Provide a design for a leachate-collection and associated leachate-removal systems to be designed and operated to function through the scheduled closure and post-closure care period of the landfill considering the factors prescribed under 30 TAC 330.333(A) through (G)	Required	330.333(A)-(G)	Yes	Attachment 12		Waste Management Unit Design
373	Part III	Submit an alternative liner designs that include a leachate management system, a demonstration by computerized design modeling that the maximum contaminant levels detailed in 30 TAC §330.331 of this title (relating to Design Criteria), Table 1 will not be exceeded at the point of compliance		330.335	No		Not Applicable	Waste Management Unit Design
374	Part III	Type IV landfills may be required to meet one or more provisions under 330.337 at ED's discretion	Informational	330.337(a)			Not Applicable	Waste Management Unit Design
375	Part III	Submit calculations to demonstrate that the weight of liner & any ballast will offset uplift by a factor of 1.2	Required	330.337(b)(1)	Yes	Attachment 10, Sections 2.5, 3.6, 11.5 and Appendix 10C and 10D.		Waste Management Unit Design

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
376	Part III	Submit calculations to demonstrate that an active or passive dewatering system will reduce hydrostatic forces by a factor of 1.2	Required	330.337(b)(2)	Yes	Attachment 10, Sections 2.5, 3.6, 11.5 and Appendix 10C and 10D.		Waste Management Unit Design
377	Part III	Provide evidence to demonstrate that the soil surrounding the facility is so poorly permeable that GW cannot exert force on liner	Required if Requested	330.337(b)(3)	Yes	Attachment 10, Section 2.5.2		Waste Management Unit Design
378	Part III	Submit evidence that the seasonal high GW is below planned excavation	Required if Requested	330.337(b)(4)	No		See Attachment 10, Section 2.5, which includes a "so poorly permeable demonstration. Additionally, the liner design (see Attachment 10) includes consideration for short- and long-term groundwater controls.	Dogian
379	Part III	Provide for liner stability during filling through dewatering &/or ballasting approved by ED	Required	330.337(c)	Yes	Attatchment 10, Section 2.5.1 and Appendix 10D	Not Applicable	Waste Management Unit Design
380	Part III	Provide a leachate collection system capable of handling leachate and groundwater inflow. Submit the calculations for maximum GW inflow	Required	330.337(d)	Yes	Attachment 12, Section 3	Design for groundwater inflow into the leachate collection system for this landfill is not applicable.	Waste Management Unit Design
381	Part III	Provide a foundation evaluation that considers the stability, settlement, and constructability prior to excavating below the seasonal high water table	Required	330.337(e)	Yes	Attachment 5		Waste Management Unit Design
382	Part III	Provide a liner quality control plan to include methods & tests to verify liner will not uplift during construction & ballast placement	Required	330.337(f)(1)	Yes	Attachment 10, Section 11.5		Waste Management Unit Design
383	Part III	Provide measurements & test results verifying that the ballast meets criteria including inspections, compaction, weight, density, thickness, & top elevation	Required	330.337(f)(2)	Yes	Attachment 10, Section 11.5		Waste Management Unit Design
384	Part III	Provide designs for any dewatering systems used for liner construction and filling, and indicate that the system will be operated until the ED determines it is no longer required	Required if Requested	330.337(g)	No		Not Applicable	Waste Management Unit Design
385	Part III	Submit (if waste is to be used as ballast) an operating plan that provides for no brush or large items in first 5 ft. of thickness	Required if Requested	330.337(h)(1)	Yes	Attachment 10, Section 11.5		Waste Management Unit Design
386	Part III	Provide (if waste is to be used as ballast) for the use of a 40,000 lb. compactor or equivalent to achieve a 1,200 lbs. per cubic yard density	Required if Requested	330.337(h)(2)	Yes	Attachment 10, Section 11.5		Waste Management Unit Design
387	Part III	Submit (if waste is to be used as ballast) methods for verifying waste as ballast compaction density not less than 1200 lbs. per cubic yard, No method is required if a 40,000 lb. compactor is used	Required if Requested	330.337(h)(3)	Yes	Attachment 10, Section 11.5		Waste Management Unit Design
388	Part III	Submit a ballast evaluation report that verifies the use of a 40,000 lb. compactor or that 1,200 lbs. per cubic yard density was achieved and must be sufficient to offset hydrostatic forces by a factor of 1.5	Required if Requested	330.337(h)(4)	Yes	Attachment 10, Section 11.5		Waste Management Unit Design
389	Part III	Provide for the adjustment of seasonal high water table, if necessary, as new data is collected	Required	330.337(i)	Yes	Attachment 4, Section 11		Waste Management Unit Design

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
390	Part III	Acknowledge that a ballast evaluation report will be submitted upon completion of placement. If ED does not respond within 14 days, discontinue dewatering or ballasting	Acknowledgement	330.337(j)	Yes	Attachment 10, Section 11		Waste Management Unit Design
391	Part III	Acknowledge that a ballast evaluation report will be submitted to verify that the liner did not undergo uplift	Acknowledgement	330.337(j)(1)	Yes	Attachment 10, Section 11		Waste Management Unit Design
392	Part III	Acknowledge that a certification that ballasting met the criteria will be submitted and signed and sealed by a P.E, and signature of permittee	Acknowledgement	330.337(j)(2)-(3)	Yes	Attachment 10, Section 11		Waste Management Unit Design
393	Part III	Provide a liner quality control plan prepared under the direction of a licensed professional engineer.	Informational	330.339(a)			Attachment 10	Waste Management Unit Design
394	Part III	Provide in the liner quality control plan procedures that address the installation and testing of a geomembrane liner, if used	Required	330.339(a)	Yes	Attachment 10, Section 4		Waste Management Unit Design
395	Part III	Submit constructed liner details, depicted on cross-sections of a typical cell showing the slope, widths, and thicknesses for compaction lifts	Required	330.339(a)(1)	No		Not applicable, there are no existing cells, i.e., constructed liner at this landfill. See Attachment 6C and 12 for specifics on the proposed liner and leachate collection systems.	Waste Management Unit Design
396	Part III	Provide soil and liner quality-control testing procedures, to include sampling frequency, all field sampling and testing, both during construction and after completion	Required	330.339(a)(2)	Yes	Attachment 10, Appendix 10A, Table 10A-1		Waste Management Unit Design
397	Part III	Acknowledge that the professional of record who signs the soil liner evaluation report or his representative should be on site during all liner construction.	Acknowledgement	330.339(a)(2)	Yes	Attachment 10, Section 1.2		Waste Management Unit Design
398	Part III	Acknowledge that quality control of construction and quality assurance of sampling and testing procedures shall follow the latest technical guidelines of the executive director.	Acknowledgement	330.339(a)(2)	Yes	Attachment 10, Section 1.1, Paragraph 1		Waste Management Unit Design
399	Part III	Provide testing and reporting evaluation procedures to prepare the soil liner evaluation reports for the facility	Required	330.339(b)(1)	Yes	Attachment 10, Section 11.1 and Section 11.2		Waste Management Unit Design
400	Part III	Submit information to specify materials, equipment, and construction methods for the compaction of clay soils and depict on a drawing	Required	330.339(b)(2)	Yes	Attachment 10, Section 3.3 and Drawing 12.3		Waste Management Unit Design
401	Part III	Submit details and drawings for the over excavation and recompaction of the in-situ soils, or the compaction of soils from a borrow source, and cross-sections of a typical cell showing the slope, widths, and thicknesses for compaction lifts	Required	330.339(b)(2)(A)	Yes	Attachment 10, Section 2		Waste Management Unit Design
402	Part III	Submit procedures to be followed when excavations, cells, or disposal areas extend into or have the potential to extend into the groundwater; in accordance with 30 TAC 330.337	Required	330.339(b)(2)(B)	Yes	Attachment 10, Section 2.5		Waste Management Unit Design
403	Part III	Provide a description of installation methods, quality control testing, reporting, following the placement of geomembrane liners	Required	330.339(b)(3)	Yes	Attachment 10, Section 4		Waste Management Unit Design

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
404	Part III	Provide quality control testing frequencies and procedures that are in accordance with the executive director's most recent guidelines	Required	330.339(c)	Yes	Attachment 10, Section 4, and Table 10A.2		Waste Management Unit Design
405	Part III	Provide a description of field sampling and testing procedures, both during construction and after completion of the lining, to be performed by a qualified professional	Required	330.339(c)(1)	Yes	Attachment 10, Appendix 10A, Table 10A.1 and Table 10A.2		Waste Management Unit Design
406	Part III	Provide for continuous on-site inspection during construction of the liner by the professional of record or his designated representative	Required	330.339(c)(2)	Yes	Attachment 10, Section 11 and Section 1.2.4, Paragraph 1		Waste Management Unit Design
407	Part III	Provide information to indicate the amount of compaction of clay liners expressed as a percentage of a maximum dry density based on a compaction test. Compaction shall have a coefficient of permeability of 1 x 10-7 centimeters per second (cm/sec) or less	Required	330.339(c)(3)	Yes	Attachment 10, Section 3.1 and 3.3.1		Waste Management Unit Design
408	Part III	Submit and define the frequency of testing These frequencies shall be expressed in numbers of tests per specific area of liner per lift or specific thickness of liner	Required	330.339(c)(4)	Yes	Attachment 10, Appendix 10A, Table 10A-1 and Table 10A-2		Waste Management Unit Design
409	Part III	Provide for laboratory permeability tests. Tests shall be either constant head with back pressure or falling head tests	Required	330.339(c)(4)(A)	Yes	Attachment 10, Section 3.2.1, and Appendix 10A, Table 10A-1		Waste Management Unit Design
410	Part III	Provide for permeability tests to include; sieve analysis, Atterberg limits, moisture-density relationships, moisture content, and thickness verification	Required	330.339(c)(4)(B) - (F)	Yes	Attachment 10, Appendix 10A, Table 10A-1		Waste Management Unit Design
411	Part III	Provide for soils used as constructed liners to have a plasticity indexequal to or greater than 15; a liquid limitequal to or greater than 30; percent passing 200 mesh sieve (-200) equal to or greater than 30%; percent passing one-inch screen100%; and coefficient of permeability less than or equal to 1 x 10-7 cm/sec.	Required	330.339(c)(5)(A)-(E)	Yes	Attachment 10, Section 3.1, Paragraph 2		Waste Management Unit Design
412	Part III	Acknowledge that permeability tests for proving the suitability of soils to be used in constructing clay liners shall be performed in the laboratory	Acknowledgement	330.339(c)(6)	Yes	Attachment 10, Section 3.2		Waste Management Unit Design
413	Part III	Provide field quality control with field density tests based on moisture-density compaction curves, Atterberg limits, and lab permeabilities of undisturbed field samples	Required	330.339(c)(6)	Yes	Attachment 10, Section 3.2		Waste Management Unit Design
414	Part III	Provide field permeability testing of in-situ soils or constructed soil liners for the floor of the excavation, in accordance with ASTM D5093	Required	330.339(c)(7)	Yes	Attachment 10, Section 3.2		Waste Management Unit Design
415	Part III	Provide field permeability testing of in-situ soils or constructed soil liners for sidewalls, in accordance with a variation of the Boutwell STEI field permeability test	Required	330.339(c)(7)	Yes	Attachment 10, Section 3.2		Waste Management Unit Design
416	Part III	Provide for quality control testing of soil liners to be performed during the construction of the liner	Required	330.339(c)(8)	Yes	Attachment 10, Section 3.2.2		Waste Management Unit Design

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
417	Part III	Provide for all soil testing and evaluation of insitu soil or constructed soil liners to be completed prior to installing the leachate collection system	Required	330.339(c)(9)	Yes	Attachment 10, Section 3.2.2		Waste Management Unit Design
418	Part III	Calculate soil and liner density as a percentage of the maximum dry density and at the corresponding optimum moisture content. Soils tests must demonstrate a coefficient of permeability no greater than 1 x 10-7 cm/sec.	Required	330.339(d)	Yes	Attachment 10, Section 3.2.1, Paragraph 2, and Section 3.3.1, Bullet 6		Waste Management Unit Design
465	Part III	Provide a description of the liner system used for excavated waste storage, processing, and screening areas to control seepage and runoff	Required	330.63(d)(7)(C)	No		Not Applicable	Waste Management Unit Design
466	Part III	a description of how waste excavation activities will comply with the minimum design and operation requirements of §330.149, §330.151, §330.165, §330.167	Required	330.63(d)(7)(D)	No		Not Applicable	Waste Management Unit Design
467	Part III	The facility size shall be limited to a liquid waste processing rate no greater than 10,000 gallons per day	Informational	330.63(d)(9)(A)			Not Applicable	Waste Management Unit Design
468	Part III	Provide documentation that the facility design and operation will be coordinated with a consultant connected with an accredited college or university or with a consultant that has demonstrated the ability to carry out scientific experiments for demonstrating new and unproven waste handling methods and submitted to the executive director.	Required	330.63(d)(9)(B)	No		Not Applicable	Waste Management Unit Design
469	Part III	Indicate that the owner or operator shall submit to the executive director an annual and final status report to document the viability of the method being demonstrated. The report, at a minimum, must document the effluent standards and solid waste standards achieved.	Required	330.63(d)(9)(B)	No		Not Applicable	Waste Management Unit Design
470	Part III	Submit a Geology Report, prepared and signed by a qualified groundwater scientist and includes a geologic map of the region with text describing the stratigraphy and lithology of the map units.	Required	330.63(e)&(1)(A)	Yes	Attachment 4		Waste Management Unit Design
471	Part III	Provide a description of the generalized stratigraphic column in the facility area. Regional stratigraphic cross-sections should be provided and must include elements listed in 330.63(e)(1)(B).	Required	330.63(e)(1)(B)	Yes	Attachment 4: Section 3.1		Waste Management Unit Design
472	Part III	Provide a description of geologic active processes, faulting, subsidence	Required	330.63(e)(2)	Yes	Attachment 4: Section 3.1.2-3.1.4		Waste Management Unit Design
473	Part III	Provide a description of the regional aquifers in the vicinity of the facility based upon published and open-file sources	Required	330.63(e)(3)(A)	Yes	Attachment 4: Section 4.1		Waste Management Unit Design
474	Part III	Provide a description for the composition of the aquifer(s)	Required	330.63(e)(3)(B)	Yes	Attachment 4: Section 4.1		Waste Management Unit Design
475	Part III	Provide the hydraulic properties of the aquifer(s)	Required	330.63(e)(3)(C)	Yes	Attachment 4: Section 4.1		Waste Management Unit Design
476	Part III	Submit information on whether the aquifers are under water table or artesian conditions.	Required	330.63(e)(3)(D)	Yes	Attachment 4: Section 4.1		Waste Management Unit Design

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
477	Part III	Submit information for the hydraulic connectivity of aquifers	Required	330.63(e)(3)(E)	Yes	Attachment 4: Section 4.1		Waste Management Unit Design
478	Part III	Provide a regional water-table contour map or potentiometric surface map for each aquifer, if available;	Required	330.63(e)(3)(F)	No		Not Available	Waste Management Unit Design
479	Part III	Provide an estimate of the rate of groundwater flow	Required	330.63(e)(3)(G)	Yes	Attachment 4: Section 4.1		Waste Management Unit Design
480	Part III	Provide the typical values or a range of values for total dissolved solids content of groundwater from the aquifers	Required	330.63(e)(3)(H)	Yes	Attachment 4: Section 8.3		Waste Management Unit Design
481	Part III	Identify recharge areas to the aquifers within five miles of the site	Required	330.63(e)(3)(I)	Yes	Attachment 4: Section 4.1		Waste Management Unit Design
482	Part III	Identify what groundwater, withdrawn from vicinity aquifers is used for and provide the ID, location, & aquifer of each well within one mile of the facility	Required	330.63(e)(3)(J)	Yes	Attachment 4: Section 4.2, Appendix III-4.B		Waste Management Unit Design
483	Part III	Provide the results of investigations of subsurface conditions. This report must describe all borings drilled on site to test soils and characterize groundwater and must include a site map drawn to scale showing the surveyed locations and elevations of the borings.	Required	330.63(e)(4)	Yes	Attachment 4: Section 5, Appendix III-4.C		Waste Management Unit Design
484	Part III	Provided a sufficient no. of borings to characterize subsurface geology.	Required	330.63(e)(4)(A)	Yes	Attachment 4: Section 5.1		Waste Management Unit Design
485	Part III	Provide for borings to be sufficiently deep to identify uppermost aquifer, hydraulically connected aquifers, and underlying aquiclude; See Figure: 30 TAC §330.63(e)(4)(B)	Required	330.63(e)(4)(B)	Yes	Attachment 4: Section 5.1, Appendix III-4.B		Waste Management Unit Design
486	Part III	Provide all borings to be conducted in accordance with established field exploration methods.	Required	330.63(e)(4)(C)	Yes	Attachment 4: Section 5.1		Waste Management Unit Design
487	Part III	Provide GW well installation, abandonment, and plugging	Required	330.63(e)(4)(D)	Yes	Attachment 4: Section 5.1, Appendix III-4.E		Waste Management Unit Design
488	Part III	Number of borings & depth may be modified with ED approval	Informational	330.63(e)(4)(E)				Waste Management Unit Design
489	Part III	Electrical resistivity information may be used to reduce the number of borings with ED approval	Informational	330.63(e)(4)(F)				Waste Management Unit Design
490	Part III	Submit cross-sections prepared from the borings; depicting the generalized strata at the facility. For small waste management units, two perpendicular cross-sections will normally suffice	Required	330.63(e)(4)(G)	Yes	Attachment 4: Section 5.2, Figures III-4.10-4.15		Waste Management Unit Design
491	Part III	Provide a narrative that describes the investigator's interpretations of the subsurface stratigraphy based upon the field investigation	Required	330.63(e)(4)(H)	Yes	Attachment 4: Section 5.2, Section 5.3		Waste Management Unit Design
492	Part III	Provide geotechnical data that describes the geotechnical properties of the subsurface soil materials and a discussion with conclusions about the suitability of the soils and strata	Required	330.63(e)(5)	Yes	Attachment 4: Section 5.2, Section 5.3, Tables III-4.6-4.7, Attachment 5		Waste Management Unit Design

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
493	Part III	Provide a laboratory report of soil characteristics determined from at least one sample from each soil layer or stratum that will form the bottom and side of the proposed excavation and from those that are less than 30 feet below the lowest elevation of the proposed excavation.	Required	330.63(e)(5)(A)	Yes	Attchment 4: Appendix III- 4.F		Waste Management Unit Design
494	Part III	Provide permeability tests to be performed according to one of the standards on undisturbed soil samples. All test results shall indicate the type of tests used and the orientation of each tested sample.	Required	330.63(e)(5)(B)	Yes	Attachment 4: Tables III-4.6-4.7, Appendix III-4.F		Waste Management Unit Design
495	Part III	Submit test results for constant head w/ back pressure	Required	330.63(e)(5)(B)(i)	Yes	Attachment 4: Tables III-4.6- 4.7, Appendix III-4.F		Waste Management Unit Design
496	Part III	Submit test results for falling head	Required	330.63(e)(5)(B)(ii)	Yes	Attachment 4: Tables III-4.6- 4.7, Appendix III-4.F		Waste Management Unit Design
497	Part III	Submit test results for sieve analysis	Required	330.63(e)(5)(B)(iii)	Yes	Attachment 4: Tables III-4.6- 4.7, Appendix III-4.F		Waste Management Unit Design
498	Part III	Submit test results for Atterberg limits	Required	330.63(e)(5)(B)(iv)	Yes	Attachment 4: Tables III-4.6- 4.7, Appendix III-4.F		Waste Management Unit Design
499	Part III	Submit test results for moisture content	Required	330.63(e)(5)(B)(v)	Yes	Attachment 4: Tables III-4.6- 4.7, Appendix III-4.F		Waste Management Unit Design
500	Part III	Submit information for the depth at which groundwater was encountered and records of after-equilibrium measurements in all borings. The cross-sections prepared in response to 330.63(e)(4)(G) must be annotated to note the level at which groundwater was first encountered	Required	330.63(e)(5)(C)	Yes	Attachment 4: Section 6.1, Table III-4.9		Waste Management Unit Design
501	Part III	Submit water levels in monitoring wells, historical water levels in table format for each monitoring well	Required	330.63(e)(5)(D)	Yes	Attachment 4: Section 6, Appendix III-4.K, Appendix III-4.L		Waste Management Unit Design
502	Part III	Submit a tabulation of GW monitoring data onsite or on adjacent units	Required	330.63(e)(5)(E)	Yes	Attachment 4: Section 6, Appendix III-4.K, Appendix III-4.L		Waste Management Unit Design
503	Part III	Identify the uppermost aquifer and any lower aquifers that are hydraulically connected to it beneath the facility	Required	330.63(e)(5)(F)	Yes	Attachment 4: Section 6		Waste Management Unit Design
504	Part III	Provide a Groundwater Sampling and Analysis Plan. Compost Permits submit per Chapter 332	Required	330.63(f)	Yes	Attachment 7		Groundwater Sampling & Analysis Plan
505	Part III	Provide a topographic map delineating waste area, property boundary, point of compliance, & GW monitoring wells	Required	330.63(f)(1)	Yes	Attachment 4: Section 9		Groundwater Sampling & Analysis Plan
506	Part III	Provide a description of any contamination plume from the unit	Required	330.63(f)(2)	No		Not applicable	Groundwater Sampling & Analysis Plan
507	Part III	Provide a delineation of contaminate plume on the topographic map	Required	330.63(f)(2)(A)	No		Not applicable	Groundwater Sampling & Analysis Plan
508	Part III	Provide the concentration of each assessment constituent in the plume	Required	330.63(f)(2)(B)	No		Not applicable	Groundwater Sampling & Analysis Plan
509	Part III	Provide an analysis of most likely pollutant pathway, include any GW modeling data & results per 330.403(e)(2), consideration of GW flow changes from construction	Required	330.63(f)(3)	Yes	Attachment 4: Section 7		Groundwater Sampling & Analysis Plan
510	Part III	Provide detailed plans and an engineering report describing the proposed groundwater monitoring program to be implemented to meet the requirements of §330.403	Required	330.63(f)(4)	Yes	Attachment 4: Section 9		Groundwater Sampling & Analysis Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
511	Part III	Submit information; supporting data, analyses to establish detection monitoring program per 330.407; If hazardous constituents in 40 CFR 258 & 330.419 have not been detected	Required	330.63(f)(5)	Yes	Attachment 4: Section 8		Groundwater Sampling & Analysis Plan
512	Part III	Submit the proposed GW monitoring system	Required	330.63(f)(5)(A)	Yes	Attachment 4: Section 9		Groundwater Sampling & Analysis Plan
513	Part III	Submit background values for each monitoring parameter or constituent listed in §330.419 of this title, or procedures to calculate such values;	Required	330.63(f)(5)(B)	Yes	Attachemnt 7: Section 4.2		Groundwater Sampling & Analysis Plan
514	Part III	Provide for a semiannual monitoring frequency	Required	330.407(a)	Yes	Attachment 7: Section 5.2		Groundwater Sampling & Analysis Plan
515	Part III	Provide for a minimum of four statistically independent background GW samples collected quarterly unless approved, background may be updated every 2 yrs. with representative of background demonstration	Required	330.407(a)(1)	Yes	Attachment 7: Section 5.1		Groundwater Sampling & Analysis Plan
516	Part III	ED may approve alternative sampling frequency but not less than annual	Informational	330.407(a)(2)				Groundwater Sampling & Analysis Plan
517	Part III	For establishing background, ED may consider previous data	Informational	330.407(a)(3)				Groundwater Sampling & Analysis Plan
518	Part III	Provide Notification of SSI to ED within 14 days of the 60-day SSI determination	Required	330.407(b)	Yes	Attachment 7: Section 5.2		Groundwater Sampling & Analysis Plan
519	Part III	Provide (if SSI is determined) a notice to the operating record immediately & establish an assessment monitoring program within 90 days, or provide for resampling within 60 days of SSI determination	Required	330.407(b)(1)-(2)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
520	Part III	Submit alternative source demonstration including Notification to ED & any local agency, within 14 days of the SSI determination, of the intent to submit ASD	Required	330.407(b)(3)-(A)	Yes	Attachment 7: Section 5.2.1.1		Groundwater Sampling & Analysis Plan
521	Part III	Submit ASD report to ED & any local agency, within 90 days of the SSI determination, certified by a qualified GW scientist	Required	330.407(b)(3)(B)	Yes	Attachment 7: Section 5.2.1.1		Groundwater Sampling & Analysis Plan
522	Part III	Provide for No filtering of samples for ASD, ED may require leachate analyses to support ASD	Required	330.407(b)(3)(C)	Yes	Attachment 7: Section 5.2.1.1		Groundwater Sampling & Analysis Plan
523	Part III	Owner/Operator may continue detection monitoring program	Informational	330.407(b)(3)(D)				Groundwater Sampling & Analysis Plan
524	Part III	Provide for assessment monitoring if no ASD satisfactory to the ED within 90 days of notice. ED may require additional point of compliance wells	Required	330.407(b)(4)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
525	Part III	Submit annual detection monitoring report within 90 days of last sampling even that includes the following	Required	330.407(c)	Yes	Attachment 7: Section 5.5.1		Groundwater Sampling & Analysis Plan
526	Part III	Submit a statement regarding occurrences of SSIs	Required	330.407(c)(1)	Yes	Attachment 7: Section 5.5.1		Groundwater Sampling & Analysis Plan
527	Part III	Submit GW monitoring results, background GW quality, statistical calculations, graphs, & drawings	Required	330.407(c)(2)	Yes	Attachment 7: Section 5.5.1		Groundwater Sampling & Analysis Plan
528	Part III	Submit GW flow rate & direction based on detection sampling water elevations, any supporting documentation	Required	330.407(c)(3)	Yes	Attachment 7: Section 5.5.1		Groundwater Sampling & Analysis Plan

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529	Part III	Provide for piezometric water level contour map and supporting documentation	Required	330.407(c)(4)	Yes	Attachment 7: Section 5.5.1		Groundwater Sampling & Analysis Plan
530	Part III	Submit recommendations for any changes	Required	330.407(c)(5)	Yes	Attachment 7: Section 5.5.1		Groundwater Sampling & Analysis Plan
531	Part III	Submit any other information required by ED	Required	330.407(c)(6)	Yes	Attachment 7: Section 5.5.1		Groundwater Sampling & Analysis Plan
532	Part III	Submit a permit amendment or modification, If detection monitoring program no longer satisfies 330.407	Required	330.407(d)	Yes	Attachment 7: Section 5.5.1		Groundwater Sampling & Analysis Plan
533	Part III	Provide a description of proposed sampling, analysis, and statistical comparison procedures to be utilized in evaluating groundwater monitoring data	Required	330.63(f)(5)(C)	Yes	Attachment 7: Section 2.4 & Section 4		Groundwater Sampling & Analysis Plan
534	Part III	Provide a statement that information, supporting data, and analyses to establish assessment monitoring program per 330.409 will be provided If hazardous constituents are present	Required	330.63(f)(6)	No		Not applicable.	Groundwater Sampling & Analysis Plan
535	Part III	Provide a statement indicating that assessment monitoring information and a description of any special waste previously handled at the facility will be provided	Required	330.63(f)(6)(A)	No		Not applicable.	Groundwater Sampling & Analysis Plan
536	Part III	Indicate that a characterization of the contaminated groundwater, including concentration of assessment constituents as defined in §330.409 of this title, will be provided	Required	330.63(f)(6)(B)	No		Not applicable.	Groundwater Sampling & Analysis Plan
537	Part III	Indicate that a list of assessment constituents as defined in §330.409 of this title for which assessment monitoring will be undertaken, will be provided	Required	330.63(f)(6)(C)	No		Not applicable.	Groundwater Sampling & Analysis Plan
538	Part III	Provide plans & engineering report describing GW monitoring system	Required	330.63(f)(6)(D)	No		Not applicable.	Groundwater Sampling & Analysis Plan
539	Part III	Provide a description of proposed sampling, analysis, and statistical comparison procedures to be utilized in evaluating groundwater monitoring data	Required	330.63(f)(6)(E)	No		Not applicable.	Groundwater Sampling & Analysis Plan
540	Part III	Provide, if hazardous constituents have exceeded the concentration limits, supporting data, and analyses to establish a corrective action program that meets the requirements of §330.411 and §330.413	Required	330.63(f)(7)	No		Not applicable.	Groundwater Sampling & Analysis Plan
541	Part III	Indicate that a characterization of the contaminated groundwater, including concentrations of assessment constituents as defined in §330.409	Required	330.63(f)(7)(A)	No		Not applicable.	Groundwater Sampling & Analysis Plan
542	Part III	Indicate that concentration limits for each constituent will be submitted	Required	330.63(f)(7)(B)	No		Not applicable.	Groundwater Sampling & Analysis Plan
543	Part III	Indicate that plans & an engineering report describing corrective action will be submitted	Required	330.63(f)(7)(C)	No		Not applicable.	Groundwater Sampling & Analysis Plan
544	Part III	Submit a description of how the monitoring program will demonstrate adequacy of corrective action	Required	330.63(f)(7)(D)	No		Not applicable.	Groundwater Sampling & Analysis Plan
545	Part III	Submit a schedule for submitting information required by 330.63(f)(7)(C) & (D)	Required	330.63(f)(7)(E)	No		Not applicable.	Groundwater Sampling & Analysis Plan
546	Part III	Criteria to determine if the facility is exempt from groundwater monitoring	Informational	330.401(a)-(c)				Groundwater Sampling & Analysis Plan

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547	Part III	Submit criteria for suspension of groundwater monitoring; the demonstration for suspension shall be certified by a qualified groundwater scientist and approved by the executive director	Required if Requested	330.401(d)	No		Not applicable.	Groundwater Sampling & Analysis Plan
548	Part III	Submit for suspension demonstration site specific data affecting contaminant fate & transport	Required	330.401(d)(1)	No		Not applicable.	Groundwater Sampling & Analysis Plan
549	Part III	Submit for suspension demonstration, contaminant fate & transport predictions	Required	330.401(d)(2)	No		Not applicable.	Groundwater Sampling & Analysis Plan
550	Part III	Provide for new solid waste management units a documented certification signed by a qualified groundwater scientist that the facility is in compliance with the groundwater monitoring requirements	Required	330.401(e)	Yes	Attachment 4: Section 9.3		Groundwater Sampling & Analysis Plan
551	Part III	Acknowledge that groundwater monitoring must be conducted throughout the active life and any required post-closure care period	Acknowledgement	330.401(f)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
552	Part III	Submit a GW monitoring system with sufficient no. of wells, location, depth to yield representative GW samples	Required	330.403(a)	Yes	Attachment 4: Section 9		Groundwater Sampling & Analysis Plan
553	Part III	Provide information on background wells used to determine background GW quality	Required	330.403(a)(1)	No		Not applicable. No groundwater water chemistry available.	Groundwater Sampling & Analysis Plan
554	Part III	Provide/identify the point of compliance wells not >600 ft. unless modeling demonstration approved	Required	330.403(a)(2)	Yes	Attachment 4: Section 9		Groundwater Sampling & Analysis Plan
555	Part III	Provide, if a multi-unit GW monitoring system is proposed; the number, spacing, and orientation of the solid waste management units within an overall waste management area; hydrogeologic setting; site history; engineering design of the units; and type of waste accepted at the units.	Required	330.403(b)(1)-(5)	No		Not applicable. Single unit monitoring system	Groundwater Sampling & Analysis Plan
556	Part III	The executive director may approve an alternative design for a groundwater monitoring system that uses other means in conjunction with monitoring wells	Informational	330.403(c)				Groundwater Sampling & Analysis Plan
557	Part III	Acknowledge that all parts of a groundwater monitoring system shall be operated and maintained so that they perform at least to design specifications	Acknowledgement	330.403(d)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
558	Part III	Provide a design certified by a qualified groundwater scientist.	Required	330.403(e)	Yes	Attachment 4: Section 9		Groundwater Sampling & Analysis Plan
559	Part III	Provide the design of the monitoring system to be based on site-specific technical information	Required	330.403(e)(1)	Yes	Attachment 4: Section 9		Groundwater Sampling & Analysis Plan
560	Part III	Multi-dimensional fate & transport model may be used to support sampling point locations	Informational	330.403(e)(2)				Groundwater Sampling & Analysis Plan
561	Part III	Provide if a multi-dimensional model is proposed, documentation of the model's ability to represent GW flow & contaminant transport	Required	330.403(e)(2)(A)	No		Not applicable.	Groundwater Sampling & Analysis Plan
562	Part III	Provide if a multi-dimensional model is proposed, a sound set of equations based on accepted theory	Required	330.403(e)(2)(B)	No		Not applicable.	Groundwater Sampling & Analysis Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
563	Part III	Provide if a multi-dimensional model is proposed, a numerical solution methods based on mathematical principals with verification & checking techniques	Required	330.403(e)(2)(C)	No		Not applicable.	Groundwater Sampling & Analysis Plan
564	Part III	Provide if a multi-dimensional model is proposed, a model calibrated against site-specific field data	Required	330.403(e)(2)(D)	No		Not applicable.	Groundwater Sampling & Analysis Plan
565	Part III	Provide if a multi-dimensional model is proposed, a sensitivity analysis for major parameters	Required	330.403(e)(2)(E)	No		Not applicable.	Groundwater Sampling & Analysis Plan
566	Part III	Provide if a multi-dimensional model is proposed, mass-balance calculations	Required	330.403(e)(2)(F)	No		Not applicable.	Groundwater Sampling & Analysis Plan
567	Part III	Provide if a multi-dimensional model is proposed, a model based on field or lab measurements that document validity of parameter values	Required	330.403(e)(2)(G)	No		Not applicable.	Groundwater Sampling & Analysis Plan
568	Part III	Acknowledge that the owner or operator shall promptly notify the executive director, and any local pollution agency with jurisdiction that has requested to be notified, in writing of changes in facility construction or operation or changes in adjacent property that affect or are likely to affect the direction and rate of groundwater flow and the potential for detecting groundwater contamination from a solid waste management unit and that may require the installation of additional monitoring wells or sampling points and that such additional wells or sampling points require a modification of the site development plan.	Acknowledgement	330.403(e)(3)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
569	Part III	Provide sampling & analysis procedures that ensure accurate results of GW quality	Required	330.405(a)	Yes	Attachment 7: Section 2		Groundwater Sampling & Analysis Plan
570	Part III	Submit GW sampling & analysis plan prior to sampling, place a copy of the approved plan in the operating record	Required	330.405(b)	Yes	Attachment 7: Section 2		Groundwater Sampling & Analysis Plan
571	Part III	Provide procedures for sample collection, preservation & shipping, analytical procedures, COC control, & QA/QC	Required	330.405(b)(1)	Yes	Attachment 7: Section 2		Groundwater Sampling & Analysis Plan
572	Part III	Provide for GW elevations measured at each point, sample from high to low elevations unless contaminated, sample un-contaminated points prior to contaminated points	Required	330.405(b)(2)	Yes	Attachment 7: Section 2		Groundwater Sampling & Analysis Plan
573	Part III	Provide sampling & analysis methods appropriate for groundwater sampling	Required	330.405(b)(3)	Yes	Attachment 7: Section 2		Groundwater Sampling & Analysis Plan
574	Part III	Provide for Type I landfills – collection of samples necessary to establish GW quality data consistent with statistical procedures for detection, assessment, corrective measures	Required	330.405(b)(3)(A)	Yes	Attachment 7: Section 3.2		Groundwater Sampling & Analysis Plan
575	Part III	Provide for no field filtered GW samples prior to analysis	Required	330.405(c)	Yes	Attachment 7: Section 2.4.1.5		Groundwater Sampling & Analysis Plan
576	Part III	Provide and establish background GW quality for detection parameters	Required	330.405(d)	Yes	Attachment 7: Section 4.2		Groundwater Sampling & Analysis Plan
577	Part III	Provide 1 or more statistical methods to evaluate detection/assessment parameters	Required	330.405(e)	Yes	Attachment 7: Section 4.1		Groundwater Sampling & Analysis Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
578	Part III	Provide parametric analysis of variance followed by multiple comparison procedures, contrast between well's mean & background mean	Required	330.405(e)(1)	Yes	Attachment 7: Section 4		Groundwater Sampling & Analysis Plan
579	Part III	Provide analysis of variance based on ranks followed by multiple comparison procedures, contrast between well's median & background median	Required	330.405(e)(2)	Yes	Attachment 7: Section 4		Groundwater Sampling & Analysis Plan
580	Part III	Provide tolerance or prediction interval procedures	Required	330.405(e)(3)	Yes	Attachment 7: Section 4		Groundwater Sampling & Analysis Plan
581	Part III	Provide a control chart approach	Required	330.405(e)(4)	Yes	Attachment 7: Section 4		Groundwater Sampling & Analysis Plan
582	Part III	Provide for any statistical method to meet the standards listed under 330.405(f)	Required	330.405(e)(5)	Yes	Attachment 7: Section 4		Groundwater Sampling & Analysis Plan
583	Part III	Provide the statistical method chosen under 330.405(e) appropriate for the distribution	Required	330.405(f)-(1)	Yes	Attachment 7: Section 4		Groundwater Sampling & Analysis Plan
584	Part III	Provide, if individual sampling point comparison to background or GW protection standard is used, for the test to be done at Type I error level not <0.01.	Required	330.405(f)(2)	Yes	Attachment 7: Section 4		Groundwater Sampling & Analysis Plan
585	Part III	Provide, If control chart is used, the specific type of chart & its parameters must be protective, consider no. of samples, distribution, & concentration range	Required	330.405(f)(3)	Yes	Attachment 7: Section 4		Groundwater Sampling & Analysis Plan
586	Part III	Provide the tolerance or prediction intervals used	Required	330.405(f)(4)	Yes	Attachment 7: Section 4		Groundwater Sampling & Analysis Plan
587	Part III	Provide that the statistical method used accounts for data below detection	Required	330.405(f)(5)	Yes	Attachment 7: Section 4		Groundwater Sampling & Analysis Plan
588	Part III	Provide for the statistical method to control or correct for seasonal, spatial variability & temporal correlation in data	Required	330.405(f)(6)	Yes	Attachment 7: Section 4		Groundwater Sampling & Analysis Plan
589	Part III	Indicate that assessment monitoring is required whenever the owner or operator determines there has been a statistically significant increase over background for one or more of the constituents listed in §330.419 of this title	Required	330.409(a)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
590	Part III	Indicate that within 90 days of determining that a statistically significant increase has occurred in accordance with §330.407(b) and not less than annually thereafter, the owner or operator shall sample and analyze the groundwater monitoring system for the full set of constituents listed in Appendix II to 40 Code of Federal Regulations (CFR) Part 258	Required	330.409(b)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
591	Part III	Indicate that a minimum of one sample shall be collected from each point of compliance well and analyzed for the 40 CFR Part 258, Appendix II constituents during each sampling event.	Required	330.409(b)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
592	Part III	Indicate that for any new constituent(s) detected in the point of compliance wells as a result of the complete Appendix II analysis, a minimum of four statistically independent samples from each background well shall be collected and analyzed to establish background levels for the additional constituent(s).	Required	330.409(b)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
593	Part III	Indicate that after sampling all point of compliance wells for Appendix II constituents, the executive director may specify an appropriate subset of wells to be sampled and analyzed for the Appendix II constituents during assessment monitoring and may delete any of the Appendix II constituents for a municipal solid waste management unit if the owner or operator can document that the removed constituents are not reasonably expected to be in or derived from the waste contained in the unit	Required	330.409(b)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
594	Part III	Provide, if the ED specifies, an alternative frequency for sampling Appendix II constituents	Required	330.409(c)(1)-(5)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
595	Part III	Indicate that Appendix II constituents results will be submitted within 60 days after each sampling event	Required	330.409(d)	Yes	Attachment 7: Section 5.5.3		Groundwater Sampling & Analysis Plan
596	Part III	Indicate that within 90 days of reporting Appendix II results & semiannually thereafter, all wells will be resampled for Appendix I & any new constituent detected from Appendix II, and that the results of resampling will be submitted within 60 days after each sampling event	Required	330.409(d)(1)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
597	Part III	Provide background concentrations for additional Appendix II constituents detected	Required	330.409(d)(2)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
598	Part III	Provide groundwater protection standards for all constituents detected in point of compliance wells	Required	330.409(d)(3)	Yes	Attachment 7: Section 3.5		Groundwater Sampling & Analysis Plan
599	Part III	Provide notification to ED, If concentrations are at or below background for 2 consecutive sampling events, and return to detection monitoring	Required	330.409(e)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
600	Part III	Continue assessment monitoring If concentrations are above background but below GW protection standards	Required	330.409(f)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
601	Part III	Indicate that no later than 60 days after each sampling event a determination whether any 40 CFR Part 258, Appendix II constituents were detected at statistically significant levels above the groundwater protection standards. If exceeded the ED & local government will be notified within 7 days of determination	Required	330.409(g)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
602	Part III	Provide the characterization and extent of release by installing additional wells as necessary	Required	330.409(g)(1)-(A)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
603	Part III	Provide for the installation of wells adjacent to the well with exceedance before next sampling event & sample new well for Appendix I & additional constituents from Appendix II	Required	330.409(g)(1)(B)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
604	Part III	Provide Notification to all persons that own or occupy the land that overlies any part of the contamination plume	Required	330.409(g)(1)(C)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
605	Part III	Provide an assessment of corrective measures within 90 days of notice to ED	Required	330.409(g)(1)(D)	Yes	Attachment 7: Section 5.4		Groundwater Sampling & Analysis Plan
606	Part III	Notify ED within 14 days of exceedance determination and intent to submit an Alternate Source Demonstration (ASD)	Required	330.409(g)(2)-(A)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
607	Part III	Submit certified ASD report within 90 days of exceedance determination	Required	330.409(g)(2)(B)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
608	Part III	Provide for no filtering of samples for ASD, ED may require leachate analyses to support ASD and continue assessment monitoring program	Required	330.409(g)(2)(C)-(D)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
609	Part III	Provide for assessment monitoring If ASD is accepted by ED, otherwise implement assessment of corrective measures	Required	330.409(g)(3)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
610	Part III	Provide for a permit amendment or modification if assessment monitoring program is no longer compliant with 330.409,	Required	330.409(g)(4)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
611	Part III	Provide for/establish GW protection standards for Appendix II constituents in the point of compliance monitoring wells	Required	330.409(h)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
612	Part III	Provide for GW protection standard for constituents for which a maximum (MCL) has been promulgated under 40 CFR Part 141, Safe Drinking Water Act Maximum contaminant level (MCL)	Required	330.409(h)(1)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
613	Part III	Provide GW protection standard for constituents for which no MCL promulgated	Required	330.409(h)(2)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
614	Part III	Provide GW protection standard for background constituents higher than MCL or health-based level	Required	330.409(h)(3)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
615	Part III	Acknowledge that the ED may establish alternative GW protection standards in accordance with 30 TAC §330.409(i)	Acknowledgement	330.409(i)	Yes	Attachment 7: Section 5.3		Groundwater Sampling & Analysis Plan
616	Part III	Submit annual assessment monitoring report within 60 days of 2nd semiannual sampling event	Required	330.409(k)	Yes	Attachment 7: Section 5.5.3		Groundwater Sampling & Analysis Plan
617	Part III	Submit a statement of any statistically significant exceedances of GW protection standards & the status of the exceedance	Required	330.409(k)(1)	Yes	Attachment 7: Section 5.5.3		Groundwater Sampling & Analysis Plan
618	Part III	Submit GW monitoring results, summary of background, statistical calculations, graphs & drawings	Required	330.409(k)(2)	Yes	Attachment 7: Section 5.5.3		Groundwater Sampling & Analysis Plan
619	Part III	Submit GW flow rate & direction based on data from sampling events, supporting documentation	Required	330.409(k)(3)	Yes	Attachment 7: Section 5.5.3		Groundwater Sampling & Analysis Plan
620	Part III	Submit a Piezometric water level contour map and supporting documentation	Required	330.409(k)(4)	Yes	Attachment 7: Section 5.5.3		Groundwater Sampling & Analysis Plan
621	Part III	Provide recommendations for any changes	Required	330.409(k)(5)	Yes	Attachment 7: Section 5.5.3		Groundwater Sampling & Analysis Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
622	Part III	Submit Any other information required by ED	Required if Requested	330.409(k)(6)	Yes	Attachment 7: Section 5.5.3		Groundwater Sampling & Analysis Plan
623	Part III	Provide detection monitoring for constituents listed in Appendix I, 40 CFR Part 258	Required	330.419(a)	Yes	Attachment 7: Section 3.3		Groundwater Sampling & Analysis Plan
624	Part III	ED may delete constituents from Appendix I if constituent not likely to be derived from waste disposed of in the landfill	Informational	330.419(b)				Groundwater Sampling & Analysis Plan
625	Part III	ED may establish alternative inorganic list, add organic or inorganic constituents based on consideration of the following	Informational	330.419(c)				Groundwater Sampling & Analysis Plan
626	Part III	Types, concentrations, quantities, persistence of waste constituents	Informational	330.419(c)(1)				Groundwater Sampling & Analysis Plan
627	Part III	Mobility, stability, persistence of constituents & their reaction products	Informational	330.419(c)(2)				Groundwater Sampling & Analysis Plan
628	Part III	Detectability of indicator & waste constituents & reaction products in groundwater	Informational	330.419(c)(3)				Groundwater Sampling & Analysis Plan
629	Part III	Concentrations & coefficients of variability of parameters or constituents in the groundwater background	Informational	330.419(c)(4)				Groundwater Sampling & Analysis Plan
630	Part III	Provide for the construction of monitoring wells to provide integrity, representative samples, prevent migration of water in bore hole, well construction must follow prescribed specifications	Required	330.421(a)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
631	Part III	Provide that wells to be drilled by a qualified TX licensed drill & supervised by PG or PE	Required	330.421(a)(1)(A)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
632	Part III	Provide a drilling method that shall not introduce contaminants. If fluid used in drilling, then use clean city water unless approved by ED. If water used provide analysis	Required	330.421(a)(1)(B)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
633	Part III	Provide borings to be at least 4 in. larger than casing. If boring in rock, a smaller annulus may be approved by the executive director	Required	330.421(a)(1)©	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
634	Part III	Provide a log of boring, signed, sealed & dated by PG or PE	Required	330.421(a)(1)(D)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
635	Part III	Provide designs for casing, screen, filter pack, & seal	Required	330.421(a)(2)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
636	Part III	Provide casing specifications; the casing should be 2 to 4 inch schedule 40 or 80 PVC, and must meet other requirements of 30 TAC §330.421(a)(2)(A)	Required	330.421(a)(2)(A)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
637	Part III	Provide screen specifications that are compatible with the casing and does not include glue, solvents, field-cut slots or filter cloths	Required	330.421(a)(2)(B)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
638	Part III	Provide filter pack specifications – clean silica sand or glass, 1 to 4 ft. above screen, etc.	Required	330.421(a)(2)(C)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
639	Part III	Provide annular seal specifications – 2 ft. thick, placed in zone of saturation, etc.	Required	330.421(a)(2)(D)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
640	Part III	Provide casing seal specifications – placed on top of annular seal, bentonite grout or cement-bentonite mix, etc.	Required	330.421(a)(2)(E)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
641	Part III	Provide specifications for the concrete pad to be placed on top of the casing seal, including the type of structural concrete used from casing seal to surface	Required	330.421(a)(3)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
642	Part III	Provide protective collar specifications – steel collar around casing, set 1 ft. into surface pad, etc.	Required	330.421(a)(4)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
643	Part III	Provide protective barrier specifications – 3 to 4 6-12 in. diameter pipes set in concrete, other types of barriers may be approved by ED	Required	330.421(a)(5)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
644	Part III	Acknowledge that when wells are installed in unusual conditions, all aspects must be approved in writing by the ED	Acknowledgement	330.421(b)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
645	Part III	Provide the removal of artifacts once monitoring well is installed and open water- bearing zones for max flow into well	Required	330.421(c)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
646	Part III	Identify well location & elevation surveyed, permanently marked	Required	330.421(d)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
647	Part III	Provide a well installation report to be submitted within 60 days of completion including boring log, description of development procedures, any sample data & sit map showing location	Required	330.421(e)	Yes	Attachment 4: Section 9.2		Groundwater Sampling & Analysis Plan
648	Part III	Provide a Landfill Gas Management Plan to comply with Subchapter I	Required	330.63(g)	Yes	Attachment 11		Landfill Gas Management Plan
649	Part III	Submit information to specify that methane concentration cannot exceed 1.25% by volume in facility structures	Required	330.371(a)(1)	Yes	Attachment 11, Section 1.2		Landfill Gas Management Plan
650	Part III	Submit information to specify that methane concentrations cannot exceed 5% by volume at permitted boundary wells, probes, subsurface soils, or other matrices	Required	330.371(a)(2)	Yes	Attachment 11, Section 1.2		Landfill Gas Management Plan
651	Part III	Provide a plan to implement routine methane monitoring where the type and frequency of monitoring is based on soil, hydrogeologic, and hydraulic conditions	Required	330.371(b)(1)(A)-(C)	Yes	Attachment 11, Section 3.1		Landfill Gas Management Plan
652	Part III	Provide a plan to implement routine methane monitoring where the type and frequency of monitoring is based on locations of facility structures, property boundaries and utility or pipelines that cross the facility boundary	Required	330.371(b)(1)(D)&(E)	Yes	Attachment 11, Section 3.2		Landfill Gas Management Plan
653	Part III	Indicate that methane monitoring will be conducted, at a minimum, quarterly.	Required	330.371(b)(2)	Yes	Attachment 11, Section 2.1, Paragraph 2		Landfill Gas Management Plan
654	Part III	Provide in the plan the necessary steps to take if methane concentrations exceed 1.25% in structures and/or 5% in boundary matrices; including notification to the ED, local officials, emergency officials, & the public	Required	330.371(c)-(1)	Yes	Attachment 11, Section 4		Landfill Gas Management Plan
656	Part III	Indicate that a remediation plan will implemented within 60 days of detection that describes the nature, extent of the problem, and the proposed remedy, The ED may require additional remedial measures	Required	330.371(c)(3)	Yes	Attachment 11, Section 5		Landfill Gas Management Plan
657	Part III	Indicate that the ED may establish alternative schedule for monitoring & exceedance actions	Required	330.371(d)	Yes	Attachment 11, Section 5		Landfill Gas Management Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
658	Part III	Provide for continuing methane monitoring and control for 30 yrs. after certification of final closure for Type I & IAE facilities. & 5 yrs. for Type IV & IVAE. Gas monitoring may be reduce with an approved no gas migration demonstration	Required	330.371(e)	Yes	Attachment 11, Section 3.3		Landfill Gas Management Plan
659	Part III	Provide for continuing methane monitoring and control for 30 yrs. after certification of final closure for Type I & IAE facilities.	Required	330.371(e)	Yes	Attachment 11, Section 1.1 and Section 3.3		Landfill Gas Management Plan
660	Part III	Provide for continuing methane monitoring and control for 5 yrs. after certification of final closure for Type IV & IVAE facilities.	Required	330.371(e)	No		Not Applicable	Landfill Gas Management Plan
661	Part III	Indicate that information may be submitted to the ED, to reduce gas monitoring and control. The information must demonstrate no potential for gas migration beyond the property boundary or into on-site structures.	Required	330.371(e)	Yes	Attachment 11, Section 3.3		Landfill Gas Management Plan
662	Part III	Provide for gas monitoring & control to be revised & maintained as needed; post-closure land use shall not interfere with the gas monitoring system and all utility trenches crossing the facility shall be vented & monitored	Required	330.371(f)	Yes	Attachment 11, Section 1, Paragraph 1		Landfill Gas Management Plan
663	Part III	Provide a description of how gases be managed & controlled	Required	330.371(g)-(1)	Yes	Attachment 11, Section 2.1, Paragraphs 2 & 3		Landfill Gas Management Plan
664	Part III	Provide a description of the proposed system, installation procedures, installation timeline, monitoring & maintenance procedures	Required	330.371(g)(2)	Yes	Attachment 11, Section 3.1.1 and Section 3.2		Landfill Gas Management Plan
665	Part III	Provide a backup plan for breakdowns	Required	330.371(g)(3)	Yes	Attachment 11, Section 3.4.		Landfill Gas Management Plan
666	Part III	Installation of an initial perimeter monitoring network at Type IAE and Type IVAE ands larger landfills may consist of portable equipment and probes provided there are no habitable structures within 3000 feet of the waste placement boundary.	Informational	330.371(h)(1)				Landfill Gas Management Plan
667	Part III	Indicate that a permanent gas monitoring system will be installed if test results show the presence of methane gas above a concentration of .5% by volume	Required	330.371(h)(1)	No		Not Applicable	Landfill Gas Management Plan
668	Part III	Provide a permanent gas monitoring system at Type I and Type IV facilities	Required	330.371(h)(2)	Yes	Attachment 11 and Drawing 11.1		Landfill Gas Management Plan
669	Part III	Provide a monitoring network design to monitor on-site structures, and any other areas that have potential gas buildup	Required	330.371(i)	Yes	Attachment 11, Section 3.2.1 and 3.2.2		Landfill Gas Management Plan
670	Part III	Provide for all monitoring probes and on-site structures to be sampled for methane during the monitoring period	Required	330.371(j)	Yes	Attachment 11, Section 3.2.1 and 3.2.2		Landfill Gas Management Plan
676	Part III	Provide a demonstration that above ground disposal area final cover slopes shall not exceed 25%. Topmost portion of final cover shall be between 2% & 6%.	Required	330.453(c)	Yes	Attachment 3, Drawings 3.1, 3.2, and 3.3, and Appendix 9A, Table 6		Closure Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
677	Part III	Provide a demonstration that a design with an excess of 25% final cover slopes may be submitted. The design must demonstrate the management of drainage, such as control flumes, diversion terraces, spillways or other acceptable methods	Required if Requested	330.453(c)	No		Not Applicable	Closure Plan
678	Part III	An alternative final cover design may be submitted to demonstrate an equivalent reduction in infiltration as the clayey soil cover infiltration layer specified under 330.453(a).	Required if Requested	330.453(d)(1)	No		Not Applicable	Closure Plan
679	Part III	An alternative final cover design may be submitted to demonstrate approved alternative final cover that achieves equivalent protection from wind & water erosion	Required if Requested	330.453(d)(2)	No		Not Applicable	Closure Plan
680	Part III	Submit information to comply with post-closure care once closure of a Type IV facility is complete	Required	330.453(f)	No		Not Applicable	Closure Plan
681	Part III	Provide designs for a final cover system consisting of not less than two feet of soil cover.	Required	330.457(a)	Yes	Attachment 9, Section 2.1 and Drawing 6C.2		Closure Plan
682	Part III	For landfills with a synthetic bottom liner, provide a final cover system design that includes a synthetic membrane with a permeability less than or equal to the bottom.	Required	330.457(a)(1)	Yes	Attachment 9, Section 2.2, Paragraph 2		Closure Plan
683	Part III	nermeability less than or equal to the hottom Provide designs for a synthetic liner with minimum thickness of 20 mils, or 60 mils in the case of high-density polyethylene, to ensure proper seaming	Required	330.457(a)(1)	Yes	Attachment 9, Section 2.2, Paragraph 2		Closure Plan
684	Part III	For landfills with no synthetic bottom liner, provide a final cover system design that includes a minimum 18-inch thick clay-rich soil cover layer with a coefficient of permeability less than or equal to any constructed bottom liner or natural subsoil present. The coefficient of permeability shall not exceed 1 x 10-5 cm/sec	Required	330.457(a)(2)	No		Not Applicable	Closure Plan
685	Part III	Provide designs for an erosion layer that consist of at least six inches of soil capable of sustaining native plant growth and that will be seeded or sodded immediately following the application of the final cover Provide designs for cover of a Class 1 cell that	Required	330.457(a)(3)	Yes	Attachment 9, Section 2.3.8.2		Closure Plan
686	Part III	consist of 4ft. clay with permeability not > 1x10 ⁻⁷ overlain by 18in. Topsoil. If waste is to be placed above Class 1 cell, it must first be covered with a four-foot layer of compacted clayrich soil and must meet the requirements of 330.457 and include a flexible membrane	Required if Requested	330.457(b)	No		Not Applicable	Closure Plan
687	Part III	Provide for permeability quality control testing of the 18-inch cover at no less than 1 test/acre and submit data to ED	Required	330.457(c)	Yes	Attachment 9, Section 2.3.1.2, Table 9-2-2		Closure Plan
688	Part III	Demonstrate that the alternative final cover will achieve equivalent reduction in infiltration as the clay-rich soil cover layer specified under 330.457(a)(1) or (2)	Required if Requested	330.457(d)(1)	No		Not Applicable	Closure Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
689	Part III	Demonstrate that the alternative final cover will provide equivalent wind & water erosion protection as the erosion layer specified in 330.457(a)(3)	Required if Requested	330.457(d)(2)	No		Not Applicable	Closure Plan
690	Part III	Submit a written closure plan describing the steps necessary to close units at any time and a description of the final cover design, methods, and procedures to install the final cover	Required	330.457(e)(1)	Yes	Attachment 9		Closure Plan
691	Part III	Provide an estimate of the largest area needing final cover	Required	330.457(e)(2)	Yes	Attachment 9, Section 3.2.1		Closure Plan
692	Part III	Provide an estimate of max volume of waste ever on-site	Required	330.457(e)(3)	Yes	Attachment 9, Section 3.2.2		Closure Plan
693	Part III	Provide a schedule for completing closure activities	Required	330.457(e)(4)	Yes	Attachment 9, Section 4		Closure Plan
694	Part III	Provide a final contour map – depicting proposed final contours, top & side slopes, surface drainage features, and 100yr flood protection	Required	330.457(e)(5)	Yes	Attachment 3, Drawings 3.1, 3.2, and 3.3		Closure Plan
695	Part III	Provide the specifics for the implementation of closure plan and place a copy of the plan in the operating record by the initial receipt of waste	Required	330.457(f)(1)	Yes	Attachment 9, Section 1		Closure Plan
696	Part III	Notify the ED in writing of the intent to close the facility, 45 days prior to initiation of closure activities	Required	330.457(f)(2)	Yes	Attachment 9, Section 4.1		Closure Plan
697	Part III	Specify in the closure plan that the operator will begin closure no later than 30 days after final receipt of waste or no later than one year if the unit has remaining capacity and additional waste may be received	Required	330.457(f)(3)	Yes	Attachment 9, Section 4.1		Closure Plan
698	Part III	Provide for closure activities to be completed within 180 days of initiation	Required	330.457(f)(4)	Yes	Attachment 9, Section 4.1		Closure Plan
699	Part III	Provide for post-closure care requirements following completion of closure. Submit PE certification of closure by registered mail with supporting documentation.	Required	330.457(f)(5)	Yes	Attachment 9, Section 4.1		Closure Plan
700	Part III	Acknowledge that following receipt of closure documents and the inspection report by the TCEQ region, the ED may acknowledge termination of operation & closure & deem the facility properly closed	Acknowledgement	330.457(f)(6)	Yes	Attachment 9, Section 4.1		Closure Plan
701	Part III	Submit a certified copy within 10 days after landfill unit closure, of the "Affidavit to the Public". The Owner and Operator shall record a certified notation to the deed that the land has been used as a landfill facility	Required	330.457(g)	Yes	Attachment 9, Section 4.1		Closure Plan
702	Part III	Indicate that notice of closure will be published in the newspaper of largest circulation 90 days prior to the initiation of a final facility closure. The notice shall provide the name, address, and physical location of the facility; the TCEQ authorization number; and the last date of intended receipt of waste.	Required	330.461(a)	Yes	Attachment 9, Section 4.1		Closure Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
704	Part III	Acknowledge that least one closure sign will be posted at every point of access and notify all persons who utilize the facility of the date of closure and the prohibition against further receipt of waste materials.	Acknowledgement	330.461(b)	Yes	Attachment 9, Section 4.1		Closure Plan
710	Part III	Submit a closure plan for Storage and Processing units to remove all waste, waste residues, and any recovered materials. Units shall be dismantled and removed off-site or decontaminated.	Required	330.459(a)	No		Not Applicable	Closure Plan For Processing Facilities
711	Part III	Provide plans for the evacuation of all material on-site to an authorized facility and the disinfecting of all contaminated water handling units, tipping areas, processing and post-processing areas (as applicable)	Required	330.459(b)	No		Not Applicable	Closure Plan For Processing Facilities
712	Part III	Acknowledge that if there is evidence of a release, the ED may require an investigation, assessment, and or corrective action.	Acknowledgement	330.459(c)	No		Not Applicable	Closure Plan For Processing Facilities
713	Part III	Submit a plan (if combustible material is stored outdoors) for closure of a recycling facility that includes collecting processed and unprocessed materials, and transporting the materials to an authorized facility for disposition	Required	330.459(d)(1)	No		Not Applicable	Closure Plan For Processing Facilities
714	Part III	Provide for the closure plan to be implemented (if combustible material is stored outdoors) and completed within 180 days following the most recent acceptance of processed or unprocessed materials	Required	330.459(d)(2)	No		Not Applicable	Closure Plan For Processing Facilities
715	Part III	Submit a Post-Closure Plan that includes a PE certification of closure, and specify that the owner or operator shall retain the right of entry to and maintain all rights-of-way in order to conduct periodic inspections for a minimum 5 yrs. after certification of closure.	Required	330.63(i)	Yes	Attachment 9, Section 6.1		Post-Closure Plan
716	Part III	Provide for maintenance and control of cover material, erosion control, vegetative growth, leachate or methane migration, and subsidence or ponding of water on the unit. If any of these problems persist for longer than the first five years of post-closure care, the owner or operator shall be responsible for their correction	Required	330.463(a)(1)	Yes	Attachment 9, Section 6.1		Post-Closure Plan
717	Part III	Acknowledge that the ED may reduce the post- closure period for the unit if all wastes and waste residues have been removed during closure	Acknowledgement	330.463(a)(1)	No		Not Applicable	Post-Closure Plan
718	Part III	Provide for continued monitoring programs, i.e., groundwater monitoring, resistivity surveys, methane monitoring, etc.; during the post-closure care period.	Required	330.463(a)(2)	Yes	Attachment 9, Section 6.1		Post-Closure Plan
719	Part III	Acknowledge that the ED may require an investigation into the nature and extent of any release from the facility and an assessment to correct an impact to groundwater	Acknowledgement	330.463(a)(3)	Yes	Attachment 9, Section 6.3		Post-Closure Plan
720	Part III	Provide for 30-year post-closure care after PE certification of closure	Required	330.463(b)(1)	Yes	Attachment 9, Section 6.1, Paragraph 1		Post-Closure Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
721	Part III	Provide for right of entry and the maintenance of all rights-of-way, conduct site maintenance and/or remediation, maintain final cover, vegetation, drainage & correct as needed	Required	330.463(b)(1)(A)	Yes	Attachment 9, Section 6.1		Post-Closure Plan
722	Part III	Provide maintenance and operation of the leachate collection system	Required	330.463(b)(1)(B)	Yes	Attachment 9, Section 6.1		Post-Closure Plan
723	Part III	Provide for maintenance and monitoring of the groundwater monitoring system per requirements of Subchapter J	Required	330.463(b)(1)(C)	Yes	Attachment 9, Section 6.1		Post-Closure Plan
724	Part III	Provide for maintenance and monitoring of gas system per requirements of Subchapter I	Required	330.463(b)(1)(D)	Yes	Attachment 9, Section 6.1		Post-Closure Plan
725	Part III	Provide for continued earth electrical resistivity surveys per site development plan	Required	330.463(b)(1)(E)	No		Not Applicable	Post-Closure Plan
726	Part III	Place a copy of the post-closure plan in the operating record by initial receipt of waste.	Required	330.463(b)(3)	Yes	Attachment 9, Section 1		Post-Closure Plan
727	Part III	Submit a description of the monitoring and maintenance activities required and the frequency at which these activities will be performed	Required	330.463(b)(3)(A)	Yes	Attachment 9, Section 6.1		Post-Closure Plan
728	Part III	Provide the name, address, & phone number of responsible person	Required	330.463(b)(3)(B)	Yes	Attachment 9, Section 7		Post-Closure Plan
729	Part III	Provide a description of the planned use of closed unit during the post closure period	Required	330.463(b)(3)(C)	Yes	Attachment 9, Section 8		Post-Closure Plan
730	Part III	Provide a detailed written estimate of the cost of post-closure care maintenance and any corrective action as described in the post-closure care plan or required by the ED per Subchapter L	Required	330.463(b)(3)(D)	Yes	Attachment 9, Section 9 and Attachment 8		Post-Closure Plan
731	Part III	Indicate that a certification of completion of post-closure care signed by a PE will be submitted at the end of the post-closure care period	Required	330.465(a)	Yes	Attachment 9, Section 6.4		Post-Closure Plan
739	Part III	Provide a closure cost estimate that equals the costs of closure of the facility, including disposition of the maximum inventories of all waste; processed and unprocessed combustible materials stored outdoors on site during the life of the facility	Required	330.505(a)(2)(A)	Yes	Attachment 9, Section 5, amd Attachment 8		Closure Cost Estimates
740	Part III	Provide a closure cost estimate that is based on the costs of hiring a third party that is not affiliated with the owner or operator; and is based on a per cubic yard and/or short ton measure for collection and disposition costs.	Required	330.505(a)(2)(B-(C)	Yes	Attachment 9, Section 5, and Attachment 8, Section 2		Closure Cost Estimates
741	Part III	Provide for the closure cost estimate & financial assurance to be increased if conditions change which increase the maximum cost of closure at any time during the active life of the facility	Required	330.505(a)(3)	Yes	Attachment 8, Section 4		Closure Cost Estimates
742	Part III	A reduction in the closure cost estimate and the amount of financial assurance may be approved if the cost estimate exceeds the maximum cost of closure at any time during the remaining life of the facility.	Required if Requested	330.505(a)(4)	Yes	Attachment 8, Section 4		Closure Cost Estimates

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
743	Part III	Provide for the maintenance of financial assurance for Recycling facilities that store combustible materials outdoors or that pose a risk	Required	330.505(b)(1)	No		Not Applicable	Closure Cost Estimates
744	Part III	Provide for the maintenance of financial assurance until closure is approved by ED.	Required	330.505(b)(2)	Yes	Attachment 8, Section 1		Closure Cost Estimates
745	Part III	Submit a Post-Closure Care Cost Estimates for the cost of hiring a third party to conduct post-closure care activities. The cost estimate shall account for the total costs of conducting post closure care for the largest area that could possibly require post-closure care in the year to follow over the entire post closure care period.	Required	330.507(a)	Yes	Attachment 8, Section 3 and Appendix 8C		Post-Closure Care Cost Estimates for Landfills
746	Part III	Submit an increase in the post-closure care cost estimate and the amount of financial assurance if changes in the post-closure care plan or the unit conditions increase the maximum costs of post-closure care	Required if Requested	330.507(a)(1)	No		Not Applicable	Post-Closure Care Cost Estimates for Landfills
747	Part III	Submit a reduction in the post-closure care cost estimate and the amount of financial assurance if the cost estimate exceeds the maximum costs of post-closure care remaining and a notice is provided to the ED of the detailed justification for the reduction of the cost estimate and the amount of financial assurance as a permit modification.	Required	330.507(a)(2)	Yes	Attachment 8, Section 4		Post-Closure Care Cost Estimates for Landfills
748	Part III	Implement a corrective action program and a detailed written cost estimate of the cost of hiring a third party to perform the corrective action program. The corrective action cost estimate shall account for the total costs of corrective action activities	Required if Requested	330.509(a)	No		Not Applicable	Corrective Action Cost Estimate
749	Part III	The corrective action cost estimate and the amount of financial assurance shall be increased if changes in the corrective action program or unit conditions increase the maximum costs of corrective action	Required if Requested	330.509(a)(1)	No		Not Applicable	Corrective Action Cost Estimate
750	Part III	A reduction in the cost estimate and the amount of financial assurance for corrective action may be approved if the cost estimate exceeds the maximum remaining costs of corrective action at any time during the remaining corrective action period	Required if Requested	330.509(a)(2)	No		Not Applicable	Corrective Action Cost Estimate
751	Part III	Provide financial assurance for the costs of the most recent corrective action program. Continuous financial assurance coverage for each corrective action program shall be provided until the facility is officially released in writing by the ED	Required if Requested	330.509(b)	No		Not Applicable	Corrective Action Cost Estimate
752	Part III	Provide financial assurance per Chapter 37, Subchapter R	Required	330.503(b)	Yes	Attachment 8, Section 3		Financial Assurance

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
753	Part III	Provide for financial assurance for post-closure cost. Continuous financial assurance coverage for post-closure care shall be provided	Required	330.507(b)	Yes	Attachment 8, Section 3		Financial Assurance
754	Part III	Provide Maps/Drawings with elements referenced under 330.57(h)(1)-(6) (Legible, Standard Engineering Scale, Dated Title and Revision Blocks, Seal, Drawing and Page No., North Arrow, Base Map Source, Legend, Section Lines)	Required	330.57(h)(1)-(6)	Yes	Attachments 1, 2, 3, and other attachments with drawings		Format-Maps/Drawings
755	Part IV	A site operating plan shall cover all on-site units in accordance with Subchapters D & E of Chapter 330.	Informational	330.65(a)			Part IV	Site Operating Plan
756	Part IV	A facility that has an environmental management system that meets both the minimum standards described in 30 TAC §90.32 of this title and the United States Environmental Protection Agency's National Environmental Performance Track is not subject to site operating plan requirements	Informational	330.65(b)			Not Applicable	Site Operating Plan
757	Part IV	In the event the executive director terminates authorization to operate under an environmental management system, the facility will comply with the site operating plan requirements within 90 days.	Informational	330.65(b)			Not Applicable	Site Operating Plan
758	Part IV	Provide procedures for recirculating leachate or gas condensate	Required if Requested	330.65(c)	Yes	Part IV, Section 4.22		Site Operating Plan
759	Part IV	Acknowledge that the site development plan, site operating plan, final closure plan, post-closure maintenance plan, landfill gas management plan, & all other documents are operating requirements & part of the operating record.	Acknowledgement	330.121(a)	Yes	Part IV, Section 7.1		Site Operating Plan
760	Part IV	Acknowledge that any deviation from the permit and incorporated plans or other related documents associated with the permit is a violation of this chapter	Acknowledgement	330.121(a)	Yes	Part IV, Section 7.1		Site Operating Plan
761	Part IV	Acknowledgment that the SLER will be submitted to the ED 14 days prior to waste disposal operations for each new disposal area	Acknowledgement	330.123	Yes	Part IV, Section 7.3		Site Operating Plan
762	Part IV	Acknowledge that all information required to be in the site operating record to be placed in the operating record within seven (7) days of completion or receipt	Acknowledgement	330.125(b)	Yes	Part IV, Section 7.1		Site Operating Plan
763	Part IV	Acknowledge that all location restriction demonstrations will be maintained in the site operating record	Acknowledgement	330.125(b)(1)	Yes	Part IV, Section 7.1, Paragraph 2		Site Operating Plan
765	Part IV	Acknowledge that all results of gas monitoring & any remediation plans relating to explosive and other gases will be maintained in the site operating record	Acknowledgement	330.125(b)(3)	Yes	Part IV, Section 7.1, Paragraph 2		Site Operating Plan
766	Part IV	Acknowledge that all unit design documentation regarding placement of leachate or gas condensate will be maintained in the site operating record	Acknowledgement	330.125(b)(4)	Yes	Part IV, Section 7.1, Paragraph 2		Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
767	Part IV	Acknowledge that all demonstration, certification, findings, monitoring, testing, and analytical data relating to groundwater monitoring and corrective action will be maintained in the site operating record	Acknowledgement	330.125(b)(5)	Yes	Part IV, Section 7.1, Paragraph 2		Site Operating Plan
768	Part IV	Acknowledge that all closure and post-closure care plans and any monitoring, testing, or analytical data relating to post-closure requirements will be maintained in the site operating record	Acknowledgement	330.125(b)(6)	Yes	Part IV, Section 7.1, Paragraph 2		Site Operating Plan
769	Part IV	Acknowledge that all cost estimates and financial assurance documentation relating to financial assurance for closure and post-closure will be maintained in the site operating record	Acknowledgement	330.125(b)(7)	Yes	Part IV, Section 7.1, Paragraph 2		Site Operating Plan
770	Part IV	Acknowledge that all documentation of compliance with small community exemption criteria will be maintained in the site operating record	Acknowledgement	330.125(b)(8)	No		Not Applicable	Site Operating Plan
771	Part IV	Acknowledge that copies of all correspondence and responses relating to the operation of the facility, modifications to the permit, approvals, and other matters pertaining to technical assistance will be maintained in the site operating record	Acknowledgement	330.125(b)(9)	Yes	Part IV, Section 7.1, Paragraph 2		Site Operating Plan
772	Part IV	Acknowledge that all documents, manifests, shipping documents, trip tickets, etc., involving special waste will be maintained in the site operating record	Acknowledgement	330.125(b)(10)	Yes	Part IV, Section 7.1, Paragraph 2		Site Operating Plan
773	Part IV	Acknowledge that records of the application rate and total amount of any spray-applied alternative daily cove applied to the working face will be maintained in the site operating record.	Acknowledgement	330.125(b)(11)	No		Not Applicable	Site Operating Plan
774	Part IV	Acknowledge that any other documents specified by the permit or Executive Director will be maintained in the site operating record	Acknowledgement	330.125(b)(12)	Yes	Part IV, Section 7.1, Paragraph 2		Site Operating Plan
775	Part IV	Acknowledge that the site operating record will maintain all required documents in an organized format and in accordance with the time frames specified in 330.125(b), and will be furnished upon request to the executive director and must be made available for inspection by the executive director	Acknowledgement	330.125(c)	Yes	Part IV, Section 7.1		Site Operating Plan
776	Part IV	Indicate that the operating record will be maintained for life & post-closure period of the facility	Required	330.125(d)	Yes	Part IV, Section 7.1,		Site Operating Plan
777	Part IV	Indicate that all training records will be maintained in accordance with 30 TAC §335.586(d) & (e)	Required	330.125(e)	Yes	Part IV, Section 7.1		Site Operating Plan
778	Part IV	Indicate that personnel operating licenses issued under 30 TAC Chapter 30, Subchapter F will be maintained in the site operating record	Required	330.125(f)	Yes	Part IV, Section 7.1		Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
779	Part IV	Indicate that the executive director may set alternative schedule for recordkeeping & notification	Required	330.125(g)	No		Not Applicable	Site Operating Plan
780	Part IV	Indicate that records documenting the annual waste acceptance rate will be maintained in the site operating record	Required	330.125(h)	Yes	Part IV, Section 7.1		Site Operating Plan
781	Part IV	Indicate that documentation of waste acceptance rate will include maintaining annual & quarterly waste summary reports required by 30 TAC §330.675	Required	330.125(h)	Yes	Part IV, Section 7.1,; and Part IV, Section 4.1		Site Operating Plan
782	Part IV	Indicate that the facility will provide the reports required by 30 TAC §330.675 to the Executive Director	Required	330.675	Yes	Part IV, Section 7.2		Site Operating Plan
783	Part IV	Indicate that if the annual waste acceptance rate exceeds the rate estimated in the landfill permit application and the waste increase is not due to a temporary occurrence, the owner or operator shall file an application to modify the permit application, including the revised estimated waste acceptance rate, in accordance with 30 TAC §305.70(k) of this title (relating to Municipal Solid Waste Permit and Registration Modifications), within 90 days of the exceedance as established by the sum of the previous four quarterly summary reports.	Required	330.125(h)	Yes	Part IV, Section 7.2		Site Operating Plan
784	Part IV	Provide a description of the function & minimum qualifications of key personnel	Required	330.127(1)	Yes	Part IV, Section 2.1		Site Operating Plan
785	Part IV	Provide a description of the minimum number, size, type and function of the equipment to be utilized at the facility	Required	330.127(2)	Yes	Part IV, Section 3, Table 3.1		Site Operating Plan
786	Part IV	Provide a description of the provisions for back- up equipment during periods of breakdown or maintenance of this listed equipment	Required	330.127(2)	Yes	Part IV, Section 3, Paragraph 2		Site Operating Plan
787	Part IV	Provide general instructions for personnel concerning operational requirements	Required	330.127(3)	Yes	Part IV, Section 2.1		Site Operating Plan
788	Part IV	Identify all applicable training requirements under 30 TAC §335.586(a) & (c) that must be followed	Required	330.127(4)	Yes	Part IV, Section 2.2, Table 2.2		Site Operating Plan
789	Part IV	Provide procedures for the detection and prevention of the disposal of prohibited wastes, including hazardous waste & PCB wastes	Required	330.127(5)	Yes	Part IV, Section 5.1		Site Operating Plan
790	Part IV	Provide procedures for random inspections of incoming loads including the inspection of compactor vehicles.	Required	330.127(5)(A)	Yes	Part IV, Section 5.2		Site Operating Plan
791	Part IV	Indicate that trained staff shall observe each load that is disposed at the landfill	Required	330.127(5)(A)	Yes	Part IV, Section 5.2		Site Operating Plan
792	Part IV	Indicate that records will be kept of all waste load inspections	Required	330.127(5)(B)	Yes	Part IV, Section 5.3		Site Operating Plan
793	Part IV	Indicate that facility personnel inspecting or observing loads must have training to recognize prohibited waste	Required	330.127(5)(C)	Yes	Part IV, Section 5.1 ang 5.4		Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
794	Part IV	Indicate that notification will be provide to executive director and to any local pollution agency with jurisdiction that has requested to be notified, of the receipt or disposal of hazardous or PCB waste	Required	330.127(5)(D)	Yes	Part IV, Section 5.5		Site Operating Plan
795	Part IV	Provide provisions for remediation of hazardous or PCB waste that has been received for disposal at the facility	Required	330.127(5)(E)	Yes	Part IV, Section 5.1, Bullet 8 and Section 5.5		Site Operating Plan
796	Part IV	Indicate that the facility will maintain a source of earthen material available to extinguish fires, sized to cover waste not covered with six inches of earthen material within one hour of detecting a fire.	Required	330.129	Yes	Part IV, Section 6.1, Bullet 6		Site Operating Plan
797	Part IV	Provide a demonstration, including calculations, showing that sufficient on-site equipment and earthen material stockpile is available to cover any waste not already covered with six inches of earthen material within one hour of detecting a fire	Required	330.129	Yes	Part IV, Section 6.1		Site Operating Plan
798	Part IV	Indicate that sufficient on-site equipment must be provided to place a six-inch layer of earthen material to cover any waste not already covered with six inches of earthen material within one hour of detecting a fire	Required	330.129	Yes	Part IV, Section 6.1		Site Operating Plan
799	Part IV	Provide fire protection standards & training procedures	Required	330.129	Yes	Part IV, Section 2.2;and Section 6.2		Site Operating Plan
800	Part IV	Identify other activities requiring fire protection and provide protection measures specific to each individual activity	Required	330.129	Yes	Part IV, Section 6.3		Site Operating Plan
801	Part IV	Indicate that if a fire occurs that is not extinguished within ten minutes of detection, the commission's regional office must be contacted immediately after detection, but no later than four hours by telephone, and in writing within 14 days with a description of the fire and the resulting response.	Required	330.129	Yes	Part IV, Section 6.2		Site Operating Plan
802	Part IV	Provide provisions for access control to the facility	Required	330.131	Yes	Part IV, Section 4.1		Site Operating Plan
803	Part IV	Provide an inspection and maintenance schedule for access control features	Required	330.131	Yes	Part IV, Section 4.1.1		Site Operating Plan
804	Part IV	Indicate that the commission's regional office, and any local pollution agency with jurisdiction that has requested to be notified, must be notified of the breach within 24 hours of detection. Indicate that the breach must be temporarily repaired within 24 hours of detection and must be permanently repaired by the time specified to the commission's regional office when it was reported in the initial breach report. Indicate that if a permanent repair can be made within eight hours of detection, no notice to the commission's regional office is required.	Required	330.131	Yes	Part IV, Section 4.1.1		Site Operating Plan
805	Part IV	Identify all unloading areas and specify maximum size of each unloading area.	Required	330.133(a)	Yes	Part IV, Section 4.2.1 and Section 4.2.2		Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
806	Part IV	Indicate that trained staff will monitor incoming loads at each unloading area	Required	330.133(a)	Yes	Part IV, Section 4.2.1 and Section 4.2.2		Site Operating Plan
807	Part IV	Indicate that the unloading of waste in unauthorized areas is prohibited.	Required	330.133(b)	Yes	Part IV, Section 4.2		Site Operating Plan
814	Part IV	At Type IV landfills, only brush, C&D, & rubbish free of putrescible and household waste are allowed	Informational	330.133(e)			Not Applicable	Site Operating Plan
815	Part IV	Submit a written procedure that will ensure that containers with any putrescible wastes are not accepted at the landfill	Required	330.133(f)(1)	No		Not Applicable	Site Operating Plan
816	Part IV	Submit a written procedure for the immediate removal of any putrescible wastes and other prohibited waste disposed of at the landfill	Required	330.133(f)(2)	No		Not Applicable	Site Operating Plan
817	Part IV	Provide a procedure for transporter certifications that will be retained at the landfill and available for inspection by the executive director	Required	330.133(f)(3)	No		Not Applicable	Site Operating Plan
818	Part IV	Acknowledge that Type IV landfills may only accept waste in enclosed containers or enclosed vehicles in accordance with 30 TAC §330.169	Acknowledgement	330.133(g)	No		Not Applicable	Site Operating Plan
819	Part IV	Provide a description of wastes that are not allowed and state the landfill's requirements for transporters	Required	330.133(h)	No		Not Applicable	Site Operating Plan
820	Part IV	Specify waste acceptance and operating hours	Required	330.135(a)	Yes	Part IV, Section 4.3		Site Operating Plan
821	Part IV	The waste acceptance hours of a municipal solid waste facility may be any time between the hours of 7:00 a.m. and 7:00 p.m., Monday through Friday, unless otherwise approved in the authorization for the facility. Waste acceptance hours within the 7:00 a.m. to 7:00 p.m. weekday span do not require other specific approval. Transportation of materials and heavy equipment operation must not be conducted between the hours of 9:00 p.m. to 5:00 a.m., unless otherwise approved in the authorization for the facility. Operating hours for other activities do not require specific approval.	Informational	330.135(a)			Part IV, Section 4.3	Site Operating Plan
822	Part IV	Specify alternative operating hours of up to five days in a calendar year to accommodate special occasions, special purpose events, holidays, or other special occurrences	Required If Requested	330.135(b)	Yes	Part IV, Section 4.3		Site Operating Plan
823	Part IV	Indicate that the facility will record in the site operating record the dates, times, and duration when any alternative operating hours are utilized	Required	330.135(d)	Yes	Part IV, Section 4.3		Site Operating Plan
824	Part IV	Indicate that a sign measuring at least 4' X 4' with letters at least three inches in height must be displayed at all entrances.	Required	330.137	Yes	Part IV, Section 4.4		Site Operating Plan
825	Part IV	Indicate that information on the sign must include the facility type, hours and days of operation, an emergency 24hr. Contact number, local fire department number & permit number	Required	330.137	Yes	Part IV, Section 4.4		Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
826	Part IV	Indicate that windblown waste and litter at the working face must be controlled by using engineering methods or measures, including portable panels, temporary fencing, and perimeter fencing or comparable engineering controls.	Required	330.139(1)	Yes	Part IV, Section 4.5		Site Operating Plan
827	Part IV	Provide a plan for daily management of litter scattered throughout the site, along fences and access roads, and at the gate	Required	330.139(2)	Yes	Part IV, Section 4.5		Site Operating Plan
828	Part IV	Indicate that no unloading, storage, disposal, or processing operations will occur within easements, buffer zones, or rights-of-way that crosses the site, and that no disposal shall occur within 25 feet of the center line of any utility line or pipeline easement, unless otherwise authorized by the executive director	Required	330.141(a)	Yes	Part IV, Section 4.6.1 and Section 4.6.2		Site Operating Plan
829	Part IV	Indicate that all pipeline and utility easements must be clearly marked with posts that extend at least six feet above ground level, spaced at intervals no greater than 300 feet	Required	330.141(a)	Yes	Part IV, Section 4.6.1		Site Operating Plan
830	Part IV	Indicate that a minimum separating distance shall be maintained between solid waste processing and disposal activities within and adjacent to the facility boundary on property owned or controlled by the owner or operator as determined by the requirements of 30 TAC §330.543. The buffer zone must provide for safe passage for fire-fighting and other emergency vehicles.	Required	330.141(b)	Yes	Part IV, Section 4.6.2		Site Operating Plan
831	Part IV	Indicate that the visibility of all required landfill markers and the benchmark must be maintained	Required	330.143(a)	Yes	Part IV, Section 4.7		Site Operating Plan
832	Part IV	Indicate that landfill markers must be inspected on a monthly basis and records of all inspections placed in the site operating record	Required	330.143(a)	Yes	Part IV, Section 4.7, Paragraph 1		Site Operating Plan
833	Part IV	indicate that all markers must be replaced within 15 days of removal, destruction, or a determination that the markers do not meet regulatory requirements.	Required	330.143(a)	Yes	Part IV, Section 4.7		Site Operating Plan
834	Part IV	Landfill markers must be installed to clearly mark significant features and that the executive director may modify specific marker requirements to accommodate unique sitespecific conditions.	Required	330.143(b)	Yes	Part IV, Section 4.7		Site Operating Plan
835	Part IV	Indicate that markers must be posts extending 6ft. above ground and not obscured	Required	330.143(b)(1)	Yes	Part IV, Section 4.7		Site Operating Plan
836	Part IV	Provide the color coding for on-site markers that is in compliance with 330.143(b)(1)(A) – (F)	Required	330.143(b)(1)(A) - (F)	Yes	Part IV, Section 4.7		Site Operating Plan
837	Part IV	Indicate that boundary markers must be placed at each corner of the facility and along boundary line at intervals not greater than 300 ft.	Required	330.143(b)(2)	Yes	Part IV, Section 4.7		Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
838	Part IV	Indicate that markers identifying the buffer zone will placed along each buffer zone boundary at intervals of no greater than 300 ft.	Required	330.143(b)(3)	Yes	Part IV, Section 4.7		Site Operating Plan
839	Part IV	Indicate that easement and right-of-way markers must be placed along the centerline of an easement and along the boundary of a right-of-way at each corner within the facility and at the intersection of the facility boundary	Required	330.143(b)(4)	Yes	Part IV, Section 4.7		Site Operating Plan
840	Part IV	Indicate that a landfill grid system must be installed unless written approval from the executive director has been received.	Required	330.143(b)(5)	Yes	Part IV, Section 4.7		Site Operating Plan
841	Part IV	Indicate that grid system will encompass at least the area expected to be filled within the next three-year period and that marks must be spaced no greater than 100 feet apart measured along perpendicular lines and that where markers cannot be seen from opposite boundaries, intermediate markers must be installed, where feasible.	Required	330.143(b)(5)	Yes	Part IV, Section 4.7		Site Operating Plan
842	Part IV	Indicate that soil liner or geomembrane markers will be placed so that areas under evaluation can be determined & maintained through construction & operation period.	Required	330.143(b)(6)	Yes	Part IV, Section 4.7		Site Operating Plan
843	Part IV	Indicate that the location of the liner markers must be tied into the landfill grid system and must be reported on each soil liner evaluation report or geomembrane liner evaluation report submitted	Required	330.143(b)(6)	Yes	Part IV, Section 4.7		Site Operating Plan
844	Part IV	Indicate that liner area markers must not be placed inside constructed areas.	Required	330.143(b)(6)	Yes	Part IV, Section 4.7		Site Operating Plan
845	Part IV	Indicate that flood protection markers must be installed for any area within a solid waste disposal facility that is within the 100-year floodplain and that areas subject to flooding must be clearly marked by means of permanent posts not more than 300 feet apart or closer if necessary to retain visual continuity.	Required	330.143(b)(7)	Yes	Part IV, Section 4.7		Site Operating Plan
846	Part IV	Indicate that a permanent benchmark must be established and accessible and must be a bronze survey marker in concrete stamped with elevation and date stamped on it and that the benchmark must be surveyed from a known United States Coast and Geodetic Survey benchmark or other reliable benchmark	Required	330.143(b)(8)	Yes	Part IV, Section 4.7		Site Operating Plan
847	Part IV	Indicate that the facility owner or operator shall take steps to encourage that vehicles hauling waste to the facility are enclosed or provided with a tarpaulin, net, or other means to effectively secure the load in order to prevent the escape of any part of the load by blowing or spilling.	Required	330.145	Yes	Part IV, Section 4.8		Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
848	Part IV	Indicate that the owner or operator shall take actions such as posting signs, reporting offenders to proper law enforcement officers, adding surcharges, or similar measures.	Required	330.145	Yes	Part IV, Section 4.8		Site Operating Plan
849	Part IV	Indicate that on days when the facility is in operation, the owner or operator shall be responsible for at least once per day cleanup of waste materials spilled along and within the right-of-way of public access roads serving the facility for a distance of two miles in either direction from any entrances used for the delivery of waste to the facility.	Required	330.145	Yes	Part IV, Section 4.8		Site Operating Plan
850	Part IV	Indicate that the facility operator will consult with the Texas Department of Transportation, county, and/or local governments with maintenance authority over the roads concerning cleanup of public access roads and rights-of-way	Required	330.145	Yes	Part IV, Section 4.8		Site Operating Plan
851	Part IV	Indicate that large, heavy, bulky items that cannot be incorporated in the regular spreading, compaction, and covering operations at landfill should be recycled and that a large item salvage area should be established & items removed often enough to prevent nuisance or discharge	Required	330.147(a)	Yes	Part IV, Section 4.9		Site Operating Plan
852	Part IV	Indicate the items that can be classified as large, heavy, or bulky. This can include, but is not limited to, white goods (household appliances), air conditioner units, metal tanks, large metal pieces, and automobiles.	Required	330.147(b)	Yes	Part IV, Section 4.9		Site Operating Plan
853	Part IV	Indicate that refrigerators, freezer, air conditioners, and any other items containing CFCs must be handled in accordance with 40 CFR 82.156(f)	Required	330.147(c)	Yes	Part IV, Section 4.9		Site Operating Plan
854	Part IV	Provide an odor management plan that addresses the sources of odors and includes general instructions to control odors or the sources of odors. The plans for odor management must include the identification of wastes that require special attention such as septage, grease trap waste, dead animals, and leachate	Required	330.149	Yes	Part IV, Section 4.10.2		Site Operating Plan
855	Part IV	Provide procedures for the control of on-site populations of disease vectors including the use of proper compaction and daily cover procedures, and the use of other approved methods when needed. The general methods and performance-based frequencies for disease vector control must be specified	Required	330.151	Yes	Part IV, Section 4.11		Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
856	Part IV	Provide a description for all weather access roads from the facility to public roads and within the facility. Indicate that tracked mud & debris on public roadway removed once a day on days when mud and associated debris are being tracked onto the public roadway. Provide a description of the specific method for controlling mud & debris	Required	330.153(a)	Yes	Part IV, Section 4.12		Site Operating Plan
857	Part IV	Indicate that tracked mud & associated debris on public roadway removed once a day on days when mud and associated debris are being tracked onto the public roadway.	Required	330.153(a)	Yes	Part IV, Section 4.12		Site Operating Plan
858	Part IV	Provide a description of the specific method for controlling mud & debris	Required	330.153(a)	Yes	Part IV, Section 4.12		Site Operating Plan
859	Part IV	Specify method of dust control or suppression	Required	330.153(b)	Yes	Part IV, Section 4.12		Site Operating Plan
860	Part IV	Provide a description, including frequency, of how all on site roadways will be maintained to minimize depressions, ruts, and potholes	Required	330.153(c)	Yes	Part IV, Section 4.12		Site Operating Plan
861	Part IV	Indicate that litter and any other debris must be picked up at least daily and taken to the working face for disposal	Required	330.153(c)	Yes	Part IV, Section 4.12		Site Operating Plan
862	Part IV	Indicate that salvaging operations must not interfere with prompt sanitary disposal of solid waste or to create public health nuisances.	Required	330.155	Yes	Part IV, Section 4.13		Site Operating Plan
863	Part IV	Indicate that salvaged items will be removed often enough to prevent becoming a nuisance, preclude the discharge of any pollutants, or to prevent an excessive accumulation of material.	Required	330.155	Yes	Part IV, Section 4.13		Site Operating Plan
864	Part IV	Indicate that Class 1 industrial and other special wastes received at the disposal facility must not be salvaged.	Required	330.155	Yes	Part IV, Section 4.13		Site Operating Plan
865	Part IV	Indicate that pesticide, fungicide, rodenticide, and herbicide containers must not be salvaged unless being salvaged through a state-supported recycling program.	Required	330.155	Yes	Part IV, Section 4.13		Site Operating Plan
866	Part IV	Indicate that scavenging is prohibited.	Required	330.155	Yes	Part IV, Section 4.13		Site Operating Plan
867	Part IV	Specify criteria for the protection of identified endangered species	Required	330.157	Yes	Part IV, Section 4.14		Site Operating Plan
868	Part IV	Indicate that landfill gas report and submittals must be maintained in operating record	Required	330.159	Yes	Part IV, Section 4.15		Site Operating Plan
869	Part IV	Indicate that within 30 days of discovery, notice will be provide to the executive director of the location of any and all existing or abandoned water wells, oil wells, natural gas wells or other wells situated within the facility.	Required	330.161(a)-(b)	Yes	Part IV, Section 4.16		Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
870	Part IV	Indicate that within 30 days of discovery, the facility will provide the executive director with notification and written certification that the water well has been capped, plugged, and closed in accordance with all applicable rules and regulations of the commission or other state agency	Required	330.161(a)	Yes	Part IV, Section 4.16		Site Operating Plan
872	Part IV	Indicate that the executive director may approve any well used to supply water at the facility that is located within the permit boundary if it is determined that the well is outside the waste footprint, it is not impacted by landfill operations, it can be demonstrated that well design and installation will prevent any crosscontamination from the waste management unit to the water well production zone and between any water bearing zones, and an approved sampling plan to include frequency and parameters is in place.	Required	330.161(a)	No		Not Applicable	Site Operating Plan
873	Part IV	Indicate that any water or other type of wells under the jurisdiction of the commission must be plugged in accordance with all applicable state requirements or additional requirements imposed by the executive director and that a copy of the well plugging report required to be submitted to the appropriate state agency and must also be submitted to the executive director within 30 days after the well has been plugged.	Required	330.161(c)	Yes	Part IV, Section 4.16		Site Operating Plan
874	Part IV	Indicate that any proposed changes to the liner installation plan as a result of any well abandonment will be submit for executive director approval as permit modification	Required	330.161(d)	Yes	Part IV, Section 4.16		Site Operating Plan
875	Part IV	Specify the methods of compaction of waste	Required	330.163	Yes	Part IV, Section 4.17		Site Operating Plan
876	Part IV	Indicate that the landfill must apply six inches of well-compacted earthen material not previously mixed with garbage, rubbish, or other solid waste at the end of each operating day to control disease vectors, fires, odors, windblown litter or waste, and scavenging, unless the executive director requires a more frequent interval.	Required	330.165(a)	Yes	Part IV, Section 4.18.2		Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
877	Part IV	Indicate that the landfill must apply six inches of well-compacted earthen material not previously mixed with garbage, rubbish, or other solid waste at least weekly to control disease vectors, fires, odors, windblown litter or waste, and scavenging, unless the executive director requires a more frequent interval.	Required	330.165(b)	No		Not Applicable	Site Operating Plan
878	Part IV	Landfills that operate on a 24-hour basis must cover the working face or active disposal area at least once every 24 hours. The executive director may require a chemical analysis of any landfill cover material. Runoff from areas that have intact daily cover is not considered as having come into contact with the working face or leachate.	Informational	330.165(a)				Site Operating Plan
879	Part IV	Indicate that all areas that have received waste but will be inactive for longer than 180 days must provide intermediate or final cover.	Required	330.165(c)	Yes	Part IV, Section 4.18.2		Site Operating Plan
880	Part IV	Indicate that all intermediate cover will be six inches of suitable earthen material that is capable of sustaining native plant growth and must be seeded or sodded following its application in order to control erosion, or must be a material approved by the executive director that will otherwise control erosion. This intermediate cover must not be less than 12 inches of suitable earthen material. The intermediate cover must be graded to prevent ponding of water. Plant growth or other erosion control features must be maintained. Runoff from areas that have intact intermediate cover is not considered as having come into contact with the working face or leachate.	Required	330.165(c)	Yes	Part IV, Section 4.18.3		Site Operating Plan
881	Part IV	Indicate that alternative daily cover may only be allowed by a temporary authorization under §305.62(k)(1)(A) of this title (relating to Municipal Solid Waste Permit and Registration Modifications) followed by a major amendment or a modification in accordance with §305.70(k)(1) of this title. Use of alternative daily cover is limited to a 24-hour period after which either waste or daily cover as defined in subsection (a) of this section must be placed.	Required If Requested	330.165(d)	No		Not Applicable	Site Operating Plan
882	Part IV	Provide a alternative daily cover operating plan that includes the information required by 30 TAC §330.165(d)(1)(A) - (E)	Required If Requested	330.165(d)(1)(A)-(E)	No		Not Applicable	Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
883	Part IV	Indicate that status reports on the alternative daily cover must be submitted on a two-month basis to the executive director during the temporary authorization period describing the effectiveness of the alternative material, any problems that may have occurred, and corrective actions required as a result of such problems.	Required If Requested	330.165(d)(2)	No		Not Applicable	Site Operating Plan
884	Part IV	Indicate that alternative daily cover must not be allowed when the landfill is closed for a period greater than 24 hours, unless the executive director approves an alternative length of time	Required If Requested	330.165(d)(3)	No		Not Applicable	Site Operating Plan
885	Part IV	Indicate that the constituents of concern in contaminated soils used as shall not exceed the concentrations listed in Table 1, Constituents of Concern and Their Maximum Leachable Concentrations, located in 30 TAC §335.521(a)(1)	Required If Requested	330.165(d)(4)	No		Not Applicable	Site Operating Plan
886	Part IV	Indicate that contaminated soils used as ADC will not contain PCB waste subject to 40 CFR Part 761	Required If Requested	330.165(d)(4)(A)	No		Not Applicable	Site Operating Plan
887	Part IV	Indicate that contaminated soils used as ADC will not contain TPH concentrations greater that 1,500 ppm unless ED approves a suitability demonstration	Required If Requested	330.165(d)(4)(B)	No		Not Applicable	Site Operating Plan
888	Part IV	ADC must not exceed constituent limits imposed on waste disposed at the facility	Required If Requested	330.165(d)(5)	No		Not Applicable	Site Operating Plan
889	Part IV	Indicate that the executive director may require the facility to test runoff from areas that have alternative daily cover for compliance with Texas Pollutant Discharge Elimination System storm water discharge limits or manage the runoff as contaminated water.	Required If Requested	330.165(d)(6)	No		Not Applicable	Site Operating Plan
890	Part IV	Provide a demonstration if there are any extreme seasonal climatic conditions that make meeting requirements of 30 TAC §330.165(a) - (d) impractical. Based on this demonstration the executive director may grant a temporary waiver from the requirements of subsections 30 TAC §330.165(a) - (d)	Required If Requested	330.165(e)	No		Not Applicable	Site Operating Plan
891	Part IV	Indicate that final cover for the landfill must be in accordance with the site closure plan and Subchapter K of Chapter 330.	Required	330.165(f)	Yes	Part IV, Section 4.18.4, Paragraph 1		Site Operating Plan
901	Part IV	indicate that enclosed containers or enclosed vehicles must only be accepted at their designated time and on the specified day in accordance with this section, commission permits, or other orders of the commission.	Required If Requested	330.169(1)(C)	No		Not Applicable	Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
902	Part IV	Indicate that a commission inspector shall be on site and shall witness the unloading process to ensure that no putrescible waste or household waste is present and that any waste considered non-allowable by the inspector must be removed from the working face and subsequently from the facility in accordance with 30 TAC §330.133	Required If Requested	330.169(1)(D)	No		Not Applicable	Site Operating Plan
903	Part IV	Indicate that each transporter delivering waste in enclosed containers or enclosed vehicles must, prior to discharging the load, provide to the landfill operator a transporter trip ticket for the route being delivered. Trip tickets must be maintained as part of the operating record.	Required If Requested	330.169(1)(E)	No		Not Applicable	Site Operating Plan
904	Part IV	Stationary compactors permitted in accordance with 30 TAC §330.7 of this title (relating to Permit Required) and municipalities having transporter routes permitted in accordance with 30 TAC §330.7 of this title are exempt from the requirements of 30 TAC §330.169(1)-(3)	Informational	330.169(4)			Not Applicable	Site Operating Plan
905	Part IV	Indicate that the landfill operator must obtain from the transporter a hauler trip ticket for a municipal transporter route or stationary compactors, as appropriate, prior to allowing discharge of the material at the landfill. These trip tickets must be maintained as a part of the operating record.	Required	330.169(4)	No		Not Applicable	Site Operating Plan
906	Part IV	Indicate that the landfill may accept special wastes consistent with the limitations established in 30 TAC §330.5(a)(2) of this title (relating to Classification of Municipal Solid Waste Facilities) and the waste acceptance plan required by 30 TAC §330.61(b) of this title (relating to Contents of Part II of the Application).	Required	330.171(a)	No		Not Applicable	Site Operating Plan
907	Part IV	Indicate that special waste not identified in 30 TAC §330.171(c)-(d) require prior written approval from the executive director.	Required	330.171(b)	Yes	Part IV, Section 4.20		Site Operating Plan
908	Part IV	Approvals will be waste-specific and/or site- specific and will be granted only to appropriate facilities operating in compliance with this chapter.	Required	330.171(b)(1)	No		Not Applicable	Site Operating Plan
909	Part IV	Indicate that requests for approval to accept special wastes must be submitted by the generator to the executive director or to a facility with an approved plan	Required	330.171(b)(2)	No		Not Applicable	Site Operating Plan
910	Part IV	Indicate that requests for approval to accept special wastes must include a description of chemical & physical characteristics of waste and a statement as to whether or not each waste is a Class 1 industrial waste as defined in §330.3 of this title, and the quantity and rate at which each waste is produced and/or the expected frequency of disposal		330.171(b)(2)(A)	No		Not Applicable	Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
911	Part IV	Indicate that a hazardous waste determination as required by 30 TAC §335.6 will be included for all Class 1 industrial waste	Required	330.171(b)(2)(B)	No		Not Applicable	Site Operating Plan
912	Part IV	Indicate that all requests for approval to accept special wastes must that include an operational plan containing the proposed procedures for handling each waste and listing required protective equipment for operating personnel and on-site emergency equipment	Required	330.171(b)(2)(C)	No		Not Applicable	Site Operating Plan
913	Part IV	Indicate that all requests for approval to accept special wastes must that include a contingency plan outlining responsibility for containment and cleanup of any accidental spills occurring during the delivery and/or disposal operation	Required	330.171(b)(2)(D)	No		Not Applicable	Site Operating Plan
915	Part IV	Indicate that soils contaminated by petroleum products, crude oils, or chemicals in concentrations of greater than 1,500 milligram per kilogram (mg/kg) total petroleum hydrocarbons; or contaminated by constituents of concern that exceed the concentrations listed in Table 1, Constituents of Concern and Their Maximum Leachable Concentrations in 30 TAC §335.521(a)(1) of this title (relating to Appendices) must be disposed in dedicated cells that meet the requirements of 30 TAC §330.331(e) of this title (relating to Design Criteria).	Required	330.171(b)(4)	No		Not Applicable	Site Operating Plan
916	Part IV	Indicate that the executive director may authorize the receipt of special waste with a written concurrence from the facility, however, the facility operator is not required to accept the waste.	Required	330.171(b)(5)	No		Not Applicable	Site Operating Plan
917	Part IV	Indicate that the executive director may revoke an authorization to accept special waste if the owner or operator does not maintain compliance with these rules or conditions imposed in the authorization to accept special waste.	Required	330.171(b)(6)	No		Not Applicable	Site Operating Plan
918	Part IV	Indicate that special waste listed under 330.171(c) may be accepted if managed per the handling procedures for each waste identified in 330.171(c)(1) - (7)	Required	330.171(c)	Yes	Part IV, Section 4.20		Site Operating Plan
919	Part IV	Indicate that used oil filters from internal combustion engines must not be intentionally and knowingly accepted for disposal at landfills permitted under this chapter except as provided in 330.171(d)(1) & (2)	Required	330.171(d)	Yes	Part IV, Section 4.20.7		Site Operating Plan
920	Part IV	Indicate that Class 1 industrial solid waste shall not be disposed in the landfill	Required	330.173(a)	Yes	Part IV, Section 5.1		Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
921	Part IV	Indicate that wastes that are Class 1 only because of asbestos content may be accepted at any Type I or Type IAE landfill that is authorized to accept regulated asbestoscontaining material (RACM). Authorization to accept this waste is implied in the authorization to accept RACM unless the acceptance of industrial wastes is prohibited by the permit. All Class 1 industrial asbestos wastes will be manifested and the owner or operator of the landfill facility shall comply with the requirements of 30 TAC §330.173(g) & (h)	Required	330.173(c)	No		Not Applicable	Site Operating Plan
922	Part IV	Indicate that the operator may not accept Class 1 without written approval and a manifest per 30 TAC §335.10	Required	330.173(b)	No		Not Applicable. Class I industrial waste is prohibited.	Site Operating Plan
923	Part IV	Indicate that requests for authorization to accept Class 1 solid wastes must be submitted in writing to the executive director	Required	330.173(d)	No		Not Applicable. Class I industrial waste is prohibited.	Site Operating Plan
924	Part IV	Indicate that a request to accept Class 1 waste must include a description of chemical & physical characteristics of the waste per 30 TAC §335.587, a hazardous waste statement, and the quantity, rate, and frequency of disposal	Required	330.173(d)(1)	No		Not Applicable. Class I industrial waste is prohibited.	Site Operating Plan
925	Part IV	Indicate that a request to accept Class 1 waste must include operating plan containing handling procedures, personnel protective & onsite emergency equipment	Required	330.173(d)(2)	No		Not Applicable. Class I industrial waste is prohibited.	Site Operating Plan
926	Part IV	Indicate that a request to accept Class 1 waste must include a written contingency plan meeting the requirements of 30 TAC §335.589	Required	330.173(d)(3)	No		Not Applicable. Class I industrial waste is prohibited.	Site Operating Plan
927	Part IV	Unless specifically authorized by the facility permit, a Type I or Type IAE landfill facility permitted after October 9, 1993, may not accept Class 1 industrial solid wastes in excess of 20% of the total amount of waste (not including Class 1 wastes) accepted during the current or previous year. The amount of waste may be determined by volume or by weight, but the same unit of measure must be used for each year, unless a variance is authorized by the executive director.	Informational	330.173(e)			Not Applicable. Class I industrial waste is prohibited.	Site Operating Plan
928	Part IV	Indicate that any authorization to accept Class 1 waste is subject to the site operating in compliance with 30 TAC §330.173 and any specific conditions required under any letter(s) of authorization. Failure to operate the site in compliance with 30 TAC §330.173 or any special conditions imposed by the executive director may result in revocation of the authorization to accept a Class 1 waste.	Required If Requested	330.173(f)	No		Not Applicable. Class I industrial waste is prohibited.	Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
929	Part IV	Indicate that Class 1 waste must be accompanied by a manifest that must be signed by the operator and copies retained for 3 yrs.	Required If Requested	330.173(g)	No		Not Applicable. Class I industrial waste is prohibited.	Site Operating Plan
930	Part IV	Indicate that a Class 1 waste acceptance report must be submitted by 25 th of the month	Required If Requested	330.173(h)	No		Not Applicable. Class I industrial waste is prohibited.	Site Operating Plan
931	Part IV	Indicate that the facility will accepted Class 2 waste provided the acceptance of this waste does not interfere with facility operation and its acceptance is in accordance with any applicable limitations in §330.5(a)(2) and the waste acceptance plan required by §330.61(b)	Required	330.173(i)	No		Not Applicable. Class I industrial waste is prohibited.	Site Operating Plan
932	Part IV	Indicate that the facility will accepted Class 3 waste provided the acceptance of this waste does not interfere with facility operation	Required	330.173(j)	No		Not Applicable. Class I industrial waste is prohibited.	Site Operating Plan
933	Part IV	Indicate that the executive director may require visual screening	Required	330.175	Yes	Part IV, Section 4.21		Site Operating Plan
934	Part IV	Provide procedures for leachate or gas condensate recirculation	Required If Requested	330.177	Yes	Part IV, Section 4.22, Paragraph 2		Site Operating Plan
935	Part IV	If facility manages Class 1, then it shall comply with 30 TAC §330.179(a)(1)-(6)	Informational	330.179(a)			Not Applicable. Class I industrial waste is prohibited.	Site Operating Plan
936	Part IV	Provide a schedule for inspecting monitoring equipment, safety and emergency equipment, and operating and structural equipment that are important to preventing, detecting, or responding to environmental or human health hazards	Required If Requested	335.585(b)	No		Not Applicable (for industrial solid waste and municipal hazardous waste)	Site Operating Plan
937	Part IV	Indicate that the inspection schedule will be maintained at facility	Required If Requested	335.585(b)(1)	No		Not Applicable	Site Operating Plan
938	Part IV	Specify the type of problems to be looked for during Class 1 waste inspection	Required If Requested	335.585(b)(2)	No		Not Applicable	Site Operating Plan
939	Part IV	Specify the frequency of inspections that is consistent with 40 CFR 264.303, and indicate that unloading areas will be inspected daily	Required If Requested	335.585(b)(3)	No		Not Applicable	Site Operating Plan
940	Part IV	Indicate that the facility must remedy any deterioration or malfunction of equipment or structures that the inspection reveals on a schedule that ensures that the problem does not lead to an environmental or human health hazard. Indicate that where a hazard is imminent or has already occurred, remedial action must be taken immediately.	Required If Requested	335.585(c)	No		Not Applicable	Site Operating Plan
941	Part IV	Indicate that the facility will maintain inspection logs that include date/time of inspection, inspectors name, observations made, date & nature of repairs	Required If Requested	335.585(d)	No		Not Applicable	Site Operating Plan
942	Part IV	Indicate that facility personnel must successfully complete a program of classroom instruction or on-the-job training that teaches them to perform their duties in a way that ensures the facility's compliance with the requirements of this 30 TAC §330.586	Required If Requested	335.586(a)	No		Not Applicable (for industrial solid waste and municipal hazardous waste)	Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
943	Part IV	Indicate that training will provided by a person trained in waste management procedures, and must include instruction that teaches facility personnel waste management procedures (including contingency plan implementation) relevant to the positions in which they are employed	Required If Requested	335.586(a)(1)	No		Not Applicable	Site Operating Plan
944	Part IV	Indicate that the training program must be designed to ensure that facility personnel are able to respond effectively to emergencies by familiarizing them with emergency procedures, emergency equipment, and emergency systems	Required If Requested	335.586(a)(2)	No		Not Applicable	Site Operating Plan
945	Part IV	Provide procedures for using, inspecting, repairing, & replacing emergency & monitoring equipment; communications or alarm systems; response to fires or explosions; response to GW contamination; & shutdown of operations	Required If Requested	335.586(a)(2)(A)-(E)	No		Not Applicable	Site Operating Plan
946	Part IV	Indicate that personnel training must be completed within 6 months	Required If Requested	335.586(b)	No		Not Applicable	Site Operating Plan
947	Part IV	Indicate that facility personnel must take part in an annual review of initial training	Required If Requested	335.586(c)	No		Not Applicable	Site Operating Plan
948	Part IV	Indicate that facility will maintain personnel records required in 335.586 in the site operating record	Required If Requested	335.586(d)	No		Not Applicable	Site Operating Plan
949	Part IV	Indicate that facility will record title of each position & employee name in that position, job description, description of type & amount of training for each position, records of training & job experience	Required If Requested	335.586(d)(1) - (4)	No		Not Applicable	Site Operating Plan
950	Part IV	indicate that training records on current personnel must be kept until closure of the facility and training records on former employees must be kept for at least three years from the date the employee last worked at the facility	Required If Requested	335.586(e)	No		Not Applicable	Site Operating Plan
951	Part IV	Indicate that the facility will follow the waste analysis requirements of 335.587	Required If Requested	335.587(a)	No		Not Applicable	Site Operating Plan
952	Part IV	Provide procedures in compliance with 335.587 to obtain chemical & physical analysis of representative samples	Required If Requested	335.587(a)(1)	No		Not Applicable	Site Operating Plan
953	Part IV	Indicate that a waste generator's records of analyses performed on the waste before the effective date of these regulations, or studies conducted on waste generated from processes similar to that which generated the waste to be managed at the facility, may be included in the data base required to comply with this paragraph. Indicate that the facility may arrange for the generator of the waste to supply the information required by this paragraph. Indicate that if the generator does not supply the information, and the owner or operator chooses to accept a waste, the owner or operator is responsible for obtaining the information required to comply with this section.		335.587(a)(1)(A)-(B)	No		Not Applicable	Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
954	Part IV	Indicate that the waste analysis may include data developed under Subchapter R of Chapter 335 (relating to Waste Classification), and existing published or documented data on a waste or on such waste generated from similar processes.	Required If Requested	335.587(a)(2)	No		Not Applicable	Site Operating Plan
955	Part IV	Indicate that waste analysis must be repeated as necessary to ensure that it is accurate and up-to-date, when the owner or operator is notified, or has reason to believe, that the process or operation generating the waste has changed and when the results of the inspection required in 335.587 indicate that the waste received at the facility does not match the waste designated on the accompanying manifest or shipping paper.		335.587(a)(3)	No		Not Applicable	Site Operating Plan
956	Part IV	Indicate that the owner or operator shall inspect and, if necessary, analyze each waste received at the facility to determine whether it matches the identity of the waste specified on the accompanying manifest or shipping paper	Required If Requested	335.587(a)(4)	No		Not Applicable	Site Operating Plan
957	Part IV	Provide a waste analysis plan that describes the procedures which the owner or operator will carry out to comply with 335.587(b)	Required If Requested	335.587(b)	No		Not Applicable	Site Operating Plan
958	Part IV	Provide procedures to prevent the ignition or reaction of wastes	Required If Requested	335.588(a)	No		Not Applicable	Site Operating Plan
959	Part IV	Indicate that the facility will take precautions to prevent, extreme heat or pressure, fire or explosions, violent reactions, toxic mist, dust, fumes, gases, flammable fumes & gases, damage to devices or facility, or threaten human health or the environment	Required If Requested	335.588(b)(1)-(5)	No		Not Applicable	Site Operating Plan
960	Part IV	Indicate that the facility will maintain documentation of compliance with 335.588(a)-(b)	Required If Requested	335.588(c)	No		Not Applicable	Site Operating Plan
961	Part IV	Provide a contingency plan that is designed to minimize hazards to human health or the environment from fires, explosions, or any unplanned sudden or non-sudden release of waste or constituents of such waste to air, soil, or surface water	Required If Requested	335.589(a)(1) & (2)	No		Not Applicable	Site Operating Plan
962	Part IV	The contingency plan must describe personnel action in response to fires, explosions, or any unplanned sudden or non-sudden release of waste or constituents of such waste to air, soil, or surface water at the facility.	Informational	335.589(b)(1)			Not Applicable	Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
963	Part IV	Provide revisions sufficient to comply with requirements of Chapter 335 to any current Spill Prevention, Control, and Countermeasures (SPCC) Plan that is in accordance with Title 40 Code of Federal Regulations (CFR) Part 112, 40 CFR Part 1510, or some other approved emergency or contingency plan, if the facility manages waste in tanks	Required If Requested	335.589(b)(2)	No		Not Applicable	Site Operating Plan
964	Part IV	Describe arrangements agreed to by local police departments, fire departments, hospitals, contractors, and state and local emergency response teams to coordinate emergency services.	Required If Requested	335.589(b)(3)	No		Not Applicable	Site Operating Plan
965	Part IV	Indicate that the owner or operator will maintain a list of names, addresses, and phone numbers (office and home) of all persons qualified to act as emergency coordinator (see subsection (e) of this section), and this list must be kept up-to-date and at the facility. Where more than one person is listed, one must be named as primary emergency coordinator and others must be listed in the order in which they will assume responsibility as alternates.	Required If Requested	335.589(b)(4)	No		Not Applicable	Site Operating Plan
966	Part IV	Provide in the contingency plan a list of emergency equipment including location, physical description, & capabilities of equipment	Required If Requested	335.589(b)(5)	No		Not Applicable	Site Operating Plan
967	Part IV	Include in the contingency plan an evacuation plan for personnel including signals for evacuation, route and alternate routes	Required If Requested	335.589(b)(6)	No		Not Applicable	Site Operating Plan
968	Part IV	Indicate that copies of the contingency plan will be maintained on-site, submitted to police, fire, hospitals, State & local emergency response services	Required If Requested	335.589(c)(1) & (2)	No		Not Applicable	Site Operating Plan
969	Part IV	Indicate that the contingency plan must be reviewed, and immediately updated, if necessary, whenever he facility permit is revised, the plan fails in an emergency, the facility changes in its design, construction, operation, maintenance, or other circumstances in a way that materially increases the potential for fires, explosions, or releases of waste or constituents of such waste, or changes the response necessary in an emergency or the list of emergency equipment changes	Required If Requested	335.589(d)(1)-(4)	No		Not Applicable	Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
970	Part IV	Indicate that at all times, there must be at least one employee either on the facility premises or on call (i.e., available to respond to an emergency by reaching the facility within a short period of time) with the responsibility for coordinating all emergency response measures. This emergency coordinator shall be thoroughly familiar with all aspects of the facility's contingency plan, all operations and activities at the facility, the location of all records within the facility, and the facility layout. In addition, this person must have the authority to commit the resources needed to carry out the contingency plan.		335.589(e)	No		Not Applicable	Site Operating Plan
971	Part IV	Indicate that whenever there is an imminent or actual emergency situation, the emergency coordinator (or his designee when the emergency coordinator is on call) shall immediately activate facility alarms or communication systems, where applicable, to notify all facility personnel and notify appropriate state or local agencies with designated response roles if their help is needed	Required If Requested	335.589(f)(1)(A)-(B)	No		Not Applicable	Site Operating Plan
972	Part IV	Indicate that whenever there is a release, fire, or explosion, the emergency coordinator shall immediately identify the character, exact source, amount, and areal extent of any released materials.	Required If Requested	335.589(f)(2)	No		Not Applicable	Site Operating Plan
973	Part IV	Indicate that the emergency coordinator shall assess possible hazards to human health or the environment that may result from the release, fire, or explosion.	Required If Requested	335.589(f)(3)	No		Not Applicable	Site Operating Plan
974	Part IV	Indicate that if the emergency coordinator determines that the facility has had a release, fire, or explosion that could threaten human health, or the environment, outside the facility and if the emergency coordinator's assessment indicates that evacuation of local areas may be advisable, the emergency coordinator shall immediately notify appropriate local authorities, and must be available to help appropriate officials decide whether local areas should be evacuated.	Required If Requested	335.589(f)(4)	No		Not Applicable	Site Operating Plan
975	Part IV	Indicate that the emergency coordinator must notify either government official or National Response Center and provide a report that includes the name & phone number of reporter, name and address of facility, time and type of incident, name and quantity of material involved, extent of injuries, and possible hazards	Required If Requested	335.589(f)(5)(A) - (F)	No		Not Applicable	Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
976	Part IV	Indicate that the emergency coordinator shall take all reasonable measures necessary to ensure that fires, explosions, and releases do not occur, recur, or spread to other waste at the facility	Required If Requested	335.589(f)(6)	No		Not Applicable	Site Operating Plan
977	Part IV	Indicate that the emergency coordinator shall monitor for leaks, pressure buildup, gas generation, or ruptures in valves, pipes, or other equipment, wherever this is appropriate if the facility stops operations in response to a fire, explosion, or release	Required If Requested	335.589(f)(7)	No		Not Applicable	Site Operating Plan
978	Part IV	Indicate that the emergency coordinator shall provide for treating, storing, or disposing of recovered waste, contaminated soil or surface water, or any other material that results from a release, fire, or explosion at the facility and shall classify all recovered waste, contaminated soil or surface water, or any other material that results from a release, fire, or explosion at the facility	Required If Requested	335.589(f)(8)	No		Not Applicable	
979	Part IV	Indicate that the emergency coordinator shall ensure that, in the affected area(s) of the facility, no waste that may be incompatible with the released material is treated, stored, or disposed of until cleanup procedures are completed and all emergency equipment listed in the contingency plan is cleaned and fit for its intended use before operations are resumed	Required If Requested	335.589(f)(9)(A) & (B)	No		Not Applicable	Site Operating Plan
983	Part IV	Indicate that nonhazardous industrial waste may be placed above natural grade provided that the conditions in §335.590(24)(F)(i) - (vi) of this title are met, except as provided in §335.590(24)(F)(vii)	Required If Requested	330.179(b)	No		Not Applicable	Site Operating Plan
984	Part IV	Provide plans and designs for the placement of nonhazardous waste above natural grade in commercial industrial nonhazardous waste landfill units that is in compliance with the requirements of 335.590(24)(F)	Required If Requested	335.590(24)(F)	No		Not Applicable	Site Operating Plan
998	Part IV	Provide for a quarterly report to be submitted that will include volume of waste received, percent solids, and the method of determining the percent solids, processed, disposed, and recycled or reused.	Required	330.9(g)(1)	No		Not Applicable (for Type V facility)	Site Operating Plan
999	Part IV	Provide in the quarterly report, the method(s) utilized to achieve at least 10% recycling or reuse of incoming material	Required	330.9(g)(1)	No		Not Applicable	Site Operating Plan
1004	Part IV	Indicate that all wastes generated by a facility must be processed or disposed at an authorized solid waste management facility	Required	330.205(b)	No		Not Applicable (for storage and processing facility)	Site Operating Plan
1005	Part IV	Indicate that all wastewaters generated by a facility shall be managed as contaminated water in accordance with 330.207	Required	330.205(c)	No		Not Applicable	Site Operating Plan
1006	Part IV	Indicate that the facility shall be designed and operated in a manner that sludges produced pass the Paint Filter Liquids Test.	Required If Requested	330.205(d)	No		Not Applicable	Site Operating Plan

ID	App. Part	Checklist Item	Item Type	Citation	Complete?	Location	Comments	Application Area
1009	Part IV	The owner or operator shall not discharge contaminated water without specific written authorization.	Informational	330.207(a)			Not Applicable	Site Operating Plan
1023	Part IV	Provide plans for process area of transfer stations that recover material from putrescibles or liquid waste. Such plans shall provide for the storage of processed and unprocessed waste & recycled materials in enclosed buildings, vessels, or containers.	Required If Requested	330.209(c)	No		Not Applicable	Site Operating Plan
1024	Part IV	Provide a plan that describes how all waste containing food wastes shall be stored in covered or closed containers that are leak-proof, durable, and designed for safe handling and easy cleaning	Required	330.211	No		Not Applicable	Site Operating Plan
1025	Part IV	Indicate that nonreusable containers shall be of suitable strength to minimize vector scavenging or rupturing.	Required	330.211(1)	No		Not Applicable	Site Operating Plan
1026	Part IV	Indicate that reusable containers must be maintained in a clean condition as not to constitute a nuisance, harbor, feed, and propagate vectors.	Required	330.211(2)	No		Not Applicable	Site Operating Plan

CITY OF WACO LANDFILL TCEQ PERMIT NO. MSW-2400 McLENNAN AND LIMESTONE COUNTIES, TEXAS

PART III SITE DEVELOPMENT PLAN NARRATIVE

Prepared for:

CITY OF WACO



Solid Waste Services 501 Schroeder Drive Waco, TX 76710



Prepared by:

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TABLE OF CONTENTS

<u>SECT</u>	<u>ION</u>		<u>PAGE</u>
LIST	OF A	CRONYMS	iii
1	INTRO	DDUCTION	III-1-1
2	SOLID	WASTE DATA	III-2-1
	2.1	POPULATION EQUIVALENT	III-2-1
	2.2	SITE OPERATING LIFE PROJECTION	III-2-1
3	DESIG	6N DATA	III-3-1
	3.1	LANDFILL METHODS	III-3-1
	3.2	WET-WEATHER OPERATIONS	III-3-1
	3.3	SITE ACCESS	III-3-2
	3.4	GEOLOGY AND GEOTECHNICAL REPORTS	III-3-3
	3.5	GROUNDWATER PROTECTION	III-3-3
	3.6	SURFACE WATER PROTECTION	III-3-5
	3.7	FLOODPLAIN PROTECTION	III-3-8
	3.8	LANDFILL CLOSURE AND POST CLOSURE-CARE	III-3-9
	3.9	LANDFILL GAS MANAGEMENT	III-3-10
	3.10	PROTECTION OF ENDANGERED SPECIES	III-3-10

Appendices

A Site Life Calculations

Attachments

1	Sita I	avout	Dlane
- 1	Sue i	avout	Pians

- 2 Fill Cross Sections
- 3 Landfill Completion Plan
- 4 Geology Report
- 5 Geotechnical/Stability Analysis
- 6A Surface Water Drainage Plan
- 6B Floodplain Evaluation
- 6C Groundwater Protection Plan
- 7 Groundwater Sampling and Analysis Plan
- 8 Closure and Post-Closure Cost Estimates
- 9 Final Closure and Post-Closure Care Plan
- 10 Soil and Liner Quality Control Plan
- 11 Landfill Gas Management Plan
- 12 Leachate and Contaminated Water Management Plan



SCS Engineers TBPE Reg. # F-3407

LIST OF ACRONYMS

ADC - Alternate daily cover

AIPG - American Institute of Professional Geologists

ASTM - American Society for Testing and Materials

BER - Ballast Evaluation Report

bgl - below ground level

BMPs - best management practices

CFR - Code of Federal Regulations

CCS - Citizens' Collection Station

CN - curve number

COC - chain-of-custody

COE - U.S. Army Corps of Engineers

CQA - construction quality assurance

EDE - estimated depth of excavation

EPA - U.S. Environmental Protection Agency

FEMA - Federal Emergency Management Agency

FIRM - Flood Insurance Rate Map

FM - farm-to-market

FMC - flexible membrane cover

FML - flexible membrane liner

FTB - film tear bond

FWS - U.S. Fish and Wildlife Service

GLER – Geomembrane Liner Evaluation Report (also referred to as FMLER)

GP - Geotechnical Professional

GQCP - Geotechnical Quality Control/Quality Assurance Professional

GWSAP - groundwater sampling and analysis plan

HDPE - high density polyethylene

HELP - Hydrologic Evaluation of Landfill Performance

LCS - leachate collection system

LEL - lower explosive limit

LFG - landfill gas

LL - liquid limit

LLDPE - linear low density polyethylene

LSOP - laboratory standard operating procedures

MCLs - maximum contaminant levels

rnsl - mean sea level

MSW - municipal solid waste

MSWR - Municipal Solid Waste Regulations

NMOCs - Nonmethane Organic Compounds

NPDES - National Pollutant Discharge Elimination System

NSPS - New Source Performance Standards

NWP - Nationwide Permit

O&M - operations and maintenance

OMC - optimum moisture content

LIST OF ACRONYMS (Continued)

PCBs - polychlorinated biphenyls

P.I. - plasticity index

POR - Professional of Record

POTW - publicly owned treatment works

PQLS - practical quantitation limits

PVC - polyvinyl chloride

QA/QC - quality-assurance/quality-control

RCRA - Resource Conservation Recovery Act

RPD - relative percent difference

SCS - Soil Conservation Service

SDP - Site Development Plan

SDR - standard dimension ratio

SLER - soils and liner evaluation report

SLQCP - soil and liner quality control plan

SOP - site operating plan

SSC - statistically significant change

TAC - Texas Administrative Code

TDS - total dissolved solids

TCEQ - Texas Commission on Environmental Quality

TPDES – Texas Pollutant Discharge Elimination System

TPWD - Texas Parks and Wildlife Department

TWDB -Texas Water Development Board

TxDOT - Texas Department of Transportation

UEL - upper explosive limit

USCS - Unified Soil Classification System

USGS - U.S. Geological Survey

USLE - Universal Soil Loss Equation

VOCs - volatile organic compounds

INTRODUCTION (30 TAC §330.63)

The City of Waco (Owner) proposes to develop and operate a Type I Municipal Solid Waste (MSW) Landfill on 502.5 acres of land located in McLennan and Limestone Counties, Texas. The landfill entrance will be located approximately 0.4 miles south of the intersection of State Highway 31 and T K Parkway (also known as Farm-to-Market [FM] 939). The waste disposal footprint will encompass approximately 175.7 acres, separated into two (2) disposal areas, with the East Disposal Area comprised of approximately 112.9 acres and West Disposal Area comprised of approximately 62.8 acres. Refer to Attachment 1 for drawings that depict the existing conditions, landfill permit boundary, waste footprint, and general site layout.

The landfill will serve residences, businesses, and industries in the communities of McLennan and Limestone County and other nearby counties transported to the landfill by municipal, private, and public haulers. The landfill will accept municipal solid waste, household waste, yard waste, commercial solid waste, Class 2 and Class 3 non-hazardous industrial wastes, construction-demolition waste, and special wastes as authorized by the Texas Commission on Environmental Quality (TCEQ). The categories of waste that will be accepted at the landfill are defined in Part I/II, Section 2.2.2 of this permit application. Any special waste accepted at the landfill will be in accordance with 30 TAC §330.171. Consistent with 30 TAC §330.15(e) the facility will not accept regulated hazardous waste, polychlorinated biphenyls (PCBs), and all other prohibited waste defined therein. Additionally, Class 1 industrial solid waste will not be accepted at this facility.

This permit application for the City of Waco Landfill has been prepared consistent with the Municipal Solid Waste Regulations (MSWR), Title 30 of the Texas Administrative Code (TAC), Chapter 330. This Site Development Plan (SDP) Narrative provides a brief overview of the contents of the permit application, including the attachments of the SDP. The SDP has been separated into Attachments 1 through 12, which were prepared consistent with 30 TAC §330.63.

SOLID WASTE DATA (30 TAC §330.63(D)(4)(D)) 2

The landfill will serve residences, businesses, and industry in the communities of McLennan and Limestone Counties and other nearby counties. As discussed in Parts I/II, Section 2.2, the landfill is expected to initially receive approximately 305,000 tons per year of solid waste (1,070 tons per day based on a 286-day operating schedule). The initial year of operation is anticipated following completion of disposal operations at the existing City of Waco Landfill (Permit No. MSW-948A), which is estimated to be 2024. The waste inflow rate is estimated to increase at a rate of approximately 1.25 percent annually over the life of the landfill. Over the life of the landfill, it is anticipated that the waste rate received at the landfill may vary as warranted by the needs of the area, market conditions, and recycling and waste diversion practices.

Consistent with 30 TAC §330.63(d)(4)(D), the following subsections describe the population equivalent and site operating life for the landfill.

2.1 POPULATION EQUIVALENT

As discussed in Parts I/II, Section 2.2.1, it is anticipated that the population served by the landfill will change over the life of the landfill as warranted by the needs of the area and market conditions. Based on an estimated 6.7 pounds of waste generated daily per person (ref: HOTCOG Regional Solid Waste Plan, 2013 Update) and an initial disposal rate of 1,070 tons per day, the number of people served by the landfill initially will be approximately 319,000 persons.

The major classifications of solid waste to be accepted at the landfill include municipal solid waste, household waste, yard waste, commercial solid waste, Class 2 and Class 3 non-hazardous industrial wastes, construction-demolition waste, and special wastes. Consistent with 30 TAC §330.15(e), the facility will not accept regulated hazardous waste, polychlorinated biphenyls (PCBs), and other prohibited waste defined herein. Additionally, Class 1 industrial solid waste will not be accepted at this facility. Waste classifications and further information on types of wastes expected to be received at the facility are included in Parts I/II, Section 2.2.2 - Properties and Characteristics of Waste.

2.2 SITE OPERATING LIFE PROJECTION

The landfill configuration provides an approximate estimate of 33 years of site operating life. Calculations and assumptions for the site operating life estimate are included in Appendix IIIA – Site Life Calculations.

3 DESIGN DATA

3.1 LANDFILL METHODS (30 TAC $\S 330.63(D)(4)(B),(C),(E)$)

The proposed landfill development method for the site is a combination of area excavation fill followed by aerial fill to the proposed landfill completion height. The landfill will be developed in two separate disposal areas, East Disposal Area and West Disposal Area. The East Disposal Area will be comprised of eight sectors, 1 through 8; and the West Disposal Area will be comprised of four sectors, 9 through 12. Each sector may be developed in multiple cells at the discretion of Owner.

The excavation sideslopes will be no steeper than 3H:1V, with an elevation of deepest excavation (EDE) of 505 feet mean sea level (ft MSL). The EDE will be achieved in the bottom of the leachate collection sump in Sector 8. Aerial fill sideslopes will be no steeper than 4H:1V and the aerial fill topslope will be no flatter than 5 percent (or 20H:1V). The maximum elevation of final cover will be no higher than 697.7 ft MSL and 661.3 ft MSL for East and West Disposal Areas, respectively. Final cover placement and closure of sectors will be in accordance with procedures set forth in the closure plan provided in Attachment 9 of this permit application.

Attachments to this application include drawings depicting the landfill development. Specifically, Attachment 1 through Attachment 3 include the following:

- Attachment 1 Site Layout Plans, include existing site contours (July 3, 2018) topography, see Drawing 1.1), excavation, elevation of deepest excavation, disposal area layout, sector layout, and sequence of sector development.
- Attachment 2 Fill Cross Sections, include cross-sections depicting the base grades, top of liner grades, maximum elevation of waste, maximum elevation of final cover, and geologic borings along the cross-sections.
- Attachment 3 Landfill Completion Plan, include proposed final contours, surface water management system, and general facility layout at landfill completion.

3.2 WET-WEATHER OPERATIONS (30 TAC §330.63(D)(4)(A)

The landfill access roads (see Attachment 1 – Site Layout Plans), including perimeter roads and other constructed interior haul roads will be constructed of crushed stone, concrete rubble, masonry demolition debris, gravel, caliche, asphalt paving, or other suitable material and will provide access from the site entrance road to the disposal area(s). The landfill access roads will be passable under inclement weather conditions to allow access to the active disposal area. To enhance operating efficiency during wet weather, the Owner may reserve an active disposal area close to the all-weather roads for wet-weather operations where development sequence allows. Furthermore, the tracking of mud and trash onto public access roadways will be minimized by removing mud and associated debris from the landfill roads and site entrance, as described in Part IV – Site Operating Plan (SOP).

3.3 SITE ACCESS (30 TAC §330.63(B)(1))

3.3.1 Access from Highway

The main public roadways providing access to the site are State Highway (SH) 31 and T K Parkway (also known as Farm-to-Market [FM] 939). The landfill entrance will be located off FM 939, approximately 0.4 miles south of the intersection of SH 31 and FM 939. Refer to Parts I/II, Section 8 - Transportation for site access and other transportation information.

The site entrance is detailed on Attachment 1, Drawing 1.5 - Entrance Facility Plan. The site entrance consists of an all-weather road, site entrance gates, scale house, and scales (initially one inbound and one outbound scale). The site entrance will also include two inbound queue lanes that provide approximately 3,300 feet of queuing length from the scales back to FM 939. Furthermore, at some point in the future, an additional inbound scale may be installed to accommodate increases in the waste acceptance rate over the site operating life.

3.3.2 All-Weather Access

The site entrance road includes an asphalt or concrete paved roadway, or other suitable material that transitions into landfill access roads, either perimeter or interior haul roads, constructed of crushed stone, concrete rubble, masonry demolition debris, gravel, caliche, asphalt paving, or other suitable material and will provide access from the site entrance road to the waste disposal area(s). The site entrance road will serve as mud control for waste hauling vehicles prior to exiting the site and returning to public-access roads. The perimeter roads will be maintained for all-weather access by site personnel. Crushed stone, concrete rubble, masonry demolition debris, gravel, caliche, asphalt paving, or other similar material will be made available, as necessary, for use in maintaining passable perimeter roads. Grading equipment or other appropriate equipment will be used to control or remove mud accumulation at least once per day on days when mud and associated debris are being tracked onto FM 939, as specified in the SOP.

3.3.3 Access Control

Vehicle access to the landfill will be controlled at the site entrance by signs that direct all landfill traffic to the working face or Citizens' Collection Station (CCS) during site operating hours. Personnel on duty at the scale house will regulate access to the landfill. The site entrance will be secured by two gates (primary and secondary entrance gates). The primary entrance gate will be opened at 5:30 AM on days that the facility is in operation to minimize queuing on FM 939, as described in the Transportation Impact Analysis (Part I/II, Appendix I/IID-2) The secondary entrance gate will remain locked outside operating hours to prevent unauthorized vehicle access to the landfill. A fence, either barbed wire, chain link, privacy, or a combination thereof will limit access around the perimeter of the landfill at the permit boundary, as described in the SOP.

The Owner will permit entry to the landfill to designated landfill personnel, solid waste haulers (including landfill customers) authorized to use the facility, TCEQ personnel, and properly identified persons whose entry is authorized by the Landfill Manager or designee. reserves the right to deny access to the landfill to persons not demonstrating a legitimate purpose for visiting. Visitors will be allowed on the active disposal area of the landfill only when accompanied by the Landfill Manager or designee.

3.4 GEOLOGY AND GEOTECHNICAL REPORTS (30 TAC §330.63(E))

The regional and local stratigraphy and lithology for the proposed landfill are summarized in Parts I/II, Section 9 and described in detail in Attachment 4 – Geology Report, including depth, thickness, geometry, soil classifications, hydraulic conductivity, and depositional history of the local geological formations. In view of the depth of low-permeability clay and shale at the facility, the geologic setting of the site is considered suitable for landfill development.

Attachment 4 also includes the results of the subsurface investigation performed at the facility. Onsite geology is characterized by three layers as follows, from the ground surface downward to a maximum drilled depth of 100 feet:

- Unit 1: consists of surficial clayey and loamy alluvium overlying silty or sandy clays with small subrounded gravel. The transition from Unit I to the underlying Unit II is transitional, and marked by increasing hardness and increasing fissility.
- Unit 2: beneath Unit I, consists of weathered silty shale with varying calcareous content. Some publications use the term "marl" to describe calcareous shale. The Unit II silty shale has thin, interbedded limestone and sand/silt partings/lenses, calcite-filled joints, and marine shell fragment fossils. Above the Unit II/Unit III line, the stratigraphy is generally more variable in color but are generally lighter-colored and have evidence of oxidation such as various rust- and yellow/brown colors. Below the Unit II/Unit III line, the stratigraphy is a homogenous very dark color, trending to black. Unit III also is less fissile than Unit II.
- Unit 3: beneath Unit II, consists of unweathered dark gray to black calcareous shale bedrock with thin, interbedded limestone and sand/silt lenses, and marine shell fragment fossils.

Attachment 5, Geotechnical/Stability Analyses, addresses the geotechnical properties of the landfill, including evaluation of the geotechnical properties of the subsurface soils, stability of the soils and strata for development of the landfill, and slope stability of the landfill.

3.5 GROUNDWATER PROTECTION (30 TAC §330.63(F) & §330.63(D)(4)(G))

3.5.1 Groundwater Monitoring System

Attachment 4, Geology Report, includes the result of the subsurface investigation, including the groundwater depth, if encountered, in the soil borings and piezometers. Also, Attachment 4 includes the elevations and gradient of groundwater across the landfill property and a detailed description of the proposed groundwater monitoring system, which will be used to verify the integrity of the liner system. Details of the plan for performing groundwater sampling, analysis, and reporting are addressed in Attachment 7 - Groundwater Sampling and Analysis Plan.

3.5.2 Liner Design

Consistent with 30 TAC §330.331(b), a soil-geomembrane composite liner system for a Type I landfill, is proposed for the landfill. Beginning from the waste and working down, the bottom liner system will be comprised of the following components:

- 24-inch thick soil protective cover;
- Single-sided geocomposite (non-woven geotextile on the top side only of geonet);
- 60-mil high-density polyethylene (HDPE) geomembrane (smooth);
- 2-foot-thick compacted clay liner ($k < 1x10^{-7}$ cm/sec); and
- Prepared subgrade (excavation grade).

The sideslope liner system will be comprised of the following components (from waste and working down):

- 24-inch thick soil protective cover;
- Double-sided geocomposite (non-woven geotextile on both sides of geonet);
- 60-mil textured HDPE geomembrane (textured on both sides);
- 2-foot-thick compacted clay liner ($k < 1x10^{-7}$ cm/sec); and
- Prepared subgrade (excavation grade).

The proposed liner system for the landfill is designed to meet the requirements outlined in 30 TAC §330.331. Attachment 10 - Soil and Liner Quality Control Plan (SLQCP) contains the construction quality control and quality assurance requirements for construction of the composite liner for the landfill.

3.5.3 Leachate Collection System

A leachate collection system (LCS) has been designed to control the accumulation of leachate within the waste disposal area during the active periods of landfilling, and after landfill closure; including being designed to meet Type I landfill requirements (30 TAC §330.331(a)(2) and §330.333) and maintaining leachate head over the liner of less than 30 centimeters. The LCS layout is shown on drawings included in Attachments 1 and 12 of this permit application. Design of the LCS is discussed in Attachment 12 - Leachate and Contaminated Water Management Plan. Information regarding materials and construction quality control and quality assurance are included in the SLQCP. The following provides a summary description of the

LCS and associated features. Additional description is provided in Attachment 12. Representative details of the LCS are presented on drawings included in Attachment 12.

The primary collection component of the LCS is the leachate drainage layer, which consists of a geonet-geotextile composite (referred to as geocomposite) placed directly over the bottom and sideslope liner systems. The geocomposite consists of a HDPE geonet with a non-woven geotextile heat bonded to one or both sides of the geonet, where single-sided geocomposite will be placed on the bottom, and double-sided geocomposite will be placed on the sideslopes of the landfill. The geocomposite will have hydraulic properties that will provide adequate drainage of leachate to the leachate collection piping and sump, thereby maintaining less than 30-cm leachate head above the bottom liner system. Calculations demonstrating the minimum required material properties for the geocomposite are presented in Attachment 12.

A 2-foot-thick protective cover will be placed over the geocomposite prior to waste placement. To facilitate drainage into the leachate collection system, chimney drains, comprised of aggregate wrapped in a non-woven geotextile, will be constructed over the leachate collection piping. Leachate entering the LCS piping will discharge into sumps located at the perimeter of the landfill. Leachate collected in the sumps will be removed via submersible pumps lowered into the sumps through a riser pipe extending up the cell sideslope.

Additional descriptions of the LCS piping and sumps, including but not limited to pipe spacing and grading; sump sizing calculations; and demonstration that pipes and perforations will be resistant to clogging and collapse, are presented in Attachment 12. Leachate and contaminated water management, including storage and disposal, is presented in Attachment 12, Sections 4 and 5, respectively.

3.6 SURFACE WATER PROTECTION (30 TAC §330.63(C)(1))

3.6.1 General

The proposed landfill is located within the drainage basin of the Brazos River. Surface water generally drains southeast from the western portion of the property towards Horse Creek and generally drains south/southwest from the eastern portion of the property towards Horse Creek and Packwood Creek.

Stormwater runoff from the developed landfill will be conveyed through a surface water management system designed in accordance with 30 TAC §330.63(c), as described in Section 3.6.3. Stormwater will be conveyed from the landfill property into natural drainage features, including Horse and Packwood Creeks. These creeks are tributaries of Soil Conservation Services Site 19 Reservoir, which discharges into Williams Creek located south of the property and eventually flows into Tehuacana Creek approximately 11 miles southwest of the property. Tehuacana Creek discharges into the Brazos River approximately 15 miles southwest of the property.

In accordance with 30 TAC §330.15(h), the landfill has been designed to prevent discharge of pollutants into waters of the State or waters of the United States, as defined by the Texas Water Code (§26.121) and the Federal Clean Water Act (§404), respectively. As described in Part I/II,

Section 10.2, the Owner will file a notice of intent (NOI) with the TCEQ and develop and implement a Stormwater Pollution Prevention Plan prior to the commencement of landfill operations to obtain coverage under the Texas Pollutant Discharge Elimination System (TPDES) General Permit, TXR050000 for Stormwater Discharges associated with Industrial Activity.

3.6.2 Site Drainage Patterns

Consistent with 30 TAC §330.63(c), the surface water management system design for the landfill complies with 30 TAC §330.303. A complete description of the site drainage patterns for both the pre- and post-development landfill conditions is presented in Attachment 6A – Surface Water Drainage Plan of this permit application. As presented in Attachment 6A, the surface water drainage features, aerial fill controls and perimeter drainage system, have been designed to avoid adversely altering existing drainage patterns, as a result of landfill development, in accordance with 30 TAC §330.63(c)(1)(D)(iii). This has been demonstrated by evaluating pre- and postdevelopment peak discharge rates and total discharge volumes at off-site discharge locations. Furthermore, the post-development locations of off-site discharges have been designed to be consistent with the pre-development conditions. The pre- and post-development hydrologic and hydraulic analysis are presented in Attachment 6A, including a description of the methodology, calculations, and results of said calculations.

3.6.3 Perimeter Drainage System

The stormwater controls for the landfill have been designed consistent with the 30 TAC §330 requirements for Type I MSW landfills. The perimeter drainage system is comprised of final cover controls (described in Section 3.6.5), perimeter drainage channels and detention basins. The perimeter drainage system has been designed for a 25-year, 24-hour storm event. The drainage features will be installed concurrent with the construction of up-gradient landfill disposal cells, such that when the cell grades are above existing grade, down-gradient drainage features are in-place, as described in Attachment 6A. Details and sizing criteria for the perimeter drainage system and associated calculations, including peak velocities, flow depths, and discharge rates are included in Attachment 6A of this permit application.

3.6.4 Below Grade

Control of stormwater run-on and runoff within excavation areas will be achieved using temporary diversion berms, ditches, and containment areas as needed. The temporary stormwater control structures will be used to divert stormwater away from the working face, thus reducing the volume of contaminated water generated during a storm event. Uncontaminated stormwater will be discharged consistent with the requirements of the TPDES General Permit.

Contaminated stormwater consists of stormwater that has come into contact with waste. Control of contaminated stormwater will be provided through temporary containment berms. Water that infiltrates into the underlying waste will be managed as leachate. Contaminated stormwater will be contained and managed at the working face in accordance with the guidelines set forth in Attachment 12 of this permit application.

3.6.5 **Aerial Fill Controls**

Additional stormwater controls will be necessary as the site is brought above grade. Temporary diversion and containment berms, channels, and containment areas will be used to separate and control uncontaminated and contaminated stormwater run-on and runoff for the aerial fill portions of the landfill.

As intermediate and final cover are placed on the landfill, vegetation will be established to provide erosion protection, as described in Attachment 6A and the SOP. Furthermore, as intermediate and final cover are placed, drainage features will be installed to control erosion and convey stormwater run-on and run-off from the landfill cover to the perimeter drainage system, as described in Section 3.6.6. Drainage features installed on the intermediate and final cover have been designed to convey stormwater associated with the 25-year, 24-hour storm event. Design details and sizing calculations, including peak velocity, flow depth, and discharge rate, for intermediate and final cover drainage features are described in Attachment 6A. In all cases, surface water run-on and runoff will be managed consistent with the 30 TAC §330, Subchapter G.

Areas that have received waste, but will be inactive for longer than 180 days will receive intermediate cover. Consistent with 30 TAC §330.165(a) and (c), runoff from areas with intact daily and/or intermediate cover will be considered uncontaminated. Also, by implementing: (1) the site design and proper operating practices; and (2) ongoing placement of daily, intermediate and final cover (as further described in Attachment 9 - Final Closure and Post-Closure Plan), contaminated water and leachate will be minimized. Details of the final cover design are provided in Attachments 6C and 9 of this permit application.

3.6.6 **Erosion and Sedimentation Control Plan**

On-site erosion and sedimentation control will be provided as follows: (1) during construction activities; and (2) as part of the ongoing operation of the landfill. Erosion and sedimentation control includes structural and non-structural controls for the intermediate and final cover systems and the perimeter drainage system. An Erosion and Sedimentation Control Plan is presented in Attachment 6A – Surface Water Drainage Plan, Section 6. Landfill management will control erosion and offsite sedimentation by implementing interim controls, as specified in §330.305(e)(2), as described in Attachment 6A, Section 6. Furthermore, permanent erosion and sedimentation controls have been incorporated into the design of the landfill at completion and the perimeter drainage system.

Additionally, in accordance with §330.305(d), the landfill design will provide effective erosional stability to top dome surfaces and embankment sideslopes during all phases of landfill operation, including the closure and post-closure care period. The Erosion and Sedimentation Control Plan (Attachment 6A, Section 6) describes and includes the following:

• Erosion calculations using the Universal Soil Loss Equation (USLE)/Revised Universal Soil Loss Equation (RUSLE) to demonstrate that erosion on intermediate and final cover will be below permissible soil losses.

- Hydraulic calculations using standard engineering principles to demonstrate that velocities in drainage swales and downchutes and on intermediate and final cover slopes will be below permissible velocities.
- Operational requirements and guidelines for implementing erosion and offsite sedimentation controls, such as non-structural and structural best management practices (BMPs) for daily cover and soil stockpiles, intermediate cover, and final cover.

These features include perimeter drainage channels that have been designed with non-erosive velocities, or in areas where erosive velocities are anticipated, erosion protection or armoring of the channels in the form of rip rap, turf reinforcement matting, rock ditch checks, gabions, dissipation blocks, or other suitable structures will be provided, as needed. Permanent drainage and erosion protection measures for the final cover system (e.g., drainage swales and downchutes) are shown in Attachment 3 - Landfill Completion Plan. Erosion control practices for daily and intermediate cover are discussed in detail in Attachment 6A. vegetation on the intermediate and final cover, drainage swales, perimeter drainage system, and buffer zones will be ongoing as the site is developed (see Part III, Attachment 9 - Final Closure and Post-Closure Plan).

3.6.7 Wetlands

Information regarding wetlands is provided in Parts I/II, Section 11.2 and Appendix I/IIE -Section 404 Jurisdictional Determination in accordance with 30 TAC §330.553(b).

3.7 FLOODPLAIN PROTECTION (30 TAC §330.63(C)(2))

A portion of the Site is within the 100-year floodplains of Horse and Packwood Creeks. The floodplain limits were obtained from the currently effective Flood Insurance Rate Maps (Panels 48309C0250C dated September 26, 2008, and 48293C0125C dated September 16, 2011) obtained from FEMA for portions of McLennan and Limestone Counties. The floodplain limits have been designated by FEMA as Zone A, which indicates that no flood elevations have yet been determined along these creeks on the Site. The proposed waste disposal footprint is located entirely outside the limits of the 100-year floodplain. In accordance with 30 TAC §330.547(a), no solid waste disposal operations will take place within the 100-year floodplain, and therefore no development is proposed in the 100-year floodplain.

Because the floodplain for the project area has been classified as Zone A, an additional flood study was performed to confirm that the proposed landfill and perimeter drainage system will not be impacted by a 100-year storm event. This 100-year flood study is presented in Attachment 6B - Floodplain Evaluation. As presented in this attachment, the waste disposal limits are not located within the 100-year flood study area, and will not be impacted by a water surface generated by a 100-year storm event. Additionally, the landfill has been designed with a perimeter berm above existing grade, which prevents washout from the 100-year storm event. Furthermore, the landfill has been designed such that there will be no surface water run-on from Horse and Packwood Creeks into the perimeter drainage system associated with a 100-year storm event. Therefore, the landfill and perimeter drainage system will not be impacted by the 100-year storm event.

Additionally, in accordance with 30 TAC §330.547(b), site operations and development will not restrict the flow or reduce the temporary storage capacity of the 100-year floodplain; nor will the site operations result in washout of solid waste associated with the 100-year floodplain, since construction within the 100-year floodplain is not proposed. Therefore, §330.63(c)(2)(D) is not applicable to this application. Furthermore, in accordance with 30 TAC §330.547(c), all storage and processing facilities (e.g., onsite citizen's collection station) will be located outside of the 100-year floodplain as delineated by FEMA and will not be impacted by the 100-year storm event, as shown in Attachment 6B.

3.8 LANDFILL CLOSURE AND POST CLOSURE-CARE (30 TAC §330.63(H), (I) & (J))

3.8.1 Final Cover Design

The final cover system will be a soil-geomembrane composite meeting the requirements of 30 TAC §330.457. Beginning from the surface and working down, the final cover system on the landfill topslopes will be comprised of the following components:

- Vegetation (native and/or introduced grasses);
- 24-inch thick (minimum) soil erosion layer, with the top six inches capable of sustaining vegetation;
- 60-mil HDPE or 40-mil linear low density polyethylene (LLDPE) geomembrane (smooth);
- 18-inch thick (minimum) clayey soil infiltration layer ($k < 1x10^{-5}$ cm/sec); and
- 6-inch-thick daily cover or 12-inch-thick intermediate cover.

Beginning from the surface and working down, the final cover system on the landfill sideslopes will be comprised of the following components:

- Vegetation (native and/or introduced grasses);
- 24-inch thick soil erosion layer, with the top six inches capable of sustaining vegetation
- Double-sided geocomposite (geotextile on both sides of geonet);
- 60-mil HDPE or 40-mil LLDPE geomembrane (textured on both sides);
- 18-inch thick (minimum) clayey soil infiltration layer ($k < 1x10^{-5}$ cm/sec); and
- 6-inch-thick daily cover or 12-inch-thick intermediate cover.

The Final Closure and Post-Closure Care Plan, which is provided in Attachment 9, includes the final closure schedule, certification of closure, and an estimate of the largest area that will ever require final cover at the landfill in the year to follow closure. The final closure cost estimate for this area is provided in Attachment 8 – Closure and Post-Closure Care Cost Estimates.

3.8.2 Post Closure Care

At the time of closure, consistent with 30 TAC Subchapter K, the landfill will enter the 30-year post-closure care period. A description of the activities required during post-closure care are described in Attachment 9 of this application. A post-closure care cost estimate is provided in Attachment 8.

3.9 LANDFILL GAS MANAGEMENT (30 TAC §330.63(G))

Attachment 11 – Landfill Gas Management Plan provides procedures for monitoring landfill gas at the landfill perimeter and within onsite structures, layout or the perimeter landfill gas monitor probes, frequency for landfill gas monitoring, and procedures to be implemented in the event landfill gas is detected above regulatory limits. Drawing 11.1 – Landfill Gas Monitoring Probe Plan, provided in Attachment 11, depicts the layout of the perimeter landfill gas monitoring probe system.

3.10 PROTECTION OF ENDANGERED SPECIES (30 TAC $\S 330.63(B)(5)$

Information regarding the protection of endangered species in accordance with 30 TAC §330.157 is provided in Parts I/II, Section 12 – Protection of Endangered or Threatened Species.

APPENDIX IIIA

SITE LIFE CALCULATIONS



SCS Engineers TBPE Reg. # F-3407

Inclusive of pages III-A-1 to III-A-3

CITY OF WACO LANDFILL TCEQ PERMIT NO. MSW - 2400 WASTE DISPOSAL CAPACITY AND SITE OPERATING LIFE CALCULATIONS

Required: Perform Disposal Capacity and Site Operating Life Calculations for Landfill

- 1. Estimate Capacity of East Disposal Area.
- 2. Estimate Capacity of West Disposal Area
- 3. Estimate Total Waste Capacity of Landfill
- 4. Estimate Site Operating Life of Landfill

Solution:

1. Estimate Capacity of East Disposal Area.

a.	Gross airspace from AutoCAD volume calculation =	18,619,819 cy		
b.	Airspace consumed by final cover (cy) =			
	112.9 acres at 3.5 feet thick =	-637,509 cy		
c.	Airspace consumed by Bottom Liner and Protective Cover =	729 591		
	112.9 acres at 4 feet thick =	-728,581 cy		
d.	Adjusted Gross Airspace Volume =	17,253,729 cy		
e.	Percent of airspace consumed by Daily and Intermediate cover =	20 percent		
f.	Net Airspace Available for Waste Disposal =	13,802,983 cy		
g.	In-place waste density =	1,200 lb/cy		
h.	Total East Waste Disposal Capacity =	8,281,790 tons		
Available East Waste Disposal Capacity (tons) = 8,281,790 tons				

2. Estimate Capacity of West Disposal Area

a.	Total airspace from AutoCAD volume calculation =	8,489,129 cy

b. Airspace consumed by final cover (cy) =

62.8 acres at

3.5 feet thick =

-354,611 cy

c. Airspace consumed by Bottom Liner and Protective Cover (assume 4' liner, Sideslopes Only) =

62.8 acres at

4 feet thick = -405,269 cy

d. Adjusted Airspace Volume = 7,729,249 cy

e. Percent of Airspace Consumed by Daily and Intermediate Cover = 20 percent (1)

f. Net Total Airspace Available for Waste Disposal = 6,183,399 cy

g. In-place Waste Density = 1,200 lb/cy

3,710,040 tons

h. Total West Waste Disposal Capacity = 3,710,040 tons

3. Estimate Total Waste Capacity of Landfill

From above:

Available East Waste Disposal Capacity (tons) = 8,281,790 tons Available West Waste Disposal Capacity (tons) = 3,710,040 tons

Available West Waste Disposal Capacity (tons) =

Maximum Inventory of Waste at Time of Closure = 11,991,829 tons

CITY OF WACO LANDFILL TCEQ PERMIT NO. MSW - 2400 WASTE DISPOSAL CAPACITY AND SITE OPERATING LIFE CALCULATIONS

4. Estimate Site Operating Life of Landfill

For the Site operating life calculations, the Waste Acceptance Rate is based on the following assumptions:

Days of operation per year = 286 days Initial Daily Waste Acceptance Rate = 1,070 tpd 1.25 % (annually) Assumed Growth Rate (Life of Landfill) = Initial Annual Waste Acceptance Rate = 305,000 tpy Maximum Inventory of Waste at Time of Closure = 11,991,829 tons

The following table calculates the waste stream growth, assuming the growth rates describe above, and the projected cumulative airspace consumed.

		Cumulative		
	MSW Inflow	Disposal Capacity	Disposal Capacity	Disposal
Year	(tons/yr)	Consumed (tons)	Remaining (tons)	Year
2024	305,000	305,000	11,686,829	1
2025	308,813	613,813	11,378,017	2
2026	312,673	926,485	11,065,344	3
2027	316,581	1,243,066	10,748,763	4
2028	320,538	1,563,605	10,428,225	5
2029	324,545	1,888,150	10,103,680	6
2030	328,602	2,216,751	9,775,078	7
2031	332,709	2,549,461	9,442,369	8
2032	336,868	2,886,329	9,105,500	9
2033	341,079	3,227,408	8,764,421	10
2034	345,343	3,572,751	8,419,079	11
2035	349,659	3,922,410	8,069,419	12
2036	354,030	4,276,440	7,715,389	13
2037	358,456	4,634,896	7,356,934	14
2038	362,936	4,997,832	6,993,997	15
2039	367,473	5,365,305	6,626,524	16
2040	372,066	5,737,371	6,254,458	17
2041	376,717	6,114,088	5,877,741	18
2042	381,426	6,495,515	5,496,315	19
2043	386,194	6,881,708	5,110,121	20
2044	391,021	7,272,730	4,719,100	21
2045	395,909	7,668,639	4,323,191	22
2046	400,858	8,069,497	3,922,333	23
2047	405,869	8,475,366	3,516,464	24
2048	410,942	8,886,308	3,105,522	25
2049	416,079	9,302,387	2,689,443	26
2050	421,280	9,723,666	2,268,163	27
2051	426,546	10,150,212	1,841,617	28
2052	431,878	10,582,090	1,409,740	29
2053	437,276	11,019,366	972,463	30
2054	442,742	11,462,108	529,721	31
2055	448,276	11,910,384	81,445	32
2056	453,880	12,364,264	-372,435	33

Remaining available capacity will be consumed during 2056 Site life is projected to be approximately 33 years.

CITY OF WACO LANDFILL TCEQ PERMIT NO. MSW-2400 McLENNAN AND LIMESTONE COUNTIES, TEXAS

PART III SITE DEVELOPMENT PLAN ATTACHMENT 1 SITE LAYOUT PLANS

Prepared for:

CITY OF WACO



Solid Waste Services 501 Schroeder Drive Waco, TX 76710



Prepared by:

SCS ENGINEERS

Texas Board of Professional Engineers, Reg. No. F-3407

Dallas/Fort Worth Office 1901 Central Drive, Suite 550 Bedford, Texas 76021 817/571-2288

Revision 0 – April 2020 SCS Project No. 16216088.00

TABLE OF CONTENTS

Drawings

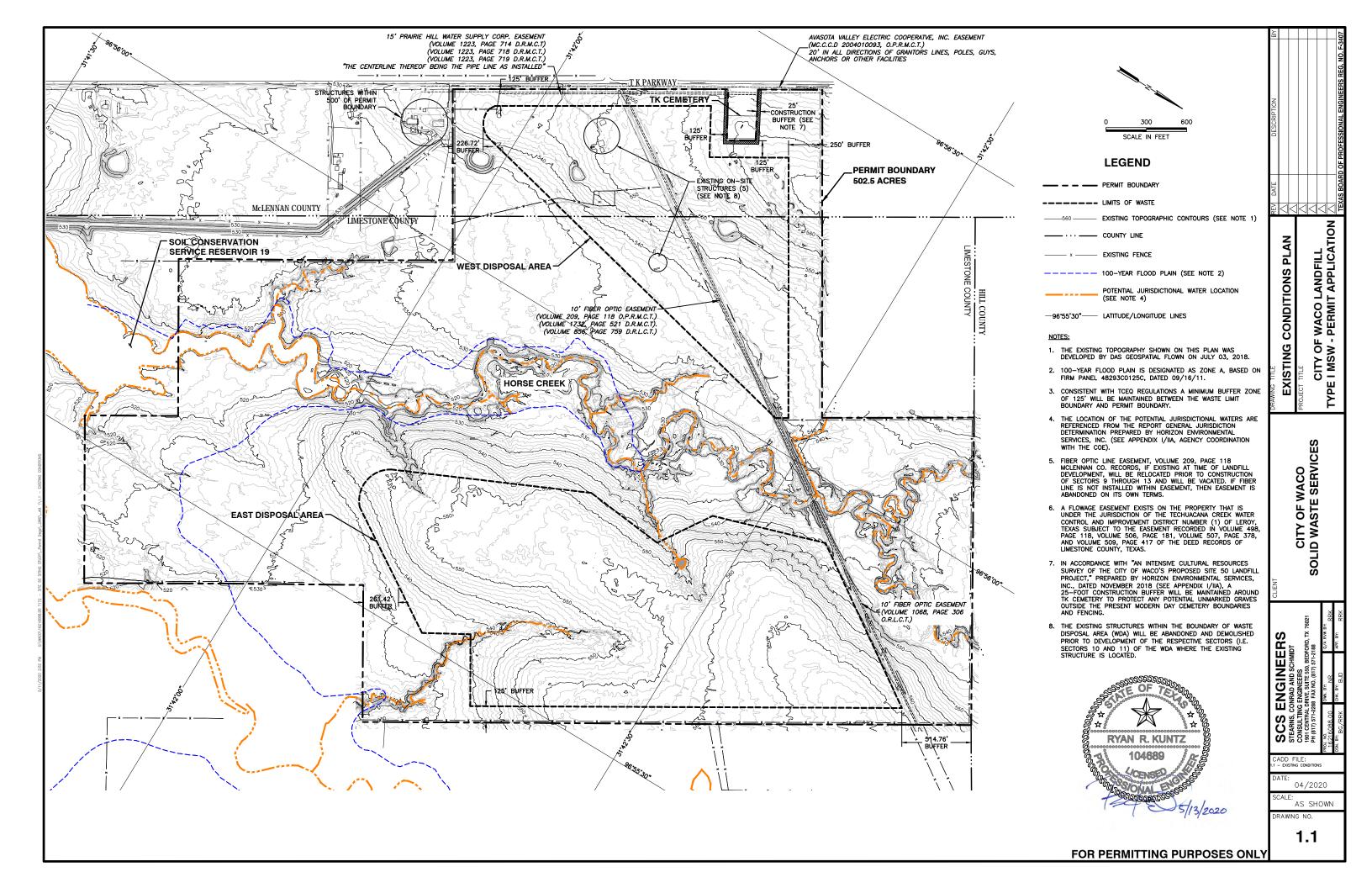
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- 1.2 Detailed Facility Layout and Sequence Plan
- 1.3 East Disposal Area Excavation Plan
- 1.4 West Disposal Area Excavation Plan
- 1.5 Entrance Facility Plan

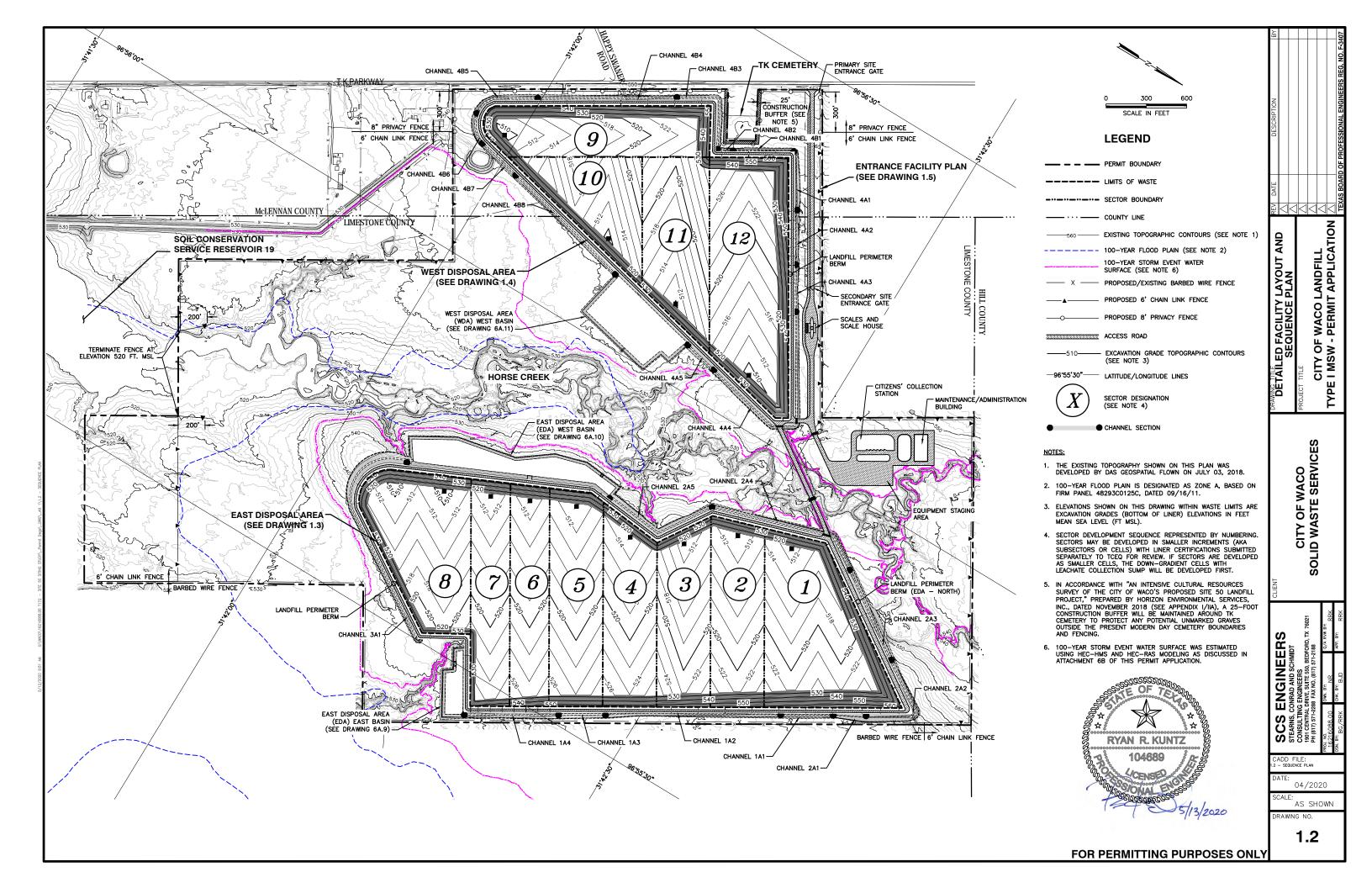
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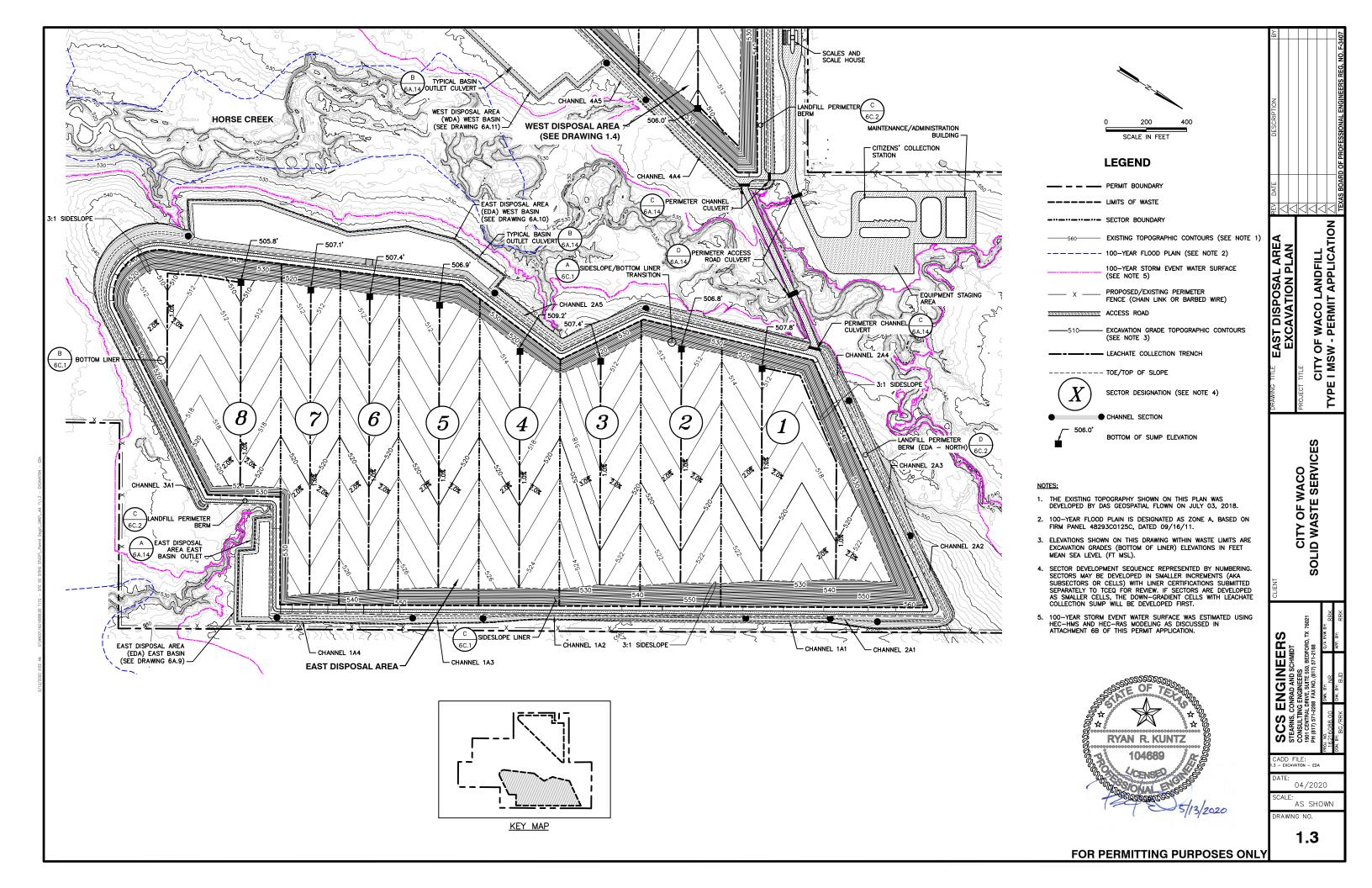
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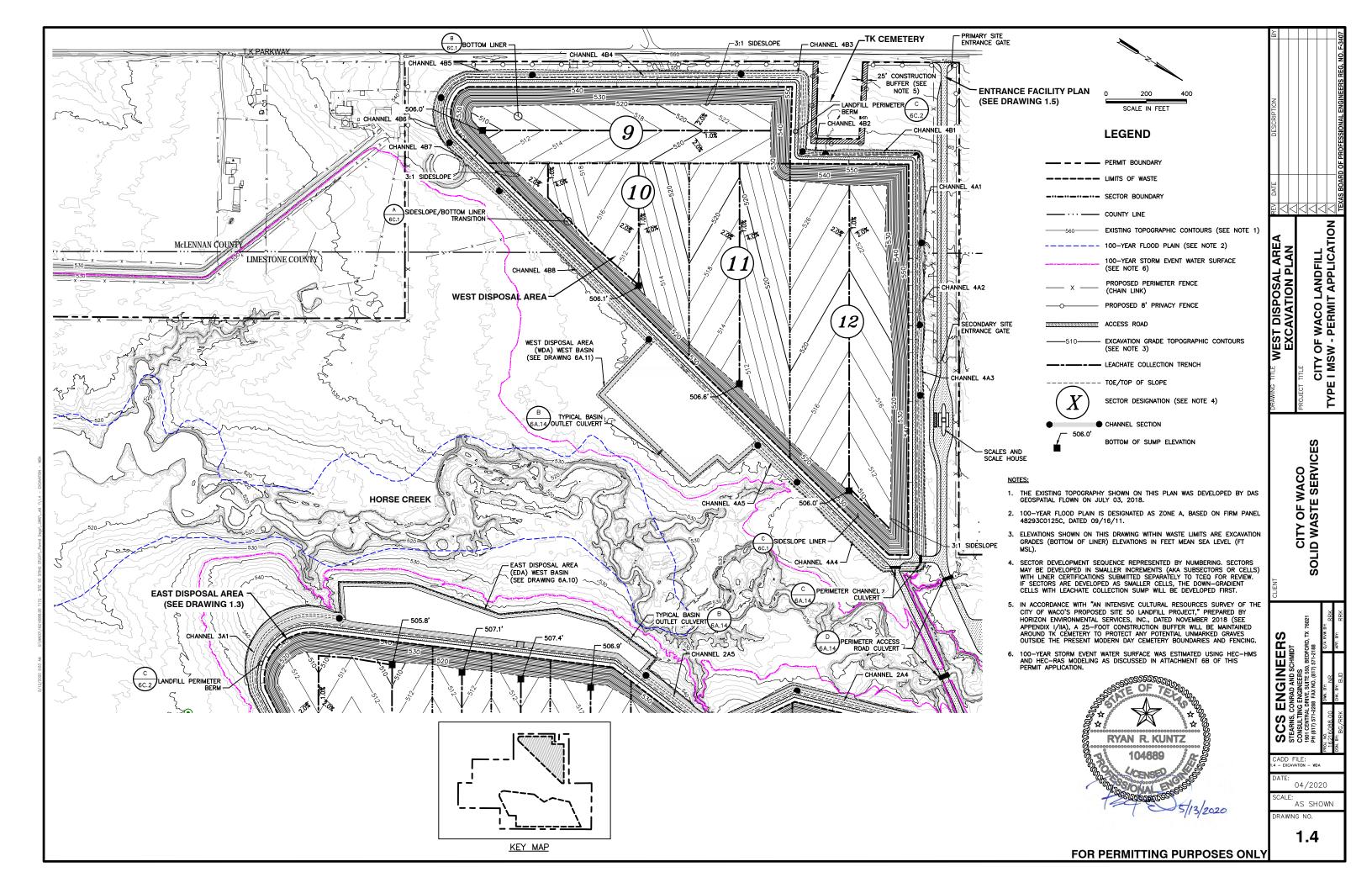
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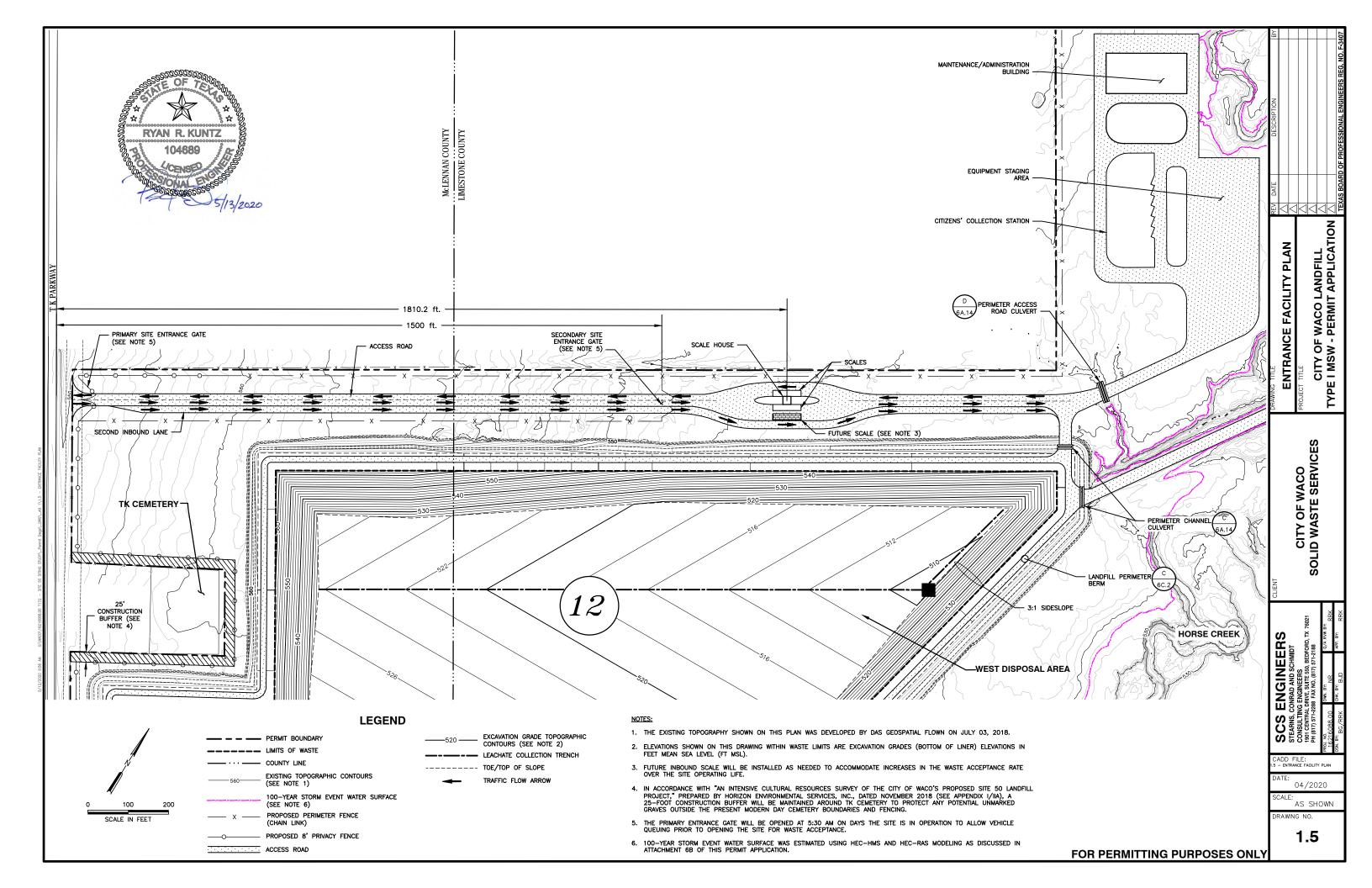
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CITY OF WACO LANDFILL TCEQ PERMIT NO. MSW-2400 McLENNAN AND LIMESTONE COUNTIES, TEXAS

PART III SITE DEVELOPMENT PLAN ATTACHMENT 2 FILL CROSS SECTIONS

Prepared for:

CITY OF WACO



Solid Waste Services 501 Schroeder Drive Waco, TX 76710



Prepared by:

SCS ENGINEERS

Texas Board of Professional Engineers, Reg. No. F-3407

Dallas/Fort Worth Office 1901 Central Drive, Suite 550 Bedford, Texas 76021 817/571-2288

Revision 0 – April 2020 SCS Project No. 16216088.00

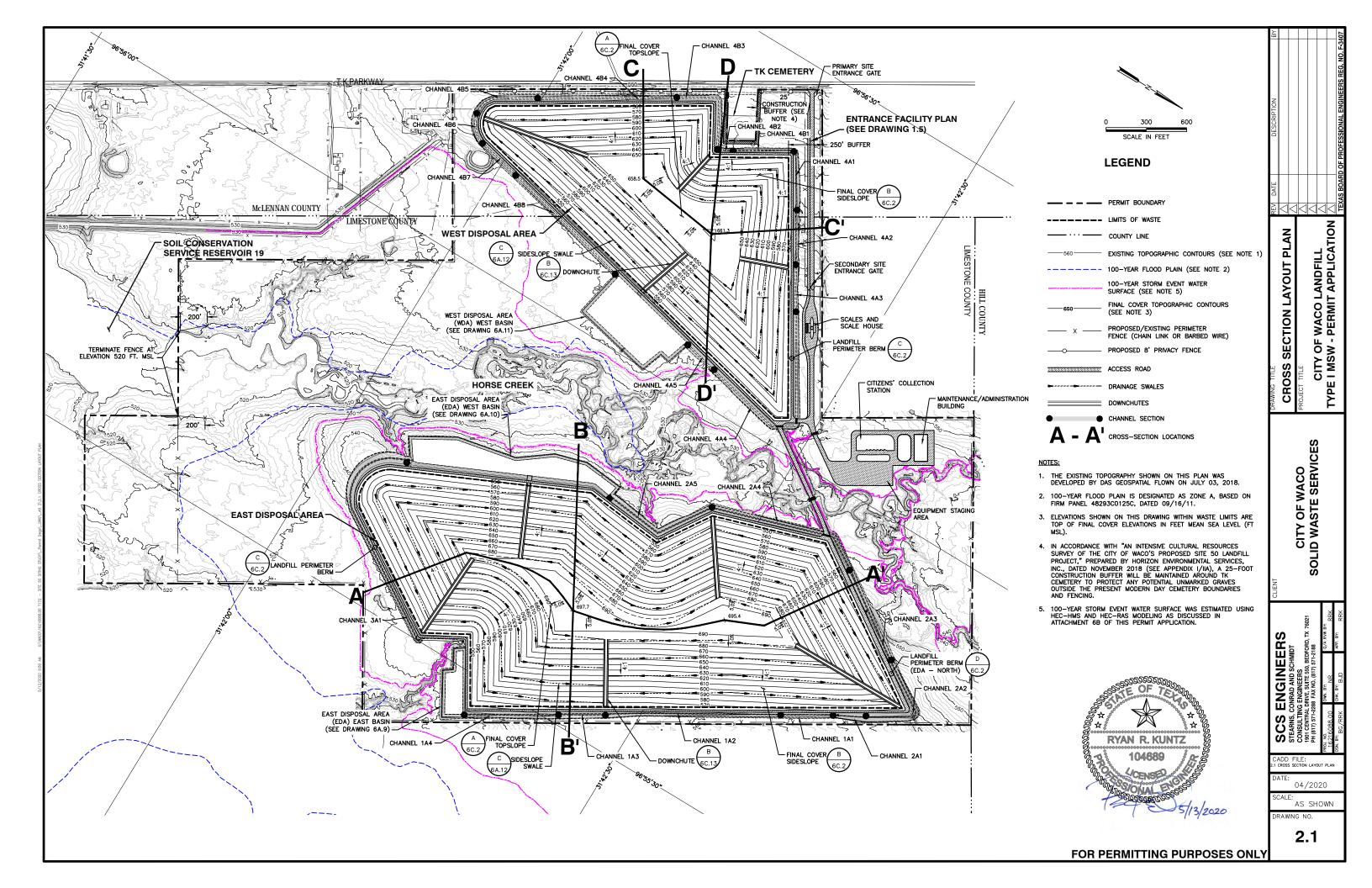
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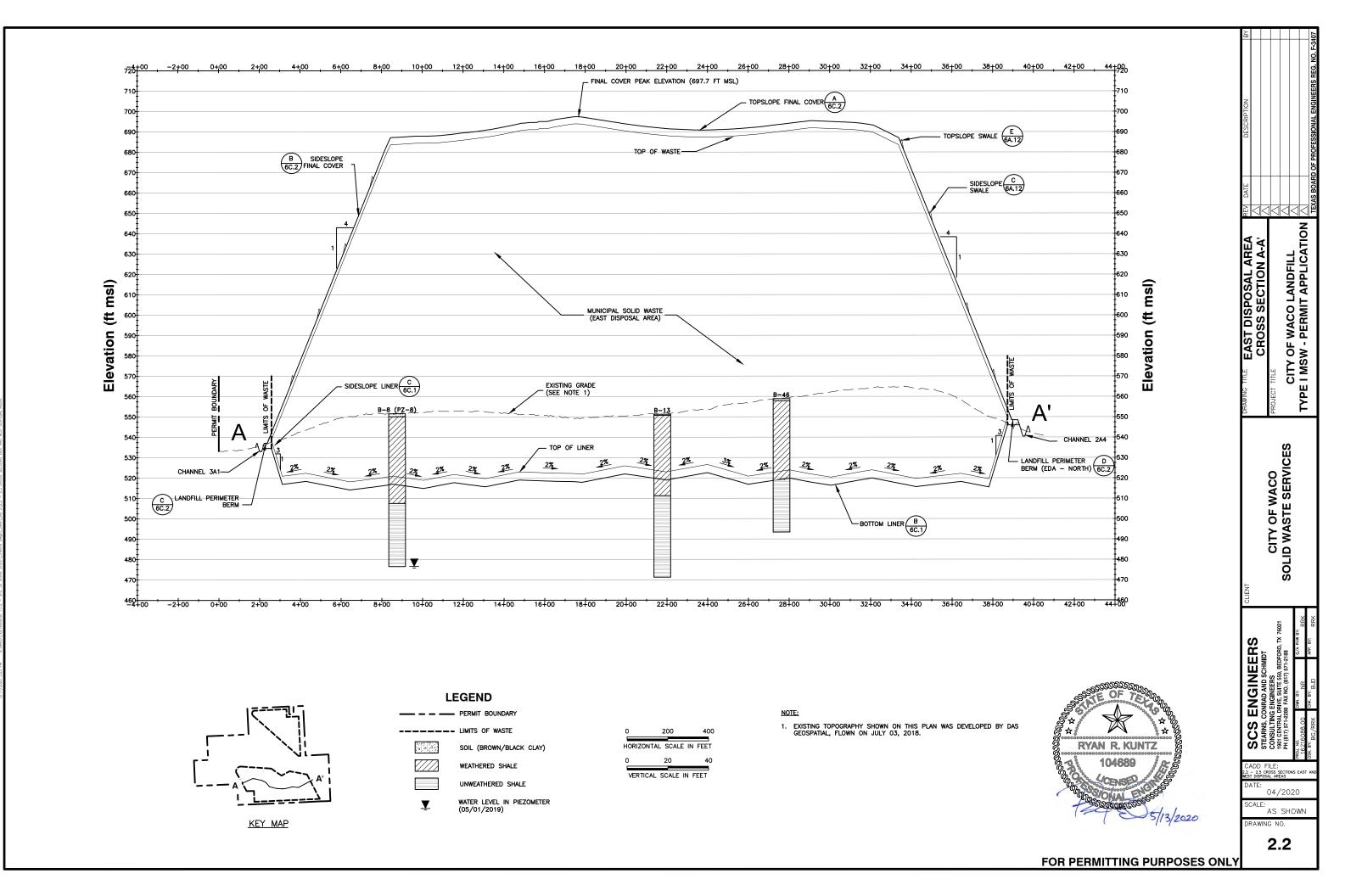
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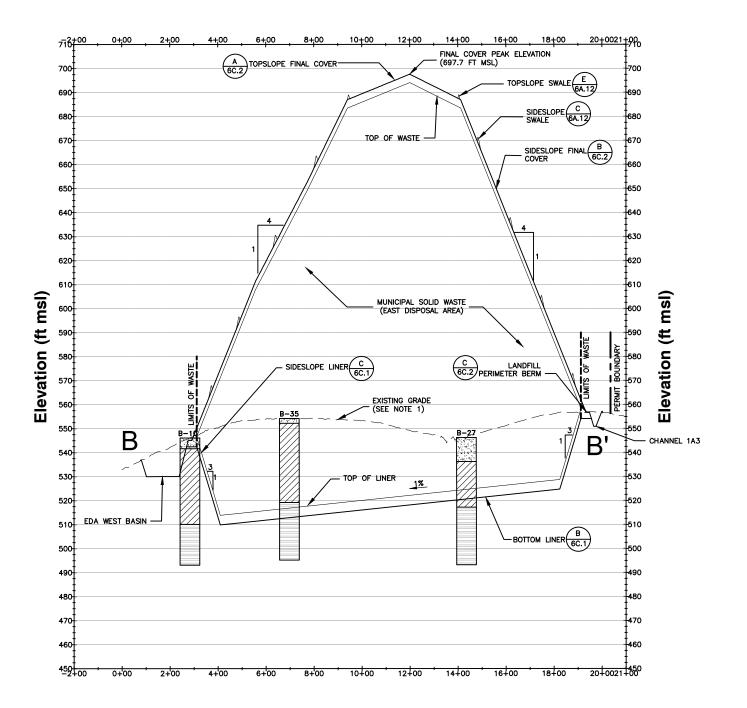
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- East Disposal Area Cross Section B-B' 2.3
- West Disposal Area Cross Sections C-C' and D-D' 2.4



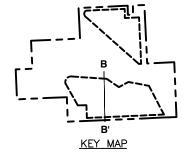
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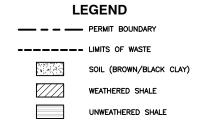












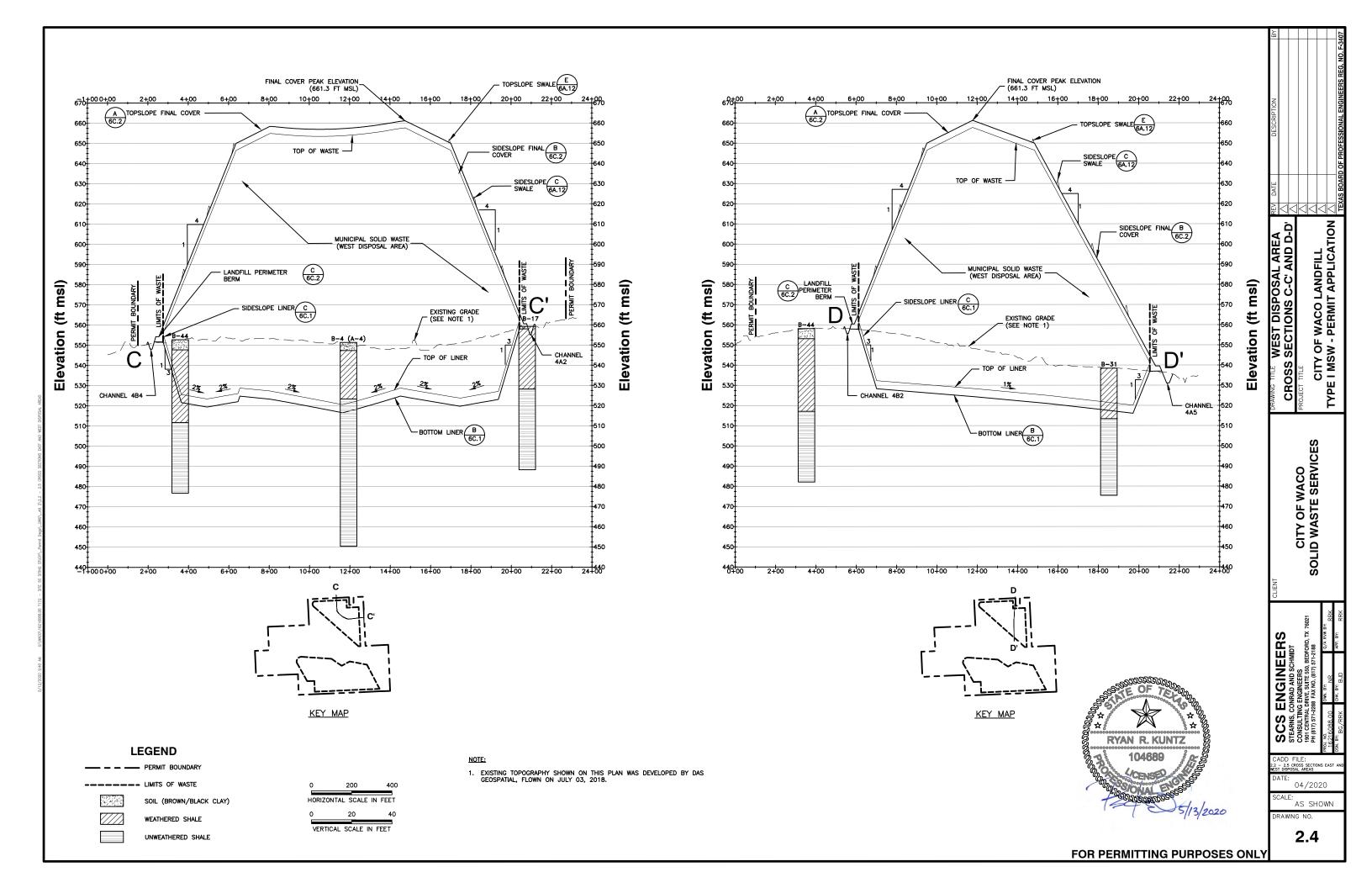
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FOR PERMITTING PURPOSES ONLY



CITY OF WACO LANDFILL TCEQ PERMIT NO. MSW-2400 McLENNAN AND LIMESTONE COUNTIES, TEXAS

PART III SITE DEVELOPMENT PLAN ATTACHMENT 3 LANDFILL COMPLETION PLAN

Prepared for:

CITY OF WACO



Solid Waste Services 501 Schroeder Drive Waco, TX 76710



Prepared by:

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1901 Central Drive, Suite 550 Bedford, Texas 76021

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Revision 0 – April 2020 SCS Project No. 16216088.00

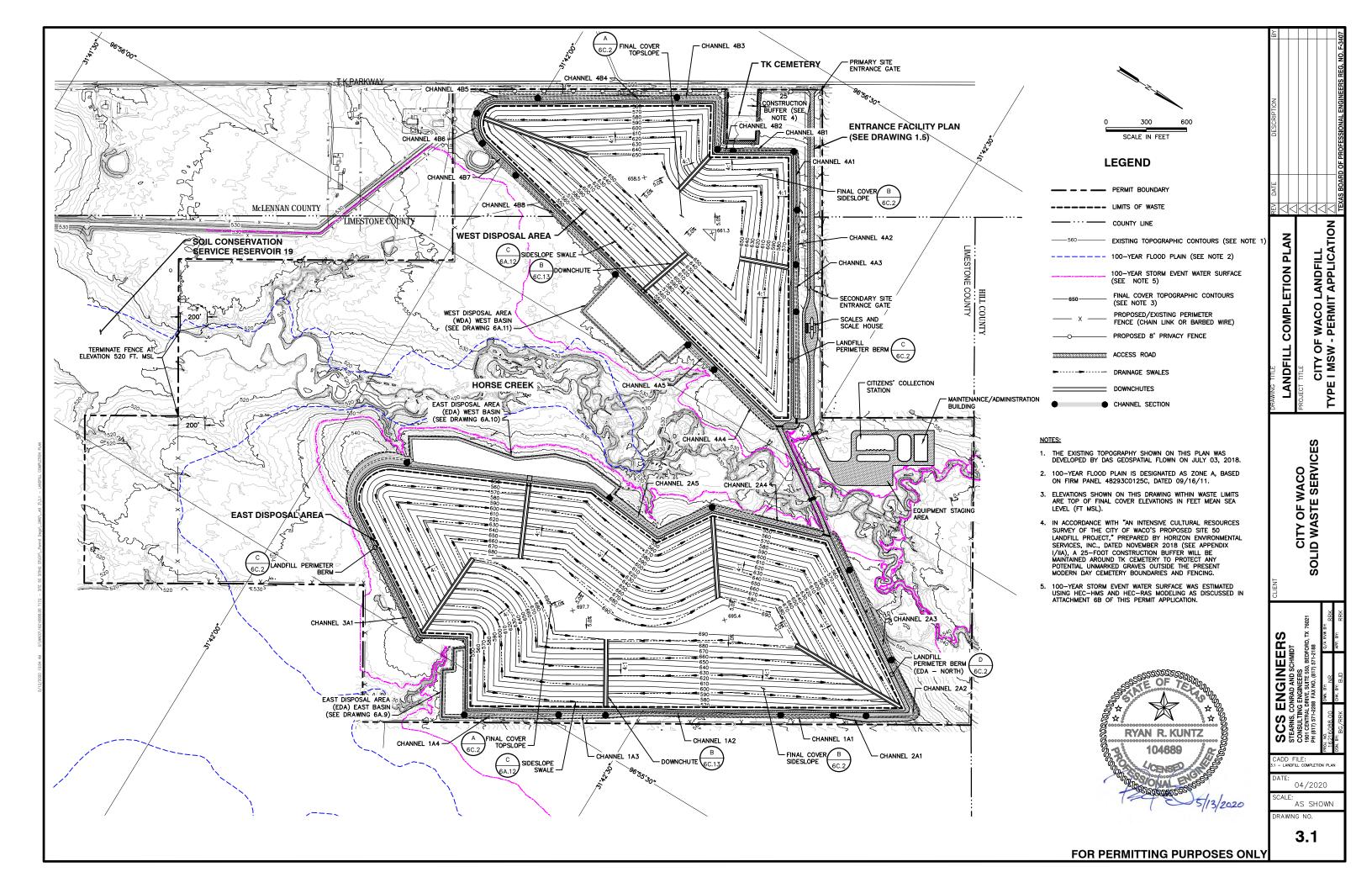
TABLE OF CONTENTS

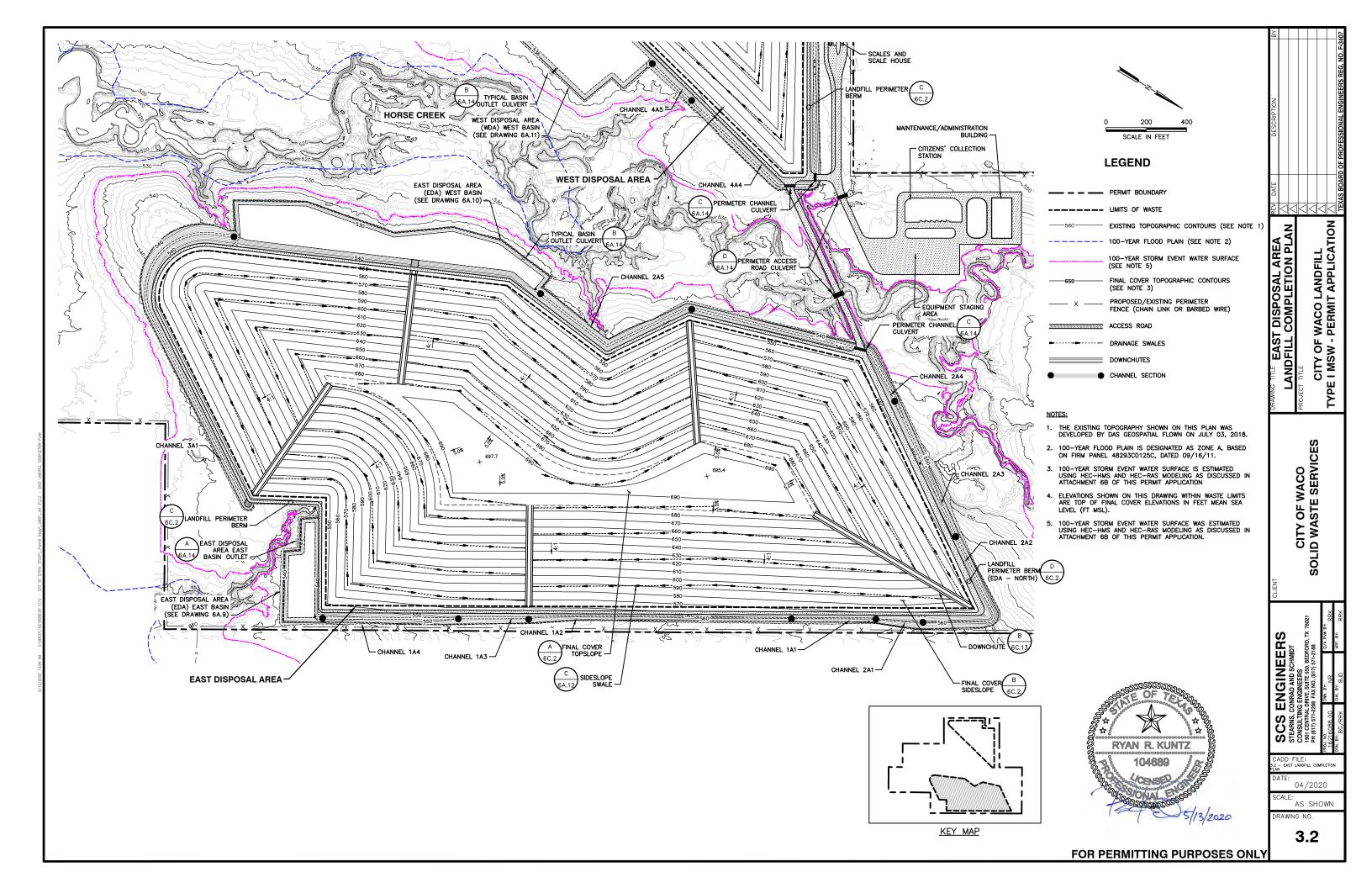
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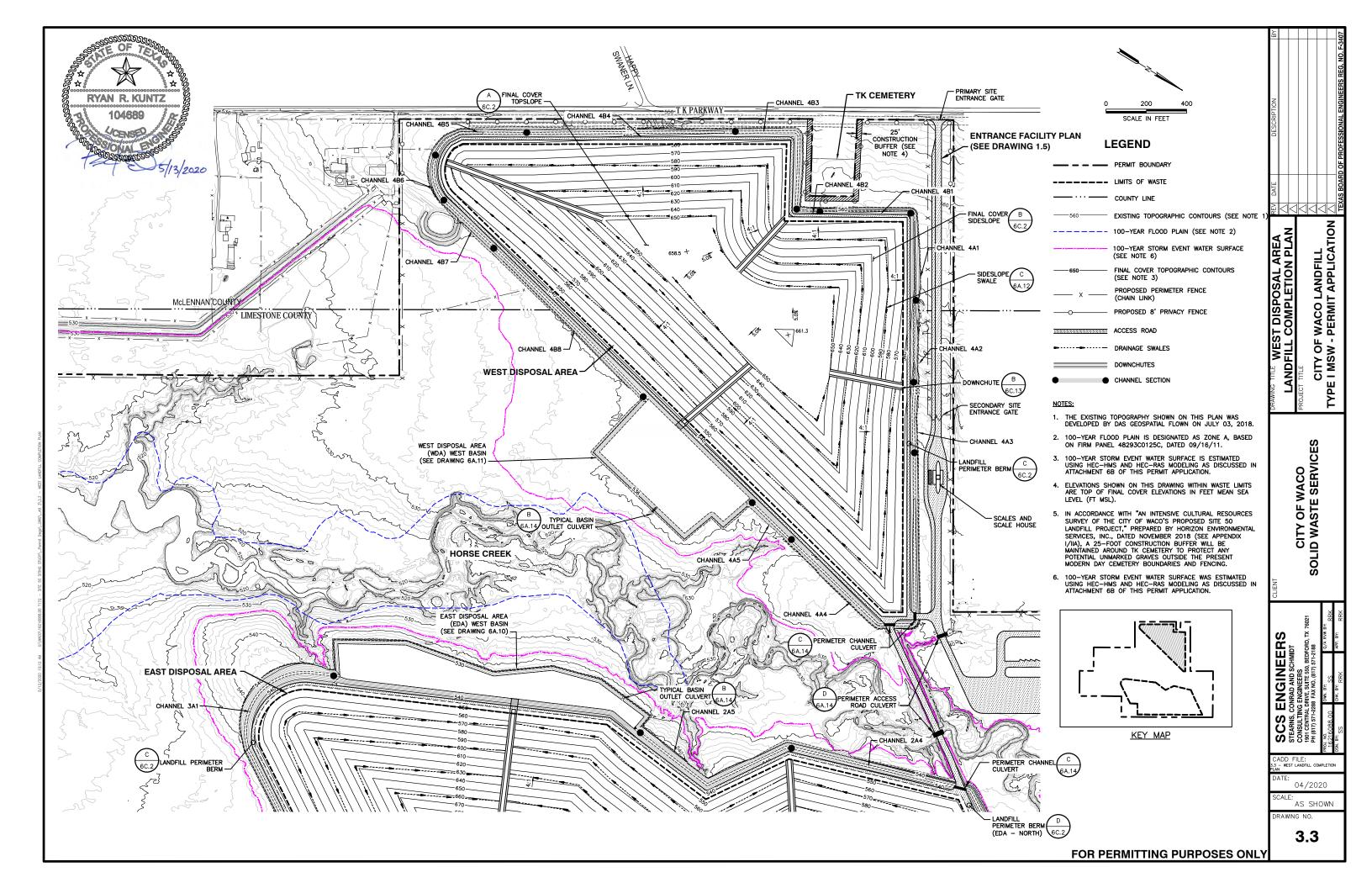
- 3.1 Landfill Completion Plan
- 3.2 East Disposal Area Landfill Completion Plan
- 3.3 West Disposal Area Landfill Completion Plan



SCS Engineers TBPE Reg. # F-3407







CITY OF WACO LANDFILL TCEQ PERMIT NO. MSW-2400 McLENNAN AND LIMESTONE COUNTIES, TEXAS

PART III - SITE DEVELOPMENT PLAN ATTACHMENT 4 GEOLOGY AND GROUNDWATER REPORT

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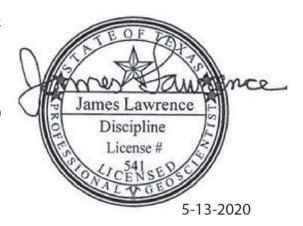


TABLE OF CONTENTS

SEC.	<u>TION</u>	<u>PAGE</u>
1	INTRODUCTION	4-1-1
2	REGIONAL PHYSIOGRAPHY, TOPOGRAPHY, AND CLIMATE	4-2-1
	2.1 PHYSIOGRAPHY AND TOPOGRAPHY	4-2-1
	2.2 CLIMATE	4-2-1
3	GEOLOGY	4-3-1
	3.1 GEOLOGIC SETTING	4-3-1
4	HYDROGEOLOGY	4-4-1
	4.1 REGIONAL HYDROGEOLOGY	4-4-1
	4.2 LOCAL GROUNDWATER USE	4-4-1
5	SUBSURFACE INVESTIGATION REPORT	4-5-1
	5.1 PREVIOUS INVESTIGATION PROGRAMS	4-5-1
		4-5-2
	5.3 SOIL ENGINEERING PROPERTIES	4-5-2 4-6-1
6	GROUNDWATER INVESTIGATION REPORTJames Lawrence	4-6-1
		4-6-1
	1810	4-6-1
	6.3 GROUNDWATER INVESTIGATION RESULTS	4-6-2
7	POLLUTANT PATHWAYS	4-7-1 20
	7.1 LOCAL HYDROGEOLOGY	4-7-1
8	GROUNDWATER QUALITY CHARACTERIZATION	4-8-1
	8.1 OVERVIEW OF THE EXISTING GROUNDWATER MONITORING SYSTEM	4-8-1
	8.2 GROUNDWATER MONITORING DATA	4-8-1
	8.3 REGIONAL GROUNDWATER QUALITY	4-8-1
9	GROUNDWATER MONITORING PLAN	4-9-1
	9.1 EXISTING GROUNDWATER MONITORING SYSTEM	4-9-1
	9.2 PROPOSED GROUNDWATER MONITORING SYSTEM	4-9-1
	9.3 GROUNDWATER MONITORING SYSTEM CERTIFICATION	4-9-3
10	GROUNDWATER SAMPLING AND ANALYSIS REQUIREMENTS	4-10-1
11	SUMMARY	4-11-1
12	REFERENCES	4-12-1

Figures

Figure - 4.1 Site Location Map

Figure - 4.2 Physiographic Map of Texas

Figure - 4.3 General Topographic Map

Figure - 4.4 Geologic Map

Figure - 4.5 Structural Cross Sections of Regional Geology and the Trinity Aquifer

Figure - 4.6 Seismic Impact Zone Map

Figure - 4.7 Tectonic Map of Texas

Figure - 4.8 Trinity Aquifer

Figure - 4.9 Boring Location Map

Figure - 4.10 Geologic Cross Section A-A'

Figure - 4.11 Geologic Cross Section B-B' Figure - 4.12 Geologic Cross Section C-C'

Figure - 4.13 Geologic Cross Section D-D'

Figure - 4.14 Geologic Cross Section E-E'

Figure - 4.15 Geologic Cross Section F-F'

Figure - 4.16 Piezometer Location Map

Figure - 4.17 VWP Location Map

Figure - 4.18 Potentiometric Map

Figure - 4.19 Proposed GWM System Map

Figure - 4.20 Typical Monitoring Well Detail

Tables

Table III-4.1 Regional Physiography

Table III-4.2 Waco Average Monthly Rainfall

Table III-4.3 Geologic Units and their Water-Bearing Properties

Table III-4.4 Recorded Wells within 1 Mile

Table III-4.5 Coordinates and Elevations of Borings

Table III-4.6 Properties of Unit II

Table III-4.7 Properties of Unit III

Existing Piezometer Completion Data Table III-4.8

Table III-4.9 Summary Initial and Static Water Level Data

Table III-4.10 Vibrating Wire Piezometer Completion Data

Table III-4.11 Vibrating Wire Piezometer Inferred Groundwater Elevation Data

Table III-4.12 Summary of Aquifer (Slug) Tests Performed by SCS Engineers

Table III-4.13 Summary of Horizontal Flow Rate Calculation Data

Table III-4.14 Proposed Monitoring Well Information

Appendices

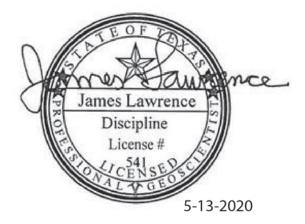
Appendix III-4.A Soil Resource Report Appendix III-4.B Well Search Data Appendix III-4.C Soil Boring Plan Appendix III-4.D **Boring Logs**

Appendix III-4.E State Well Reports

Appendix III-4.F Geotechnical Investigation Reports

Vibrating Wire Piezometer Manual and Calibration Forms
5-13-2020 Appendix III-4.G

Appendix III-4.H	Standpipe Piezometer Completion Data
Appendix III-4.I	Vibrating Wire Piezometer Completion Data
Appendix III-4.J	Precipitation and Groundwater Elevation Data
Appendix III-4.K	Standpipe Piezometer Historic Water Level Data
Appendix III-4.L	Vibrating Wire Piezometer Historic Water Level Data
Appendix III-4.M	Slug Test Data



1 INTRODUCTION

This document is the Geology and Groundwater Report for the City of Waco Landfill, Permit No. MSW-2400 (Landfill), and has been prepared in accordance with 30 Texas Administrative Code (TAC) §330.63(e). The landfill is a Type I municipal solid waste (MSW) landfill as defined in 30 TAC §330.5. This report summarizes available data related to regional and site-specific geologic and hydrogeologic conditions, as well as aquifers in the area of the Landfill in accordance with 30 TAC §330.63(e). This document also includes sections related to Groundwater Characterization and establishes a Groundwater Monitoring System design in accordance with 30 TAC §330.63(f).

2 REGIONAL PHYSIOGRAPHY, TOPOGRAPHY, AND CLIMATE

2.1 PHYSIOGRAPHY AND TOPOGRAPHY

The Landfill will be located approximately 0.4 miles south of the intersection of State Highway 31 and T K Parkway (also known as Farm-to-Market [FM] 939) (Figure-4.1). The Landfill lies in the eastern portion of the Great Plains physiographic province of Texas, near the boundary between the Great Plains Province and the Coastal Plains Province (Wermund, 1996, Figure-4.2). In earlier publications, this area was referred to as the Black Prairie Subprovince, which occupied the central and north central regions of Texas. The Black Prairie Subprovince is bounded on the north by the Red River and on the south by the Colorado River. This area consists of gently rolling hills that are occasionally broken by streams flowing west to east through the region that generally form wide, shallow valleys (Figure-4.3). Elevations in this region vary from approximately 400 feet mean sea level (ft-msl) to 750 ft-msl (Hill, 1901).

Horse Creek flows through the center of the landfill property, separating topographic highs to the east and west that drain into the creek. Horse Creek transports waters from a northern watershed and the landfill property topographic highs to a dammed reservoir (Soil Conservation Service, Site 19 Reservoir) south of the property. Packwood Creek and Williams Creek both flow generally from east to west and are located east and southeast of the Landfill property. Horse Creek and Packwood Creek/Williams Creek transport surface waters from north and east, respectively, and discharge into the referenced reservoir that releases into Williams Creek. In the most eastern area of the Landfill, water is transported into Packwood Creek via unnamed tributaries. Regional physiography is shown on Figure-4.2. The distances to local surface water bodies and drainage features are shown in Table III-4.1.

The minimum surface elevation of the property is approximately 515 ft-msl around the lake area in the southern area of the site. The maximum elevation of the property is approximately 570 ft-msl located near the northeast boundary (Figure-4.3).

2.2 CLIMATE

The climate in the Waco area is sub-humid, with area rainfall averaging approximately 34.7 inches per year (averaged between 1981 and 2010 at the Waco-McGregor Municipal Airport; source: www.usclimatedata.com). A table with the average monthly rainfall in the Waco area over the 29 years is provided in Table III-4.2.

Revision 0 4-2-1 SCS ENGINEERS

3 GEOLOGY

3.1 GEOLOGIC SETTING

The regional geology is comprised primarily of geologic formations of the Late Cretaceous Gulfian and Comanche Series (McCoy et al, 1992). Figure-4.4 depicts the surface geology in the region. Regional geology and stratigraphy is depicted in Table III-4.3 with the Landfill stratigraphic position shown (Baker et al., 1990; Tetco, 1987). Rocks exposed at the surface in McLennan and Limestone Counties generally consist of Cretaceous Taylor Group (Wolfe City Formation) shalemarl, sand, silt, and clay, as well as near-surface Tertiary/Quaternary sands, gravels, silts, and clay sediments deposited near and along stream channels (U.S. Department of Agriculture, 1991 and 1992). The Cretaceous rocks of the Great Plains region of Texas represent shallow to marginal marine depositional environments caused by a series of transgressions and regressions (Hill, 1901). These deposits consist primarily of sandstones, shales, and carbonates, which represent different stages in the transgression-regression sequence.

Site stratigraphy details, including geologic age, lithology, variations in lithology, thickness, depth, geometry, hydraulic conductivity, and depositional history are included below and in Section 5.2. A geologic map of the area is included as Figure-4.4 and a regional structural cross-section depicting the distribution of geologic units is included as Figure-4.5.

Regional geologic units as depicted on the Geologic Atlas of Texas, Waco sheet (excerpted in Figure-4.4), include the Lower and Upper Cretaceous Systems from the Travis Peak Formation to the Pecan Gap Chalk, with Tertiary/Quaternary sediments deposited near and along stream channels. These formations consist of clastic materials, with grain sizes ranging from clay to sand and gravel. Most stratigraphic units of the Great Plains thicken towards the Gulf of Mexico as a result of subsidence of the depositional basin and rising of the land surface (Figure-4.5). Formation outcrops generally trend north-northeast to south-southwest, sub-parallel with the coast.

The Taylor Group is the uppermost geologic unit in the region of the Landfill property, consisting of the Pecan Gap Chalk, Wolfe City Formation and the Ozan Formation (Table III-4.3) and is generally overlain by Tertiary/Quaternary sediments deposited near and along stream channels. The Pecan Gap Chalk consists of chalk in the lower part grading up to a chalky marl. The Wolfe City Formation consists of shale-marl, sand, silt, and clay. The Ozan Formation consists of a calcareous claystone with increasing upward contents of silt and sand (Barnes, 1967; 1970). Underlying the Taylor Group are the Austin and Eagle Ford Groups, consisting primarily of chalk and calcareous shale with interbedded limestone lenses and numerous bentonite layers (Charvat, 1985; Barnes, 1970).

Underlying the Austin and Eagle Ford Groups is the Pepper Shale Formation (Woodbine Group) consisting of very dark grey, non-calcareous, pyritic shale; grading into the Woodbine Formation sand north of the Brazos River (Barnes, 1970). Underlying the Pepper Shale, the Del Rio Clay Formation (Washita Group) is mostly clay, with some thin lenticular beds of highly calcareous siltstone and limestone (Barnes, 1970). The Del Rio Clay is known as the Grayson Marl in some publications (Barnes, 1970).

Underlying the Del Rio Clay are the Georgetown Limestone Formation and the Main Street Limestone, which are medium grained, chalky limestones with some calcareous shale interbeds (Barnes, 1970). Underlying the Georgetown Formation and the Main Street Limestone are the

Pawpaw Formation, and Weno Limestone undivided, which are described as marl with interbedded limestone, and limestone with interbedded marl, respectively (Barnes, 1970).

Underlying the Pawpaw Formation and Weno Limestone are the Denton Clay, Fort Worth Limestone, and Duck Creek Limestone (Barnes, 1970). These formations are comprised primarily of limestone and represent the lower part of the Washita Group and are underlain by the Kiamichi Clay and Edwards Limestone. In some areas the units of the Washita Group from the Main Street Limestone to the Duck Creek Limestone are mapped as Georgetown Formation (Barnes, 1970). The Kiamichi Clay is clay, shale, and limestone. The Edwards Limestone is a massive limestone with abundant chert nodules; together these represent the upper units of the Fredericksburg Group (Barnes, 1970). The Kiamichi Clay is discontinuous and is mapped with the Edwards Limestone. Underlying the Edwards Limestone is the Comanche Peak Limestone and the Walnut Clay. The Comanche Peak Limestone is a hard limestone with numerous shale interbeds. The Walnut Clay consists primarily of clay, limestone, and shale (Barnes, 1970) and acts as the confining unit for the Trinity Aguifer (U.S.G.S., 1996). Underlying the Walnut Clay is the Paluxy Sand and Glen Rose Formation of the Trinity Aquifer. The Paluxy Sand is a quartz sand, fine to very fine-grained, with thin interbeds of shale and limestone. The Glen Rose Formation consists of limestone, clay, marl, and sand (Barnes, 1970). The Paluxy Sand and Glen Rose Formations represent the uppermost formations of the Trinity Aquifer (U.S.G.S., 1996).

Stratigraphic positions of these geologic units, with corresponding hydrogeologic units, are presented in Table III-4.3. Figure-4.5 depicts a regional geologic cross section.

3.1.1 Fault Areas

A site-specific fault and seismic impact zone evaluation was conducted as part of a permit application by SCS Engineers. The fault study for this characterization conducted by SCS consisted of the following:

- 1. Review of published geologic maps, literature, and fault/structural studies of the area.
- 2. Review of published surficial fault maps.
- 3. Review of aerial photographs.
- 4. A site field investigation which included inspections of existing stream cut walls and surrounding roads for surface displacement.

Figure-4.6 depicts seismic impact zones. Figure-4.7 is a regional tectonic map. The fault, seismic, and tectonic maps indicate that the Landfill is located between two fault zones: the Balcones Fault Zone and the Mexia-Talco-Luling Fault Zone. The Balcones Fault Zone is located south and west of the Landfill, while the Mexia-Talco-Luling Fault Zone is located to the east. The closest mapped faults to the Landfill are normal faults downthrown to the east; all of which are well over a mile away. The closest fault lies within the Balcones Fault Zone, and is probably structurally related to this family of faults. The most prominent tectonic feature on Figure-4.7 is the Ouachita Tectonic Front (Ewing, 1991), which is a deep-seated thrust fault zone located over 10 miles west of the Landfill. Faults in this zone are identified only by deep seismic data and other geophysical data and do not propagate to the ground surface.

The Waco Uplift is a structural feature approximately eight miles wide (east-west) by 80 miles long (north-south) associated with the Balcones/Ouachita trend. The western boundary is approximately twenty miles west of the Landfill (Caran, 1981).

Baylor University (located in the City of Waco) has conducted geologic, structural, and fault studies of the Waco area. Hayward (1978) identified small displacement faults in the Waco area Austin Chalk Formation which are thought to be growth faults. The description and photographs of these faults were used to assist in the site field investigation described in Section 5.0.

Based on review of the aforementioned documentation, the Landfill is not located within one-half mile of an active fault nor experiences differential subsidence; therefore, the requirements of 30 TAC §330.555(a, b) are met.

3.1.2 Seismic Impact Zones

The location restriction criterion in 30 TAC §330.557 requires that new disposal units and lateral expansions not be located in seismic impact zones unless the owner or operator can demonstrate that all containment structures, including liners, leachate collection systems, and surface water control systems are designed to resist the maximum horizontal acceleration in lithified earth material for the Landfill. A seismic impact zone is defined as an area with a 10 percent or greater probability that the maximum horizontal acceleration in lithified earth material, expressed as a percentage of the earth's gravitational pull (g), will exceed 0.10 g in 250 years. If the maximum horizontal acceleration is less than or equal to 0.10 g, then the design of the unit will not need to incorporate an evaluation of seismic effects.

Areas within the United States where seismic effects need to be evaluated, as determined by the United States Geological Survey (USGS), are shown on Figure-4.6. As indicated on this figure, the Landfill property is not located within a seismic impact zone as defined by 30 TAC §330.557.

3.1.3 Unstable Areas

The location restriction criteria in 30 TAC §330.559 require engineering measures to be incorporated into the design of a disposal unit located in an unstable area to ensure that the integrity of the structural components of the disposal unit will not be disrupted. Unstable areas, by definition, are areas susceptible to natural or human-induced events or forces that are capable of impairing the integrity of some or all structural components (e.g., liners, leachate collection systems, final covers, etc.) of a disposal unit. Unstable areas can include poor foundation conditions, areas susceptible to mass movement, salt domes, or karst terrain.

Based on information from existing geological and geotechnical data, unstable areas due to poor foundation conditions, areas susceptible to mass movement, salt domes, or karst terrain do not exist at, or immediately adjacent to the Landfill.

3.1.4 Erosion Potential

30 TAC §330.63(e)(2) requires an evaluation of active geologic processes in the vicinity of the Landfill, including the potential for erosion. The potential for erosion due to surface water processes, such as overland flow, channeling, gullying, and fluvial processes, including meandering streams and undercut banks, has been evaluated by SCS.

The Landfill surface drainage generally flows towards the north-south trending Horse Creek located near the center of the Landfill and/or to the south towards the Soil Conservation Service Site 19 Reservoir within or beyond the southerly limits of the property. Thus, the eastern Landfill drainage is generally to the west and south, whereas the western Landfill drainage is to the east and south. Erosional processes are primarily limited to those produced by periods of heavy rainfall. The Landfill topography results in moderate surface erosion during periods of heavy rainfall. This erosion is limited by the vegetation with cohesive clay-rich soils and sediments that outcrop over most of the Landfill area. Mass wasting has not been observed at the Landfill.

The General Soil Map of Texas (USDA, 2008) shows that the Landfill is located within the Texas Blackland Prairie area that includes Houston Black-Heiden-Wilson soils. The Limestone and McLennan County Soil Surveys (U.S. Department of Agriculture, 1991 and 1992) along with the USDA Web Soil Survey (2008), provided in Appendix III-4.A, indicate the following soil associations occur on the Landfill area:

- Axtell fine sandy loam, 1 to 3 percent slopes,
- Crockett loam, 1 to 3 percent slopes,
- Crockett loam, 3 to 5 percent slopes,
- Ferris clay, 5 to 15 percent slopes, eroded,
- Ferris-Heiden complex, 2 to 5 percent slopes, eroded,
- Heiden clay, 1 to 3 percent slopes,
- Heiden clay, 3 to 5 percent slopes,
- Tinn clay, 0 to 1 percent slopes, frequently flooded,
- Whitesboro loam, frequently flooded,
- Wilson clay loam, 0 to 2 percent slopes.

Aerial photographs (consistent with site observations) indicate that the predominant soil associations present at the Landfill are the Axtell fine sandy loam series and the Wilson clay loam series. These series consist of moderately well drained, moderately low to high permeable soils that are derived from clay and clay loam materials from Upper Cretaceous shales, marls, and/or mudstones. Typically, the Axtell series is found on steeper slopes than the Wilson series. The surface sediments consist of dark brown to dark gray silty clays and clay loams. The available water holding capacity of the Axtell and Wilson series is moderate.

The topographic high on the northwestern side of the Landfill consists primarily of the Crockett loam and Heiden clay series. These series consist of moderately well to well drained, very low to moderately low permeability soils that are derived from clayey residuum weathered from Upper Cretaceous shales, marls, and mudstones. The surface sediments consist of dark grayish brown clay and the available water holding capacity is moderate. Portions of the Landfill's east side also are covered in Heiden clay series.

Aerial photographs (consistent with site observations) also indicate the presence of the Tinn clay series on the topographic low areas of the Landfill along Horse Creek and associated drainages. This series, which frequently floods, consists of moderately well drained, very low to moderately low permeable soils that are derived from Holocene-age sediments along the stream. Whitesboro loam is also located along a topographic low of the Packwood Creek near the southeast corner of the Landfill, consisting of moderately well drained, moderately high to highly permeable soils derived from loamy alluvium of Holocene age of mixed sources. The available water holding capacity of the Tinn clay and Whitesboro loam series is moderate to high, respectively.

Other lesser distributed soil series include the Ferris clay and Ferris-Heiden complex series located in northern portions of the east and west sides of the Landfill. Both soils consist of well drained, very low to moderately permeable soils that formed from clayey residuum materials from Upper Cretaceous shales, marls, and/or mudstones. The available water holding capacity of both series is moderate.

4 HYDROGEOLOGY

4.1 REGIONAL HYDROGEOLOGY

The Trinity Aquifer is the State-defined major aquifer in this region, underlying an area of approximately 41,000 square miles (U.S.G.S., 1996; Ashworth and Hopkins, 1995). The regional extent of the Trinity Aquifer is depicted in Figure-4.8. Approximately 800 feet of stratigraphy separates the base of the Landfill from the top of the Trinity Aquifer (Figure-4.5); at least 500 feet of this geology has a low hydraulic conductivity. (Holloway, 1961; Klemt et al., 1975; Nordstrom, 1982) therefore, there is no hydraulic connection between shallow groundwater at the Landfill and the Trinity Aquifer. The Trinity Aquifer is composed primarily of Cretaceous sandstone, sand, silt, clay, shale, conglomerate, and carbonates. The stratigraphic units that make up the Trinity Aquifer are the Travis Peak, Glen Rose, and Paluxy Formations (U.S.G.S., 1996); see Figure-4.5 and Table III-4.3.

The beds of the Trinity Aquifer dip gently to the south-southeast, towards the Gulf of Mexico, and aquifer thickness increases in that direction. Groundwater gradient is to the southeast except where affected by local pumping, which has created water-level declines of up to 400 feet in the Waco area (Baker et al., 1990). The transmissivity of the Trinity Aquifer varies widely due to lithology changes, from about 80 to 5,700 square feet per day (ft2/d), and the storage coefficient ranges from about 0.00002 to 0.026 (U.S.G.S., 1996). Wells in the Trinity Aquifer generally yield 50 to 500 gallons per minute (gpm), though some have yielded as much as 2,000 gpm (U.S.G.S., 1996). Recharge to the Trinity Aquifer is primarily from precipitation falling in the outcrop areas, over 50 miles west of the Landfill (Baker et al., 1990).

The Trinity Aquifer within the area of the Landfill is under confined conditions (STGCD, 2015). The basal Walnut Clay of the Fredericksburg Group functions as the regional upper confining unit to the underlying Trinity Aquifer (Baker et al., 1990). The Walnut Clay is approximately 125 to 175 feet thick in the vicinity of the Landfill (Table III-4.3) (Barnes, 1970).

The approximate altitude of water levels in the Trinity aquifer from local water wells is shown on Table III-4.4. A regional water-table contour map or potentiometric surface map of the Trinity Aquifer is not available for this region.

4.2 LOCAL GROUNDWATER USE

Water supply wells were identified by a review of records on file at the Texas Water Development Board and in accordance with §330.56(d)(4)(J). No wells were identified within the Landfill boundaries (other than the piezometers installed as part of this investigation). The only wells within one mile of the Landfill were installed for oil and gas exploration, as identified in Parts I/II, Section 7.2. The closest water supply wells are greater than 3 miles from the Landfill. There were no water wells located by the records search within a one-mile radius of the Landfill, also as described in Parts I/II, Section 7.2.

The closest water wells to the Landfill noted in the records search are located between 3 and 7 miles from the Landfill. Most of these wells were installed for domestic-public supply purposes and completed in the geologic formations that comprise the Trinity Aquifer. The Trinity Aquifer wells are located northeast, northwest, southwest and south of the Landfill. Only two wells east and southeast of the Landfill were screened in shallow deposits, e.g., the Navarro-Taylor units.

Table III-4.4 and Appendix III-4.B provide well search data. Table III-4.4 provides the locations for these wells and the aquifers in which they are completed (30 TAC §330.63(e)(3)(J)). The closest water well utilized for public supply is approximately 3.6 miles southwest of the Landfill.

The Landfill is unlikely to impact these wells for several reasons. First, the minimum horizontal distance of all the wells from the Landfill is greater than 3.5 miles. Most of the wells produce water from the Trinity Aquifer, which is located approximately 800 feet vertically below the Landfill (Holloway, 1961). Secondly, the soil liner systems that will be installed in the disposal cells provide a low-permeability barrier to prevent the release of potential contaminants. Finally, in the unlikely event a release were to occur, the low-permeability of the natural soils and bedrock below the Landfill will restrict groundwater flow and the groundwater monitoring wells installed on the perimeter will detect the release, which will prompt measures to mitigate the release.

5 SUBSURFACE INVESTIGATION REPORT

5.1 PREVIOUS INVESTIGATION PROGRAMS

A soil boring plan for the Landfill was submitted September 7, 2018 and approved by the TCEQ in a letter dated October 4, 2018. Soil boring investigations of the Landfill began with drilling conducted in January 2018. A total of 5 borings (A-1 through A-5) were completed at that time, with depths ranging from 48 feet to 101 feet-bgs. A second phase of drilling occurred during October 2018 through January 2019, in which an additional 42 borings (B-6 through B-47) were advanced between 28 to 80 feet in depth (see Appendix III-4.C – Soil Boring Plan). In December 2019, additional deep borings were drilled adjacent to B-9 and B-43 to depths of 135 feet and 150 feet, respectively. Conventional standpipe piezometers were installed in the following ten borings: B-1 (PZ-1), B-3 (PZ-3), B-8 (PZ-8), B-9 (PZ-9), B-18 (PZ-18), B-20 (PZ-20), B-33 (PZ-33), B-41 (PZ-41), B-43 (PZ-43), and B-47 (PZ-47). Boring logs are included in Appendix III-4.D. State well reports are included in Appendix III-4.E.

Water level measurements obtained in the ten conventional standpipe piezometer installations described above indicated groundwater was observed in four out of ten piezometers. In order to obtain additional groundwater data, Vibrating Wire Piezometers [VWPs] were installed in 24 locations. VWPs are further described in Section 6.2. Initially, 17 shallow VWPs were installed at locations correlating to the existing conventional standpipe piezometers [10 VWPs] and seven other locations of interest corresponding to existing borings. Subsequently, in order to observe deeper Unit III conditions, an additional seven deep VWPs were installed at locations corresponding to existing conventional standpipe piezometers, for a total of 24 VWPs installed during the investigation.

The number and depth of borings were included in the determination to meet the requirements of 30 TAC §330.63(e)(4)(A) and (B) for the Landfill, as described in the boring plan that was approved by the TCEQ (Appendix III-4.C). A summary of borings with elevations and coordinates is provided in Table III-4.5. The Elevation of Deepest Excavation (EDE) is 505 ft-msl. As listed, 22 borings were advanced to an elevation 30 feet below the EDE and 2 borings [9D and 43D] were advanced to an elevation 100 feet below the EDE, whereas the total depth of the remaining 23 borings were generally drilled to an elevation 5-10 feet below the EDE. The locations of all the Landfill borings are shown on Figure-4.9.

The borings were advanced using hollow stem augers and were either completed as piezometers to provide groundwater elevation data or were plugged in accordance with 16 TAC §76.702 and §76.1004. Soil samples were collected during auger advancement utilizing Shelby tubes, two-foot split spoons (also used to collect standard penetration tests for geotechnical purposes), or five-foot NX continuous split barrels.

The boring logs from the site investigations are attached as Appendix III-4.D. Laboratory data on soil samples obtained during the investigations are found in Appendix III-4.F and summarized in Part III, Attachment 5, Geotechnical/Stability Analysis.

5.2 SITE STRATIGRAPHY

Site stratigraphy is consistent with the regional geologic setting described in Section 3.1. Site stratigraphy is illustrated through a series of 6 cross-sections (A-A' to F-F'), as shown on Figure-4.10 through Figure-4.15. These cross-sections utilize the borings completed by SCS Engineers.

Various parts of this application use the terms "shale" and "clay". Shale is classified by geologists as a rock-like material consisting primarily of the mineral clay. In shallower [near-surface] stratigraphy, where the lithology is a softer, more plastic material, the term "clay" is used as the descriptor. In deeper sections, the clay lithifies (hardens) due to overburden pressures and transitions to a more rock-like, fissile material termed "shale". This change from overlying clay to underlying shale is often transitional.

The geology observed in the site exploration program consisted primarily of clay and shale, with minor amounts of larger grain sizes. Three stratigraphic units have been identified at the Landfill:

- Unit I consists of surficial clayey and loamy alluvium overlying silty or sandy clays with small subrounded gravel. The Unit I thickness ranged between 1.5 and 29 feet. The transition from Unit I to the underlying Unit II is transitional, and marked by increasing hardness and increasing fissility.
- Unit II, beneath Unit I, consists of weathered silty shale with varying calcareous content. Some publications use the term "marl" to describe calcareous shale. The Unit II silty shale has thin, interbedded limestone and sand/silt partings/lenses, calcite-filled joints, and marine shell fragment fossils. The top of Unit II was encountered at elevations ranging from approximately 503.3 feet-msl to 558.1 feet-msl. The thickness of Unit II ranged between 7 and 37.5 feet. The transition from Unit II to the underlying Unit III is marked by a color change caused by the downward limit of oxidation. Above the Unit II/Unit III line, the stratigraphy is generally more variable in color but are generally lighter-colored and have evidence of oxidation such as various rust- and yellow/brown colors. Below the Unit II/Unit III line, the stratigraphy is a homogenous very dark color, trending to black. Unit III also is less fissile than Unit II.
- Unit III, beneath Unit II, consists of unweathered dark gray to black calcareous shale bedrock with thin, interbedded limestone and sand/silt lenses, and marine shell fragment fossils. The top of Unit III was encountered at elevations ranging from approximately 492.0 feet-msl to 531.85 feet-msl. Landfill borings did not encounter the bottom of Unit III.

The bottom of the landfill excavation will be founded in Unit II or Unit III, depending on the location and depth of the cell excavation. Laboratory testing has been completed on samples of all three units, in accordance with the requirements of 30 TAC §330.63(e)(5). The geotechnical evaluation of Landfill materials and slope/waste stability is included in Part III, Attachment 5, Geotechnical/Stability Analysis. This design report presents the geotechnical summary and engineering evaluations and analyses. These analyses indicate that the soils at the Landfill are suitable for the intended purpose.

5.3 SOIL ENGINEERING PROPERTIES

Table III-4.6 summarizes the engineering properties of Unit II, based on the results from geotechnical investigations conducted by SCS Engineers. The test method utilized during the investigation is listed in the table. No piezometers were screened exclusively in Unit II. Hydraulic

SCS ENGINEERS Revision 0 4-5-2

conductivity values obtained during the investigation [see Section 6.3] by slug test represent values at the screened interval at the Unit II/Unit III interface.

Table III-4.7 summarizes the properties of Unit III, based on the results from geotechnical investigations conducted by SCS Engineers. The test method utilized during the investigation is listed in the table. Hydraulic conductivity results obtained during the investigation are based on slug test results performed on the piezometers screened in Unit III.

6 GROUNDWATER INVESTIGATION REPORT

6.1 STANDPIPE PIEZOMETERS

Subsurface soil borings have been drilled at the landfill for geological and hydrogeological characterization. Standpipe piezometers were installed in ten of these borings, as described in Section 5.1. A map of standpipe piezometer locations is provided in Figure-4.16. Piezometer completion information is tabulated in Table III-4.8. Stabilized water level data are tabulated in Table III-4.9. Six of ten existing standpipe piezometers did not have groundwater present. To provide additional data, vibrating wire piezometers were installed as further detailed below.

6.2 VIBRATING WIRE PIEZOMETERS

Vibrating wire piezometers (VWP) are pressure transducers that measure pore-water pressure. VWPs can detect pore-water pressure faster than conventional standpipe piezometers in low-permeability materials, because a newly installed standpipe piezometer may fill with water very slowly as it comes to equilibrium with groundwater. A newly installed VWP has a relatively much smaller cavity to fill with water, and therefore comes to equilibrium faster.

The VWP system consists of a pressure transducer, signal cable, and a readout device. It is installed as a dedicated instrument using a conventional drilling rig. After a borehole is drilled, the device is placed at the desired depth in filter media sand, and grouted from there to the ground surface.

After installation, pore-water enters the transducer through a filter and presses upon a diaphragm. This causes the diaphragm to deflect. This deflection is measured as a change in tension and frequency of vibration of the vibrating wire element. The square of the vibration frequency is directly proportional to the pressure applied to the diaphragm. The resulting pressure reading is a measure of water head pressure at that location. This water head pressure can be converted to a calculated groundwater elevation using device calibration information supplied for each device by the manufacturer. The Geokon 4500 VWP device was used for this investigation. The User Manual for the Geokon 4500 series and the calibration forms for each device are provided in Appendix III-4.G.

Seventeen VWP installations occurred in July 2019 through August 2019, two VWP installations occurred in October 2019, and five VWP installations occurred in December 2019; for a total of 24 VWP installations. Piezometer and VWP completion data are included in Appendix III-4.H and Appendix III-4.I, respectively. A summary of the VWP installations is provided in Table III-4.10. A map of VWP locations is provided in Figure-4.17.

6.2.1 Shallow VWPs

From July 2019 through August 2019, 17 VWPs were installed at various depths to provide a spatial distribution of these VWPs to characterize the weathered/unweathered shale formation. Results showed that 5 of 17 VWPs (VWP-1, VWP-3, VWP-18, VWP-30, and VWP-44) indicated the presence of water, resulting in calculated groundwater elevations shown in Table III-4.11. Therefore, the data indicate the remaining 13 VWPs and the six adjacent dry standpipe piezometers were completed above any saturated zone.

Revision 0 4-6-1 SCS ENGINEERS

Initial readings from VWP-20 indicated a small amount of water may have been carried down the borehole during drilling, but this dissipated to the in situ condition of no water indicated at this location.

6.2.2 Deep VWPs

In October 2019, to verify whether a continuous zone of saturation was located below existing dry standpipe piezometers and VWPs, two additional VWPs (VWP 41D and VWP 47D) were installed to a target elevation of 400 feet msl. Both VWPs indicated the presence of water, resulting in calculated groundwater elevations of 422 ft-msl (VWP-41D) and 416 ft-msl (VWP-47D) (see Table III-4.11). These data provide evidence of an existing continuous lower groundwater system.

To verify data from VWP-41D and VWP-47D, in December 2019, five additional deep VWPs (VWP-8D, VWP-9D, VWP-18D, VWP-33D, VWP-43D) were installed to the same target elevation of 400 feet msl. All five VWPs indicated the presence of water, resulting in calculated groundwater elevations ranging from approximately 408 feet to 518 feet (see Table III-4.11).

Due to shallow groundwater indicated by adjacent groundwater elevation readings of 519 feet at PZ-18 and 523 feet at VWP-18, casing was used during the installation of VWP-18D to eliminate infiltration from the upper groundwater system to the lower system within the borehole (Appendix III-4.I). Casing was set to an elevation of 461 feet. VWP-18D exhibits a stabilized calculated groundwater elevation of approximately 484 feet.

VWP-8D and VWP-9D both exhibited calculated groundwater elevations above the elevations of adjacent shallow VWPs (VWP-8 and VWP-9) and elevations of the bottom of screen elevation for adjacent standpipe piezometers (PZ-8 and PZ-9) at their corresponding locations. VWP-8 and VWP-9 transducers have zero water pressure, and PZ-8 and PZ-9 have both remained dry. The higher calculated groundwater elevations of VWP-8D and VWP-9D are attributed to being under elevated pore pressure not propagated to the elevations of the adjacent [higher] shallow VWPs and standpipe piezometers, due to the very low hydraulic conductivity and resulting slow travel/equilibration time. These observations indicate that shallower groundwater may occur in isolated pods.

6.3 **GROUNDWATER INVESTIGATION RESULTS**

Two groundwater zones were identified as a result of site field investigations, classified by elevation as "shallow" and "deep" zones that are not marked by significant changes in lithology. The shallow zone is considered unconfined and consists of isolated "pods" of saturation that are not always present everywhere at the site. The unconfined nature of this shallow saturation is due to the shallow occurrence and proximity to the ground surface. These zones of shallow saturation are discontinuous and do not appear to be connected to each other or to the deep zone. The deep zone is considered confined and is continuously saturated. The confined nature of this deep saturation zone is due to the depth, isolation from the atmosphere, and elevated pressure readings of some of the deep VWPs [see Section 6.2.2].

A comparison of precipitation records and water level data from newly installed piezometers in the east and west units of the Landfill is presented as Appendix III-4.J. Tabulated historic water level data, collected from piezometers from October 2018 to February 2020, are provided in Appendix III-4.K. Tabulated historic water level data, collected from VWPs from July 2019 to

February 2020, are provided in Appendix III-4.L. Using the deep VWP data, a potentiometric map of the groundwater flow system present on the Landfill was prepared and is included as Figure-4.18. The slug test results from the Landfill piezometers are provided in Appendix III-4.M.

Groundwater flow direction was determined using deep VWP data. The Landfill groundwater flows towards the south-southeast (Figure-4.18), consistent with local and regional topography. Shallow VWP and piezometer data were excluded from the flow direction interpretation because of the limited, disconnected nature of isolated pockets of groundwater at higher elevations.

6.3.1 Slug Testing

Slug testing was implemented in piezometers to determine hydraulic properties (Appendix III-4.M). The shale of lower Unit II and uppermost Unit III contains isolated pockets of groundwater. In limited locations, this is the uppermost water bearing unit below the landfill. The slug testing was conducted in piezometers with groundwater from the shallow zone, which is considered unconfined [see Section 6.3]. Seven of the ten piezometers installed were screened in the lower Unit II/upper Unit III zone. Slug tests were performed on PZ-1, PZ-3, PZ-18, and PZ-20 in the east and west areas to determine hydraulic conductivity. Results are summarized in Table III-4.12; Appendix III-4.M provides slug test data. A summary of hydraulic conductivity calculations is presented in Table III-4.12.

Slug tests performed at PZ-1 and PZ-18 used both the falling and rising head methods. The falling head method is implemented by introducing a "slug" into the water column, causing a temporary rise in head. The rising head method requires removing the "slug" from the water column, causing a temporary fall in head. The drop or rise in water level was then monitored with respect to time to determine hydraulic conductivity, using a logging pressure transducer. The results were analyzed using the Bouwer and Rice method.

An alternative falling head method was employed at PZ-3 and PZ-20 because the well screens were not fully submerged. Ten gallons of potable water were introduced into each well, such that the well screen was fully submerged. As the water level fell, a logging transducer recorded the falling head. The results were calculated using the Bouwer and Rice method.

6.3.2 Horizontal Flow Calculation

Horizontal travel velocities were estimated for the Unit II/III interface using the following formula:

 $V_a = (K*I)/(7.5*N)$ (Driscoll, 1986)

> V_a = actual travel velocity where:

> > K = hydraulic conductivity of the aquifer (geometric mean)

I = hydraulic gradient

N = effective porosity (5%) (Driscoll, 1986)

The hydraulic gradient was measured as the difference in water elevations between VWP-18D (483.9 feet-msl) and VWP-33D (408.1 feet-msl) divided by the distance between the two VWPs in feet (3,120 feet). Measurements were taken from the February 2020 potentiometric map (see Figure-4.18).

Horizontal travel times of the uppermost groundwater (Unit II/Unit III interface) were determined to represent (1) the overall Landfill area, (2) the overall Landfill area regarding Unit II, (3) the eastern area of the Landfill, and (4) the western area of the Landfill. An upper and lower bound predicted horizontal flow rate was also determined using the highest and lowest hydraulic conductivities recorded from SCS performed slug tests. Values used for horizontal flow calculations and horizontal flow rates are as shown in Table III-4.13.

The highest hydraulic conductivity value was recorded at PZ-3. The predicted upper horizontal flow rate from this location was 0.035 feet per year.

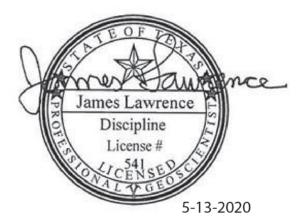
The lowest hydraulic conductivity value was recorded at PZ-18. The predicted lower horizontal flow rate from this location was 0.007 feet per year.

The horizontal travel time of the uppermost groundwater (Unit II/Unit III interface) across the entire Landfill area (PZ-1, PZ-3, PZ-18, PZ-20) was determined to be approximately 0.012 feet per year.

The horizontal travel time of the uppermost water across the Landfill area for Unit II (PZ-1, PZ-3, and PZ-20) was determined to be approximately 0.014 feet per year.

The horizontal travel time of the uppermost groundwater (lower Unit II/upper Unit III interface) in the eastern area of the Landfill (PZ-18, PZ-20) was approximately 0.009 feet per year.

The horizontal travel time of the uppermost groundwater (Unit II/Unit III interface) in the western area of the Landfill (PZ-1, PZ-3) was approximately 0.014 feet per year.



7 POLLUTANT PATHWAYS

Regionally, the groundwater generally flows in a southeast direction towards the Gulf of Mexico. Locally, the groundwater flows in a similar south to southeast direction. Excavation in the area of the Landfill will likely alter the groundwater flow path by creating a depression in the water table, and a resulting inward gradient. This may cause shallow groundwater in the eastern unit of the Landfill to flow west, and the western unit to flow east.

The sidewalls of the Landfill will be excavated partly in the weathered shale (Unit II), and partly in the underlying unweathered shale (Unit III). The base is generally in the unweathered shale. A potential release to the weathered shale zone would be expected to generally follow flow paths shown in Figure-4.18, moving downgradient to the south-southeast. Any potential leachate release in the unweathered shale is expected to also generally follow flow paths shown in Figure-4.18, moving down-gradient to the south-southeast. Potential leachate releases to the weathered zone or shallow unweathered zone (beneath the base of the Landfill) would be expected to move laterally and down-gradient. Potential releases are not expected to migrate downward into the lowerpermeability zones of the unweathered shale because this is a lower-permeability, higherresistance flow path. The predicted lateral flow of groundwater along bedding planes is due to horizontal hydraulic conductivity being generally greater than vertical hydraulic conductivity in flat lying sedimentary rocks, as hydraulic conductivity decreases with increasing depth (Heath, 1983; Harlow and Lecain, 1993). The Landfill groundwater monitoring system is designed to monitor the uppermost formation capable of yielding significant quantities of ground water (sufficient groundwater present in a well that can be sampled) encountered below the Landfill. Section 9.0 addresses the design of the proposed groundwater monitoring system.

The Facility will promptly notify, in writing, the Texas Commission on Environmental Quality (TCEQ), and any local pollution agency with jurisdiction that has requested to be notified, of future changes in facility construction or operation or changes in adjacent properties that affect, or are likely to affect, the direction and rate of groundwater flow and the potential for detecting groundwater contamination from a solid waste management unit.

7.1 LOCAL HYDROGEOLOGY

The Trinity Aquifer [see Section 4.1], which underlies the Landfill property, all of McLennan County, and the northwest corner of Limestone County, produces the majority of the total groundwater used in the area surrounding the Landfill (STGCD, 2015). In the Landfill area, Gulfian and Upper Comanche Series deposits (Table III-4.3) represent the upper most stratigraphy and are not considered hydrogeologic/aquifer type units due to their low permeability. The shallow stratigraphy in the Landfill vicinity does contain water, but is not considered a regional or local aquifer due to the inability to deliver enough usable water to a water supply well. The shallow clay/shale stratigraphy primarily transmit fluids via higher weathered zones with increased fissility/joints. The shallowest groundwater at the Landfill is at the base of Unit II. In the Landfill area, the deeper unweathered shale-marl stratigraphy of Unit III will act as an aquitard that inhibits vertical movement of groundwater due to decreased fissility and increased hardness, and resulting lower permeability.

8 GROUNDWATER QUALITY CHARACTERIZATION

This section presents information on the current groundwater monitoring program and groundwater quality data at the Landfill to address the groundwater quality findings in accordance with 30 TAC §330.63(f)(5) through (7). Details of the proposed groundwater monitoring program are discussed in Section 9.0 of this report.

8.1 OVERVIEW OF THE EXISTING GROUNDWATER MONITORING SYSTEM

This Landfill is a solid waste landfill. It has no existing groundwater monitoring system.

8.2 GROUNDWATER MONITORING DATA

Groundwater at the Landfill has not been sampled or analyzed. There are no existing monitoring wells at the Landfill.

8.3 REGIONAL GROUNDWATER QUALITY

Water quality varies throughout the Trinity Aquifer. Well records searched in the area of the Landfill show total dissolved solids (TDS) concentrations typically ranging from to 700-3,400 (mg/L). The majority of the wells in the vicinity of the Landfill are completed in the Hosston member of the Travis Peak Formation, which has a mean TDS concentration of 915 mg/l (Baker et al., 1990). The approximate altitude of water levels in the Trinity aquifer are listed in Table III-4.4.

The basal Walnut Clay of the Fredericksburg Group functions as the regional upper confining unit to the underlying Trinity Aquifer (Baker et al., 1990). The Walnut Clay is approximately 125 to 175 feet thick in the vicinity of the Landfill (Table III-4.3) (Baker et al., 1990 and Tetco, 1987). The base of the Walnut-i.e., the top of the Trinity Aquifer—is approximately 800 feet below the Landfill.

Revision 0 4-8-1 SCS ENGINEERS

9 GROUNDWATER MONITORING PLAN

9.1 EXISTING GROUNDWATER MONITORING SYSTEM

No groundwater monitoring wells currently exist at the Landfill.

9.2 PROPOSED GROUNDWATER MONITORING SYSTEM

The locations and depths of the monitoring wells are designed to determine the quality of groundwater passing the point of compliance and to detect groundwater impact from the waste units, and prior to any contaminants entering deeper portions of the stratigraphy interpreted as the Wolfe City Formation (30 TAC §330.403(a)(2)). The potential pathways for contaminant movement from the waste units are expected to be lateral [horizontal] via shale fractures that develop primarily horizontally as the overlying sediments unload over geologic time due to erosion.

Site drilling indicates that groundwater was generally not initially observed upon completion of a boring. Due to the sporadic distribution of site groundwater, two monitoring wells will be installed at each location, one with a specified shallow depth ("A" series) and the other with a specified deep depth ("B" series). Each well will be installed with a 40-foot monitoring well screen due to the sporadic distribution of groundwater. A map of the proposed groundwater monitoring system is provided in Figure-4.19.

Based on the groundwater conditions shown on Figure-4.18, the proposed monitoring system will consist of twelve upgradient wells and fifty-six downgradient wells (Figure-4.19).

Initial proposed monitoring well installations will begin at the eastern disposal area of the Landfill, where waste will first be disposed. The eastern side monitoring well names begin with the designation 'P1'; western side well names begin with 'P2'. The letter 'A' denotes a shallow well and the letter 'B' denotes a deep well. Fourteen proposed monitoring wells will be installed prior to landfill operation (P1-MW 1 A/B, P1-MW 2 A/B, P1-MW 16 A/B, P1-MW 17 A/B, P1-MW 18 A/B, P1-MW 19 A/B, P1-MW 20 A/B). The remaining proposed monitoring wells will be installed when waste is within 1,000 feet of the proposed monitoring well location. Installation details for proposed monitoring wells are described below and in Table III-4.14. The new monitoring wells will be sampled for background data for eight quarters in accordance with the Groundwater Sampling and Analysis Plan (GWSAP, see Attachment 7). Semiannual detection monitoring will then be implemented in accordance with GWSAP.

Monitoring wells will be constructed in accordance with the Proposed Monitoring Well Construction Details indicated in Figure-4.20, which is in conformance with requirements outlined within 30 TAC §330.421(a)(2). A qualified Texas-licensed driller will drill and install monitoring wells using equipment and methods that are appropriate for the Landfill conditions. A licensed professional geoscientist or engineer who is familiar with the geology of the area will supervise drilling, develop a detailed lithologic description of the boring, monitor well installation, and oversee well development (30 TAC §330.421(a)(1)(A)). The boring will be at least 4-inches larger than the outer diameter of the well casing and screen. If water is used in drilling, it will be from a potable source, and a current chemical analysis will be provided with the monitoring well installation report. A licensed professional geoscientist or engineer who is familiar with the

geology of the area will supervise or make a boring log for each monitoring well and shall seal, sign, and date the boring log.

After a monitoring well is installed, it will be developed until excessive turbidity due to drilling/installation has been removed and field measurements of pH, specific conductance, and temperature have stabilized in accordance with 30 TAC §330.421(c). Development may be accomplished through the use of pumping and/or bailing.

Upon completion of well installation activities, a registered professional surveyor will survey the locations with vertical measurements to the nearest 0.01-foot and referenced to mean sea level (with year of the sea-level datum shown). Survey points for each well will include the top of PVC casing (with referenced point marked), top of protective cap, and ground surface adjacent to the well pad. Horizontal locations will be determined to the nearest tenth of a second for latitude and longitude or accurately located relative to the Landfill grid system (30 TAC §330.421(d)).

Within 60 days of well completion, well installation and construction information will be submitted to the TCEQ on current forms. The report will include a detailed geologic log, any test results, a description of development procedures, and a site map (to scale) showing the location of all monitoring wells and the point of compliance (30 TAC §330.421(e)). Any monitoring well that is damaged to the extent that it is no longer suitable for sampling will be reported to the TCEQ with a recommendation to repair or replace the well (30 TAC §330.421(f)). Any monitoring well that is no longer used shall be properly abandoned and plugged in accordance with 16 TAC §76.702 and 76.1004 with prior authorization in writing from the TCEQ.

The wells will be operated and maintained so that they will yield representative groundwater samples for the appropriate hydrogeologic unit throughout the life of the groundwater monitoring program (30 TAC §330.421(a) and (e) and §330.403(d)). Groundwater monitoring will be conducted throughout the active life and the closure and post-closure care period of the Landfill.

9.3 GROUNDWATER MONITORING SYSTEM CERTIFICATION

I, James Lawrence, Texas P.G. #541, have reviewed the groundwater monitoring well system installation plan for the Landfill. In my professional opinion, the proposed groundwater monitoring system has been designed in accordance with 30 TAC §330.63(f) and §330.401(e).

James Lawrence
Discipline
License #

5-13-2020

Signature of Qualified Groundwater Scientist

Seal

GROUNDWATER SAMPLING AND ANALYSIS REQUIREMENTS 10

In accordance with 30 TAC §330.63(f) and 330.405, a Groundwater Sampling and Analysis Plan (GWSAP) was developed, which describes sampling and analysis procedures that are designed to ensure monitoring results provide an accurate representation of groundwater quality at the background and point of compliance monitoring wells. This plan is included in Attachment 7.

SCS ENGINEERS 4-10-1 Revision 0 May 2020

11 SUMMARY

This report, prepared in accordance with 30 Texas Administrative Code (TAC) §330.63(e), summarizes available data from site investigations and previous reports related to regional and local geology and aquifers in the area, the occurrence and distribution of groundwater in the area of the Landfill, and establishes a groundwater monitoring system design.

The Landfill is underlain by bedrock material of the Cretaceous Taylor Group (Wolfe City Formation) consisting primarily of calcareous clay/shale, with minor amounts of sand and silt, as well as near-surface Tertiary/Quaternary sands, gravels, silts, and clay sediments deposited near and along stream channels (U.S. Department of Agriculture, *Soil Survey of McLennan County*, 1992; U.S. Department of Agriculture, *Soil Survey of Limestone County*, 1991). After the subsurface investigation, strata at the Landfill were divided into three units (Unit I, Unit II, Unit III). Unit I consists of surficial alluvial silts overlying silty or sandy clays with small subrounded gravel. Unit II consists of weathered calcareous shale with calcareous silty clay and thin, interbedded limestone and sand/silt lenses, calcite filling joints, and fossils. Unit III consists of unweathered gray calcareous shale with thin, interbedded limestone, sand/silt lenses, and fossils. The Landfill will be excavated into Units I, II, and III, which will provide a stable foundation. The low permeability of this stratigraphy provides additional containment beyond that provided by the engineered liner system. The uppermost water-bearing unit at the Landfill is the Unit II/III shale, which is confined with depth by the unweathered, lower permeability material.

Based on a review of this data, and on the results of geotechnical investigations conducted at the Landfill, the Landfill is suitable for use as a Type I MSW landfill.

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Revision 0 4-12-1 SCS ENGINEERS

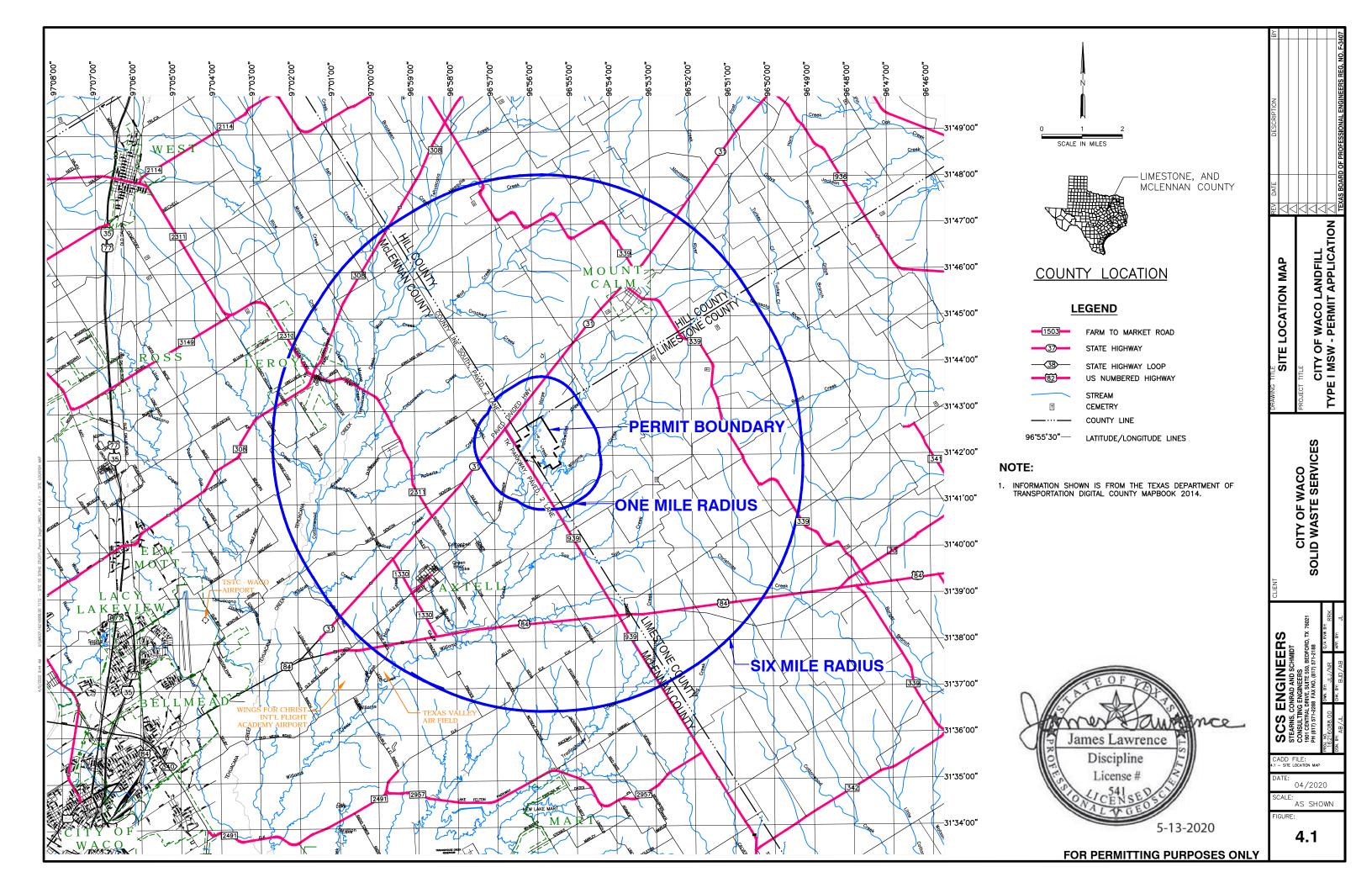
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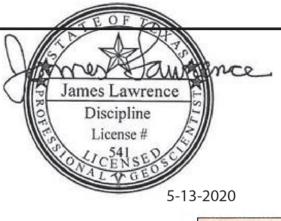
Revision 0 4-12-2 SCS ENGINEERS

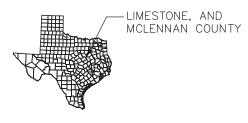
FIGURES

- Figure 4.1 Site Location Map
- Physiographic Map of Texas Figure - 4.2
- General Topographic Map • Figure - 4.3
- Figure 4.4 Geologic Map
- Figure 4.5 Structural Cross Sections of Regional Geology and the Trinity Aquifer
- Figure 4.6 Seismic Impact Zone Map
- Figure 4.7 Tectonic Map of Texas
- Figure 4.8 Trinity Aquifer
- Figure 4.9 **Boring Location Map**
- Figure 4.10 Geologic Cross Section A-A'
- Figure 4.11 Geologic Cross Section B-B'
- Figure 4.12 Geologic Cross Section C-C'
- Figure 4.13 Geologic Cross Section D-D'
- Figure 4.14 Geologic Cross Section E-E'
- Figure 4.15 Geologic Cross Section F-F'
- Figure 4.16 Piezometer Location Map
- Figure 4.17 VWP Location Map
- Figure 4.18 Potentiometric Map
- Figure 4.19 Proposed GWM System Map
- Figure 4.20 Typical Monitoring Well Detail

SCS ENGINEERS Revision 0 May 2020







COUNTY LOCATION



PROVINCE	MAX. ELEV. (ft)	MIN. ELEV. (ft)	TOPOGRAPHY	GEOLOGIC STRUCTURE	BEDROCK TYPES
Gulf Coastal Plains					
Coastal Prairies	300	0	Nearly flat prairie, <1 ft/mi to Gulf	Nearly flat strata	Deltaic sands and muds
Interior Coastal Plains	800	300	Parallel ridges (questas) and valleys	Beds tilted toward Gulf	Unconsolidated sands and muds
Blackland Promis	1000	450	Low rolling terrain	Beds tilted south and east	Chalks and marls
Grand Franks	1250	450	Low stairstep hills west; plains east	Strata dip east	Calcareous east; sandy west
	3000	450	Flat upper surface with box canyons	Beds dip south; normal faulted	Limestones and dolomites
Finis Catyons	2000	1200	Steep-walled canyons		Limestones and dolomites
	4200	1700	Mesa-formed terrain; highs to west	Unfaulted, near-horizontal beds	Carbonates and alluvial sediments
Control Towns Uplift	2000	800	Knobby plain; surrounded by questas	Centripetal dips, strongly faulted	Granites; metamorphics; sediments
North Contral Plants	3000	900	Low north-south ridges (questas)	West dip; minor faults	Limestones, sandstones, shales
High Plains					
Central	4750	2900	Flat prairies slope east and south	Slight dips east and south	Eolian silts and fine sands
Canadian Breaks	3800	2350	Highly dissected; local solution valleys		
Southern	3800	2200	Flat; many playas; local dune fields		
Epeln and Fange	8750	1700	North-south mountains and basins	Some complex folding and faulting	Igneous; metamorphics; sediments

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TEXAS BOARD OF PROFESSIONAL ENGINEERS REG. NO. F-3407

TYPE I MSW - PERMIT APPLICATION

CITY OF WACO LANDFILL

CITY OF WACO SOLID WASTE SERVICES

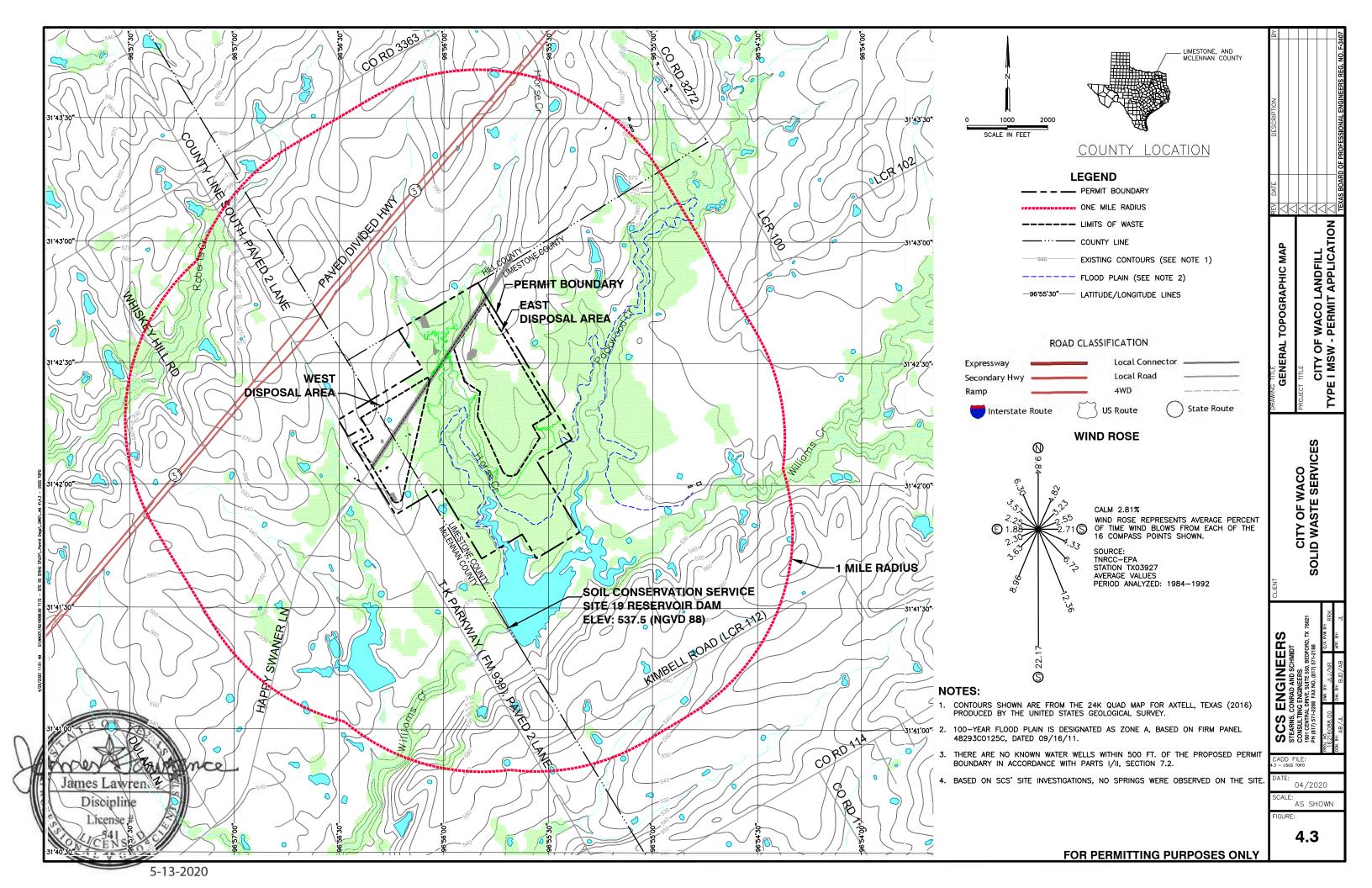
PHYSIOGRAPHIC MAP OF TEXAS

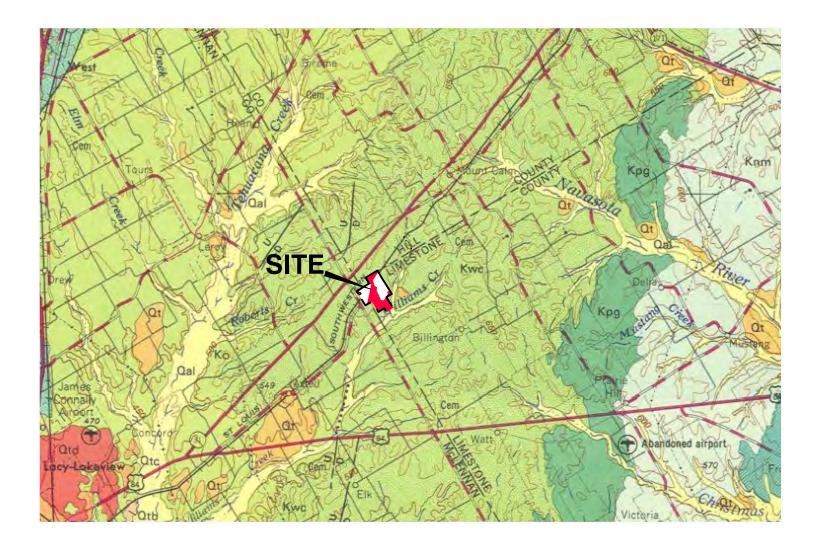
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4.2 - PHYSIOGRAPHIC MAP OF TEXAS

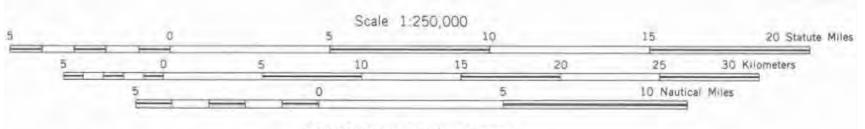
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4.2







CONTOUR INTERVAL 50 FEET

TRANSVERSE MERCATOR PROJECTION

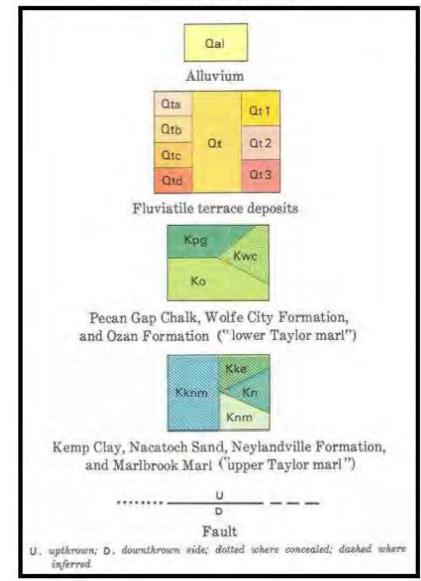
1980 MAGNETIC DECLINATION FOR THIS SHEET VARIES FROM 9°30' EASTERLY FOR THE CENTER OF THE WEST EDGE TO 8°30' EASTERLY FOR THE CENTER OF THE EAST EDGE, MEAN ANNUAL CHANGE IS 0°02' WESTERLY.

GEOLOGIC ATLAS OF TEXAS, WACO SHEET

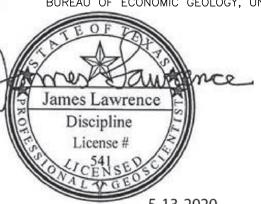
LLOYD WILLIAM STEPHENSON MEMORIAL EDITION

REPRINTED 1979

EXPLANATION



BUREAU OF ECONOMIC GEOLOGY, UNIVERSITY OF TEXAS AT AUSTIN.



CITY OF WACO LANDFILL
TYPE I MSW - PERMIT APPLICATION

CITY OF WACO SOLID WASTE SERVICES

GEOLOGIC MAP

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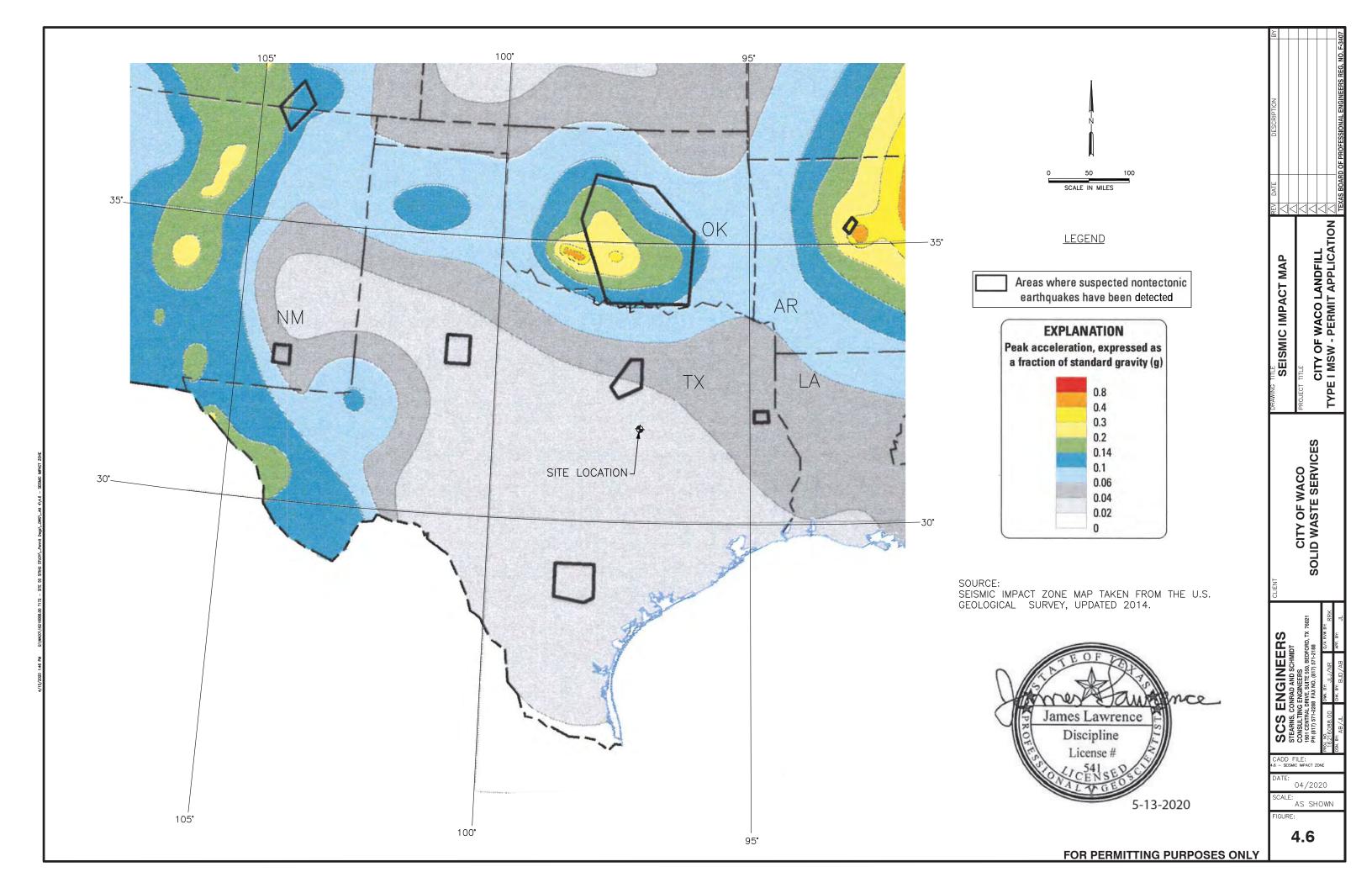
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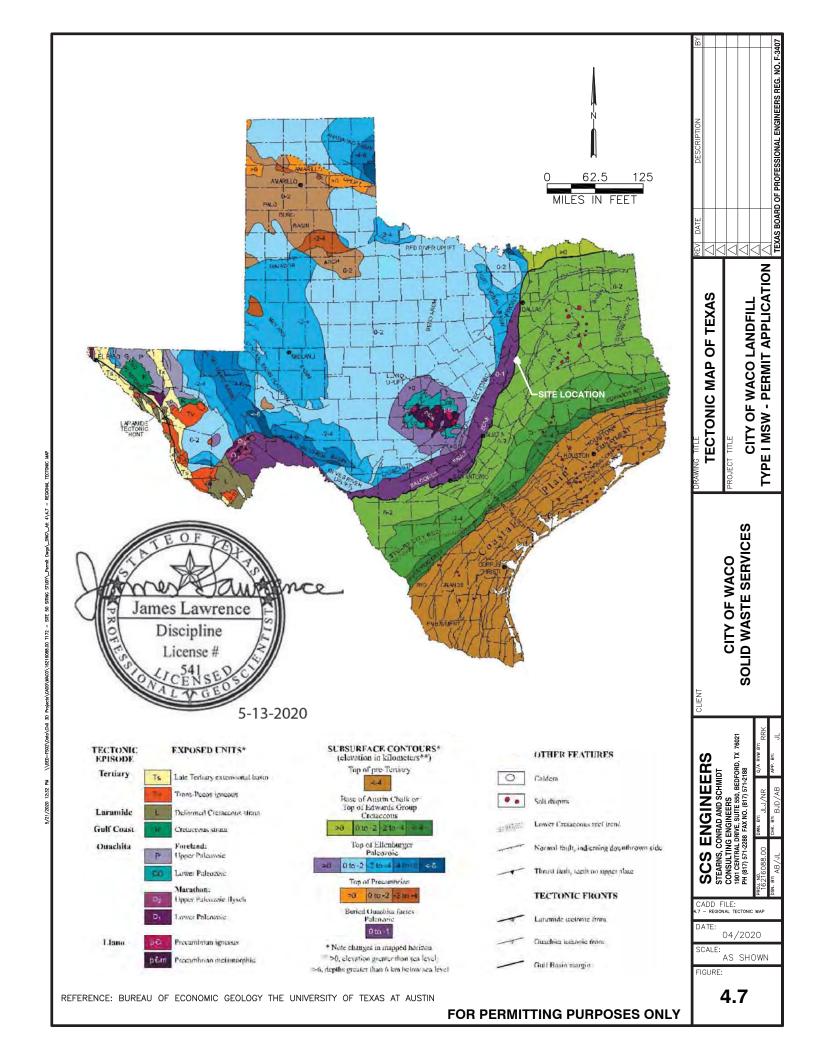
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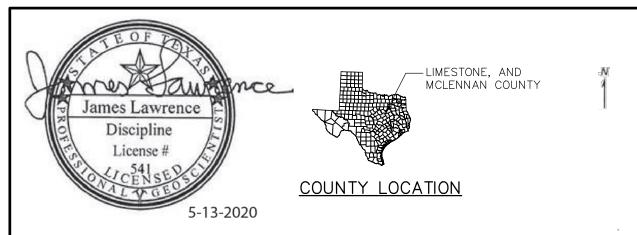
FOR PERMITTING PURPOSES ONLY

Structural Cross Sections of the Trinity Aquifer 1,500 1,000 500 Younger formations Sea level -1,000 **TYPE I MSW - PERMIT APPLICATION** STRUCTURAL CROSS SECTIONS OF -1,500CITY OF WACO LANDFILL -2,000-2,500-3,000 COUNTY LOCATION; LIMESTONE, AND MCLENNAN COUNTY SITE **LOCATION** 2,000 1,600 Washita and Paluxy Formation Fredericksburg groups 1,200 Woodbine Group 800 SOLID WASTE SERVICES Younger formations CITY OF WACO Travis Peak / Twin Pearsall Member Mountains Formation 400 Hosston Member -800 -1,200 & Balcones Fault Zone 1,600 Hensell Member Cow Creek Member -2,000 Travis Peak / Twin nmett Member Sligo Member Mountains Formation -2,400-2,800 -3.200-3,600 CONRAD AND SCHMIDT ING ENGINEERS AL DRIVE, SUITE 550, BEDFORD, TX 76021 -2288 FAX NO. (817) 571-2188 Structural cross sections across the northern Trinity Aquifer, shown in shades of green (image **ENGINEERS** modified from Klemt, et al., 1975; Nordstrome, 1982). SCS James Lawrence Discipline 04/2020 Source: AS SHOWN George, Peter G., Robert E. Mace, Rima Petrossian, 2011, Aquife 5-13-2020 Board Report 380. Pg. 69. 4.5

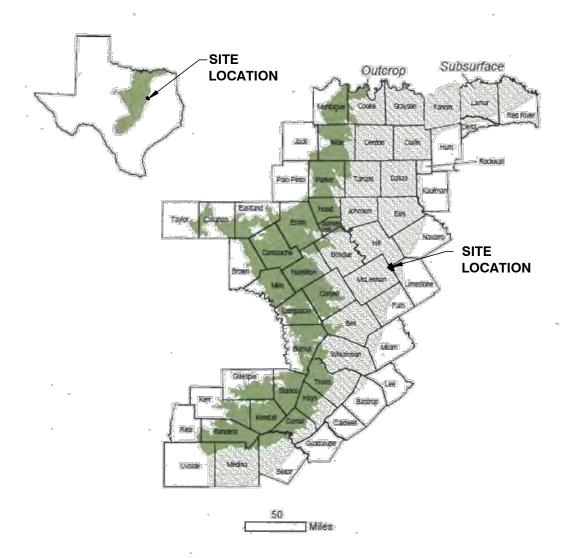
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Trinity Aquifer



Map showing the spatial distribution of the northern Trinity Aquifer, as depicted in shades of green The proposed Site is located at and near the northwest corner of Limestone County and parts of eastern McLennan County.

Source:

George, Peter G., Robert E. Mace, Rima Petrossian, 2011, Aquifers of Texas: Texas Water Development Board Report 380. Pg. 67.

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	CLIENT	DRAWING TITLE	REV DATE	DESCRIPTI
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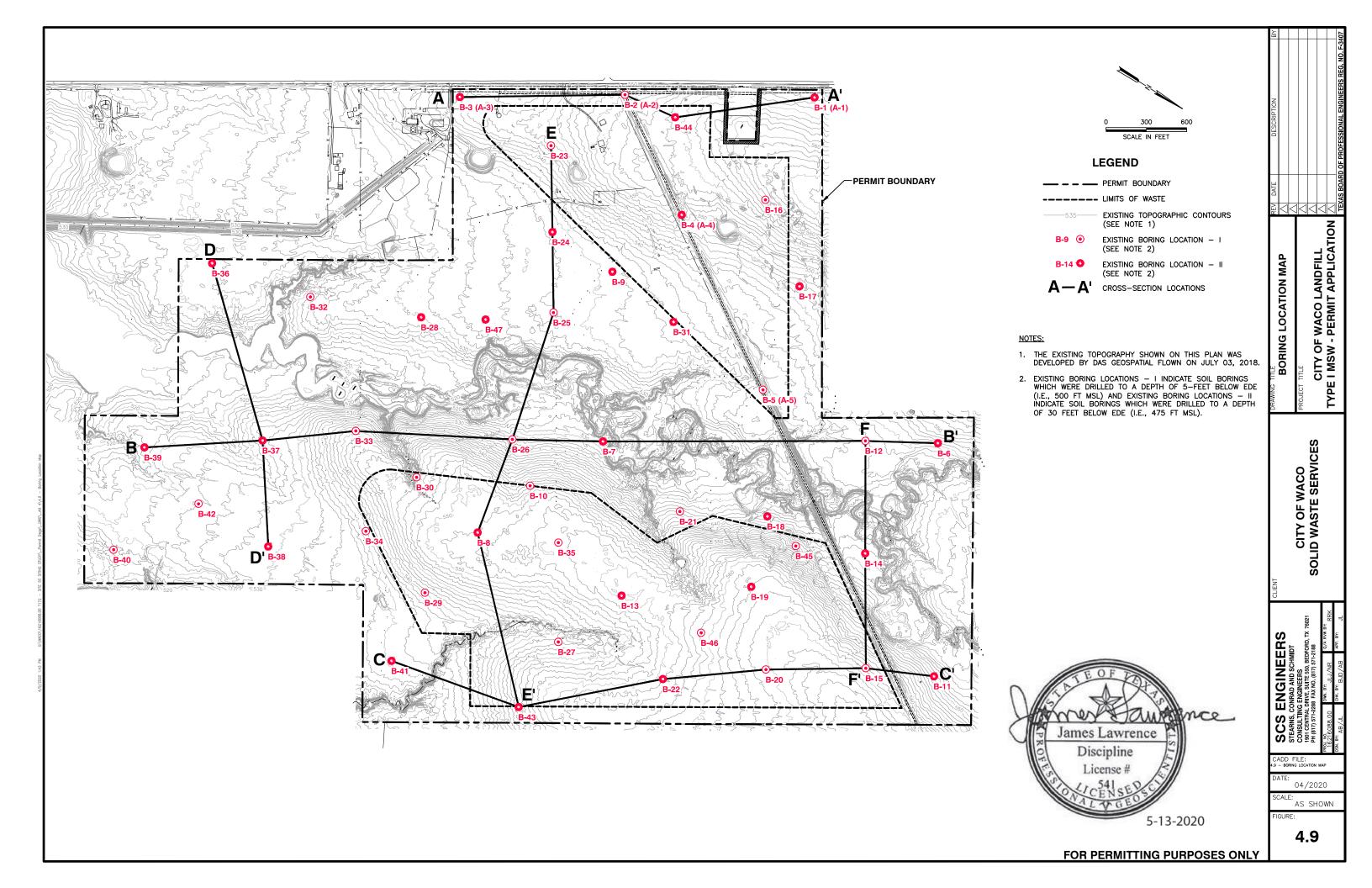
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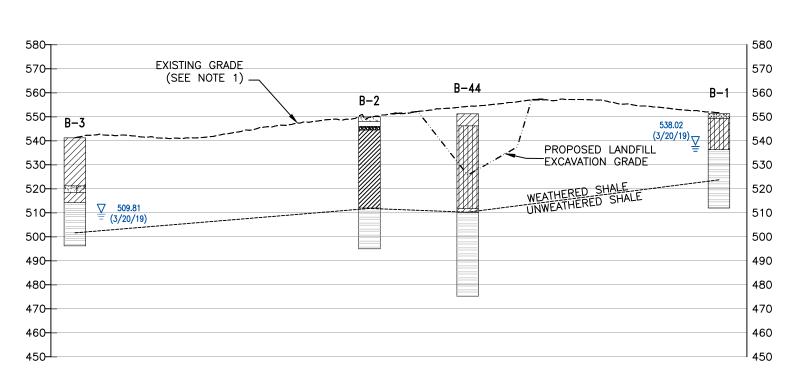
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04/2020

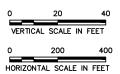
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FIGURE:

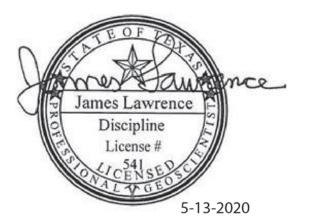
4.8







CROSS SECTION A-A'



LEGEND:

EXISTING GRADE (SEE NOTE 1) WEATHERED/UNWEATHERED SHALE TRANSITIONAL CONTACT PROPOSED LANDFILL EXCAVATION GRADE

538.02 ∑ $(3/20/19)^{-1}$

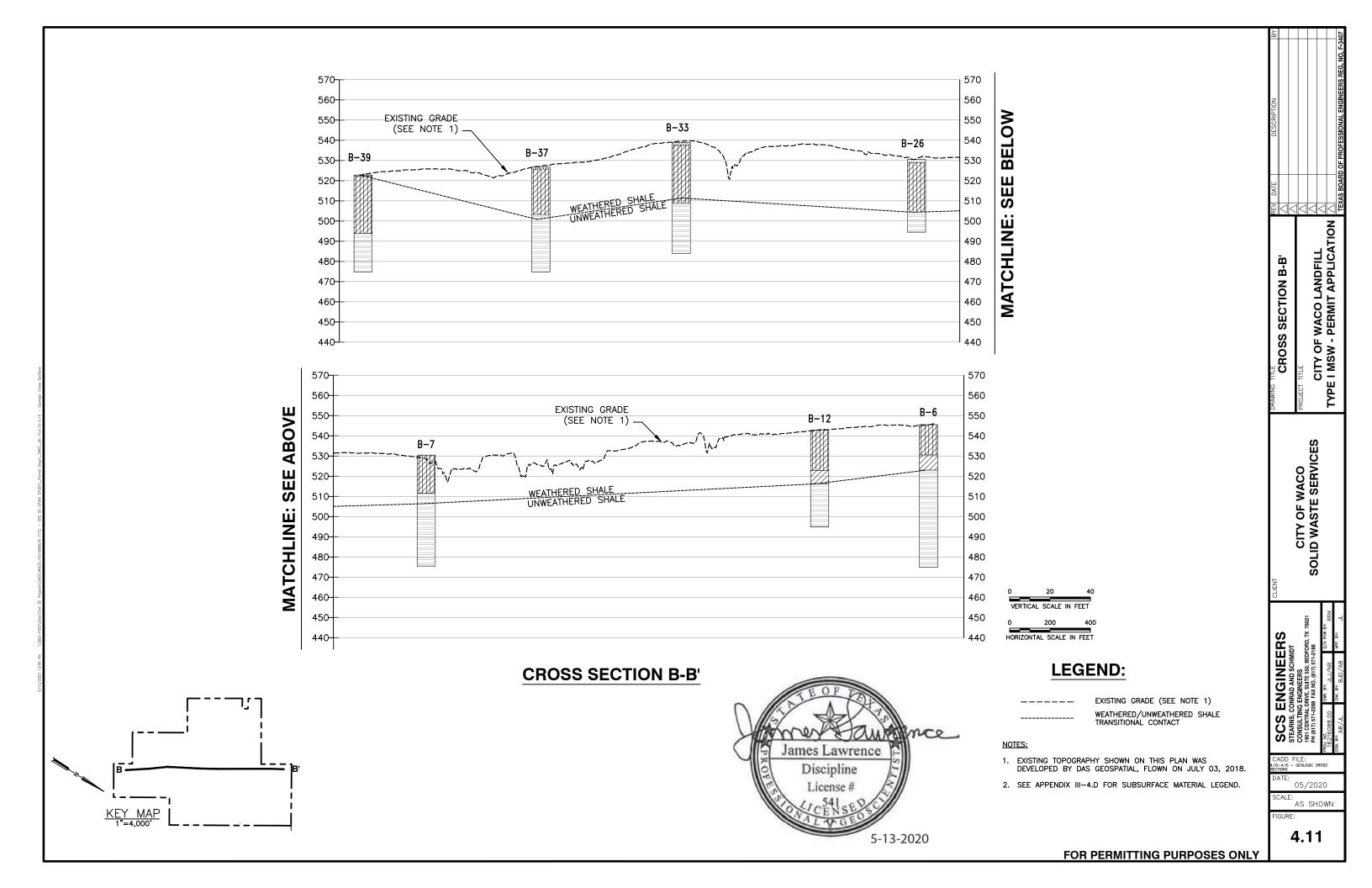
WATER LEVEL IN PIEZOMETER (DATE OF WATER LEVEL READING)

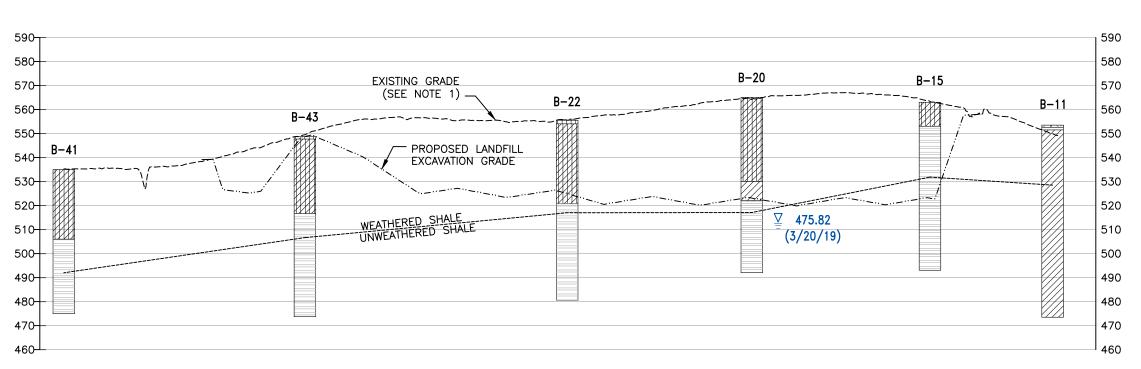
- 1. EXISTING TOPOGRAPHY SHOWN ON THIS PLAN WAS DEVELOPED BY DAS GEOSPATIAL, FLOWN ON JULY 03, 2018.
- 2. SEE APPENDIX III-4.D FOR SUBSURFACE MATERIAL LEGEND.

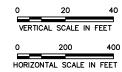
CITY OF WACO LANDFILL TYPE I MSW - PERMIT APPLICATION CITY OF WACO SOLID WASTE SERVICES SCS ENGINEERS STEARNS, CONRAD AND SCHMIDT CADD FILE: .10-4.15 - GEOLOGIC CROSS 05/2020 AS SHOWN 4.10

CROSS SECTION A-A'

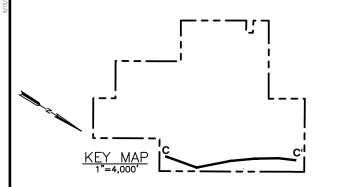
FOR PERMITTING PURPOSES ONLY







CROSS SECTION C-C'





LEGEND:

EXISTING GRADE (SEE NOTE 1) WEATHERED/UNWEATHERED SHALE TRANSITIONAL CONTACT PROPOSED LANDFILL EXCAVATION GRADE **475.82** <u>▽</u> WATER LEVEL IN PIEZOMETER $(3/20/19)^{-1}$ (DATE OF WATER LEVEL READING)

- 1. EXISTING TOPOGRAPHY SHOWN ON THIS PLAN WAS DEVELOPED BY DAS GEOSPATIAL, FLOWN ON JULY 03, 2018.
- 2. SEE APPENDIX III-4.D FOR SUBSURFACE MATERIAL LEGEND.

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ENGINEERS CONRAD AND SCHMIDT

05/2020

AS SHOWN

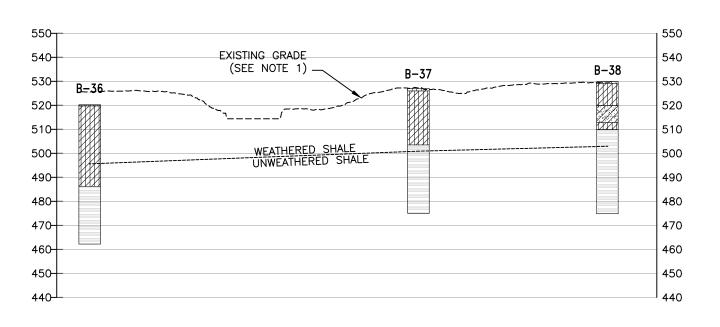
CITY OF WACO LANDFILL TYPE I MSW - PERMIT APPLICATION

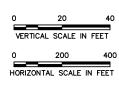
CITY OF WACO SOLID WASTE SERVICES

CROSS SECTION C-C'

4.12

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CROSS SECTION D-D'

LEGEND:

---- EXISTING GRADE (SEE NOTE 1)
----- WEATHERED/UNWEATHERED SHALE TRANSITIONAL CONTACT



NOTES

- EXISTING TOPOGRAPHY SHOWN ON THIS PLAN WAS DEVELOPED BY DAS GEOSPATIAL, FLOWN ON JULY 03, 2018.
- 2. SEE APPENDIX III-4.D FOR SUBSURFACE MATERIAL LEGEND.

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CITY OF WACO LANDFILL TYPE I MSW - PERMIT APPLICATION

CITY OF WACO SOLID WASTE SERVICES

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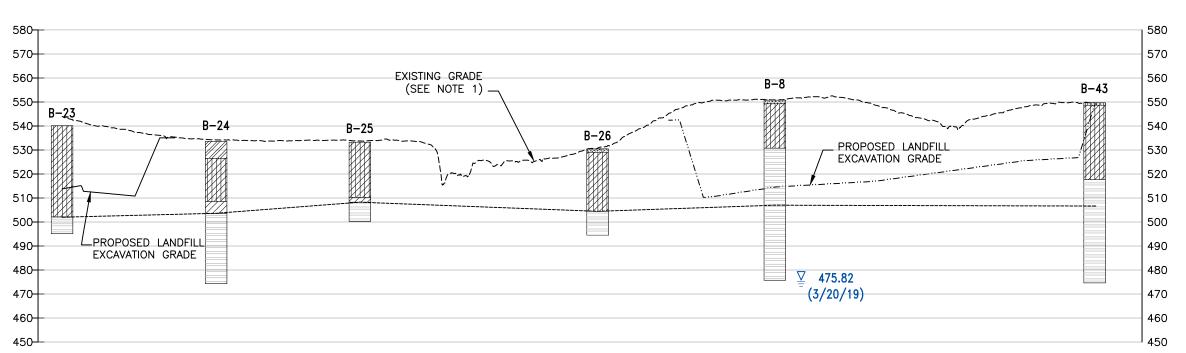
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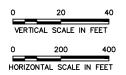
05/2020 SCALE: AS SHOWN

CROSS SECTION D-D'

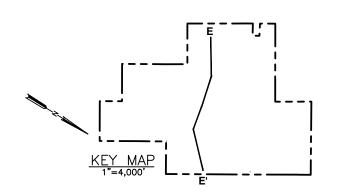
FOR PERMITTING PURPOSES ONLY

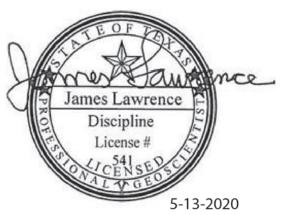
MASS-1-000/21/6 PM APP 1"=4,0000'





CROSS SECTION E-E'





LEGEND:

EXISTING GRADE (SEE NOTE 1)

WEATHERED/UNWEATHERED SHALE
TRANSITIONAL CONTACT
PROPOSED LANDFILL EXCAVATION GRADE

475.82
WATER LEVEL IN PIEZOMETER
(3/20/19) (DATE OF WATER LEVEL READING)

NOTES:

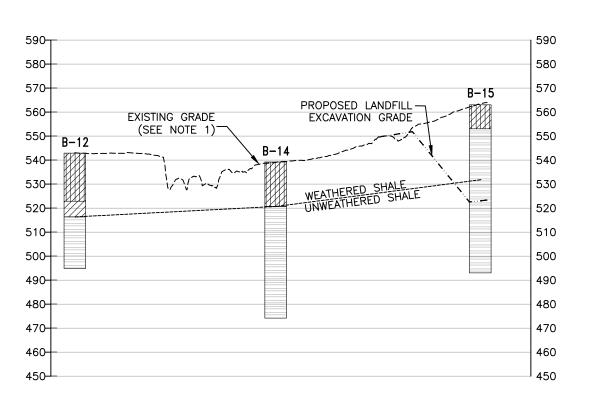
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- 2. SEE APPENDIX III-4.D FOR SUBSURFACE MATERIAL LEGEND.

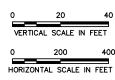
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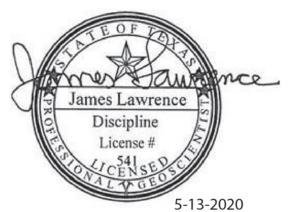
CROSS SECTION E-E'

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CROSS SECTION F-F'



LEGEND:

EXISTING GRADE (SEE NOTE 1) WEATHERED/UNWEATHERED SHALE TRANSITIONAL CONTACT PROPOSED LANDFILL EXCAVATION GRADE

- 1. EXISTING TOPOGRAPHY SHOWN ON THIS PLAN WAS DEVELOPED BY DAS GEOSPATIAL, FLOWN ON JULY 03, 2018.
- 2. SEE APPENDIX III-4.D FOR SUBSURFACE MATERIAL LEGEND.

SCS ENGINEERS
STEARNS, CONRAD AND SCHMIDT

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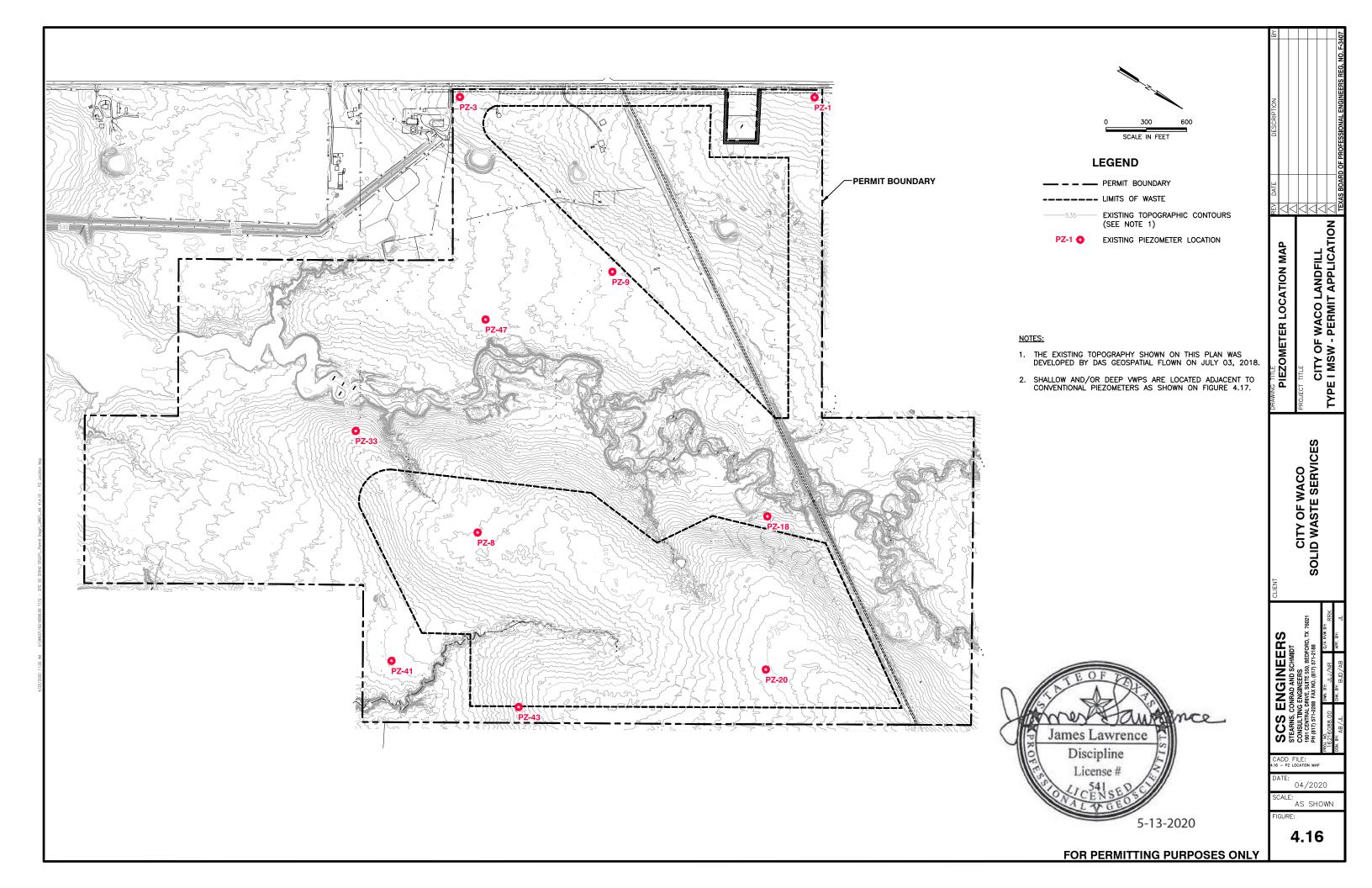
05/2020 AS SHOWN

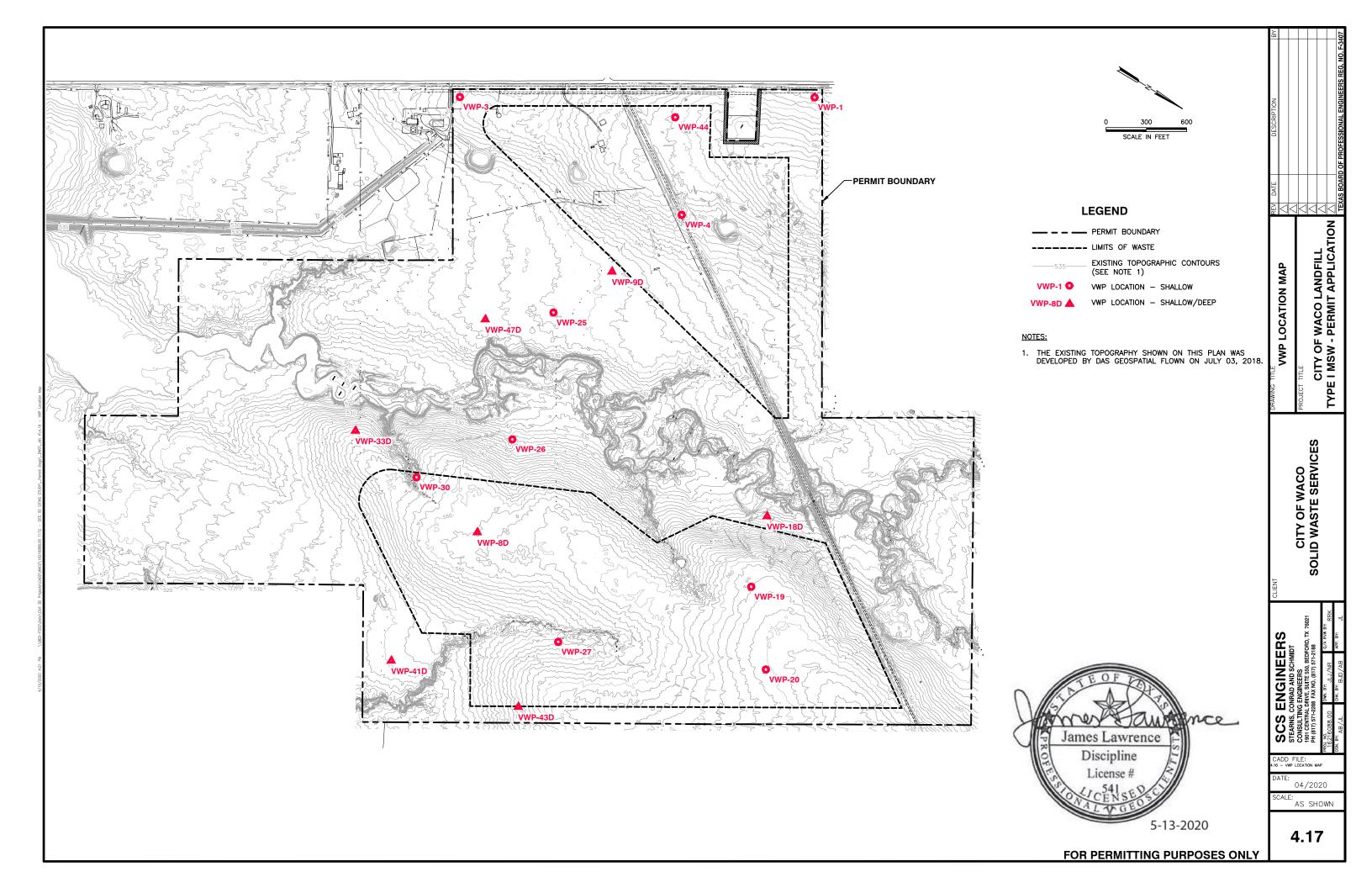
CITY OF WACO LANDFILL TYPE I MSW - PERMIT APPLICATION

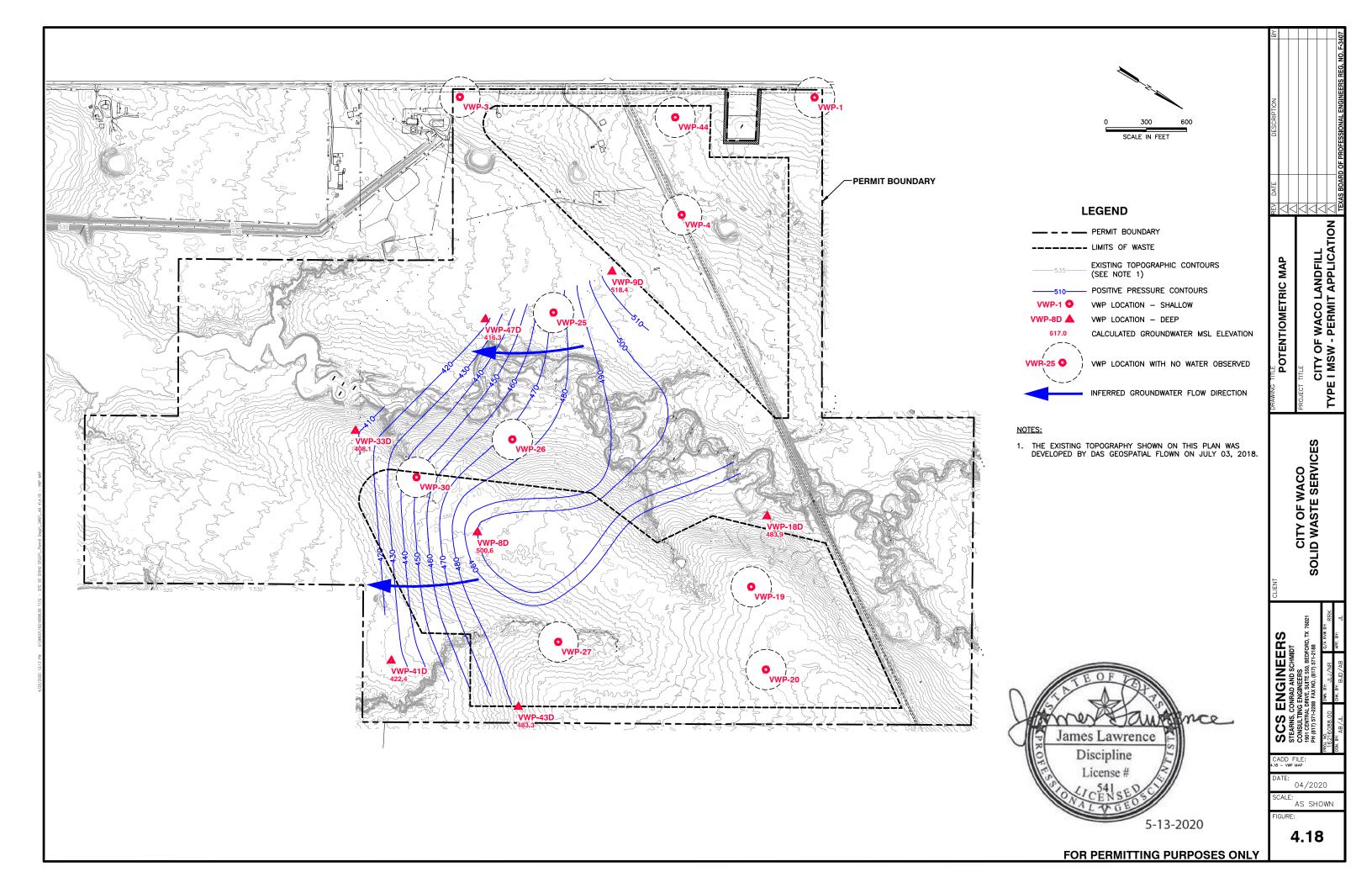
CITY OF WACO SOLID WASTE SERVICES

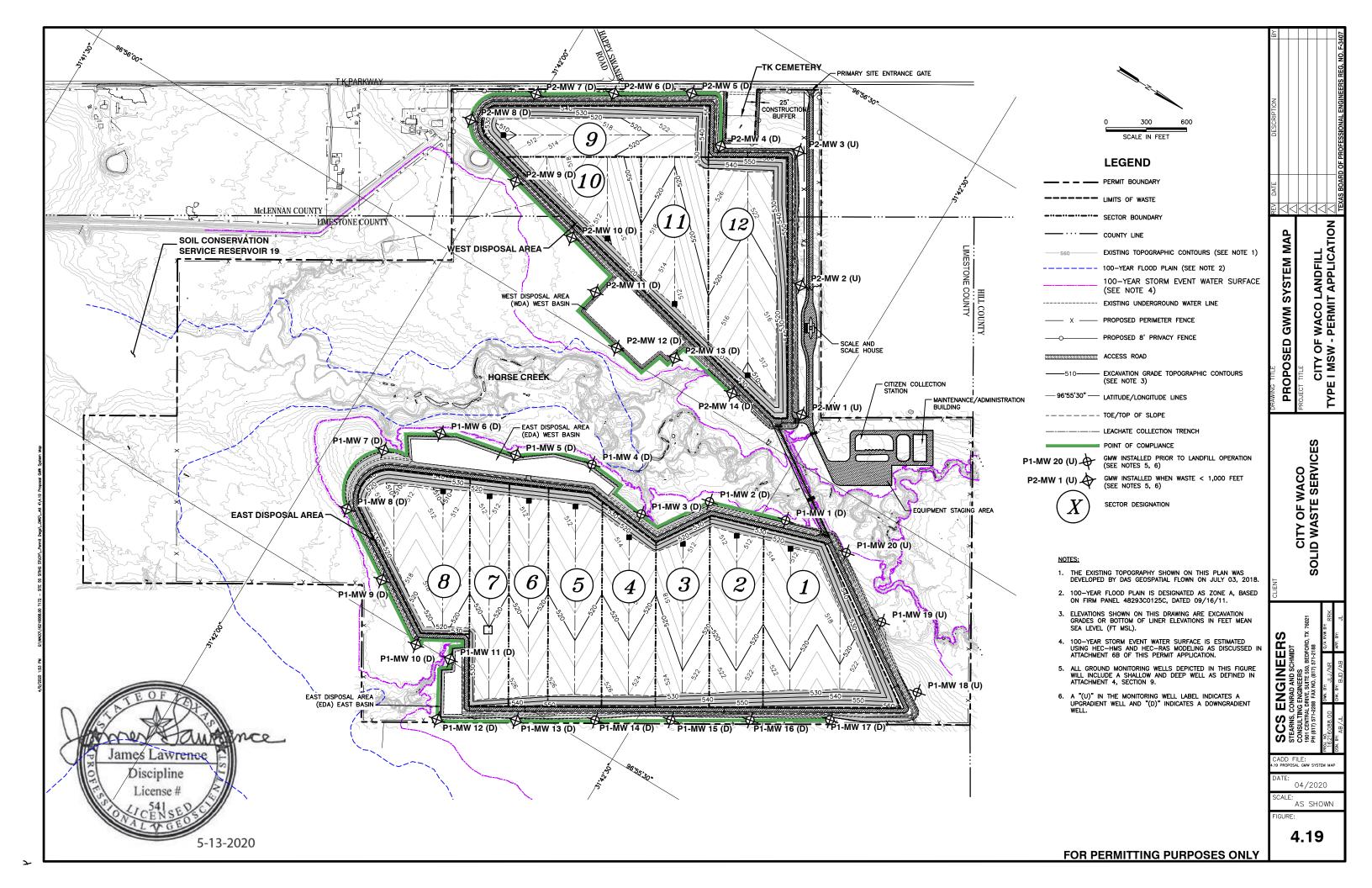
CROSS SECTION F-F

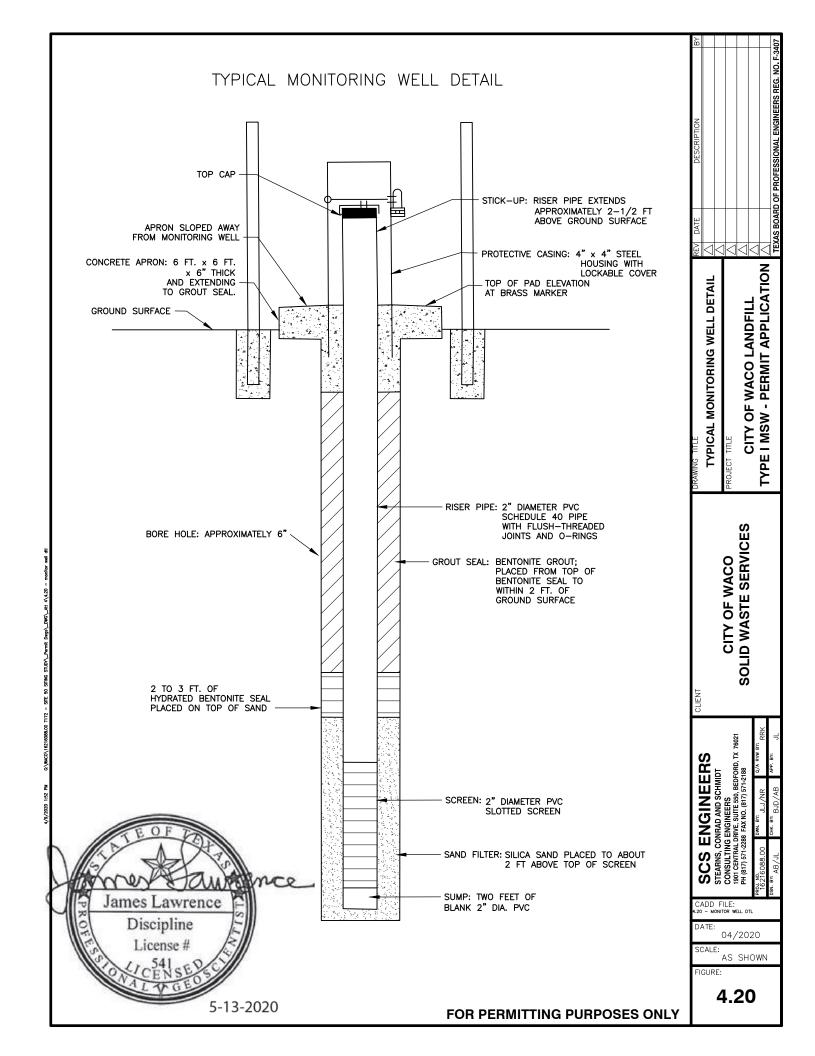
4.15 FOR PERMITTING PURPOSES ONLY











TABLES

- Table III-4.1 Regional Physiography
- Table III-4.2 Waco Average Monthly Rainfall
- Table III-4.3 Geologic Units and their Water-Bearing Properties
- Table III-4.4 Recorded Wells within 1 Mile
- Table III-4.5 Coordinates and Elevations of Borings
- Table III-4.6 Properties of Unit II
- Table III-4.7 Properties of Unit III
- Table III-4.8 Existing Piezometer Completion Data
- Table III-4.9 Summary Initial and Static Water Level Data
- Table III-4.10 Vibrating Wire Piezometer Completion Data
- Table III-4.11 Vibrating Wire Piezometer Inferred Groundwater Elevation Data
- Table III-4.12 Summary of Aquifer (Slug) Tests Performed by SCS Engineers
- Table III-4.13 Summary of Horizontal Flow Rate Calculation Data
- Table III-4.14 Proposed Monitoring Well Information

Table III-4.1 Regional Physiography

Body of Water	Approximate Distance from the Landfill Property	Direction from the Landfill
Horse Creek	0 ft	Within, North to South
Unnamed Lake (soil conservation service site 19 reservoir)	O+ ft	Within, South
Packwood Creek	400 ft	East
Williams Creek	1,700 ft	South

7 6 Precipitation, Inches 5 4.29 3.43 3.15 3.07 3 2.83 2.68 2.64 2.13 2.05 2 1 0 JAN **FEB** MAR APR MAY JUN JUL AUG SEP OCT NOV DEC Monthly Precipitation (Averaged over 29 Years)

Table III-4.2 Waco Average Monthly Rainfall

(Averaged between 1981 and 2010 at the Waco-Mcgregor Municipal Airport; source: www.usclimate.com).

Table III-4.3 Geologic Units and their Water-Bearing Properties (Modified From Baker et al., 1990; Tetco, 1987)

System	Series	Group	Formation	Hydrogeologic Unit	Approximate Thickness in Site Vicinity (ft)
		Taylor	Pecan Gap Chalk	Not a named hydrogeologic unit	0
		Site ->	Wolfe City Formation	"	300
	Gulfian		Ozan Formation	"	500-775
	Guirian	Austin	Austin Chalk	"	30
			South Bosque Shale	"	120
		Eagle Ford	Lake Waco Formation	"	75
		Woodbine	Pepper shale	"	60
			Del Rio Clay	"	70-90
			Georgetown Formation and Main Street Limestone	"	25-35
	Unnor		Pawpaw Formation and Weno Limestone	"	16-55
Cretaceous	Upper Comanche Series	Washita	Denton Clay, Fort Worth Limestone, and Duck Creek Limestone	"	53-76
Cretaceous			Edwards Limestone and Kiamichi Clay Comanche Peak	"	20-77
		Fredericksburg	Limestone	"	50-100
			Walnut Clay	"	125-175
			Paluxy Sand	Upper Trinity Aquifer	<71
			Glen Rose Formation	Middle Trinity Aquifer	200-375
			Travis PeakJHensell Sand Member	Middle Trinity Aquifer	175
	Lower Comanche		Travis Peak/Pearsall Member	Middle Trinity Aquifer	85
	Series		Travis Peak/Cow Creek Member	Middle Trinity Aquifer	130
		Trinity	Travis Peak/Hammet Shale Member	Middle Trinity Aquifer	140
			Travis Peak/Sligo and Hosston Member	Lower Trinity Aquifer	1,680

Table III-4.4 Recorded Wells Within 1 Mile of the Landfill and Beyond

Aquifer*	Well Number - Grid	Use	Owner	Well Depth (ft BGS)	Altitude of Land Surface (ft MSL)	Date	Depth to Water (ft BGS)	Water Level Elev (ft MSL)		
	Wells within the one-mile radius									
N/A	3917201 39-17-2	Unused (Oil or Gas)	S.H. Riggs	2030	560 (from topo)	1951	N/A	N/A		
N/A	3917601 39-17-6	Unused (Oil or Gas)	Ralph Spence, Bill Hughes (Paul Collins No.	3187	531 (from topo)	1961	N/A	N/A		
		Clo	sest water wells	beyond the or	ne-mile radius					
N/A (3.7 mi NW)	299719 39-17-1	Closed- Loop Geothermal	New Residence	300 (of clay)	510 (from topo)	9/21/12	N/A	N/A		
Trinity- Hosston (5.3 mi NW)	4024301 40-24-3	Public Supply	Leroy-Tours- Gerald WSC Well #1	2863	495	1958	52-435	443-60		
Trinity- Travis Peak (5.1 mi NW)	4024302 40-24-3	Industrial	#2	2312	492					
Trinity- Hosston (6.9 mi NW)	4024201 40-20-2	Public Supply	Leroy-Tours- Gerald WSC Whiskey Hollow	2620	522	7/1980	132	390		
Trinity- Hosston (6.9 mi NW)	4024201 40-24-2	Public Supply	Leroy-Tours- Gerald WSC #2	2670	522	7/1980	132	390		
Trinity (3.6 mi SW)	3917701 39-17-7	Public Supply	Axtell WSC Well #1	3129	529	1959	9.67	519.33		
Trinity- Hosston (5.8 mi SW)	3917702 39-17-7	Public Supply	Moore Water System	3250	457	7/16/83	390	67		
Trinity (6.4 mi SW)	277481 40-32-3	Irrigation	Stuart Parsons	3001	451 (from topo)	11/22/11	499	-48		
Trinity- Hosston	3925201 39-25-2	Public Supply	Elk-Oaklake WSC	3148	517	6/9/80	399-863	118- -346		

Aquifer*	Well Number - Grid	Use	Owner	Well Depth (ft BGS)	Altitude of Land Surface (ft MSL)	Date	Depth to Water (ft BGS)	Water Level Elev (ft MSL)
(5.5 mi SW)								
Trinity- Hosston (4 mi S)	3917901 39-17-9	Public Supply	Prairie Hill WSC	3375	561	6/25/65	80-494	481-67
Trinity- Hosston (4.4 mi S)	3917903 39-17-9	Public Supply	Prairie Hill WSC	3275	529	6/9/80	483	46
Navarro Taylor (6.6 mi SE)	3918801 39-18-8	Domestic	Mary Whitten	19	622	3/1/65	2.3-18	619.7- 604
Trinity- Hosston (6.8 mi SE)	3918802 39-18-8	Public Supply	Prairie Hill WSC	3942	595 (from topo)	1963	47-88	548-507
Navarro Taylor (3.8 mi East)	3918101 39-18-1	Historical Observation Well (plugged)	Grady Crawford	22	621 (from topo)	2010	4.21- 13.21	616.8- 607.8
Trinity- Hosston (4.2 mi NE)	3909902 39-09-9	Public Supply	Birome WSC Well #1	3250	621	9/10/65	145-205	476-416
Trinity- Hosston (4.2 mi NE)	3909903 39-09-9	Public Supply	Birome WSC Well #2	3311	623	10/16/92	144	479

^{* (}direction from Landfill)

Table III-4.5 Coordinates and Elevations of Borings Advanced at the Site by SCS Engineers

Boring Number	Easting	Northing	Hollow Stem Auger Type	Ground Elevation (ft-msl)	Depth Drilled (ft-bgs)	Elevation of Bottom (ft-msl)
B-1 (PZ-1)	3353867.3	10599904.81	7 1/4	551.74	39.5	512.24
B-2	3354595.81	10598697.6	7 1/4	549.78	55.0	494.78
B-3 (PZ-3)	3355259.69	10597665.32	7 1/4	541.20	45.0	496.2
B-4	3355130.33	10599528	7 1/4	550.04	101.0	449.04
B-5	3355913.87	10600728.3	7 1/4	541.38	47.0	494.38
B-6	3355562.96	10602041.9	7 1/4	545.55	70.7	474.85
B-7	3356670.83	10599929.6	8 1/4	530.50	55.5	475
B-8 (PZ-8)	3357935.82	10599489.18	8 1/4	550.34	75.0	475.34
B-9 (PZ-9)	3355762.31	10599314.37	8 1/4	535.30	40.0	495.30
B-9 cont.	3355762.31	10599314.37	8 1/4	535.30	135.0	400.30
B-10	3356199.16	10602404.1	8 1/4	545.40	53.0	492.4
B-11	3357048	10602933.5	7 1/4	553.50	78.5	475
B-12	3355833.07	10601575	8 1/4	542.85	48.0	494.85
B-13	3357768.09	10600645.6	8 1/4	555.15	80.0	475.15
B-14	3356543.77	10602016.3	8 1/4	539.20	65.5	473.7
B-15	3357265.27	10602471.1	7 1/4	563.35	70.0	493.35
B-16	3354706.01	10599996.8	8 1/4	560.25	61.0	499.25
B-17	3355568.96	10600519.6	7 1/4	546.75	71.0	475.75
B-18 (PZ-18)	3356694.76	10601254.04	8 1/4	534.84	56.0	478.84
B-19	3357202	10601429	7 1/4	562.05	87.0	475.05
B-20 (PZ-20)	3357666.42	10601846.53	7 1/4	564.68	73.0	491.68
B-21	3357008	10600682	8 1/4	538.75	45.0	493.75
B-22	3358132.03	10601234	8 1/4	555.00	80.0	475
B-23	3355207.68	10598431	8 1/4	540.08	45.7	494.38
B-24	3355746.69	10598780.1	7 1/4	533.63	59.2	474.43
B-25	3356251.06	10599102.9	7 1/4	533.25	33.0	500.25
B-26	3356929.04	10599457.3	8 1/4	530.45	36.0	494.5
B-27	3358308.89	10600427.7	8 1/4	546.65	53.0	493.65
B-28	3356800.71	10598286.7	8 1/4	529.6	55.0	474.6
B-29	3358523.03	10599393	8 1/4	540.25	45.0	495.25
B-30	3357828.13	10598886.4	8 1/4	543.05	48.0	495.05
B-31	3355837.8	10599897	8 1/4	537.55	63.0	474.55
B-32	3357077.27	10597864.5	8 1/4	526.3	32.0	494.3
B-33 (PZ-33)	3357774.62	10598320.64	8 1/4	539.20	55.0	484.2
B-34	3358367.31	10598778.6	8 1/4	535.65	41.0	494.65
B-35	3357682.18	10600037.4	8 1/4	553.3	59.0	494.3
B-36	3357239.12	10596730.2	8 1/4	532.5	58.0	474.5
B-37	3358201.19	10597770.6	8 1/4	526.9	52.0	474.9
B-38	3358847.64	10598223.2	8 1/4	529.85	55.0	474.85
B-39	3358709.87	10597052.3	8 1/4	522.95	48.0	475
B-40	3359476.22	10597259.9	8 1/4	522.80	28.0	494.8
B-41 (PZ-41)	3359083.91	10599450.64	8 1/4	534.62	60.0	474.62
B-42	3358523.73	10597484.3	8 1/4	527.00	32.0	495.0
B-43 (PZ-43)	3358875.54	10600433.69	8 1/4	548.86	75.0	473.86
B-43 cont.	3358875.54	10600433.69	8 1/4	548.86	150	398.86
B-44	3354540.62	10599103.1	7 1/4	551.20	76.0	475.20
B-45	3356769.83	10601549.1	8 1/4	545.50	51.0	494.5

Boring Number	Easting	Northing	Hollow Stem Auger Type	Ground Elevation (ft-msl)	Depth Drilled (ft-bgs)	Elevation of Bottom (ft-msl)
B-46	3357689.45	10601293.2	8 1/4	559.25	65.4	493.85
B-47 (PZ-47)	3356561.53	10598701.96	8 1/4	532.48	57.4	475.08

msl = mean sea level

b.g.s indicates depth is measured from below ground surface

Table III-4.6 Properties of Unit II

	East Disp	oosal Area	West Disp	Test	
Lab Test	Average	Number of Tests	Average	Number of Tests	Method
Moisture Content	17	19	19	16	ASTM D2216
Liquid Limit	63	21	68	18	ASTM D4318
Plasticity Index	42	21	46	18	ASTM D4318
Permeability (cm/s)	1.94 x 10 ⁻⁸	1	1.94 x 10 ⁻⁸	1	EM 1110-2- 1906
Hydraulic Conductivity (cm/s)**	2.14 x 10 ⁻⁸	2	2.31 x 10 ⁻⁸	2	EM 1110-2- 1906
Hydraulic Conductivity (cm/s) (geometric mean)	2.05 x 10 ⁻⁸	1	3.07 x 10 ⁻⁸	3	Slug Test

^{**} Both arithmetic (a) and geometric (g) mean used in calculating average.

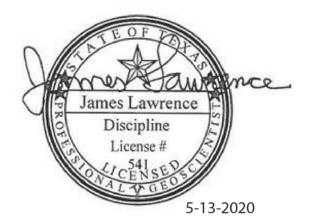


Table III-4.7 Properties of Unit III

	East D	risposal Area	West l	Disposal Area	Total Made al	
Lab Test	Average	Number of Tests	Average	Number of Tests	Test Method	
Moisture Content	14	17	16	10	ASTM D2216	
Liquid Limit	58	17	65	10	ASTM D4318	
Plasticity Index	38	17	43	10	ASTM D4318	
Permeability (cm/s)	n/a	n/a	n/a	n/a	EM 1110-2- 1906	
Hydraulic Conductivity (cm/s)**	n/a	n/a	n/a	n/a	EM 1110-2- 1906	
Hydraulic Conductivity (cm/s) (geometric mean)	1.84 x 10 ⁻⁸	2	n/a	n/a	Slug Test	

^{**} Both arithmetic (a) and geometric (g) mean used in calculating average.

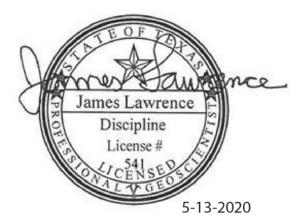


Table III-4.8 Existing Piezometers Completion Data

Monitor	Drilled Ground Surface		Top of Pipe	Screen		Filter Pack	
Well No.	Depth (ft b.g.s)	Elevation (ft-msl)	Elevation (ft-msl)	Depth to Top (ft)	Depth to Base (ft)	Depth to Top (ft)	Depth to Base (ft)
PZ-1	39.5	551.7	555.12	19.19	39.19	16.00	39.47
PZ-3	45.0	541.2	544.21	24.53	44.53	21.5	44.76
PZ-8	75.0	550.3	553.39	54.47	74.47	52.70	74.70
PZ-9	40.0	535.3	539.44	18.28	38.28	15.90	38.48
PZ-18	56.0	534.8	537.80	25.18	45.18	22.80	45.50
PZ-20	73.0	564.7	567.77	44.00	64.00	42.00	64.00
PZ-33	55.0	539.2	542.49	34.63	54.63	33.00	54.90
PZ-41	60.0	534.6	538.04	28.58	48.58	24.00	48.77
PZ-43	75.0	548.9	551.31	28.20	48.20	24.00	48.45
PZ-47	57.4	532.5	536.16	10.00	30.00	8.00	30.00

Ground-surface elevations are to the nearest tenth of a foot above mean sea level (msl) and are based on as-built monitoring well and piezometer survey elevations. Top of casing elevations are to the nearest hundredth of a foot. b.g.s indicates depth is measured from below ground surface.

Table III-4.9 Summary of Initial and Static Water Level Data

Boring/Well Number	Initial Water Level (ft-msl)	Static Water Level (ft-msl)	Date of Static Water Level Reading
B-1 (PZ-1)*	531.29	539.04	2/25/2020
B-3 (PZ-3)*	495.86 (dry)	510.65	2/25/2020
B-8 (PZ-8)*	476.30 (dry)	476.30 (dry)	2/25/2020
B-9 (PZ-9)*	510.05	501.45 (dry)	2/25/2020
B-18 (PZ-18)*	511.25	519.4	2/25/2020
B-20 (PZ-20)*	557.20	512.27	1/30/2020
B-33 (PZ-33)*	484.95 (dry)	484.95 (dry)	2/25/2020
B-41 (PZ-41)*	486.41 (dry)	486.41 (dry)	2/25/2020
B-43 (PZ-43)*	501.37 (dry)	500.86 (dry)	2/25/2020
B-47 (PZ-47)*	502.15 (dry)	502.18 (dry)	2/25/2020

^{* =} Piezometer installed in bore hole.

- 1. Initial water level information shown in this table was taken from the piezometers following installation.
- 2. PZ-1, PZ-3, PZ-9, and PZ-47 are piezometers in the west disposal area.
- 3. PZ-8, PZ-18, PZ-20, PZ-33, PZ-41, and PZ-43 are piezometers in the east disposal area.
- 4. PZ-1, PZ-3, PZ-9, PZ-20, PZ-41, and PZ-43 are screened in the weathered and unweathered shale-marl zones and across the interface.
- 5. PZ-8, PZ-18, PZ-33 are screened in the unweathered shale-marl zone, below the interface.
- 6. PZ-47 is screened in the weathered shale-mark zone, above the interface.

Table III-4.10 Summary of Vibrating Wire Piezometers Completion Data

VWP No.	Drilled Depth (ft b.g.s)	Ground Surface Elevation (ft- msl)	VWP Elevation (ft- msl)	VWP Depth (ft)	Bentonite Backfill Depth to Top (ft)	Filter Pack Depth to Top (ft)	Bentonite Seal Depth to Top (ft)
VWP-1	35.0	551.4	522.5	28.9	29.0	27.9	24.9
VWP-3	38.0	540.9	506.6	34.3	34.5	33.3	30.3
VWP-4	28.7	549.6	527.0	22.6	22.8	21.6	18.6
VWP-8	68.0	550.9	486.3	64.6	64.8	63.6	60.6
VWP-8D	160.0	551.0	400.0	151.0		150.0	147.0
VWP-9	35.0	535.3	506.9	28.4	28.5	27.3	24.3
VWP-9D	145.0	535.0	400.0	135.0		134.0	131.0
VWP-18	37.0	534.6	499.6	35.0	35.2	34.2	31.0
VWP-18D	145.0	535.0	400.0	135.0		134.0	131.0
VWP-19	53.0	562.1	511.0	51.1	51.3	50.3	47.0
VWP-20	56.5	564.6	510.1	54.5	54.7	53.7	51.0
VWP-25	32.0	533.8	505.0	28.8	29.0	27.8	24.8
VWP-26	24.8	530.5	506.0	24.5		23.5	20.5
VWP-27	30.0	546.7	520.0	26.7	27.0	25.7	23.0
VWP-30	40.0	544.0	506.0	38.0	38.1	37.0	34.0
VWP-33	48.0	538.6	494.8	43.8	44.0	42.8	39.8
VWP-33D	150.0	539.0	401.0	138.0		137.0	134.0
VWP-41	39.0	534.8	496.4	38.4	38.7	37.5	34.5
VWP-41D	145.0	535.0	402.0	133.0		132.0	129.0
VWP-43	40.0	549.5	511.5	38.0	38.3	37.0	34.0
VWP-43D	160.0	549.0	400.0	149.0		148.0	145.0
VWP-44	55.0	554.4	505.2	49.2	49.3	48.2	45.2
VWP-47	23.5	532.6	512.4	20.2	20.4	19.2	16.2
VWP-47D	142.0	532.0	400.0	132.0		131.0	128.0

Ground-surface and VWP elevations are to the nearest tenth of a foot above mean sea level (msl) and are based on piezometer survey elevations. b.g.s indicates depth is measured from below ground surface.

Table III-4.11 Summary of Vibrating Wire Piezometers Calculated Groundwater Elevations

VWP No.	Ground Surface Elevation (ft- msl)	VWP Elevation (ft- msl)	Temperature (°C)	Pressure (PSI)	Pressure Head (feet H ₂ O)	Calculated Groundwater Elevation (ft- msl)	Date of Reading
VWP-1	551.4	522.5	21.5	7.9	18.2	540.7	2/25/2020
VWP-3	540.9	506.6	21.5	2.5	6.0	512.6	2/25/2020
VWP-4	549.6	527.0	21.4	-0.1	-0.2	526.8 (dry)	2/25/2020
VWP-8	550.9	486.3	20.0	0.0	0.0	486.3 (dry)	2/25/2020
VWP-8D	551.0	400.0	21.8	43.5	100.64	500.6	2/25/2020
VWP-9	535.3	506.9	21.5	0.0	0.0	506.9 (dry)	2/25/2020
VWP-9D	535.0	400.0	22.5	51.2	118.4	518.4	2/25/2020
VWP-18	534.6	499.6	20.8	10.1	23.4	523.0	2/25/2020
VWP-18D	535.0	400.0	22.2	36.3	83.9	483.9	2/25/2020
VWP-19	562.1	511.0	21.6	-0.4	-1.0	510.0 (dry)	2/25/2020
VWP-20	564.6	510.1	21.7	0.0	0.0	510.1 (dry)	2/25/2020
VWP-25	533.8	505.0	19.7	0.0	0.0	505.0 (dry)	2/25/2020
VWP-26	530.5	506.0	20.5	-0.1	-0.3	505.7 (dry)	2/25/2020
VWP-27	546.7	520.0	21.4	-0.1	-0.3	519.7 (dry)	2/25/2020
VWP-30	544.0	506.0	20.2	1.5	3.4	509.4	2/25/2020
VWP-33	538.6	494.8	21.5	0.0	0.0	494.8 (dry)	2/25/2020
VWP-33D	539.0	401.0	22.1	3.1	7.1	408.1	2/25/2020
VWP-41	534.8	496.4	19.7	0.0	0.0	496.4 (dry)	2/25/2020
VWP-41D	535.0	402.0	21.3	8.8	20.3	422.4	2/25/2020
VWP-43	549.5	511.5	20.3	0.0	0.0	511.5 (dry)	2/25/2020
VWP-43D	549.0	400.0	21.8	36.0	83.3	483.3	2/25/2020
VWP-44	554.4	505.2	22.0	3.5	8.1	513.3	2/25/2020
VWP-47	532.6	512.4	20.5	0.0	0.0	512.4 (dry)	2/25/2020
VWP-47D	532.0	400.0	21.1	7.1	16.3	416.3	2/25/2020

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Ground-surface and VWP elevations are to the nearest tenth of a foot above mean sea level ons), and are based on piezometer survey elevations.

T-4-13

James Lawrence

Discipline

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May 2020

Table III-4.12 Summary of Aquifer (Slug) Tests Performed by SCS Engineers

Piezometer Designation	Unit Tested	Slug Test Method	Hydraulic Conductivity (cm/sec)		
D7 A 1	11/111	D D.:	Slug in: 2.03 x 10 ⁻⁸ cm/sec		
PZA-1	II/III	Bouwer-Rice	Slug out: 2.04 x 10 ⁻⁸ cm/sec		
PZA-3	II/III	Bouwer-Rice	Slug in: 6.97 x 10 ⁻⁸ cm/sec		
PZ-18	III	Bouwer-Rice	Slug in: 1.44 x 10 ⁻⁸ cm/sec		
PZ-10	m	bouwer-kice	Slug out: 2.36 x 10 ⁻⁸ cm/sec		
PZ-20	II/III	Bouwer-Rice	Slug in: 2.05 x 10 ⁻⁸ cm/sec		
Geometric Mean Hydraulic Conductivity = 2.42 x 10 ⁻⁸ cm/sec					
Arithmetic Mean Hydraulic Conductivity = 2.82 x 10 ⁻⁸ cm/sec					



Table III-4.13 Estimated Ground Water Velocities

Location	Hydraulic Conductivity (k)* (cm/sec) (Geometric Mean)	Hydraulic Gradient (i)**	Average Effective Porosity (n)***	Velocities (v) ft/day	Velocity (v) ft/year
Entire Area (PZA-1, PZA-3, PZ-18, PZ-20)	2.42 x 10 ⁻⁸	0.024	0.05	3.2 x 10 ⁻⁵	0.012
Unit II (PZA-1, PZA-3, PZ-20)	2.77 x 10 ⁻⁸	0.024	0.05	3.84 x 10 ⁻⁵	0.014
West Disposal Area (PZA-1, PZA-3)	3.07 x 10 ⁻⁸	0.024	0.05	3.84 x 10 ⁻⁵	0.014
East Disposal Area (PZ-18, PZ-20)	1.91 x 10 ⁻⁸	0.024	0.05	2.56 x 10 ⁻⁵	0.009
PZA-3 (High)	6.97 x 10 ⁻⁸	0.024	0.05	9.6 x 10 ⁻⁵	0.035
PZ-18 (Low)	1.44 x 10 ⁻⁸	0.024	0.05	1.92 x 10 ⁻⁵	0.007

^{*} Hydraulic conductivity estimated from slug test results.



^{**} Gradient estimated from February 2020 potentiometric map (Figure III-4.17)

^{***} Typical porosity for shale (Driscoll, 1986)

Table III-4.14 Proposed Monitoring Well Information

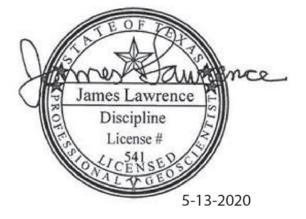
Monitor Well No.	Cell Location	Installation	Northing	Easting	Estimated Ground Surface Elevation (ft-msl)	Proposed Well Bottom Elevation (ft-msl)	Proposed Screen Elevation (ft-msl)	Expected Water Elevation (ft-msl)
P1-MW 1-A (D)	East	Prior to Landfill Operation	10601388.5'	3356636.7'	537.3	482	482-522	520
P1-MW 1-B (D)	East	Prior to Landfill Operation	10601388.5'	3356636.7'	537.3	400	400-440	520
P1-MW 2-A (D)	East	Prior to Landfill Operation	10600835.2'	3356820.8'	534.9	500	480-520	520
P1-MW 2-B (D)	East	Prior to Landfill Operation	10600835.2'	3356820.8'	534.9	400	400-440	520
P1-MW 3-A (D)	East	Waste < 1,000 feet	10600455.1'	3357167.6'	539.9	500	485-525	515
P1-MW 3-B (D)	East	Waste < 1,000 feet	10600455.1'	3357167.6'	539.9	400	400-440	515
P1-MW 4-A (D)	East	Waste < 1,000 feet	10599949.8'	3357049.5'	535.5	480	480-520	510
P1-MW 4-B (D)	East	Waste < 1,000 feet	10599949.8'	3357049.5'	535.5	400	400-440	500
P1-MW 5-A (D)	East	Waste < 1,000 feet	10599428.7'	3357289.6'	535.5	480	480-520	510
P1-MW 5-B (D)	East	Waste < 1,000 feet	10599428.7'	3357289.6'	535.5	400	400-440	480
P1-MW 6-A (D)	East	Waste < 1,000 feet	10598871.8'	3357451.8'	536.9	482	482-522	500
P1-MW 6-B (D)	East	Waste < 1,000 feet	10598871.8'	3357451.8'	536.9	400	400-440	440
P1-MW 7-A (D)	East	Waste < 1,000 feet	10598575.5'	3357780.2'	541.0	486	486-526	500
P1-MW 7-B (D)	East	Waste < 1,000 feet	10598575.5'	3357780.2'	541.0	400	400-440	410
P1-MW 8-A (D)	East	Waste < 1,000 feet	10598576.0'	3358302.8'	534.4	479	479-519	500
P1-MW 8-B (D)	East	Waste < 1,000 feet	10598576.0'	3358302.8'	534.4	400	400-440	410
P1-MW 9-A (D)	East	Waste < 1,000 feet	10599071.8'	3358618.2'	534.9	480	480-520	500
P1-MW 9-B (D)	East	Waste < 1,000 feet	10599071.8'	3358618.2'	534.9	400	400-440	420
P1-MW 10-A (D)	East	Waste < 1,000 feet	10599550.5'	3358887.5'	536.5	481	481-521	500
P1-MW 10-B (D)	East	Waste < 1,000 feet	10599550.5'	3358887.5'	536.5	400	400-440	430
P1-MW 11-A (D)	East	Waste < 1,000 feet	10599811.3'	3358835.5'	537.2	482	482-522	510

Monitor Well No.	Cell Location	Installation	Northing	Easting	Estimated Ground Surface Elevation (ft-msl)	Proposed Well Bottom Elevation (ft-msl)	Proposed Screen Elevation (ft-msl)	Expected Water Elevation (ft-msl)
P1-MW 11-B (D)	East	Waste < 1,000 feet	10599811.3'	3358835.5'	537.2	400	400-440	460
P1-MW 12-A (D)	East	Waste < 1,000 feet	10599973.5'	3359272.3'	535.2	480	480-520	510
P1-MW 12-B (D)	East	Waste < 1,000 feet	10599973.5'	3359272.3'	535.2	400	400-440	480
P1-MW 13-A (D)	East	Waste < 1,000 feet	10600475.2'	3358969.8'	548.7	494	494-534	510
P1-MW 13-B (D)	East	Waste < 1,000 feet	10600475.2'	3358969.8'	548.7	400	400-440	480
P1-MW 14-A (D)	East	Waste < 1,000 feet	10600975.4'	3358654.1'	557.9	503	503-543	515
P1-MW 14-B (D)	East	Waste < 1,000 feet	10600975.4'	3358654.1'	557.9	400	400-440	480
P1-MW 15-A (D)	East	Waste < 1,000 feet	10601450.3'	3358350.5'	559.1	504	504-544	520
P1-MW 15-B (D)	East	Waste < 1,000 feet	10601450.3'	3358350.5'	559.1	400	400-440	500
P1-MW 16-A (D)	East	Prior to Landfill Operation	10601952.9'	3358044.6'	562.9	508	508-548	520
P1-MW 16-B (D)	East	Prior to Landfill Operation	10601952.9'	3358044.6'	562.9	400	400-440	520
P1-MW 17-A (D)	East	Prior to Landfill Operation	10602455.6'	3357728.7'	568.7	514	514-554	520
P1-MW 17-B (D)	East	Prior to Landfill Operation	10602455.6'	3357728.7'	568.7	400	400-440	520
P1-MW 18-A (U)	East	Prior to Landfill Operation	10602898.2'	3357210.8'	557.1	502	502-542	520
P1-MW 18-B (U)	East	Prior to Landfill Operation	10602898.2'	3357210.8'	557.1	400	400-440	520
P1-MW 19-A (U)	East	Prior to Landfill Operation	10602401.2'	3356897.4'	539.8	485	485-525	520
P1-MW 19-B (U)	East	Prior to Landfill Operation	10602401.2'	3356897.4'	539.8	400	400-440	520
P1-MW 20-A (U)	East	Prior to Landfill Operation	10601906.1'	3356610.0'	539.5	485	485-525	520
P1-MW 20-B (U)	East	Prior to Landfill Operation	10601906.1'	3356610.0'	539.5	400	400-440	520
P2-MW 1-A (U)	West	Waste < 1,000 feet	10601080.1'	3355911.8'	541.3	486	486-526	520

Monitor Well No.	Cell Location	Installation	Northing	Easting	Estimated Ground Surface Elevation (ft-msl)	Proposed Well Bottom Elevation (ft-msl)	Proposed Screen Elevation (ft-msl)	Expected Water Elevation (ft-msl)
P2-MW 1-B (U)	West	Waste < 1,000 feet	10601080.1'	3355911.8'	541.3	400	400-440	520
P2-MW 2-A (U)	West	Waste < 1,000 feet	10600561.9'	3355105.9'	546.9	492	492-532	535
P2-MW 2-B (U)	West	Waste < 1,000 feet	10600561.9'	3355105.9'	546.9	400	400-440	535
P2-MW 3-A (U)	West	Waste < 1,000 feet	10600028.3'	3354261.3'	561.9	507	507-547	540
P2-MW 3-B (U)	West	Waste < 1,000 feet	10600028.3'	3354261.3'	561.9	400	400-440	540
P2-MW 4-A (D)	West	Waste < 1,000 feet	10599509.0'	3354533.4'	558.2	503	503-543	525
P2-MW 4-B (D)	West	Waste < 1,000 feet	10599509.0'	3354533.4'	558.2	400	400-440	525
P2-MW 5-A (D)	West	Waste < 1,000 feet	10599116.9'	3354318.4'	553.8	499	499-539	515
P2-MW 5-B (D)	West	Waste < 1,000 feet	10599116.9'	3354318.4'	553.8	400	400-440	515
P2-MW 6-A (D)	West	Waste < 1,000 feet	10598627.3'	3354628.1'	549.0	494	494-534	515
P2-MW 6-B (D)	West	Waste < 1,000 feet	10598627.3'	3354628.1'	549.0	400	400-440	515
P2-MW 7-A (D)	West	Waste < 1,000 feet	10598137.9'	3354937.1'	541.7	487	487-527	515
P2-MW 7-B (D)	West	Waste < 1,000 feet	10598137.9'	3354937.1'	541.7	400	400-440	515
P2-MW 8-A (D)	West	Waste < 1,000 feet	10597808.8'	3355366.0'	542.7	488	488-528	515
P2-MW 8-B (D)	West	Waste < 1,000 feet	10597808.8'	3355366.0'	542.7	400	400-440	515
P2-MW 9-A (D)	West	Waste < 1,000 feet	10598355.8'	3355575.5'	534.7	480	480-520	515
P2-MW 9-B (D)	West	Waste < 1,000 feet	10598355.8'	3355575.5'	534.7	400	400-440	500
P2-MW 10-A (D)	West	Waste < 1,000 feet	10598926.3'	3355714.8'	534.9	480	480-520	515
P2-MW 10-B (D)	West	Waste < 1,000 feet	10598926.3'	3355714.8'	534.9	400	400-440	500
P2-MW 11-A (D)	West	Waste < 1,000 feet	10599286.1'	3355952.6'	535.1	480	480-520	515
P2-MW 11-B (D)	West	Waste < 1,000 feet	10599286.1'	3355952.6'	535.1	400	400-440	440
P2-MW 12-A (D)	West	Waste < 1,000 feet	10599642.5'	3356227.9'	535.5	480	480-520	515
P2-MW 12-B (D)	West	Waste < 1,000 feet	10599642.5'	3356227.9'	535.5	400	400-440	440
12-B (D)	11 031	feet	10077044.0	5556221.7	333.3	400	100 770	770

Monitor Well No.	Cell Location	Installation	Northing	Easting	Estimated Ground Surface Elevation (ft-msl)	Proposed Well Bottom Elevation (ft-msl)	Proposed Screen Elevation (ft-msl)	Expected Water Elevation (ft-msl)
P2-MW 13-A (D)	West	Waste < 1,000 feet	10600060.5'	3356061.2'	535.3	480	480-520	515
P2-MW 13-B (D)	West	Waste < 1,000 feet	10600060.5'	3356061.2'	535.3	400	400-440	490
P2-MW 14-A (D)	West	Waste < 1,000 feet	10600549.7'	3356070.2'	536.9	482	482-522	515
P2-MW 14-B (D)	West	Waste < 1,000 feet	10600549.7'	3356070.2'	536.9	400	400-440	490

Proposed shallow well bottom elevations are 55 feet below ground surface elevations. Proposed deep well bottom elevations will all be set at 400 ft-msl.



APPENDIX III-4.A SOIL RESOURCE REPORT





Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants Custom Soil Resource Report for Hill County, Texas, Limestone County, Texas, and McLennan County, Texas

City of Waco Landfill - Site 50



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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Contents

Preface	2
How Soil Surveys Are Made	5
Soil Map	
Soil Map	
Legend	
Map Unit Legend	
Map Unit Descriptions	
Hill County, Texas	
44—Heiden clay, 5 to 8 percent slopes	15
74—Tinn clay, 0 to 1 percent slopes, frequently flooded	
80—Wilson clay loam, 1 to 3 percent slopes	
Limestone County, Texas	
AxB—Axtell fine sandy loam, 1 to 3 percent slopes	
CrB—Crockett loam, 1 to 3 percent slopes	21
FeD2—Ferris clay, 5 to 15 percent slopes, eroded	22
FhC2—Ferris-Heiden complex, 2 to 5 percent slopes, eroded	
HeB—Heiden clay, 1 to 3 percent slopes	26
To—Tinn clay, 0 to 1 percent slopes, frequently flooded	28
W—Water	29
Wf—Whitesboro loam, frequently flooded	29
WnA—Wilson clay loam, 0 to 2 percent slopes	30
McLennan County, Texas	33
CrB—Crockett loam, 3 to 5 percent slopes	
HeC—Heiden clay, 3 to 5 percent slopes	34
WnA—Wilson clay loam, 0 to 2 percent slopes	36
References	38

How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

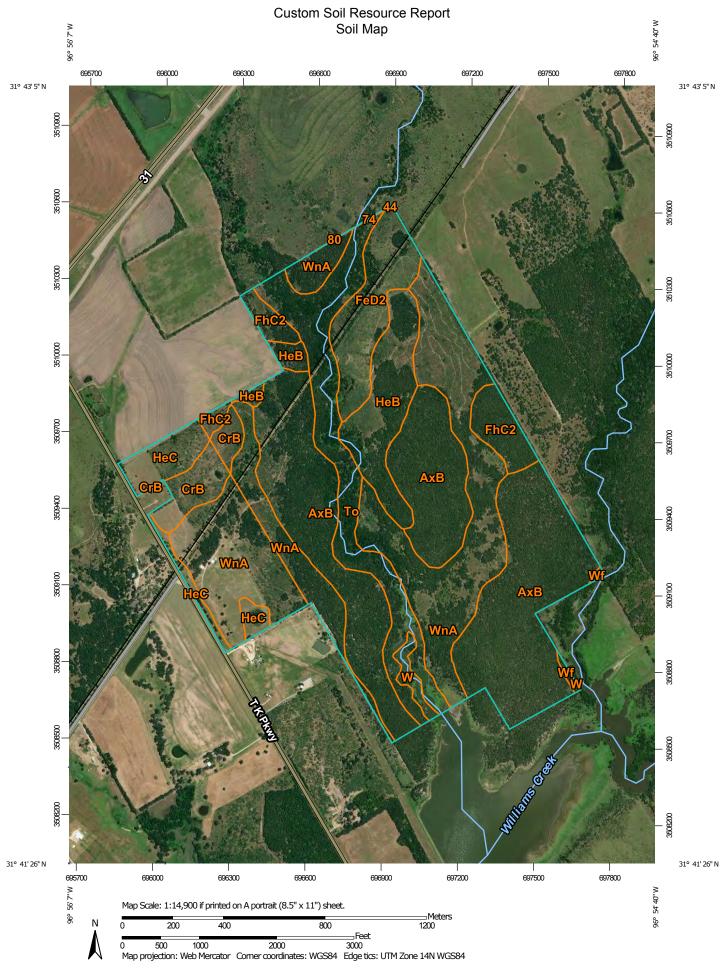
Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons

-

Soil Map Unit Lines

Soil Map Unit Points

Special Point Features

(©)

Blowout

 \boxtimes

Borrow Pit

Ж

Clay Spot

 \Diamond

Closed Depression

×

Gravel Pit

00

Gravelly Spot

0

Landfill

٨.

Lava Flow

Marsh or swamp

2

Mine or Quarry

0

Miscellaneous Water
Perennial Water

0

Rock Outcrop

4

Saline Spot

. .

Sandy Spot

0

Severely Eroded Spot

Δ :

Sinkhole

20

Sodic Spot

Slide or Slip

8

Spoil Area

۵

Stony Spot
Very Stony Spot

Ø) V

Wet Spot

Other

Δ

Special Line Features

Water Features
Streams and Canals

Transportation

ansport

Rails

~

Interstate Highways

US Routes

 \sim

Major Roads

 \sim

Local Roads

Background

The

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at scales ranging from 1:20,000 to 1:24,000.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Hill County, Texas

Survey Area Data: Version 16, Sep 15, 2018

Soil Survey Area: Limestone County, Texas Survey Area Data: Version 15, Sep 14, 2018

Soil Survey Area: McLennan County, Texas Survey Area Data: Version 17, Sep 14, 2018

Your area of interest (AOI) includes more than one soil survey area. These survey areas may have been mapped at different scales, with a different land use in mind, at different times, or at different levels of detail. This may result in map unit symbols, soil properties, and interpretations that do not completely agree across soil survey area boundaries.

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 16, 2016—Nov 29, 2017

MAP LEGEND

MAP INFORMATION

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI	
44	Heiden clay, 5 to 8 percent slopes	0.0	0.0%	
74	Tinn clay, 0 to 1 percent slopes, frequently flooded	0.1	0.0%	
80	Wilson clay loam, 1 to 3 percent slopes	0.0	0.0%	
Subtotals for Soil Survey Area		0.2	0.0%	
Totals for Area of Interest		527.7	100.0%	

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI		
AxB	Axtell fine sandy loam, 1 to 3 percent slopes	182.8	34.6%		
CrB	Crockett loam, 1 to 3 percent slopes	4.5	0.9%		
FeD2	Ferris clay, 5 to 15 percent slopes, eroded	32.0	6.1%		
FhC2	Ferris-Heiden complex, 2 to 5 percent slopes, eroded	19.6	3.7%		
HeB	Heiden clay, 1 to 3 percent slopes	38.7	7.3%		
То	Tinn clay, 0 to 1 percent slopes, frequently flooded	58.8	11.1%		
W	Water	4.3	0.8%		
Wf	Whitesboro loam, frequently flooded	1.2	0.2%		
WnA	Wilson clay loam, 0 to 2 percent slopes	110.8	21.0%		
Subtotals for Soil Survey Area		452.7	85.8%		
Totals for Area of Interest		527.7	100.0%		

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
CrB	Crockett loam, 3 to 5 percent slopes	12.0	2.3%
HeC	Heiden clay, 3 to 5 percent slopes	19.5	3.7%
WnA	Wilson clay loam, 0 to 2 percent slopes	43.3	8.2%
Subtotals for Soil Survey Area		74.9	14.2%
Totals for Area of Interest		527.7	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas

shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Hill County, Texas

44—Heiden clay, 5 to 8 percent slopes

Map Unit Setting

National map unit symbol: 2sshq

Elevation: 250 to 720 feet

Mean annual precipitation: 36 to 45 inches Mean annual air temperature: 63 to 66 degrees F

Frost-free period: 245 to 278 days

Farmland classification: Not prime farmland

Map Unit Composition

Heiden and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Heiden

Setting

Landform: Ridges

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Microfeatures of landform position: Linear gilgai

Down-slope shape: Linear Across-slope shape: Convex

Parent material: Clayey residuum weathered from mudstone

Typical profile

A1 - 0 to 8 inches: clay A2 - 8 to 22 inches: clay Bss - 22 to 44 inches: clay CBd - 44 to 80 inches: clay

Properties and qualities

Slope: 5 to 8 percent

Depth to restrictive feature: 40 to 65 inches to densic material

Natural drainage class: Well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 40 percent

Gypsum, maximum in profile: 5 percent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 12.0

Available water storage in profile: Moderate (about 7.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: D

Ecological site: Southern Blackland (R086AY011TX)

Hydric soil rating: No

Minor Components

Ferris, moderately eroded

Percent of map unit: 10 percent

Landform: Ridges

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Microfeatures of landform position: Linear gilgai

Down-slope shape: Linear Across-slope shape: Convex

Ecological site: Southern Eroded Blackland (R086AY009TX)

Hydric soil rating: No

Heiden, moderately eroded

Percent of map unit: 5 percent

Landform: Ridges

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Microfeatures of landform position: Linear gilgai

Down-slope shape: Convex Across-slope shape: Concave

Ecological site: Southern Eroded Blackland (R086AY009TX)

Hydric soil rating: No

74—Tinn clay, 0 to 1 percent slopes, frequently flooded

Map Unit Setting

National map unit symbol: 2vtgr Elevation: 330 to 750 feet

Mean annual precipitation: 35 to 47 inches
Mean annual air temperature: 63 to 68 degrees F

Frost-free period: 226 to 263 days

Farmland classification: Not prime farmland

Map Unit Composition

Tinn and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Tinn

Setting

Landform: Flood plains

Landform position (three-dimensional): Tread Microfeatures of landform position: Circular gilgai

Down-slope shape: Linear Across-slope shape: Concave

Parent material: Calcareous clayey alluvium

Typical profile

A - 0 to 17 inches: clay Bss - 17 to 57 inches: clay Bkssy - 57 to 80 inches: clay

Properties and qualities

Slope: 0 to 1 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Moderately well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: Frequent Frequency of ponding: None

Calcium carbonate, maximum in profile: 25 percent

Gypsum, maximum in profile: 2 percent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 2.0

Available water storage in profile: Moderate (about 8.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: D

Ecological site: Clayey Bottomland (R086AY013TX)

Hydric soil rating: No

Minor Components

Whitesboro

Percent of map unit: 10 percent

Landform: Flood plains

Microfeatures of landform position: Circular gilgai

Down-slope shape: Linear Across-slope shape: Concave

Ecological site: Loamy Bottomland (R086AY012TX)

Hydric soil rating: No

Gladewater

Percent of map unit: 5 percent Landform: Flood plains Down-slope shape: Concave

Across-slope shape: Concave

Ecological site: Clayey Bottomland (R086AY013TX)

Hydric soil rating: Yes

80—Wilson clay loam, 1 to 3 percent slopes

Map Unit Setting

National map unit symbol: 2wg9f

Elevation: 200 to 770 feet

Mean annual precipitation: 34 to 48 inches Mean annual air temperature: 64 to 67 degrees F

Frost-free period: 243 to 262 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Wilson and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wilson

Setting

Landform: Stream terraces, stream terraces Landform position (three-dimensional): Tread

Down-slope shape: Linear Across-slope shape: Concave

Parent material: Loamy and/or clayey alluvium derived from mudstone

Typical profile

Ap - 0 to 7 inches: clay loam Btss - 7 to 31 inches: clay Btkss - 31 to 36 inches: clay Btkssyg - 36 to 42 inches: clay Btkyg - 42 to 80 inches: clay loam

Properties and qualities

Slope: 1 to 3 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Moderately well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.06 to 0.20 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 20 percent

Gypsum, maximum in profile: 15 percent

Salinity, maximum in profile: Very slightly saline to moderately saline (2.0 to 8.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 10.0

Available water storage in profile: Moderate (about 7.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: D

Ecological site: Southern Claypan Prairie (R086AY004TX)

Hydric soil rating: No

Minor Components

Burleson

Percent of map unit: 10 percent

Landform: Stream terraces, stream terraces Landform position (three-dimensional): Tread

Microfeatures of landform position: Circular gilgai, circular gilgai

Down-slope shape: Linear Across-slope shape: Linear

Ecological site: Southern Blackland (R086AY011TX)

Hydric soil rating: No

Crockett

Percent of map unit: 5 percent Landform: Ridges, stream terraces

Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Interfluve, tread

Down-slope shape: Linear Across-slope shape: Convex

Ecological site: Southern Claypan Prairie (R086AY004TX)

Limestone County, Texas

AxB—Axtell fine sandy loam, 1 to 3 percent slopes

Map Unit Setting

National map unit symbol: 2shg6

Elevation: 200 to 790 feet

Mean annual precipitation: 33 to 47 inches Mean annual air temperature: 65 to 67 degrees F

Frost-free period: 240 to 270 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Axtell and similar soils: 87 percent Minor components: 13 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Axtell

Setting

Landform: Stream terraces, stream terraces

Landform position (three-dimensional): Tread

Down-slope shape: Linear

Across-slope shape: Linear, convex

Parent material: Clayey alluvium of pleistocene age derived from mudstone

Typical profile

A - 0 to 10 inches: fine sandy loam

Btss - 10 to 18 inches: clay Btk1 - 18 to 46 inches: clay Btk2 - 46 to 80 inches: clay

Properties and qualities

Slope: 1 to 3 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Moderately well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.06 to 0.20 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 15 percent

Gypsum, maximum in profile: 5 percent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 5.0

Available water storage in profile: Moderate (about 7.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: D

Ecological site: Claypan Savannah (R087AY003TX)

Minor Components

Mabank

Percent of map unit: 7 percent

Landform: Stream terraces, stream terraces Landform position (three-dimensional): Tread

Down-slope shape: Linear Across-slope shape: Concave

Ecological site: Southern Claypan Prairie (R086AY004TX)

Hydric soil rating: No

Rader

Percent of map unit: 6 percent

Landform: Stream terraces, stream terraces

Landform position (three-dimensional): Tread

Down-slope shape: Linear

Across-slope shape: Convex, concave, linear Ecological site: Sandy Loam (R087AY005TX)

Hydric soil rating: No

CrB—Crockett loam, 1 to 3 percent slopes

Map Unit Setting

National map unit symbol: 2ssh6

Elevation: 280 to 860 feet

Mean annual precipitation: 34 to 43 inches Mean annual air temperature: 63 to 67 degrees F

Frost-free period: 234 to 271 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Crockett and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Crockett

Setting

Landform: Ridges

Landform position (two-dimensional): Shoulder, summit Landform position (three-dimensional): Interfluve

Down-slope shape: Linear Across-slope shape: Convex

Parent material: Loamy residuum weathered from shale of cretaceous age

Typical profile

A - 0 to 8 inches: loam Btss - 8 to 25 inches: clay Btkss - 25 to 45 inches: clay BCk - 45 to 53 inches: clay

Cdk - 53 to 72 inches: clay loam

Properties and qualities

Slope: 1 to 3 percent

Depth to restrictive feature: 43 to 60 inches to densic bedrock

Natural drainage class: Moderately well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.03 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 30 percent

Gypsum, maximum in profile: 2 percent

Salinity, maximum in profile: Nonsaline to slightly saline (0.0 to 4.0 mmhos/cm)

Sodium adsorption ratio, maximum in profile: 10.0

Available water storage in profile: Moderate (about 8.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: D

Ecological site: Southern Claypan Prairie (R086AY004TX)

Hydric soil rating: No

Minor Components

Normangee

Percent of map unit: 10 percent

Landform: Ridges

Landform position (two-dimensional): Shoulder, summit Landform position (three-dimensional): Interfluve

Down-slope shape: Linear Across-slope shape: Convex

Ecological site: Southern Claypan Prairie (R086AY004TX)

Hydric soil rating: No

Wilson

Percent of map unit: 5 percent Landform: Stream terraces

Landform position (three-dimensional): Tread

Down-slope shape: Linear Across-slope shape: Concave

Ecological site: Southern Claypan Prairie (R086AY004TX)

Hydric soil rating: No

FeD2—Ferris clay, 5 to 15 percent slopes, eroded

Map Unit Setting

National map unit symbol: ddcz Elevation: 400 to 1,000 feet

Mean annual precipitation: 28 to 42 inches
Mean annual air temperature: 64 to 70 degrees F

Frost-free period: 230 to 260 days

Farmland classification: Not prime farmland

Map Unit Composition

Ferris, eroded, and similar soils: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Ferris, Eroded

Setting

Landform: Ridges

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Microfeatures of landform position: Linear gilgai

Down-slope shape: Linear Across-slope shape: Convex

Parent material: Residuum weathered from calcareous shale in eagleford shale

and taylor marl formations of cretaceous age

Typical profile

H1 - 0 to 4 inches: clay H2 - 4 to 45 inches: clay H3 - 45 to 80 inches: clay

Properties and qualities

Slope: 5 to 15 percent

Depth to restrictive feature: 40 to 60 inches to densic bedrock

Natural drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 30 percent

Gypsum, maximum in profile: 5 percent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 5.0

Available water storage in profile: Moderate (about 6.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: D

Ecological site: Northern Eroded Blackland (R086AY008TX)

FhC2—Ferris-Heiden complex, 2 to 5 percent slopes, eroded

Map Unit Setting

National map unit symbol: 2sshj Elevation: 400 to 720 feet

Mean annual precipitation: 42 to 44 inches
Mean annual air temperature: 63 to 66 degrees F

Frost-free period: 232 to 254 days

Farmland classification: Not prime farmland

Map Unit Composition

Ferris, eroded, and similar soils: 50 percent Heiden, eroded, and similar soils: 40 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Ferris, Eroded

Setting

Landform: Ridges

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Microfeatures of landform position: Linear gilgai

Down-slope shape: Linear Across-slope shape: Convex

Parent material: Clayey residuum weathered from mudstone

Typical profile

Ap - 0 to 10 inches: clay Bkss1 - 10 to 30 inches: clay Bkss2 - 30 to 45 inches: clay Cdk - 45 to 60 inches: clay

Properties and qualities

Slope: 3 to 5 percent

Depth to restrictive feature: 39 to 60 inches to densic bedrock

Natural drainage class: Well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 30 percent

Gypsum, maximum in profile: 5 percent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 12.0

Available water storage in profile: Moderate (about 7.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: D

Ecological site: Southern Eroded Blackland (R086AY009TX)

Hydric soil rating: No

Description of Heiden, Eroded

Setting

Landform: Ridges

Landform position (two-dimensional): Backslope, shoulder Landform position (three-dimensional): Interfluve, side slope

Microfeatures of landform position: Linear gilgai

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Clayey residuum weathered from mudstone

Typical profile

Ap - 0 to 5 inches: clay A - 5 to 15 inches: clay Bkss1 - 15 to 38 inches: clay Bkss2 - 38 to 64 inches: clay CBdk - 64 to 80 inches: clay

Properties and qualities

Slope: 2 to 4 percent

Depth to restrictive feature: 48 to 65 inches to densic material

Natural drainage class: Well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 40 percent

Gypsum, maximum in profile: 5 percent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 12.0

Available water storage in profile: High (about 9.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: D

Ecological site: Southern Eroded Blackland (R086AY009TX)

Hydric soil rating: No

Minor Components

Houston black

Percent of map unit: 5 percent

Landform: Ridges

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Interfluve

Microfeatures of landform position: Linear gilgai

Down-slope shape: Convex Across-slope shape: Convex

Ecological site: Southern Blackland (R086AY011TX)

Hydric soil rating: No

Ferris, moderately eroded

Percent of map unit: 5 percent

Landform: Ridges

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Microfeatures of landform position: Linear gilgai

Down-slope shape: Linear Across-slope shape: Convex

Ecological site: Southern Eroded Blackland (R086AY009TX)

Hydric soil rating: No

HeB—Heiden clay, 1 to 3 percent slopes

Map Unit Setting

National map unit symbol: 2v1v9 Elevation: 290 to 1,020 feet

Mean annual precipitation: 33 to 45 inches Mean annual air temperature: 63 to 68 degrees F

Frost-free period: 224 to 278 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Heiden and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Heiden

Setting

Landform: Ridges

Landform position (two-dimensional): Summit, shoulder

Landform position (three-dimensional): Interfluve Microfeatures of landform position: Linear gilgai

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Clayey residuum weathered from mudstone

Typical profile

Ap - 0 to 6 inches: clay A - 6 to 18 inches: clay Bkss - 18 to 58 inches: clay CBdk - 58 to 70 inches: clay

Properties and qualities

Slope: 1 to 3 percent

Depth to restrictive feature: 40 to 65 inches to densic material

Natural drainage class: Well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 40 percent

Gypsum, maximum in profile: 5 percent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 12.0

Available water storage in profile: High (about 9.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: D

Ecological site: Southern Blackland (R086AY011TX)

Hydric soil rating: No

Minor Components

Houston black

Percent of map unit: 10 percent

Landform: Ridges

Landform position (two-dimensional): Shoulder, summit Landform position (three-dimensional): Interfluve

Microfeatures of landform position: Circular gilgai

Down-slope shape: Convex Across-slope shape: Linear

Ecological site: Southern Blackland (R086AY011TX)

Hydric soil rating: No

Ferris

Percent of map unit: 5 percent

Landform: Ridges

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Microfeatures of landform position: Linear gilgai

Down-slope shape: Linear Across-slope shape: Convex

Ecological site: Southern Eroded Blackland (R086AY009TX)

To—Tinn clay, 0 to 1 percent slopes, frequently flooded

Map Unit Setting

National map unit symbol: 2vtgr Elevation: 330 to 750 feet

Mean annual precipitation: 35 to 47 inches Mean annual air temperature: 63 to 68 degrees F

Frost-free period: 226 to 263 days

Farmland classification: Not prime farmland

Map Unit Composition

Tinn and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Tinn

Setting

Landform: Flood plains

Landform position (three-dimensional): Tread Microfeatures of landform position: Circular gilgai

Down-slope shape: Linear Across-slope shape: Concave

Parent material: Calcareous clayey alluvium

Typical profile

A - 0 to 17 inches: clay Bss - 17 to 57 inches: clay Bkssy - 57 to 80 inches: clay

Properties and qualities

Slope: 0 to 1 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Moderately well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: Frequent Frequency of ponding: None

Calcium carbonate, maximum in profile: 25 percent

Gypsum, maximum in profile: 2 percent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 2.0

Available water storage in profile: Moderate (about 8.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: D

Ecological site: Clayey Bottomland (R086AY013TX)

Hydric soil rating: No

Minor Components

Whitesboro

Percent of map unit: 10 percent

Landform: Flood plains

Microfeatures of landform position: Circular gilgai

Down-slope shape: Linear Across-slope shape: Concave

Ecological site: Loamy Bottomland (R086AY012TX)

Hydric soil rating: No

Gladewater

Percent of map unit: 5 percent Landform: Flood plains Down-slope shape: Concave Across-slope shape: Concave

Ecological site: Clayey Bottomland (R086AY013TX)

Hydric soil rating: Yes

W-Water

Map Unit Composition

Water: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Wf—Whitesboro loam, frequently flooded

Map Unit Setting

National map unit symbol: ddf9 Elevation: 170 to 570 feet

Mean annual precipitation: 34 to 40 inches Mean annual air temperature: 63 to 70 degrees F

Frost-free period: 225 to 275 days

Farmland classification: Not prime farmland

Map Unit Composition

Whitesboro and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Whitesboro

Setting

Landform: Flood plains
Down-slope shape: Linear

Across-slope shape: Concave

Parent material: Loamy alluvium of holocene age drived from mixed sources

Typical profile

H1 - 0 to 26 inches: loam H2 - 26 to 58 inches: clay loam H3 - 58 to 80 inches: sandy clay loam

Properties and qualities

Slope: 0 to 1 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to

high (0.57 to 1.98 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: Frequent Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Available water storage in profile: High (about 9.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: B

Ecological site: Loamy Bottomland (R086AY012TX)

Hydric soil rating: No

Minor Components

Unnamed, hydric

Percent of map unit: 8 percent Landform: Depressions Hydric soil rating: Yes

Unnamed

Percent of map unit: 7 percent

Hydric soil rating: No

WnA—Wilson clay loam, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2wg9b

Elevation: 380 to 870 feet

Mean annual precipitation: 37 to 42 inches Mean annual air temperature: 64 to 67 degrees F

Frost-free period: 250 to 255 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Wilson and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wilson

Setting

Landform: Stream terraces

Landform position (three-dimensional): Tread

Down-slope shape: Linear Across-slope shape: Concave

Parent material: Loamy and/or clayey alluvium derived from mudstone

Typical profile

Ap - 0 to 7 inches: clay loam Btss - 7 to 31 inches: clay Btkss - 31 to 36 inches: clay Btkssyg - 36 to 42 inches: clay Btkyg - 42 to 80 inches: clay loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Moderately well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.06 to 0.20 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 20 percent

Gypsum, maximum in profile: 15 percent

Salinity, maximum in profile: Very slightly saline to moderately saline (2.0 to 8.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 10.0

Available water storage in profile: Moderate (about 7.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: D

Ecological site: Southern Claypan Prairie (R086AY004TX)

Hydric soil rating: No

Minor Components

Burleson

Percent of map unit: 10 percent

Landform: Stream terraces, stream terraces Landform position (three-dimensional): Tread

Microfeatures of landform position: Circular gilgai, circular gilgai

Down-slope shape: Linear Across-slope shape: Linear

Ecological site: Southern Blackland (R086AY011TX)

Hydric soil rating: No

Crockett

Percent of map unit: 5 percent

Landform: Ridges

Landform position (two-dimensional): Summit, shoulder

Landform position (three-dimensional): Interfluve

Down-slope shape: Linear Across-slope shape: Convex

Ecological site: Southern Claypan Prairie (R086AY004TX)

McLennan County, Texas

CrB—Crockett loam, 3 to 5 percent slopes

Map Unit Setting

National map unit symbol: 2vv4y

Elevation: 380 to 610 feet

Mean annual precipitation: 35 to 37 inches Mean annual air temperature: 65 to 67 degrees F

Frost-free period: 240 to 270 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Crockett and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Crockett

Setting

Landform: Ridges

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Linear Across-slope shape: Convex

Parent material: Loamy residuum weathered from shale of cretaceous age

Typical profile

A - 0 to 8 inches: loam Btss - 8 to 25 inches: clay Btkss - 25 to 45 inches: clay BCk - 45 to 53 inches: clay Cdk - 53 to 72 inches: clay loam

Properties and qualities

Slope: 3 to 5 percent

Depth to restrictive feature: 43 to 60 inches to densic bedrock

Natural drainage class: Moderately well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.03 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 30 percent

Gypsum, maximum in profile: 2 percent

Salinity, maximum in profile: Nonsaline to slightly saline (0.0 to 4.0 mmhos/cm)

Sodium adsorption ratio, maximum in profile: 10.0

Available water storage in profile: Moderate (about 8.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: D

Ecological site: Southern Claypan Prairie (R086AY004TX)

Hydric soil rating: No

Minor Components

Heiden

Percent of map unit: 10 percent

Landform: Ridges

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Microfeatures of landform position: Linear gilgai

Down-slope shape: Linear Across-slope shape: Convex

Ecological site: Southern Blackland (R086AY011TX)

Hydric soil rating: No

Wilson

Percent of map unit: 5 percent Landform: Stream terraces

Landform position (three-dimensional): Tread

Microfeatures of landform position: Open depressions

Down-slope shape: Linear Across-slope shape: Concave

Ecological site: Southern Claypan Prairie (R086AY004TX)

Hydric soil rating: No

HeC—Heiden clay, 3 to 5 percent slopes

Map Unit Setting

National map unit symbol: 2v1vc

Elevation: 260 to 890 feet

Mean annual precipitation: 33 to 42 inches
Mean annual air temperature: 63 to 68 degrees F

Frost-free period: 233 to 260 days

Farmland classification: All areas are prime farmland

Map Unit Composition

Heiden and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Heiden

Setting

Landform: Ridges

Landform position (two-dimensional): Shoulder, backslope Landform position (three-dimensional): Side slope, interfluve

Microfeatures of landform position: Linear gilgai

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Clayey residuum weathered from mudstone

Typical profile

Ap - 0 to 6 inches: clay Bkss1 - 6 to 18 inches: clay Bkss2 - 18 to 58 inches: clay CBdk - 58 to 80 inches: clay

Properties and qualities

Slope: 3 to 5 percent

Depth to restrictive feature: 40 to 65 inches to densic material

Natural drainage class: Well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 40 percent

Gypsum, maximum in profile: 5 percent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 12.0

Available water storage in profile: High (about 9.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: D

Ecological site: Southern Blackland (R086AY011TX)

Hydric soil rating: No

Minor Components

Houston black

Percent of map unit: 10 percent

Landform: Ridges

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Microfeatures of landform position: Circular gilgai

Down-slope shape: Convex Across-slope shape: Linear

Ecological site: Southern Blackland (R086AY011TX)

Hydric soil rating: No

Ferris, moderately eroded

Percent of map unit: 5 percent

Landform: Ridges

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope Microfeatures of landform position: Linear gilgai

Down-slope shape: Linear Across-slope shape: Convex

Ecological site: Southern Eroded Blackland (R086AY009TX)

WnA—Wilson clay loam, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2wg9b

Elevation: 380 to 870 feet

Mean annual precipitation: 37 to 42 inches Mean annual air temperature: 64 to 67 degrees F

Frost-free period: 250 to 255 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Wilson and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wilson

Setting

Landform: Stream terraces

Landform position (three-dimensional): Tread

Down-slope shape: Linear Across-slope shape: Concave

Parent material: Loamy and/or clayey alluvium derived from mudstone

Typical profile

Ap - 0 to 7 inches: clay loam Btss - 7 to 31 inches: clay Btkss - 31 to 36 inches: clay Btkssyg - 36 to 42 inches: clay Btkyg - 42 to 80 inches: clay loam

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Moderately well drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.06 to 0.20 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 20 percent

Gypsum, maximum in profile: 15 percent

Salinity, maximum in profile: Very slightly saline to moderately saline (2.0 to 8.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 10.0

Available water storage in profile: Moderate (about 7.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: D

Ecological site: Southern Claypan Prairie (R086AY004TX)

Hydric soil rating: No

Minor Components

Burleson

Percent of map unit: 10 percent

Landform: Stream terraces, stream terraces Landform position (three-dimensional): Tread

Microfeatures of landform position: Circular gilgai, circular gilgai

Down-slope shape: Linear Across-slope shape: Linear

Ecological site: Southern Blackland (R086AY011TX)

Hydric soil rating: No

Crockett

Percent of map unit: 5 percent

Landform: Ridges

Landform position (two-dimensional): Summit, shoulder

Landform position (three-dimensional): Interfluve

Down-slope shape: Linear Across-slope shape: Convex

Ecological site: Southern Claypan Prairie (R086AY004TX)

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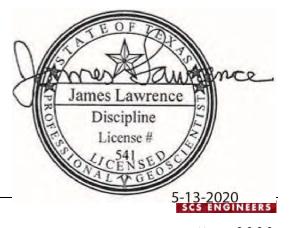
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May 2020

APPENDIX III-4.B WELL SEARCH DATA





Assessment, Compliance and Permitting Support

May 1, 2018

James Lawrence, P.G. SCS Engineers 1901 Central Drive, Suite 550 Bedford, Texas 76021

Re:

500 Ft. Radial Water Well Search

Waco Site 50

Happy Swaner Lane

Limestone and McLennan Counties

Atlas Job #18-04-020

Mr. Lawrence:

Atlas Environmental Research has performed a water well search for the above referenced site using the records of the Texas Water Development Board (TWDB) and the Texas Commission on Environmental Quality (TCEQ). Included in this report you will find a complete well listing sorted by the different types of files in the state's water well system. You will also find a map delineating water wells within the area of review and copies of all available drillers logs.

Please do not hesitate to call me at (512) 339-4155 if you have any questions concerning this project or questions concerning Atlas' water well research protocol. Thank you for utilizing Atlas' research services to meet your environmental information needs. I look forward to being of service to you in the future.

Sincerely.

Scott Anderson

Research Consultant

Enclosures/SA/

Atlas E.R. Water Well Search

Waco Site 50 Happy Swaner Lane Limestone and McLennan Counties Atlas Job #18-04-020

Atlas Environmental Research has located 0 water wells in the area of review.

Located Water Wells - 0

Plotted Water Wells - 0

Partially Numbered Water Wells - 0

Unnumbered Water Wells - 0

Public Water Supply Wells - 0

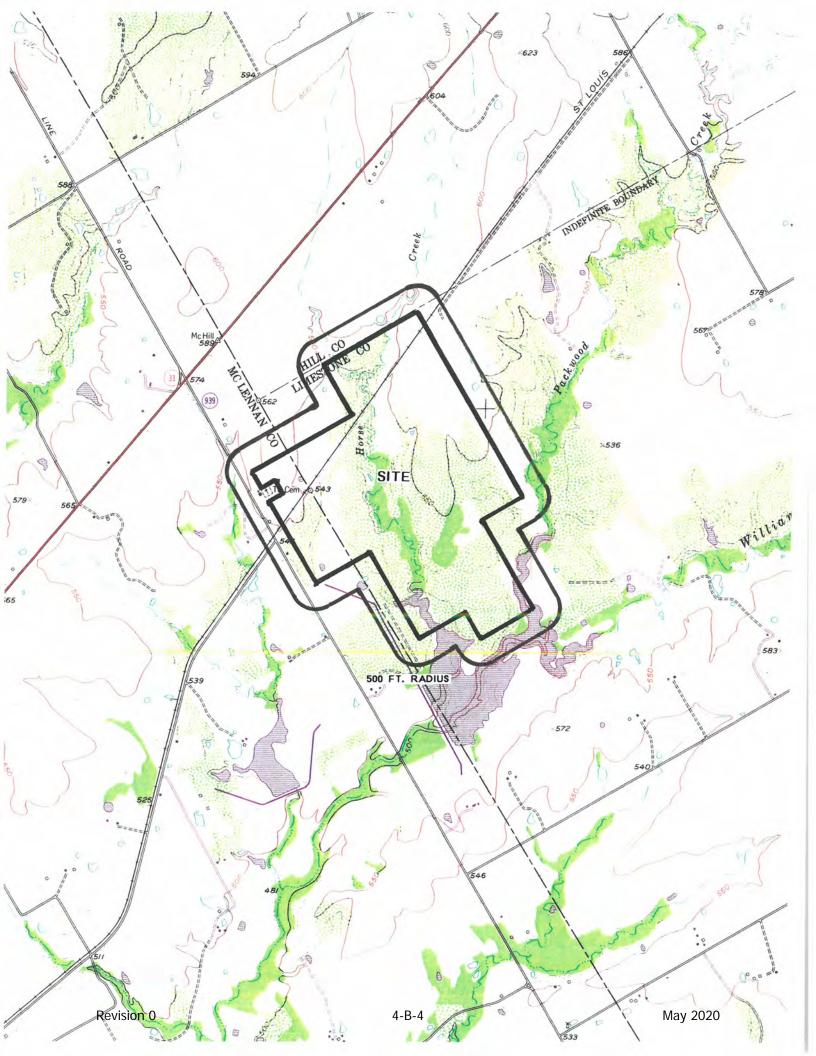
These wells have been labeled on the attached map with the final portion of the state well number. This portion of the state well number has also been highlighted on the corresponding drillers log. The information for each USGS quadrangle utilized for the well location map is listed below.

Quadrangle Axtell, Texas Date

1956 (Photorevised 1978)

Contours 10 Feet

Quadrangle Scale: 1:24000; 1" = 2000'





Assessment, Compliance and Permitting Support

May 1, 2018

James Lawrence, P.G. SCS Engineers 1901 Central Drive, Suite 550 Bedford, Texas 76021

Re:

One Mile Radial Water Well Search

Waco Site 50

Happy Swaner Lane

Limestone and McLennan Counties

Atlas Job #18-04-020

Mr. Lawrence:

Atlas Environmental Research has performed a water well search for the above referenced site using the records of the Texas Water Development Board (TWDB) and the Texas Commission on Environmental Quality (TCEQ). Included in this report you will find a complete well listing sorted by the different types of files in the state's water well system. You will also find a map delineating water wells within the area of review and copies of all available drillers logs.

Please do not hesitate to call me at (512) 339-4155 if you have any questions concerning this project or questions concerning Atlas' water well research protocol. Thank you for utilizing Atlas' research services to meet your environmental information needs. I look forward to being of service to you in the future.

Sincerely,

Scott Anderson

Research Consultant

Enclosures/SA/

Atlas E.R. Water Well Search

Waco Site 50 Happy Swaner Lane Limestone and McLennan Counties Atlas Job #18-04-020

Atlas Environmental Research has located 2 water wells in the area of review.

39-17-201 39-17-601

Plotted Water Wells - 0

Partially Numbered Water Wells - 0

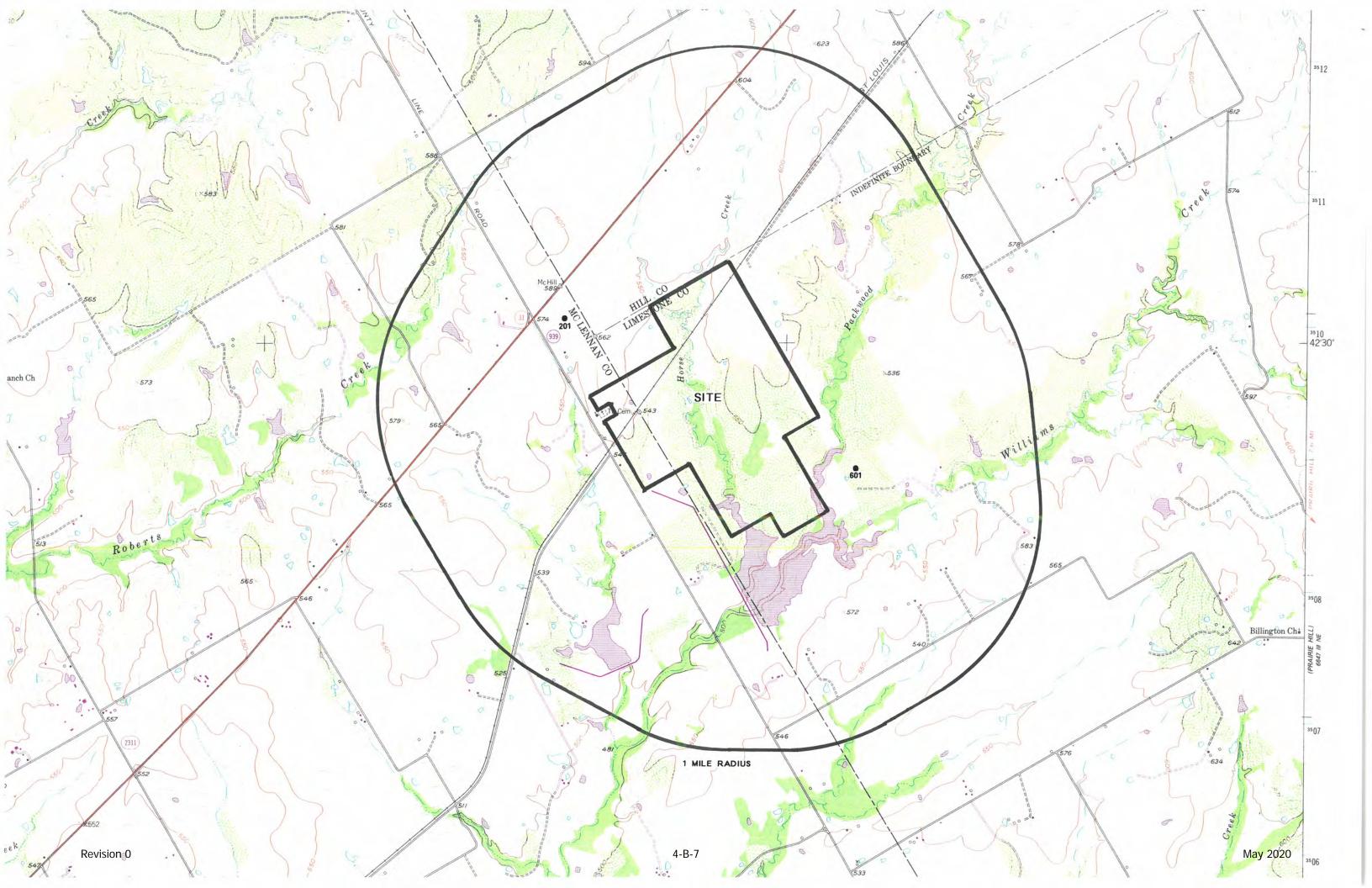
Unnumbered Water Wells - 0

Public Water Supply Wells - 0

These wells have been labeled on the attached map with the final portion of the state well number. This portion of the state well number has also been highlighted on the corresponding drillers log. The information for each USGS quadrangle utilized for the well location map is listed below.

QuadrangleDateContoursAxtell, Texas1956 (Photorevised 1978)10 Feet

Quadrangle Scale: 1:24000; 1" = 2000'



CROSS REFERENCE SHEET

Name or Subject

CR-GWID

MCLENNAN L

Located Well Data ST 39-17-201 Date

Regarding

Electric Log

SEE

Name or Subject

GW-SC ELECTRIC LOG FILE

Q-29

TWDBS-M-3

Revision 0

4-B-8

May 2020





GWDB Reports and Downloads

Well Basic Details

Scanned Documents

State Well Number	3917201		
County	McLennan		
River Basin	Brazos		
Groundwater Management Area	8		
Regional Water Planning Area	G - Brazos G		
Groundwater Conservation District	Southern Trinity GCD		
Latitude (decimal degrees)	31.709723		
Latitude (degrees minutes seconds)	31° 42′ 35″ N		
Longitude (decimal degrees)	-96.935278		
Longitude (degrees minutes seconds)	096° 56' 07" W		
Coordinate Source	+/- 1 Minute		
Aquifer Code	NOT-APPL - Aquifer Code Is No Applicable to this Well		
Aquifer	Unassigned		
Aquifer Pick Method			
Land Surface Elevation (feet above sea level)	560		
Land Surface Elevation Method	Interpolated From Topo Map		
Well Depth (feet below land surface)	2030		
Well Depth Source	Another Government Agency		
Drilling Start Date			
Drilling End Date	0/0/1951		
Drilling Method			
Borehole Completion			

Well Type	Oil or Gas
Well Use	Unused
Water Level Observation	None
Water Quality Available	No
Pump	None
Pump Depth (feet below land surface)	
Power Type	
Annular Seal Method	
Surface Completion	
Owner	S. H. Riggs
Driller	Grindstaff No.1
Other Data Available	
Well Report Tracking Number	
Plugging Report Tracking Number	
U.S. Geological Survey Site Number	
Texas Commission on Environmental Quality Source Id	
Groundwater Conservation District Well Number	
Owner Well Number	
Other Well Number	
Previous State Well Number	
Reporting Agency	
Created Date	
Last Update Date	

Remarks

Casing - No Data

Well Tests - No Data

Lithology - No Data

Annular Seal Range - No Data

Borehole - No Data

Plugged Back - No Data

Filter Pack - No Data

Packers - No Data





		l Measurements		
	No Dat	ta Available		





Water Quality Analysis - No Data Available

GWDB DISCLAIMER: Except where noted, all of the information provided in the Texas Water Development Board (TWDB) Groundwater Database (http://www.twdb.texas.gov/groundwater/data/gwdbrpt.asp) is believed to be accurate and reliable; however, the TWDB assumes no responsibility for any errors appearing in rules or otherwise. Further, TWDB assumes no responsibility for the use of the information provided. PLEASE NOTE that users of these data are responsible for checking the accuracy, completeness, currency and/or suitability of all information themselves. TWDB makes no guarantees or warranties as to the accuracy, completeness, currency, or suitability of the information provided via the Groundwater Database (GWDB). TWDB specifically disclaims any and all liability for any claims or damages that may result from providing GWDB data or the information it contains. For additional information or answers to questions concerning the TWDB GWDB, contact the Groundwater Data Team at GroundwaterData@twdb.texas.gov.

CROSS REFERENCE SHEET

Name or Subject

CR-GWTD LIMESTONE

Located Well Data SD 39-17-601 Date

Regording

Electric Log

SEE

Name or Subject

GW-SC ELECTRIC LOG FILE

Q-143

TWDBS-M-3

Revision 0

4-B-12

May 2020





GWDB Reports and Downloads

Well Basic Details

Scanned Documents

State Well Number	3917601
County	Limestone
River Basin	Brazos
Groundwater Management Area	8
Regional Water Planning Area	G - Brazos G
Groundwater Conservation District	
Latitude (decimal degrees)	31.700278
Latitude (degrees minutes seconds)	31° 42' 01" N
Longitude (decimal degrees)	-96.911389
Longitude (degrees minutes seconds)	096° 54' 41" W
Coordinate Source	+/- 1 Second
Aquifer Code	NOT-APPL - Aquifer Code Is Not Applicable to this Well
Aquifer	Unassigned
Aquifer Pick Method	
Land Surface Elevation (feet above sea level)	531
Land Surface Elevation Method	Interpolated From Topo Map
Well Depth (feet below land surface)	3187
Well Depth Source	Another Government Agency
Drilling Start Date	
Drilling End Date	0/0/1961
Drilling Method	
Borehole Completion	

Well Type	Oil or Gas
Well Use	
Water Level Observation	None
Water Quality Available	No
Pump	
Pump Depth (feet below land surface)	
Power Type	
Annular Seal Method	
Surface Completion	
Owner	Paul Collins No.1
Driller	Ralph Spence and Bill Hughes
Other Data Available	
Well Report Tracking Number	
Plugging Report Tracking Number	
U.S. Geological Survey Site Number	
Texas Commission on Environmental Quality Source Id	
Groundwater Conservation District Well Number	
Owner Well Number	
Other Well Number	
Previous State Well Number	
Reporting Agency	U.S. Geological Survey
Created Date	7/25/1996
Last Update Date	7/25/1996

Remarks

Casing - No Data

Well Tests - No Data

Lithology - No Data

Annular Seal Range - No Data

Borehole - No Data

Plugged Back - No Data

Filter Pack - No Data

Packers - No Data





No Data Available





Water Quality Analysis - No Data Available

GWDB DISCLAIMER: Except where noted, all of the information provided in the Texas Water Development Board (TWDB) Groundwater Database (http://www.twdb.texas.gov/groundwater/data/gwdbrpt.asp) is believed to be accurate and reliable; however, the TWDB assumes no responsibility for any errors appearing in rules or otherwise. Further, TWDB assumes no responsibility for the use of the information provided. PLEASE NOTE that users of these data are responsible for checking the accuracy, completeness, currency and/or suitability of all information themselves. TWDB makes no guarantees or warrantee as to the accuracy, completeness, currency, or suitability of the information provided via the Groundwater Database (GWDB). TWDB specifically disclaims any and all liability for any claims or damages that may result from providing GWDB data or the information it contains. For additional information or answers to questions concerning the TWDB GWDB, contact the Groundwater Data Team at GroundwaterData@twdb.texas.gov.



Assessment, Compliance and Permitting Support

May 1, 2018

James Lawrence SCS Engineers 1901 Central Drive, Suite 550 Bedford, Texas 76021

Re:

Oil & Gas Well Search Waco Site 50 Happy Swaner Lane

Limestone and McLennan Counties

Atlas Job #18-04-020

Mr. Lawrence:

Atlas Environmental Research has performed an oil & gas well search for the above referenced site using the records of the Texas Railroad Commission (TRC). The following is a well listing sorted by the status shown on the TRC's maps.

Producing Wells - 0 Locations

Plugged Wells – 3 Locations

Map ID: A

Map ID: B

Map ID: C

Canceled Permits - 0 Locations

Please call me at (512) 339-4155 if you have any questions concerning this project or questions concerning Atlas' oil & gas well research protocol. Thank you for utilizing Atlas' research services to meet your environmental information needs. I look forward to being of service to you in the future.

Sincerely,

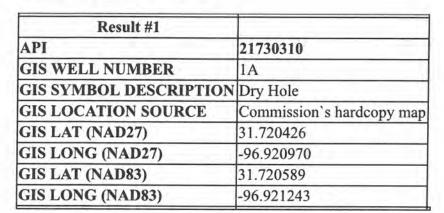
Scott Anderson

Research Consultant



GIS Identify Results - Well Location Attributes

Number of identify results: 1



OPERATOR/WELLBORE	
WELLBORE STATUS	DRY
LAST PERMIT ISSUED	265676
LAST PERMIT OPERATOR NUMBER	089953
LAST PERMIT OPERATOR	BRAZOS PRODUCTION COMPANY INC
LAST PERMIT LEASE NAME	HAWKINS, R. M. "A"
TOTAL DEPTH	0
SURFACE LOCATION	Land
ABSTRACT	373
SURVEY	B. M. HUNTER
BLOCK	
SECTION	
DISTANCE 1	5475
DIRECTION 1	NEL
DISTANCE 2	3475
DIRECTION 2	NWL
PLUGGING RECORD	
DATE PLUGGED	03/26/1985
PLUG DEPTH	769
PLUGGING OPERATOR	BRAZOS PROD. CO.
PLUGGED LEASE	HAWKINS



GIS Identify Results - Well Location Attributes



Result #1	
API	21730312
GIS WELL NUMBER	3
GIS SYMBOL DESCRIPTION	Dry Hole
GIS LOCATION SOURCE	Commission's hardcopy map
GIS LAT (NAD27)	31.719254
GIS LONG (NAD27)	-96.921318
GIS LAT (NAD83)	31.719417
GIS LONG (NAD83)	-96.921592

OPERATOR/WELLBORE	
WELLBORE STATUS	DRY
LAST PERMIT ISSUED	271372
LAST PERMIT OPERATOR NUMBER	089953
LAST PERMIT OPERATOR	BRAZOS PRODUCTION COMPANY INC
LAST PERMIT LEASE NAME	HAWKINS, R.M.
TOTAL DEPTH	0
SURFACE LOCATION	Land
ABSTRACT	373
SURVEY	B. M. HUNTER
BLOCK	
SECTION	
DISTANCE 1	3520
DIRECTION 1	NWL
DISTANCE 2	5475
DIRECTION 2	NEL
PLUGGING RECORD	
DATE PLUGGED	04/17/1985
PLUG DEPTH	575
PLUGGING OPERATOR	BRAZOS PROD. CO.
PLUGGED LEASE	HAWKINS



GIS Identify Results - Well Location Attributes

Number of identify results: 1

Result #1	
API	293
GIS WELL NUMBER	1
GIS SYMBOL DESCRIPTIO	N Dry Hole
GIS LOCATION SOURCE	Commission's hardcopy map
GIS LAT (NAD27)	31.706381
GIS LONG (NAD27)	-96.912253
GIS LAT (NAD83)	31.706545
GIS LONG (NAD83)	-96.912525



APPENDIX III-4.C SOIL BORING PLAN



Environmental Consulting & Contracting

August 14, 2018 Revised September 7, 2018 for minor hole relocations and one text revision

SCS Project 16216088.00

Mr. Chance Goodin–Manager, Waste Permits Division Texas Commission on Environmental Quality 12100 Park 35 Circle, MC-124 Building F Austin, Texas 78753

Subject:

Soil Boring Plan for a New Proposed Type I Municipal Solid Waste Landfill

McLennan and Limestone Counties, Texas

Dear Mr. Goodin:

SCS Engineers, on behalf of the City of Waco (The City), is herein submitting a Soil Boring Plan (SBP) for a new proposed Type I solid waste landfill (Landfill) in McLennan and Limestone Counties, Texas. As part of the permit application process for a new solid waste landfill, and as required in 30 TAC 330.63(e)(4), the following SBP is submitted for TCEQ review and approval. This document has been revised from the August 14, 2018 original to incorporate minor changes in hole locations requested by TCEQ in a site meeting dated August 31, 2018. A text addition has also been made to reflect that a demonstration will be incorporated in the full permit application regarding constituent travel times addressed in 30 TAC 330.63(e)(4)(B).

As described below, a total of 47 soil borings are proposed to characterize the 502.5-acre site for this permit application. Five of the soil borings are from a previous subsurface investigation at the site. Forty-two new soil borings are proposed. Piezometers will be installed to gather hydrogeologic data and sufficiently evaluate groundwater conditions on site.

PROPERTY LOCATION AND DESCRIPTION

The proposed Landfill property permitted area consists of approximately 502.5 acres. It is located about 16 miles northeast of the center of Waco, Texas on FM 939. (Figure 1).

REGIONAL GEOLOGY/HYDROGEOLOGY

Regional geology and stratigraphy is depicted in Table 1. Rocks exposed at the surface in McLennan and Limestone Counties generally consist of Taylor Group formations of Cretaceous marl, sand, and clay, as well as near-surface Tertiary/Quaternary sands, gravels and clay sediments deposited near and along stream channels (U.S. Department of Agriculture, Soil Survey of McLennan County, 1992; U.S. Department of Agriculture, Soil Survey of Limestone County, 1991).

The site location and detail are shown in Figures 1 and 2. The site topographic elevation ranges from about 570 feet msl (mean sea level) on the eastern side to about 540 feet msl on the western side. The site is directly underlain by the Wolfe City Formation. The Wolfe City Formation consists of Cretaceous period marl, sand, sandstone, and clay (Flawn, 1970). Surficial sediments above the Wolfe City consist of clayey and loamy alluvium, with some gravel observed in upland areas of the site. Table 1 shows stratigraphy in the site vicinity (Baker et al., 1990).

TABLE 1. Cretaceous Geologic and Hydrogeologic Units in McLennan County

System	Series	Group	Formation	Hydrogeologic Unit	Approximate Area Thickness (ft)	
		Taylor	Pecan Gap Chalk	Not a named hydrogeologic unit	215	
Site→		The state of the s	Wolfe City	и	300	
	Gulfian		Ozan	"	500-775	
	Guillan	Austin	Austin Chalk	ж -	30	
		Eagle Ford	South Bosque Shale	n .	120	
			Lake Waco		75	
		Woodbine	Pepper Shale		60	
			Del Rio Clay		70-90	
Coman			Georgetown and Main Street Limestone	A	25-35	
		he	Pawpaw and Weno Limestone	*	16-55	
	Upper Comanche Series		Denton Clay, Fort Worth Limestone, and Duck Creek Limestone		53-76	
		Fredericksburg	Edwards Limestone and Kiamichi Clay		20-77	
			Fredericksburg	Limestone	Comanche Peak Limestone	*
			Walnut Clay	*	125-175	
Lower Comanche Series			Paluxy Sand	Upper Trinity Aquifer	<71	
			Glen Rose	Middle Trinity Aquifer	200-375	
	Comanche		Travis Peak/Hensell Sand Member	Middle Trinity Aquifer	175	
	Series	Series Trinity	Travis Peak/Pearsall Member	Middle Trinity Aquifer	85	
	7		Travis Peak/Cow Creek Member	Middle Trinity Aquifer	130	
			Travis Peak/Hammet Shale Member	Middle Trinity Aquifer	140	
			Travis Peak/Sligo and Hosston Member	Lower Trinity Aquifer	1,680	

PROPOSED SITE EXPLORATION

As previously mentioned, the proposed Landfill permit boundary encompasses approximately 502.5 acres. As described below, a total of 47 soil borings are proposed to characterize the site for this permit application. Five of the soil borings are from a previous subsurface investigation at the site. 42 new soil borings are proposed. Piezometers will be installed to gather hydrogeologic data and sufficiently evaluate groundwater conditions on site.

Table 2 lists the requirements for number of borings as listed in 30 TAC 330.63(e)(4)(B). For an area of 500 to 550 acres, 44 to 47 total soil borings are required, of which 22 to 24 must be 30 feet below the Elevation of Deepest Excavation (EDE) of 505 feet msl, the remaining borings must be five feet below the EDE of 505 feet msl.

Table 3 lists the number of borings at a depth of 5 or 30 feet below the EDE. Boring locations are shown in Figure 2. Tables 4 and 5 below tabulate the existing and proposed borings and depths below ground surface (bgs).

The proposed boring plan will meet the requirements of 30 TAC 330.63(e)(4)(B). Borings will allow identification of the uppermost water bearing zone, which based on existing site exploration is a shallow water table in the low-permeability Wolfe City sediments. This zone is the "uppermost monitorable water", i.e., it is the first occurrence of monitorable water beneath the Landfill footprint and is therefore the most appropriate horizon for monitoring the Landfill. The first perennial, State-designated aquifer below the site is the Trinity Aquifer, the upper boundary of which occurs at least 600 feet below the EDE (Baker et al., 1990). A test hole drilled to the first perennial aquifer beneath the site (i.e., the Trinity) will not be required because the depth to the aquifer is more than 300 feet below the EDE and it is estimated that the 600 feet of low-permeability sediments between the site and the Trinity Aquifer will for all practical purposes prevent migration to the Trinity Aquifer (this will be documented in the full permit application, see below). Note that 30 TAC 330.63(e)(4)(B) states (in part)

"Aquifers more than 300 feet below the lowest excavation and where the estimated travel times for constituents to the aquifer are in excess of 30 years plus the estimated life of the site need not be identified through borings."

A demonstration will be prepared as a part of the permit application documenting that the "uppermost monitorable water" at the site is not hydraulically interconnected to the Trinity Aquifer due to a minimum of 600 feet of low-permeability sediments that exist between the base of the proposed Landfill and the Trinity Aquifer.

Figure 2 illustrates existing and proposed soil boring locations, which are tabulated in Tables 3, 4, and 5 below. All proposed drilling locations are subject to feasibility of drilling at that location, as controlled by areas of steep site topography, dense vegetation, or muddy conditions. If the location of a proposed soil boring deviates by more than 200 feet from the proposed location, TCEQ concurrence will be sought through a letter requesting a modification to the SBP.

Proposed new soil borings, listed in Table 5, will be continuously sampled from the ground surface to an elevation that meets the requirement of being 5 or 30 feet below EDE. Upon completion to total depth, water level depth will be checked prior to grouting from total depth to the ground surface. Any

piezometer installation, abandonment, and plugging will be performed in accordance with 30 TAC §330.63(e)(4)(D), including applicable rules in Title 16 TAC Chapter 76, §76.72 and §76.104.

TABLE 2. TCEQ Regulatory Requirements (30 TAC 330.63(e)(4)(B))

Size of Area in Acres	Number of Borings	Min. No. of Borings 30 Feet below the Elev. of Deepest Excavation	
5 or less	2-4	2	
5-10	4-6	3	
10-20	6-10	5	
20-50	10-15	7	
50-100	15-20	7-12	
100-150	20-23	12-13	
150-200	23-26	13-15	
200-250	26-29	15-16	
250-300	29-32	16-17	
300-350	32-35	17-18	
350-400	35-38	18-20	
400-450	38-42	20-21	
450-500	42-44	21-22	
500-550	44-47	22-24	
550-600	47-50	24-26	
More than 600	Determined in consultation with the executive director		

TABLE 3. Soil Borings Summary

	Number of Borings 5 feet Below EDE	Number of Borings 30 feet Below EDE	Total Number of Borings
Existing Borings	2	3	5
Proposed Borings	21	21	42
Total	23	24	47

TABLE 4. Tabulation of Existing Soil Borings (See Figure 2) EDE = 505 feet msl

Boring Number	Surface Elevation (ft msl)	Depth bgs (feet)	Bottom Elevation (ft msl)	Longitude	Latitude	5 Feet Below EDE	30 Feet Below EDE
B-1 (A-1)	551.7	82	469.7	96°55'59.14" W	31°42'16.87" N	No	Yes
B-2 (A-2)	549.8	55	494.8	96°55'51.13" W	31°42'04.71" N	Yes	No
B-3 (A-3)	541.1	72	469.1	96°55'43.82" W	31°41'54.30" N	No	Yes
B-4 (A-4)	550.0	101	449.0	96°55'44.66" W	31°42'12.76" N	No	Yes
B-5 (A-5)	541.4	47.75	493.6	96°55'35.17" W	31°42'24.40" N	Yes	No

Note - (A-1) reflects existing borehole

TABLE 5. Tabulation of Proposed Soil Borings (See Figure 2) EDE = 505 feet msl

Boring Number	Surface Elevation (ft msl)	Depth bgs (feet)	Bottom Elevation (ft msl)	Longitude	Latitude	5 Feet Below EDE?	30 Feet Below EDE?
B-6	546.2	71.2	475	96°55'38.76" W	31° 42' 37.50" N	Yes	Yes
B-7	522.0	47.0	475	96°55'26.69" W	31° 42' 16.27" N	No	Yes
B-8	550.0	75.0	475	96°55'12.21" W	31° 42' 11.53" N	No	Yes
B-9	536.7	36.7	500	96°55'37.42" W	31° 42′ 10.46″ N	Yes	No
B-10	542.0	42.0	500	96°55'31.27" W	31° 42' 40.89" N	Yes	No
B-11	553.5	78.5	475	96°55'21.26" W	31° 42' 45.87" N	Yes	Yes
B-12	542.2	42.2	500	96°55'35.80" W	31° 42' 32.80" N	Yes	No
B-13	550.3	75.3	475	96°55'13.74" W	31° 42' 23.02" N	No	Yes
B-14	540.0	65.0	475	96°55'27.42" W	31° 42′ 36.95″ N	No	Yes
B-15	565.0	65	500	96°55'18.91" W	31° 42' 41.23" N	Yes	No
B-16	557.7	57.7	500	96°55'49,40" W	31° 42′ 17.53" N	Yes	No
B-17	542.5	67.5	475	96°55'44.44" W	31° 42' 22.90" N	No	Yes
B-18	532.3	57.3	475	96°55'27.00" W	31° 42′ 28.96″ N	No	Yes
B-19	560.1	85.1	475	96°55'21.32" W	31° 42′ 31.48″ N	No	Yes
B-20	567.4	67.4	500	96°55'14.49" W	31° 42′ 34.93″ N	Yes	No
B-21	538.8	38.8	500	96°55'21.94" W	31° 42′ 22.76″ N	Yes	No
B-22	558.7	83.7	475	96°55'9.32" W	31° 42′ 28.73″ N	No	Yes
B-23	540.1	40.1	500	96°55'44.15" W	31° 42' 01.89" N	Yes	No
B-24	533.6	58.6	475	96°55'37.79" W	31° 42' 05.18" N	No	Yes
B-25	530.4	30.4	500	96°55'31.84"W	31° 42' 08.22" N	Yes	No
B-26	528.1	28.1	500	96°55'20.63"W	31° 42′ 10.29″ N	Yes	No

TABLE 5. Tabulation of Proposed Soil Borings (See Figure 2) (Continued)

EDE = 505 feet msl

Boring Number	Surface Elevation (ft msl)	Depth bgs (feet)	Bottom Elevation (ft msl)	Longitude	Latitude	5 Feet Below EDE ?	30 Feet Below EDE?
B-27	549.8	49.8	500	96°55'7.56" W	31° 42' 20.70" N	Yes	No
B-28	530.0	55.0	475	96°55'25.77" W	31° 41′ 59.98″ N	No	Yes
B-29	540.9	40.9	500	96°55'5.45" W	31° 42' 10.40" N	Yes	No
B-30	543.8	43.8	500	96°55'13.67" W	31° 42' 05.60" N	Yes	No
B-31	535.8	60.8	475	96°55'36.34" W	31° 42' 16.20" N	No	Yes
B-32	524.0	24.0	500	96°55'22.49" W	31° 41' 52.18" N	Yes	No
B-33	540.1	40.1	500	96°55'14.49" W	31° 42' 00.02" N	Yes	No
B-34	538.8	38.8	500	96°55'7.47" W	31° 42' 04.37" N	Yes	No
B-35	550.1	50.1	500	96°55'14.95" W	31° 42' 17.03" N	Yes	No
B-36	520.1	45.1	475	96°55'21.25" W	31° 41' 44.45" N	No	Yes
B-37	525.7	50.7	475	96°55'9.75" W	31° 41' 54.45" N	No	Yes
B-38	530.6	55.6	475	96°55'2.11" W	31° 41′ 58.73″ N	No	Yes
B-39	520.1	45.1	475	96°55'4.12" W	31° 41' 47.19" N	No	Yes
B-40	520.0	20.0	500	96°54'55.18" W	31° 41' 49.01" N	Yes	No
B-41	534.6	59.6	475	96°54'58.94" W	31° 42' 10.80" N	No	Yes
B-42	522.3	22.3	500	96°55'2.27" W	31° 41' 52.71" N	Yes	No
B-43	523.6	48.6	475	96°55'01.00" W	31° 42' 20.59" N	No	Yes
B-44	551.2	76.2	475	96°55'51.63" W	31° 42' 08.74" N	Yes	Yes
B-45	547.7	47.7	500	96°55'24.97" W	31° 42′ 32.26″ N	Yes	No
B-46	560.1	60.1	500	96°55'14.42" W	31° 42' 29.45" N	Yes	No
B-47	530.1	55.1	475	96°55'28.39" W	31° 42' 04.16" N	No	Yes

B - indicates borehole location

TABLE 6. Proposed Boring Coordinates (See Figure 2)

Boring Number	Northing	Easting
B-1 (A-1)	10599904.81	3353867.3
B-2 (A-2)	10598697.55	3354595.81
B-3 (A-3)	10597665.32	3355259.69
B-4 (A-4)	10599528.02	3355130.33
B-5 (A-5)	10600728.27	3355913.87
B-6	10602041.85	3355562.957
B-7	10599929.57	3356670.828
B-8	10599489.18	3357935.817
B-9	10599314.37	3355762.305
B-10	10602404.05	3356199.158
B-11	10602933.53	3357047.997
B-12	10601574.98	3355833.068
B-13	10600645.61	3357768.091
B-14	10602016.3	3356543.767
B-15	10602471.11	3357265.269
B-16	10599996.76	3354706.007
B-17	10600519.55	3355568.959
B-18	10601210.43	3356604.769
B-19	10601479.99	3357087.392
B-20	10601846.53	3357666.418
B-21	10600597.63	3357060.87
B-22	10601234.03	3358132.028
B-23	10598431.01	3355207.682
B-24	10598780.11	3355746.691
B-25	10599102.89	3356251.059
B-26	10599457.29	3356929.036
B-27	10600427.67	3358308.895
B-28	10598286.72	3356800.71
B-29	10599392.97	3358523.03
B-30	10598886.39	3357828.13
B-31	10599896.96	3355837.802
B-32	10597864.54	3357077.273
B-33	10598320.64	3357774.619
B-34	10598778.59	3358367.308
B-35	10600037.42	3357682.178

TABLE 6. Proposed Boring Coordinates (See Figure 2) (Continued)

Boring Number	Northing	Easting
B-36	10596730.18	3357239. 121
B-37	10597770.64	3358201.19
B-38	10598223.17	3358847.638
B-39	10597052.31	3358709.871
B-40	10597259.85	3359476.221
B-41	10599450.64	3359083.912
B-42	10597484.34	3358523.734
B-43	10597783.63	3359150.691
B-44	10599103.09	3354540.616
B-45	10601549.1	3356769.826
B-46	10601293.23	3357689.447
B-47	10598701.96	3356561.531

Mr. Chance Goodin August 14, 2018 *Revised September 7, 2018* Page 9

CONCLUSION

We believe the existing site soil borings used in combination with the additional soil borings and piezometers will sufficiently characterize the site geology, hydrogeology, and engineering properties of the surface and subsurface strata at the site in accordance with 30 TAC 330.63(e)(4) and (5).

Please contact Jim Lawrence at (817) 358-6106 if you have comments or require additional information.

Sincerely,

James Lawrence, P.G.

Manager, Groundwater Services

SCS ENGINEERS

TBPE Registration No. F-3407

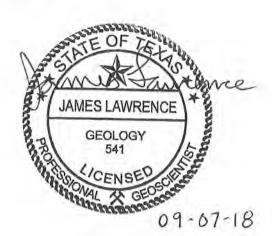
Ryan Kuntz, P.E. Project Director SCS ENGINEERS

Attachments: Figure 1: Area Map

Figure 2: Soil Boring Plan

cc: Charles Dowdell, City of Waco

TCEQ Regional Office 9 Kevin D. Yard, P.E., BCEE



Mr. Chance Goodin August 14, 2018 *Revised September 7, 2018* Page 10

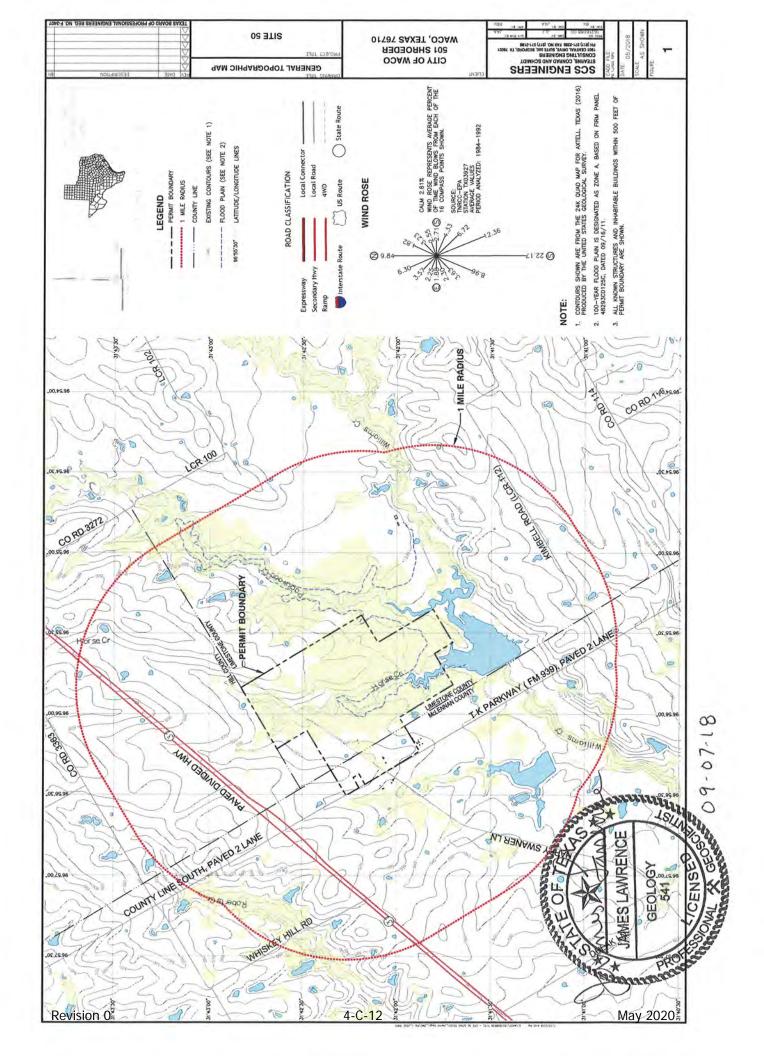
REFERENCES

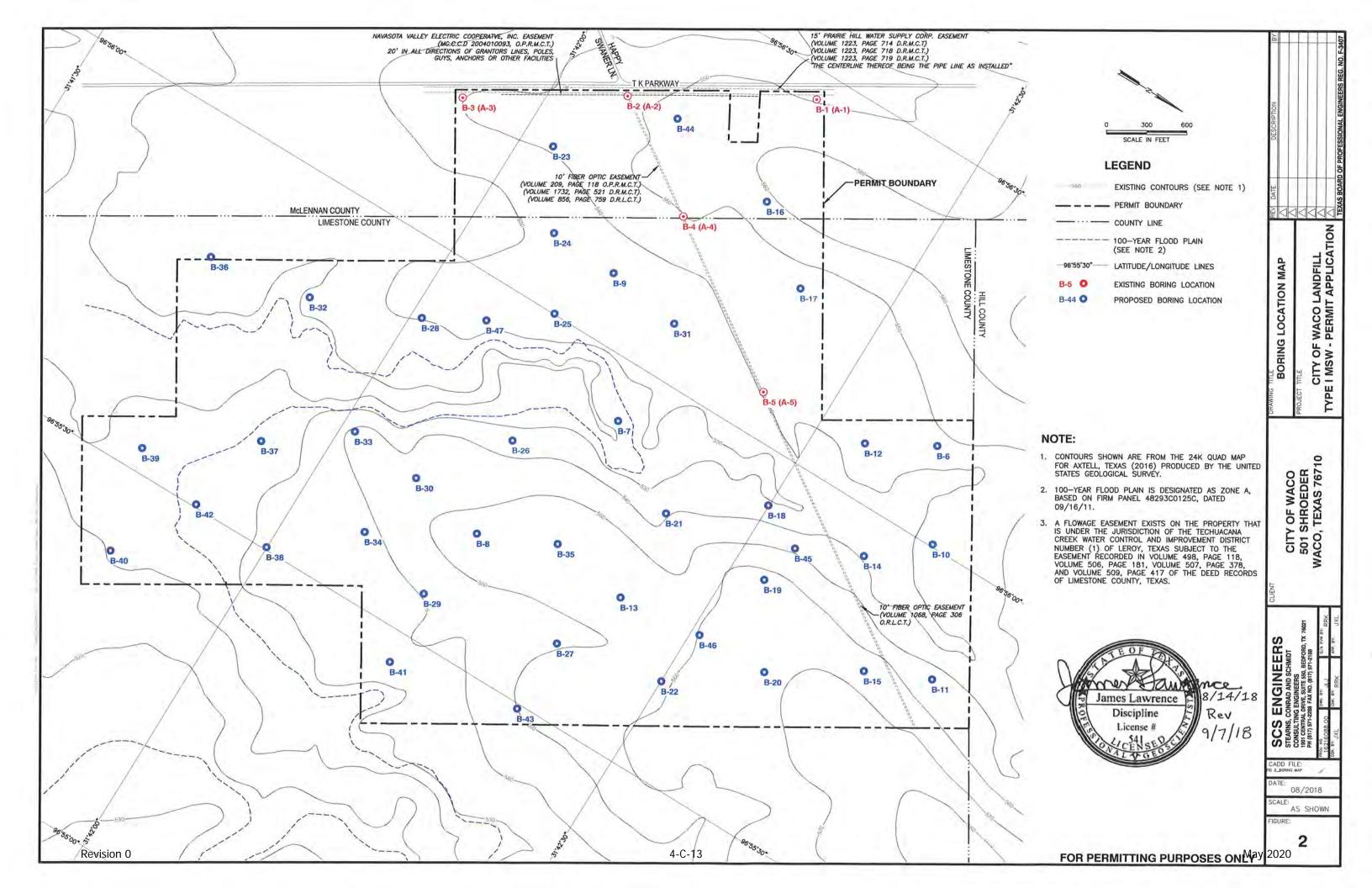
Baker B., Duffin, G., Flores, R., and Lynch, T, Evaluation of Water Resources in Part of Central Texas, Texas Water Development Board Report 319, 1990.

Flawn, P. Geologic Atlas of Texas—Waco Sheet. Bureau of Economic Geology, The University of Texas at Austin. 1970.

U.S. Department of Agriculture, Soil Survey of Limestone County, 1991.

U.S. Department of Agriculture, Soil Survey of McLennan County, 1992





APPENDIX III-4.D BORING LOGS



SCS Engineers 1901 Central Dr Ste. 550 Bedford, TX 76021

CLIENT City of Waco

PROJECT SYMBOL LEGEND

PROJECT NAME City of Waco Landfill

MSW-2400 PROJECT LOCATION Axtell, Texas **PROJECT NUMBER** 16216088.00

MATERIAL GRAPHICS

CH: USCS High Plasticity Clay



CL: USCS Low Plasticity Clay



CL-ML: USCS Low Plasticity Silty Clay



CLS: USCS Low Plasticity Sandy Clay





LIMESTONE: Limestone



MH: USCS Elastic Silt



ML: USCS Silt



NO CORE



SC: USCS Clayey Sand



May 2020

SHALE: Shale

SP: USCS Poorly-graded Sand



SP-SC: USCS Poorly-graded Sand with Clay



TOPSOIL: Topsoil

Sample Type



SPT: Standard Penetration Test



ST: Shelby Tube

NOTE: If no symbol for sample type is shown: Sample Type = NXCB

	1901 C Bedford	entral Dr d, Texas one: 817	ive S 7602	TE 550 1						BORING NUMB	ER B-	I (A-1) PAGE 1 OF	: 3
	CLIEN	T City o	f Wa	00					PROJECT NAI	ME City of Waco Landfill MSW	-2400		
	PROJE	ECT NUM	IBER	16216088.00					PROJECT LO	CATION Waco, Texas			
	DATE	STARTE	D 1/	25/18	COMP	LETED	1/26	6/18	GROUND ELE	VATION _551.67 ft	E SIZE 7.2	25 inches	
				CTOR West Drillin									
				Hollow stem auge						OF DRILLING No Groundy	vater		
				lbrand			7 .1 1	awrence		OF DRILLING No Groundy			
	NOTES									DRILLING No Groundwater			
	о ОЕРТН (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG			I	MATERIAL DESCRIPTION			
		ST1	75	PP = 3.5 tsf 0-16 feet logged	sc	71 7		(SC)					
		311	75	from previous		1/ 1//	2.0		ous log drilled 1/2				549.7
		ста	ΕO	drilling in January 2018				(CH) Clay, o	lark brown, hard	, moist, calcareous			
		ST2	50	PP = 4.5+ tsf	1			Pebbles 2-4	ft				
	 5	СТЗ	50	DD - 4.5. tof									
		ST3	50	PP = 4.5+ tsf				Color obono	o to light brown	at 6 ft			
.GPJ					1			Color chang	e to light brown	at o it			
ACO		ST4	75	PP = 4.5+ tsf	CH								
50 W								Color chang	e to brown-grey	at 8 ft			
SITE	 10	ST5	80	PP = 4.5+ tsf									
CTS	_ 10 _			PP = 4.5+ tsf				Color chanc	a ta raddish bra	wn at 10 ft			
SOJE		ST6	85	MC = 31% LL = 83			40.0	Color Chang	e to reddish brov	wir at 10 it			- 20 -
T/PF				PI = 58	\vdash		12.0	(CH) Clay, r	eddish brown, w	ith gray sand, soft, moist		;	539.7
MGIN		ST7	95	PP = 4.5+ tsf				, , ,					
Ä				PP = 4.5+ tsf	СН								
SABE	15	ST8	95	MC = 30% LL = 89									
ENŢ				PI = 63	 		16.0	(CH) Clay (irev to brown wi	th silty sand lenses, hard, moist			535.7
COM		ST9	80	PP = 4.5+ tsf					-	arrolly barra forfices, flara, filolog			
C/DC				PP = 4.5+ tsf	СН			Fossii fragm	ents 16-18 ft				
UBLI		ST10	90	MC = 22%									
RS/P	_ 20 _			LL = 79 PI = 56	 		20.0	(SC) Clayou	sand grov to da	ark grey, clay is reddish brown,	oft cliabtly		531.7
\USE		ST11	50	PP = 4.5+ tsf							soit, slightly	Saturateu	
3-C					sc			Quartz and	calcite pebbles t	hroughout			
14:3		ST12	70	PP = 4.5+ tsf									
25/19							24.0	(CLI) Clave		المعاد والمعاد والأرب والمعاد			527.
T - 4/	25	ST13	80	PP = 4.5+ tsf	СН					brown, with sand lenses, hard, r	noist		
3.GD							26.0		s are saturated quartz pebbles tl	proughout		_ !	525.7
SLA		ST14	70	PP = 4.5+ tsf	СН				· · · · · · · · · · · · · · · · · · ·	ith grey sand, soft, saturated		/	
TD U					J		28.0	, , ,				<u>_ </u>	523.7
NT S		ST15	50	PP = 4.5+ tsf				Calcite and	quartz throughou	ut			
<u>-</u> -	30	0110	50	11 - 4.01 (3)				Unweathere	d shale begins a	at 28 ft		Weathered	
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 4/25/19 14:33 - C:\USERS\PUBLIC\DOCUMENTS\BENTLEY\G\NT\PROJECTS\SITE 50 WACO. GPJ	<u> </u>									c gray, very stiff to hard, hard, c	alcareous	Unweathered	
TP /	_ 1							Fossil fragm	ents throughout				
BH/			100	MC = 14% LL = 66				_	_				
RAL	7			PI = 43				Slity sand le	nses throughout				
3ENE	35												
∪		Revisio	n 0	1				4-[)-3	(Continued Next Page)	May	2020	

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

BORING NUMBER B-1 (A-1) PAGE 2 OF 3

CLIENT City of \	Waco		PROJECT NAME _City of Waco Landfill MSW-2400
PROJECT NUMB	ER 16216088.00		PROJECT LOCATION Waco, Texas
GE DEPTH (ft) (ft) SAMPLE TYPE/NUMBER	% TESTS AND REMARKS	U.S.C.S. GRAPHIC	MATERIAL DESCRIPTION
	00		Silty Clay Shale, gray to dark gray, very stiff to hard, hard, calcareous Fossil fragments throughout Silty sand lenses throughout (continued)
	98 MC = 14% LL = 73 PI = 52		
	35		
55 55 60 70 70 70 75 75 75 75 75 75 75 75 75 75 75 75 75	94		
5 60	81		
5	MC = 18% LL = 72 PI = 52		
1	000		
75	92		
Revision	U		4-D-4 (Continued Next Page) May 2020

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

BORING NUMBER B-1 (A-1)

PAGE 3 OF 3

CLIENT City of Waco

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 4/25/19 14:33 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ

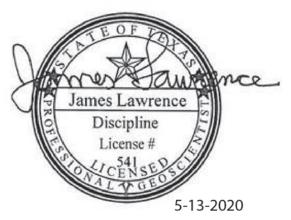
PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00

PROJECT LOCATION Waco, Texas

(f) 75	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S. GRAPHIC LOG	MATERIAL DESCRIPTION	
 80		27			Silty Clay Shale, gray to dark gray, very stiff to hard, hard, calcareous Fossil fragments throughout Silty sand lenses throughout <i>(continued)</i>	
		100			82.0	469.7

Bottom of borehole at 82.0 feet.



Revision 0 4-D-5 May 2020

	ENGIN								WELL N	IUME	BER E	3-1 (PZ-1)
	Central Dr rd, Texas											PAGE 1 OF 2
	none: 817											
CLIEN	AT City	f \//~-	20					DDO IECT NAME CIT	of Macal andfill M	16/1/ 242	0	
1	NT <u>City o</u>							PROJECT NAME City PROJECT LOCATION		1377-240	U	
1			16216088.00	COMP	ETER	10/4/	18	_		NUI E 61.	7E 0.05	inches
			<u>/4/18</u> C TOR BEST Drilli							IULE 31	<u>0.25</u>	1110105
1			•	_						ındıcts		
			Continuous Fligh			, , .		AT TIME OF DRIL				
		ı. Der	stine	CHEC	LED BY	r <u>J. Lá</u>	awrence		-			
NOTE								$ \underline{Y}$ AFTER DRILLING	21.38 π / Elev 5	30.32 ft		
O DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	REMARKS	U.S.C.S.	GRAPHIC LOG			MATERIAL DESCRIPTI	ON		WEI	LL DIAGRAM
					12 1/1/2		Silty Clay, d	ark brown, slightly moist to	o moist, soft			
_	1				1/ 1//	2.0				549.7		
]						(CL-ML) Silt	y Clay, red/orange to brown to stiff, with orange stair	vn, slightly moist			
							to moist, iiff	i to sun, with brange stair	mig in joints			
5												
<u> </u>												
01 01 01 01 01 01 01 01 01 01 01 01 01 0]			_								
				CL-								
10				-								
3[]											
]											
]											
15	1					15.0				536.7		
							Silty Clay SI	nale, orange-brown mottle	d brown, slightly	300.1		
-	1		MC = 23%				ITIOIST, STITT, I	non-calcareous, very weat	nerea			
	1	12	LL = 75									
-	1		PI = 53									
20	1		Fines = 93%									
j 20	\forall							e to orange-brown mottled	d tan to light gray		目	
-						$ar{ar{A}}$	and calcare	ous at 20 feet		:		
<u>'</u>	†	90										
<u>-</u>	1											
										1		
25	H			+								
}-											目	
} -		22										
<u>-</u>		32	Weathered to			28.0	Silty Clay SI	nale, gray to dark gray, ve	ry stiff to hard	523.7		
-			Unweathered zone				slightly mois	t to dry, calcareous, unwe	eathered	-		
30	\sqcup		20116	_			Slight orang	e staining in joints 30-39 f	eet.		目	
							Jugin Jidily				目	
-												
20 25 25 30 30 35		60										
; 												
35							<u> </u>	. ,				
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WELL NUMBER B-1 (PZ-1) PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021

Telephone: 817-571-2288

CLIENT City of Waco

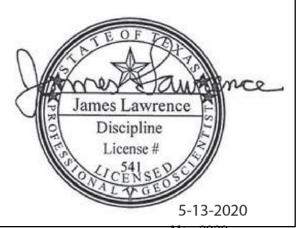
PROJECT NAME _ City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00

PROJECT LOCATION Waco, Texas

			10210000.00			11100201 2007111011	
(#) 25	SAMPLE TYPE/NUMBER	RECOVERY %	REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
		107	MC = 19% LL = 69 PI = 45 Fines = 97%			Silty Clay Shale, gray to dark gray, very stiff to hard, slightly moist to dry, calcareous, unweathered Slight orange staining in joints 30-39 feet. (continued)	

Bottom of borehole at 39.0 feet.



May 2020

Revision 0

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ

4-D-7

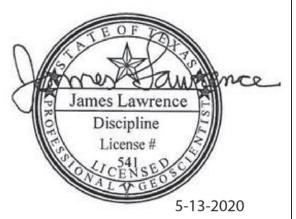
ion ()

SCS ENGINEERS **BORING NUMBER B-2 (A-2)** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 1/22/18 **COMPLETED** <u>1/23/18</u> GROUND ELEVATION 549.78 ft HOLE SIZE 7.25 inches DRILLING CONTRACTOR West Drilling **GROUND WATER LEVELS:** DRILLING METHOD Hollow stem auger/air rotary AT TIME OF DRILLING _--- No water LOGGED BY T. Millbrand CHECKED BY J. Lawrence AT END OF DRILLING _--- No water **NOTES** AFTER DRILLING ---TYPE/NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG SAMPLE RECOVERY DEPTH (ft) U.S.C.S. **TESTS** MATERIAL DESCRIPTION (SC) Topsoil, dark brown, soft, dry ST1 100 PP = 0 tsfSC 11. 111 2.0 547.8 No Recovery 545.8 (GW-GM) Gravel, with dark brown silt, loose, moist 4-5-7 GW-100 (12)GM 544.3 2 inch limestone layer at 5.5 feet 6-8-11 BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 100 (CH) Clay, dark gray, hard, moist, calcareous (19)Color change to mottled gray/brown at 6 feet ST2 100 PP = 4.5+ tsf 10 Color change to brown at 8 feet PP = 4.5+ tsf Limestone pebbles 8-12 ft MC = 20%ST3 100 LL = 71 537.8 PI = 51 (CH) Clay, brown, with fine sand, hard, moist 100 ST4 PP = 4.5 + tsfColor change to reddish brown at 14 feet 15 ST5 100 PP = 4.5 + tsfPP = 4.5+ tsf Color change to brown at 16 feet MC = 18%ST6 100 Limestone pebbles 16-18 feet LL = 69 PI = 48ST7 100 PP = 4.5 + tsf20 100 PP = 4.5 + tsfST8 527.8 (CH) Sandy Clay, brown/grey, hard, moist, calcareous ST9 100 PP = 4.5 + tsf25 Calcite and quartz throughout 24-26 ft ST10 100 PP = 4.5 + tsfST11 100 PP = 4.5 + tsfPP = 4.5 + tsfST12 100 30 PP = 4.5+ tsf MC = 21% ST13 100 LL = 74 Color change to brown at 32 feet PI = 52ST14 100 PP = 4.5 + tsf

4-D-8

Revision 0

BORING NUMBER B-2 (A-2)
PAGE 2 OF 2 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas SAMPLE TYPE/NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY DEPTH (ft) U.S.C.S. **TESTS** MATERIAL DESCRIPTION 35 PP = 4.5+ tsf 100 ST15 Color change to dark brown at 36 feet Shale pieces throughout 36-38 feet СН ST16 100 PP = 4.5 + tsf511.8 Shale, dark grey, with limestone lenses throughout, hard, calcareous ST17 188 PP = 4.5 + tsf40 90 45 MC = 13% 100 LL = 56 PI = 36 50 100 55 494.8 Bottom of borehole at 55.0 feet.



Revision 0 4-D-9 May 2020

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C.;USERS\PUBLIC:DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ

BORING NUMBER B-3 (A-3) ENGINEERS 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 1/31/18 **COMPLETED** 1/31/18 **GROUND ELEVATION** 541.1 ft HOLE SIZE 7.25 inches **DRILLING CONTRACTOR** West Drilling **GROUND WATER LEVELS:** DRILLING METHOD Hollow stem auger/air rotary AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Millbrand CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY DEPTH (ft) **TESTS AND** MATERIAL DESCRIPTION **REMARKS** Topsoil ST1 50 PP = 4.5 + tsf1/ 1/1/ 2.0 539.1 Clay, brown/redbrown, with chalk layers, moist, hard ST2 100 PP = 4.5 + tsfPebbles 2-4 ft 5 ST3 80 PP = 4.5 + tsfST4 90 PP = 4.5 + tsf8.0 533.1 Clay, mottled red/gray/brown, with saturated fine sand layers, hard, moist ST5 100 PP = 4.5 + tsfIncreasing hardness with depth 10 ST6 90 PP = 4.5 + tsfST7 100 PP = 4.5 + tsf15 ST8 100 PP = 4.5 + tsfST9 100 PP = 4.5 + tsfST10 80 PP = 4.5 + tsf20 100 PP = 4.5 + tsf70 PP = 4.5 + tsf25 Mineral deposits at 26 ft ST13 90 PP = 4.5 + tsfST14 100 PP = 4.5 + tsf30 Shale pieces at 30 ft 100 ST15 PP = 4.5 + tsf32.0 Weathered 509.1 Sand, brown/gray, with minor clay and mineral deposit layers, saturated, soft ST16 100 PP = 4.5 + tsf34.0 507.1 No Recovery Revision 0 4-D-10 May 2020 (Continued Next Page)

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 4/25/19 14:14 - C.\USERSIPUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GP.

BORING NUMBER B-3 (A-3) 1901 Central Drive STE 550 PAGE 2 OF 2 Bedford, Texas 76021 Telephone: 817-571-2288 **CLIENT** City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas SAMPLE TYPE/NUMBER RECOVERY **TESTS** AND MATERIAL DESCRIPTION **REMARKS** 35 No Recovery (continued) 38.0 503.1 PP = 4.5+ tsf Shale, dark gray to black, hard, dry, calcareous, with limestone and Unweathered Weathered to 100 fine sand layers up to 1/8" thick unweathered zone Very little sand 40-45 feet 98 Limestone layer 1/2 thick at 45 feet 45 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 4/25/19 14:14 - C:USERSIPUBLIC/DOCUMENTS/BENTLEY/GINT/PROJECTS/SITE 50 WACO.GPJ 97 50 100 55 100 James Lawrence Discipline 60 98 5-13-2020 65 More sand layers 1/8" thick throughout at 65 feet 98 70 Fossil fragments 70-72 feet. 100 469.1 Bottom of borehole at 72.0 feet.

SCS ENGINEERS **WELL NUMBER B-3 (PZ-3)** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 10/10/18 **COMPLETED** 10/10/18 **GROUND ELEVATION** 541.1 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine **CHECKED BY** J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater TYPE/NUMBER GRAPHIC LOG RECOVERY SAMPLE DEPTH (ft) U.S.C.S. **TESTS AND** MATERIAL DESCRIPTION WELL DIAGRAM **REMARKS** Blind Drill 5 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 10 15 20 521.1 (SP-SC) Sand, brown, soft, moist to wet, with traces of SPclay, fine to medium grained SC 518.5 52 √518.3 Silty Clay, dark brown, hard to stiff, moist (CL) Silty Clay, orange-brown mottled brown, hard, slightly moist, calcareous, with weathered shale 25 CL MC = 18% 514.1 LL = 60Silty Clay Shale, gray with orange-brown staining, very 78 hard, slightly moist, calcareous, with mineral desposits PI = 36in fractures, weathered Fines = 93% 30 74 No mineral deposits 35-39 feet

4-D-12 (Continued Next Page)

May 2020

Revision 0

WELL NUMBER B-3 (PZ-3) PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00 PROJECT LOCATION Waco, Texas

FIC	JECT NON	IDLI	102 10000.00			FROSECT EGGATION Waco, Texas	
S DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
40	- - - - - -	56 70	Weathered to Unweathered zone MC = 16% LL = 63 PI = 43 Fines = 96%	,		Silty Clay Shale, gray with orange-brown staining, very hard, slightly moist, calcareous, with mineral desposits in fractures, weathered No mineral deposits 35-39 feet (continued) Silty Clay Shale, dark gray, very hard, slightly moist to dry, calcareous, unweathered 45.0	
						Dettem of berehele at 45.0 feet	

Bottom of borehole at 45.0 feet.



May 2020 Revision 0 4-D-13

SCS ENGINEERS **BORING NUMBER B-4 (A-4)** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 1/23/18 **COMPLETED** <u>1/23/18</u> **GROUND ELEVATION** 550.04 ft HOLE SIZE 7.25 inches **DRILLING CONTRACTOR** West Drilling **GROUND WATER LEVELS:** $\sqrt{2}$ AT TIME OF DRILLING 48.77 ft / Elev 501.27 ft **DRILLING METHOD** Hollow stem auger/air rotary **T** AT END OF DRILLING 96.59 ft / Elev 453.45 ft LOGGED BY T. Millbrand CHECKED BY J. Lawrence **NOTES** AFTER DRILLING _--- No Groundwater TYPE/NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY SAMPLE DEPTH (ft) U.S.C.S. **TESTS** AND MATERIAL DESCRIPTION **REMARKS** (SC) Topsoil/Fill material ST1 75 PP = 0 tsfSC 11/ 2.0 548.0 Topsoil/Fill material, with dakr brown clay, soft, moist 2-3-5 SPT1 75 (8) 546.0 (CH) Clay, dark brown, hard, moist, calcareous 5 ST2 50 PP = 4.5 + tsfBH / TP / WELL - GINT STD US LAB.GDT - 4/25/19 14:14 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GP\ ST3 75 PP = 4.5 + tsfColor change to light brown at 8 feet ST4 PP = 4.5 + tsf50 Pebbles throughout 8-10 ft 10 PP = 4.5+ tsf MC = 21%50 ST5 LL = 75 PI = 51 ST6 70 PP = 4.5 + tsf15 60 PP = 4.5 + tsfST7 Color change to mottled brown/grey at 16 feet ST8 80 PP = 4.5 + tsfSand lenses throughout 18-20 feet ST9 75 PP = 4.5 + tsf20 ST10 PP = 4.5 + tsf80 PP = 4.5+ tsf MC = 21% ST11 11 = 74PI = 5325 ST12 80 PP = 4.5 + tsfST13 80 PP = 4.5 + tsf522.0 PP = 4.5+ tsf Clayey shale, dark grey, fissile, calcareous

Sand lenses throughout Fossil fragments throughout

Shale, dark grey to black, with limestone lenses, hard, calcareous

520.0

30.0

ST14

ST15

30

50

100

85

Weathered to

unweathered

zone

PP = 4.<u>5+ tsf</u>

MC = 13%

LL = 55 PI = 37

BORING NUMBER B-4 (A-4) PAGE 2 OF 3

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

ГССР	none: 81	7-57 1-	2200				
	IT <u>City o</u>			00			PROJECT LOCATION Waco Toyas
PROJ		IBER	16216088	.00			PROJECT LOCATION Waco, Texas
DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
							Shale, dark grey to black, with limestone lenses, hard, calcareous
40		98					Sand lenses throughout Fossil fragments throughout (continued)
45		98			-		
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 4/25/19 14:14 - C:\USERS\PUBLIC\DOCUMENT\PRO\GINT\PRO		98		MC = 13% LL = 62 PI = 44	-		⊻
ENIS/BENILE Y/GINI/PH		98					
NUSERS/PUBLIC/DOCUM		98			-		
B.GDI - 4/25/19 14:14 - C		97			_		
/WELL - GINT STD US LAB		98			-		
GENERAL BH / TP	Revisio	98 on 0					4-D-15 (Continued Next Page) May 2020

BORING NUMBER B-4 (A-4)
PAGE 3 OF 3

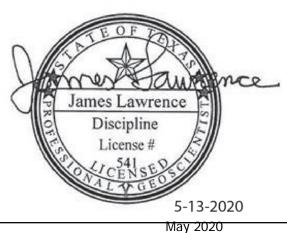
1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00 PROJECT LOCATION Waco, Texas

	PROJI	ECT NUM	IBER	16216088	.00			PROJECT LOCATION Waco, Texas
	DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
Ī	70							Shale, dark grey to black, with limestone lenses, hard, calcareous
Ī						1		Sand lenses throughout Fossil fragments throughout <i>(continued)</i>
	_							Fossil fragments throughout (continued)
			100					
-	80							
-	- +					-		
ŀ								
Į			98					
	85							
2	-			-		-		
\CO.G								
50 W			99		MC = 14% LL = 74			
SSITE	90				PI = 53			
JECTS	_]							
INPRO								
V\GIN_			100					
NTLE	 95 _		100					
ITS/BE	_ 95 _							
UMEN	_]							Ā
Spoc	-							
UBLIC			99					
ERS/F	100_							140
C:\US								101.0 449.0 Bottom of borehole at 101.0 feet.
4:14 -								
5/19 1								
T - 4/2!								EOFT
B.GD								
US LA								mer du noce
TSTD								James Lawrence
- GIN								Discipline
WELL								Discipline License #
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 4/25/19 14:14 - C.\USERS\PUBLIC\DOCUMENTS\BENTLE\MGINT\PROJECTS\SITE 50 \WACO.GPJ								1,541,686
¹L BH								VAL TO GEOS
ENER/								5-13-2020
ਹ		Revisio	n 0					4-D-16 May 2020



Revision 0

SCS ENGINEERS **BORING NUMBER B-5 (A-5)** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 1/25/18 **COMPLETED** 1/25/18 **GROUND ELEVATION** 541.38 ft HOLE SIZE 7.25 inches **DRILLING CONTRACTOR** West Drilling **GROUND WATER LEVELS: DRILLING METHOD** Hollow stem auger/air rotary AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Millbrand CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater, but muddy probe **NOTES** AFTER DRILLING _--- No Groundwater TYPE/NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY DEPTH (ft) U.S.C.S. **REMARKS** MATERIAL DESCRIPTION (SC) Topsoil/ Fill Material 4-11-10 SPT 90 SC 11.11 (21)No recovery 1.5-2 feet 2.0 539.4 Fill Material 4-7-8 SPT2 (15)No recovery 3.5-4 537.4 Fill material, dark brown, with clay, hard, moist 5 4-6-8 SPT3 50 (14)No reocvery 5.5-6 feet 535.4 (CH) Clay, light brown, with fill material, hard, moist, calcareous GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 4/25/19 14:14 - C:USERSIPUBLICIDOCUMENTSIBENTLEY.GINTNPROJECTSISITE 50 WACO.GP. ST1 60 Color change to mottled brown/grey at 8 feet ST2 40 10 531.4 (CH) Clay, mottled light brown/grey, with fine sand, hard, moist, ST3 70 calcareous MC = 16% ST4 100 LL = 62 Color change to light reddish brown at 14 feet PI = 41 15 ST5 40 ST6 40 523.4 (CH) Clay, reddish brown, with grey sand, hard, moist, calcareous ST7 60 Calcite and Quartz throughout 20 ST8 95 MC = 18% ST9 LL = 66 PI = 46 25 ST10 60 515.4 Shale, dark grey to black, with limestone lenses, hard, calcareous Weathered to 70 ST11 unweathered zone Silty sand lenses throughout ST12 50 Fossil fragments 30-35 feet 30 MC = 17%93 LL = 63PI = 42

4-D-17

Revision 0

BORING NUMBER B-5 (A-5) PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021

Telephone: 817-571-2288

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00

PROJECT LOCATION Waco, Texas

(#) (#)	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	
							Shale, dark grey to black, with limestone lenses, hard, calcareous	
40		100					Silty sand lenses throughout	
 45		95						
WACO.GP3		100					47.8 Rottom of borehole at 47.8 feet	493.6

Bottom of borehole at 47.8 feet.



May 2020 Revision 0 4-D-18

SCS ENGINEERS **BORING NUMBER B-6** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 10/25/18 **COMPLETED** <u>10/26/18</u> **GROUND ELEVATION** 545.55 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine **CHECKED BY** J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. SAMPLE DEPTH (ft) **TESTS AND** MATERIAL DESCRIPTION REMARKS (CL-ML) Silty Clay, brown to reddish brown with orange-brown staining, soft to stiff, moist, with traces of gravel, organic CL-50 ML 540<u>.6</u> 5 (CL-ML) Silty Clay, orange-brown mottled gray, hard, slightly moist, slightly calcareous 50 ST1 Chalk in fractures/joints 5-10 feet PP = 4.5 tsf45 10 CI -ML Silty lenses 10-15 feet 50 PP = 4.0 tsf50 15 530.6 (CL) Silty Clay, orange-brown mottled brown-tan with some gray, hard, slightly moist, slightly calcareous, with weathered shale 38 PP = 4.5 tsf 66 CL 20 29 ST4 22.5 523.1 PP = 4.5 + tsf70 Silty Shale, gray to dark gray, very hard, slightly moist, calcareous Weathered to Unweathered Orange-brown staining at 22.5-23.5 feet zone 25 21 ST5 PP = 4.5 + tsf84 30 Thin limestone layers in fractures at 30-50 feet 21 PP = 4.5 + tsf84 Revision 0 4-D-19 May 2020 (Continued Next Page)

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ

BORING NUMBER B-6 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS** AND REMARKS MATERIAL DESCRIPTION 35 Silty Shale, gray to dark gray, very hard, slightly moist, calcareous 17 PP = 4.5 + tsf98 40 80 45 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 21 ST8 PP = 4.5+ tsf 84 Shells at 50-51 feet 50 80 55 17 PP = 4.5 + tsf100 60 James Lawrence 94 Discipline License # 65 80 PP = 4.5+ tsf 5-13-2020 474.9 70.7 Bottom of borehole at 70.7 feet. 29 ST10 Revision 0 4-D-20 May 2020

SCS ENGINEERS **BORING NUMBER B-7** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas **DATE STARTED** 1/9/19 COMPLETED 1/9/19 **GROUND ELEVATION** 530.5 ft **HOLE SIZE** 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine CHECKED BY J. Lawrence AT END OF DRILLING --- No Groundwater ▼ AFTER DRILLING 31.00 ft / Elev 499.50 ft **NOTES LYPE/NUMBER** GRAPHIC LOG RECOVERY U.S.C.S. **TESTS AND** MATERIAL DESCRIPTION **REMARKS** (CL-ML) Silty Clay, dark brown to olive brown, soft to hard, moist, with trace gravel CL 62 ML 5 525.5 (CL-ML) Silty Clay, olive brown to brown with some orange-brown and gray mottling, firm to stiff, moist, with trace sub-angular gravel and pebbles CL-100 ML 10 520.5 (CL-ML) Silty Clay, orange-brown mottled gray and brown, stiff, slightly moist to moist, calcareous 50 CL-15 ML 52 511.5 Shale Marl, dark gray with trace of orange-brown mottling, hard to stiff, slightly moist, with silty/limey lenses, calcareous Weathered to unweathered transition zone 60 Weathered to 506.5 Unweathered Shale Marl, dark gray, hard, slightly moist, with silty/limey lenses and fossils, zone 25 calcareous, unweathered 60 30 Very wet zones 31-32 feet 86 May 2020 Revision 0 4-1)-21 (Continued Next Page)

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ

BORING NUMBER B-7

PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

PROJECT NUMBER 16216088.00

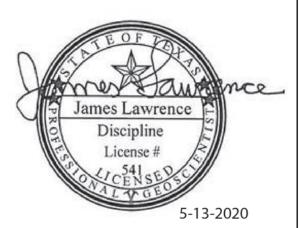
CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT LOCATION Waco, Texas

HTGD 35	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
 40		60				Shale Marl, dark gray, hard, slightly moist, with silty/limey lenses and fossils, calcareous, unweathered
 45		50				
150 DAW 06 = 50		80				
		50				55.0 475.5 Bottom of borehole at 55.0 feet.

Bottom of borehole at 55.0 feet.



4-D-22 May 2020 Revision 0

SCS ENGINEERS **WELL NUMBER B-8 (PZ-8)** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 11/27/18 **COMPLETED** <u>11/28/18</u> **GROUND ELEVATION** 550.8 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine **CHECKED BY** J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater TYPE/NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY SAMPLE DEPTH (ft) U.S.C.S. **TESTS** AND MATERIAL DESCRIPTION WELL DIAGRAM **REMARKS** Clayey Silt, dark brown, firm, moist, with roots and organics 111 1.5 549.3 (CL-ML) Silty Clay, gray to light gray, stiff to 100 hard, moist to slightly moist, with white calcareous chalky material Trace of light gravel and orange-brown 5 staining 6.5-10 feet CL-ML 38 11-20-23 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 100 (43)PP = 4.0-4.5+ tsf 100 10 10.0 540.8 (CL-ML) Silty Clay, orange-brown stained PP = 3.5 tsfgray and brown, stiff to hard, slighty moist, 50 ST2 calcareous, with white chalky material and 11 = 67silty gray interbeds 63 PI = 50Fines = 85% 15 CL-ML 33 20-26-35 ST3 100 (61)PP = 4.0-4.5 tsf 93 SPT2 20 530.8 Silty Clay (Weathered Shale Marl), orange-brown mottled gray and brown, hard, 21 ST4 slighty moist, calcareous 56 PP = 4.5 tsfWhite chalky material and silty gray interbeds 20-25 feet 25 29 18-29-43 100 (72)PP = 4.5-4.5 + tsf64 30 21 ST6 67 PP = 4.5 tsfCrystalline material in joints/bedding 35-43.8

May 2020

(Continued Next Page)

Revision 0

WELL NUMBER B-8 (PZ-8) 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas SAMPLE TYPE/NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY DEPTH (ft) U.S.C.S. **TESTS** AND MATERIAL DESCRIPTION WELL DIAGRAM **REMARKS** 35 Silty Clay (Weathered Shale Marl), orange-brown mottled gray and brown, hard, 15-24-28 21 (52)slighty moist, calcareous 100 100 PP = 4.0-4.5 + tsfSPT4 40 PP = 4.5 + tsf25 MC = 16% ST8 DD = 106 pcf LL = 58 68 PI = 38 43.8 507.0 Fines = 92% Silty Clay Shale Marl, gray, hard, slightly moist, calcareous, with silty/micaceous 45 Weathered to Unweathered lenses and fossil remnants in interbeds, zone unweathered 17 28-50 ST9 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\S\ITE 50 WACO.GPJ 78 Orange-brown staining 47-55 feet 100 PP = 4.5+ tsf SPT5 50 PP = 4.5 + tsf17 MC = 14% ST10 DD = 116 pcf 70 LL = 58 PI = 37Fines = 97% 55 ST11 17 SPT6 93 PP = 4.5 + tsf60 100 65 17 James Lawrence Discipline 61 PP = 4.5 + tsf70 5-13-2020 70

Revision 0

	ENGINE						WELL N	UMBER B-9 (PZ-9)			
	Engineer Central I							PAGE 1 OF 4			
Ste.	550										
	ord, TX 7							0)44 0 400			
- 1	NT City o						PROJECT NAME _ City of Waco Landfill M	SW-2400			
- 1											
							GROUND ELEVATION 535.3 ft	HOLE SIZE 8.25 inches			
- 1						ing					
		-	Continuous Flight								
- 1						D BY J. Lawrence					
NOTI	ES						AFTER DRILLING				
O DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION	WELL DIAGRAM			
	_	92		CL- ML		moist to moi and shells	y Clay, dark brown to gray, stiff, slightly ist, organic rich, with limestone fragments e to gray at 2.5 feet	n			
5	1					5.0		500.0			
_ 5	ST1	40	PP = 4.5+ tsf MC = 15%			5.0 (CL-ML) Silt hard, slightly	y Clay, light gray/tan mottled orange-brown, v moist, with minor sub-round gravel	530.3			
-	_	78	LL = 53 PI = 35 Fines = 75%	CL- ML							
10 - - -	ST2	36				Silty Clay St yellow-brown with trace of	nale, gray and orange-brown mottled n, hard, slightly moist to dry, calcareous, gravel	525.3			
ECTS/SITE 50 WACO.GPJ		44	PP = 4.5+ tsf			Chalk/limest	one in joints 15-20 feet	ш			
				1		Color chang	e to orange-brown mottled gray at 20 feet				
EY/GINT/PRC	ST3	24 57	PP = 4.5+ tsf			Limestone le	enses in fractures 25-28.5 feet	ш			
ERIE/BENT				_							
1:23 - L:\\AL	ST4	24 57	PP = 4.5+ tsf MC = 20% DD = 105 pcf LL = 67								
25 - TC			PI = 47 Fines = 91%			Σ					
US LAB.GI	ST5	20	PP = 4.5+ tsf								
GINT STD - 30		67	Weathered to Unweathered zone				nale, very hard, dry, calcareous, with ch lenses in fractures	506.8			
GENERAL BH / TP / WELL - GINT STD US LAB GDT - 2/5/20 11:23 - L:WALERIEBENTLEY/GINTPROJ	ST6	20	PP = 4.5+ tsf			Orange-brov	vn staining in joints 28.5-20 feet				
GENERAL 35	Revisio	on 0				4-D	-25 (Continued Next Page)	May 2020			

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SCS Engineers
1901 Central Dr
Ste. 550
Bedford, TX 76021

WELL NUMBER B-9 (PZ-9)
PAGE 2 OF 4

	α.	%							
35 35	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM
-	ST7	16	PP = 4.5+ tsf MC = 15% DD = 116 pcf LL = 62				Silty Clay Shale, very hard, dry, calcareous, with carbonate rich lenses in fractures		
40			PI = 42 Fines = 89%			40.0	40-45' no sample recovery	495.3	
- 45 - -		100				45.0	Shale with minor, very fine sand. Dark gray, hard to very hard, damp to moist, well laminated	490.3	
50		100		_					
- - - 55		100							
60		100	LL = 63 PI = 41 MC = 15% Fines = 99%				Obala with a single constant and Dark was a bould a surro		
- - - - 65		100					Shale with minor, very fine sand. Dark gray, hard to very hard, damp to moist, laminated		
- - - 70		100							
		100		-					

SCS ENGINEERS

SCS Engineers 1901 Central Dr

WELL NUMBER B-9 (PZ-9)
PAGE 3 OF 4

Ste. 550 Bedford, TX 76021

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

	ECT NUM		16216088.00			PROJECT LOCATION Waco, Texas	
DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
 80		100	LL = 64 PI = 42 MC = 14% Fines = 93%			75-80' small fossils present	
 85		100				Becoming harder with depth	
 90		100					
GENERAL BH / IP / WELL - GIN IS ID US LABS GIN - 25520 11:23 - 1:10 APL 10 APL 1		100				Fewer laminations with depth	
100 Y		100					
		100					
100 P P P P P P P P P P P P P P P P P P		100	LL = 73 PI = 51 MC = 15% Fines = 97%			Shale with minor, very fine sand. Dark gray, very hard,	
GENERAL BH / IB /	Revisio	100				moist, trace lamination 4-D-27 (Continued Next Page)	May 2020

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SCS Engineers 1901 Central Dr Ste. 550

WELL NUMBER B-9 (PZ-9)
PAGE 4 OF 4

Bedford, TX 76021 CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER _ 16216088.00

PROJECT LOCATION Waco, Texas

	FKOJE	LC1 NOW	IDEK	10210000.00			PROJECT LOCATION _Waco, Texas	
	DEPTH (#)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
	 120		100					
	 125		100				Becoming harder with depth	
	130		100				Fewer laminations with depth	
RIE/BENTLEY/GINT/PROJECTS/SITE 50 WACO.GPJ	 135		100	LL = 74 PI = 49 MC = 16% Fines = 89%			Shale with minor, very fine sand. Dark gray, very hard, moist, scarce lamination 400.3	
EY/GINT\PROJEC	100					•	Bottom of borehole at 135.0 feet.	
I:23 - L:\VALERIE\BENTL								
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/5/20 11:23 - L:\VALE							James Lawr Discipling License #	: JEM
GE		Revisio	n O				4-D-28	May 2020



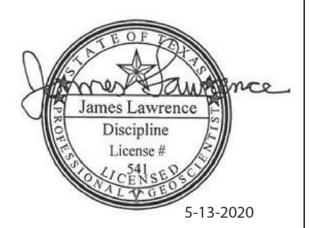
May 2020 Revision 0 4-D-28

1901	Central D	rive S	TE 550					BORING NUMBER B-10 PAGE 1 OF 1
	ord, Texas ohone: 81							
CLIE	NT City o	of Wa	co					PROJECT NAME _City of Waco Landfill MSW-2400
- 1			16216088	.00				PROJECT LOCATION Waco, Texas
- 1			2/13/18		D 12	2/13/18	3	
			CTOR BES					GROUND WATER LEVELS:
- 1				s Flight Auger				AT TIME OF DRILLING No Groundwater
				CHECKED	BY J	. Lawr	ence	AT END OF DRILLING No Groundwater
NOT								AFTER DRILLING No Groundwater
O DEPTH	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION
_					МН	Ш	1.0	(MH) Clayey Silt to Silty Clay, brown, soft to firm, moist, with roots and organics
-	-	80			CL- ML			(CL-ML) Silty Clay, brown, stiff, moist, with traces of sub-rounded gravel and roots
<u>ا</u> ۔	-						4.5	54
5								(CL-ML) Silty Clay, orange-brown mottled brown and gray, stiff, moist,
2	ST1	33 94	15-20-26					with silty to very fine sand lenses and white chalky material
0.0.6		94	(46)	PP = 4.0-4.5 tsf				
× -	SPT1	100		11 - 4.0-4.3 (3)				
E 50	-							
10_					-			
	_	33		PP = 4.5 tsf				
<u>8</u>	ST2			MC = 19%				
		71		LL = 65				
D X				PI = 41				
BENTLEYGINTIPROJECTSISITE 50 WACO.GPJ				Fines = 90%				
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C:\USERS\PUBLIC\DOCUMENTS\BE Column	ST3	100	20-30-37 (67)	PP = 4.0-4.5 tsf	CL- ML			
JSERS	-	21						
)- C:\	ST4	56	-	PP = 4.0-4.5 tsf				
15:50	-	30		FF = 4.0-4.5 (SI				
25	1							
TOS				PP = 4.0-4.5 tsf				
LAB.	ST5	21 100	17-27-34 (61)	MC = 15%				
I SN C	SPT3	100	(01)	DD = 108 pcf				
STD	-	.55		LL = 54				
- GINI	-			PI = 33 Fines = 94%				
30				1 11165 - 9470				
_ WE	-	21					1	Crystalline pockets 30-34 feet
T	ST6		_					
HH-	1	78		PP = 4.5 tsf				
Ā- ₹	1						34.0	51
ভ <u>35</u>	Povici)n ()					<u> </u>	T) 70 May 2020
	Revisio	ט ווע					4	-D-29 (Continued Next Page) May 2020

BORING NUMBER B-10 1901 Central Drive STE 550 PAGE 2 OF 2 Bedford, Texas 76021 Telephone: 817-571-2288 **CLIENT** City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas

SAMPLE TYPE/NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY DEPTH (ft) U.S.C.S. **TESTS** AND MATERIAL DESCRIPTION **REMARKS** 35 Shale Marl, gray, hard, slightly moist, with occasional orange-brown staining and silty lenses, calcareous, weathered Weathered to 36.0 512.0 21 Unweathered 50 ST7 zone 28 Transition zone (continued) 100 PP = 4.5 + tsfSPT4 Shale Marl, gray, hard, slightly moist, with fossil remnants and silty/limey lenses, calcareous, unweathered 40 PP = 4.5 + tsf17 MC = 14% ST8 LL = 59 87 PI = 39Fines = 92% 45 17 34-50 SPT5 95 50 33 495.0

Bottom of borehole at 53.0 feet.



Revision 0 4-D-30 May 2020

SCS ENGINEERS **BORING NUMBER B-11** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 **CLIENT** City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 11/5/18 **COMPLETED** <u>11/5/18</u> **GROUND ELEVATION** 553.5 ft HOLE SIZE 7.25 inches **DRILLING CONTRACTOR** West Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY A. Valerio CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS AND** MATERIAL DESCRIPTION **REMARKS** Topsoil, dark brown 1 0 552.5 (CL) Clay, dark brown to orange-tan, medium firm, with some organic material 95 CL 5 548.5 (CL) Clay, orange brown, very soft to very hard, dry, with minor silt GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ ST₁ PP = 0-4.5 + tsf100 CL 10 543.5 10.0 (CL) Clay, medium brown, firm to hard, dry, with minor orange silt 100 PP = 2.5-4.5 + tsf15 CL ST3 PP = 2.5-4.0 tsf 20 533.5 PP = 1.0-3.5 tsf (CL) Clay, medium to dark brown, firm to moderately firm, dry, with minor orange and gray silt MC = 21%ST4 DD = 95 pcf50 CL LL = 75 PI = 49Fines = 89% 25 528.5 (CL) Clay, dark gray, soft to very firm, dry, with minor orange silt PP = 0.5-4.5+ tsf ST5 Weathered to CL 93 Unweathered zone 30 523.5 (CL) Clay, very dark gray, very firm, with minor light gray silt and pebbles Sand/Silt parting at 33 feet PP = 4.0-4.5 + tsfCL 518.5 Revision 0 May 2020

4-1)-31

(Continued Next Page)

BORING NUMBER B-11

PAGE 2 OF 3

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

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Revision 0

CLII	ENT City	of Wa	00			PROJECT NAME City of Waco Landfill MSW-2400
PRO	PROJECT NUMBER _16216088.00					PROJECT LOCATION _Waco, Texas
DEPTH (#)	=	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
- - - 40	ST	7 75	PP = 2.0-4.5+ tsf			(CL) Clay, very dark gray, medium firm to very firm, dry, with some very dark gray weathered shale Minor silty sand 40-45 feet
- - - - 45	- - -	95				
SISITE 50 WACO.GPJ	ST	95	PP = 3.5-4.5+ tsf MC = 13% DD = 120 pcf LL = 55 PI = 33 Fines = 86%			
TP / WELL - GINT STD US LAB.GDT - 2/4/19 16:50 - C:\USERS\PUBLIC\DOCUMENT\S\BENTLE\Y\G\N\T\PROUGHT\PROUGT\PROUGT\PROUGT\PROUGT\PROUGT\PROUGT\PROUGT\PROUGT\PROUGT\PROUGT\PROUGT\PROUGT\PROUGT\PROUGT\P	- - -	75		CL		Limey, white, calcareous, pebbles up to 1/2" at 54 feet Minor calcareous silt with few pebbles up to 1/8" at 58 feet
RS/PUBLIC/DOCUMENTS/	ST	95	PP = 0.5-4.5 tsf			
IDT - 2/4/19 15:50 - C:\USE 	- - -	98				
- GINT STD US LAB.GI	- ST10	95	PP = 1.0-4.5+ tsf			Minor limey pebbles <1/8" at 67 feet
TP/WELL						Minor calcareous silt and pebbles <1/8" 70-75 feet

(Continued Next Page)

BORING NUMBER B-11

PAGE 3 OF 3

1901 Central Drive STE 550 Bedford, Texas 76021

Telephone: 817-571-2288

CLIENT City of Waco

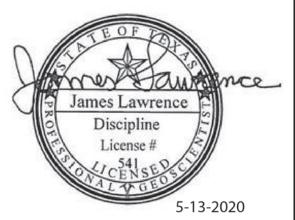
PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER _16216088.00

PROJECT LOCATION Waco, Texas

DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
 80		99		CL		80.0 473.5

Bottom of borehole at 80.0 feet.



May 2020

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ

SCS ENGINEERS **BORING NUMBER B-12** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 10/12/18 **COMPLETED** 10/12/18 **GROUND ELEVATION** 542.85 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine **CHECKED BY** J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS AND** MATERIAL DESCRIPTION REMARKS (CL-ML) Silty Clay, brown, soft to firm, slightly moist to moist Organic 0-5 feet 93 Shell fragments 3-5 feet Minor amounts of small sub-rounded gravel 3-10 feet 5 CL-Mineral deposits in joints/bedding 5-10 feet ML 38 PP = 4.5 + tsf68 10 532.9 10.0 (CL-ML) Silty Clay, orange-brown mottled gray, hard, slightly moist, with traces of roots/organics, calcareous 29 Mineral desposits in fractures and traces of gravel 10-15 feet PP = 4.5 + tsf50 Very fine sandy lenses in fractures 15-20 feet 15 ML 21 PP = 4.5+ tsf 50 20 (CL) Silty Clay, orange-brown mottled brown to light gray, hard, slightly moist, calcareous, with weathered shale ST4 Very fine sandy lenses 20-25 feet PP = 4.5+ tsf 60 CL 25 Weathered to 516.4 38 Unweathered ST5 Silty Clay Shale, dark gray, moderately to very hard, slightly moist, calcareous zone PP = 4.5+ tsf Sandy lenses 26.5-30 feet Trace of shell fragments 30-35 feet 30 17 ST₆ PP = 4.5 + tsf100 Revision 0 May 2020 4-1)-34 (Continued Next Page)

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ

BORING NUMBER B-12

PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

PROJECT NUMBER 16216088.00

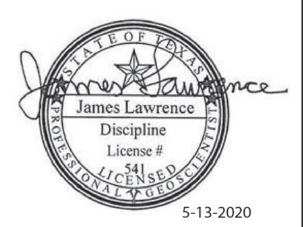
CLIENT City of Waco

PROJECT NAME _City of Waco Landfill MSW-2400

PROJECT LOCATION Waco, Texas

35 (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	
						Silty Clay Shale, dark gray, moderately to very hard, slightly moist, calcareous	
	ST7	21				Much softer and more calcareous 40-45 feet	
		50	PP = 3.5-4.5 + tsf			Very hard 45-48 feet	
40							
 45		66					
VACO.GP3	ST8	100 25	PP = 4.5+ tsf		4	8.0	04.9

Bottom of borehole at 48.0 feet.



Revision 0 4-D-35 May 2020

SCS ENGINEERS **BORING NUMBER B-13** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 11/29/18 **COMPLETED** <u>12/4/18</u> **GROUND ELEVATION** 555.15 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS AND** MATERIAL DESCRIPTION **REMARKS** 554.7 0.5 Silt, brown, soft, slightly moist, organic (CL-ML) Silty Clay, brown to orange-brown stained brown and gray, firm, with traces of sub-rounded gravel and chalk CL-56 ML5 550.2 (CL-ML) Silty Clay, orange-brown stained brown and gray, stiff to hard, slightly ST1 100 moist, calcareous, with silty lenses in interbeds, weathered GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ White chalky material 5-10 feet 76 PP = 3.5-4.0 tsf 10 100 ST2 45 PP = 3.5-4.5 + tsf15 ST3 100 SPT2 73 PP = 4.5+ tsf 20 CL-ML 100 ST4 54 PP = 4.5 + tsf25 ST5 100 SPT3 80 PP = 4.5 + tsf30 100 ST6 Weathered shale throughout 33-39.9 feet 100 PP = 4.5 + tsfMay 2020 Revision 0 4-D-36 (Continued Next Page)

BORING NUMBER B-13 1901 Central Drive STE 550 PAGE 2 OF 3 Bedford, Texas 76021 Telephone: 817-571-2288 **CLIENT** City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS** AND MATERIAL DESCRIPTION **REMARKS** 35 (CL-ML) Silty Clay, orange-brown stained brown and gray, stiff to hard, slightly PP = 4.5+ tsf ST7 100 MC = 20% moist, calcareous, with silty lenses in interbeds, weathered DD = 109 pcf CL-100 LL = 66 ML PI = 43Fines = 94% Weathered to Unweathered 515.3 40 Silty Clay Shale, gray, hard, slightly moist to moist, calcareous, unweathered zone 100 ST8 Orange-brown staining in joints at 40-41 feet 56 PP = 4.5 + tsf45 Fossil/shell fragments 45-50 feet PP = 4.5 + tsfSTS 100 MC = 15% GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ SPT5 DD = 112 pcf 60 LL = 51 PI = 33Fines = 95% 50 100 ST10 PP = 4.5+ tsf 60 55 ST11 100 SPT6 100 PP = 4.5 + tsf60 50 65 100 ST12 PP = 4.5 + tsf43 70 40 Revision 0 4-D-37 May 2020 (Continued Next Page)

BORING NUMBER B-13

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

PAGE 3 OF 3

CLIENT _City of Waco

PROJECT NAME _City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00

PROJECT LOCATION Waco, Texas

24 DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	
 - 80		60				Silty Clay Shale, gray, hard, slightly moist to moist, calcareous, unweathered	475.2

Bottom of borehole at 80.0 feet.



7 13 2020

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ

SCS ENGINEERS **BORING NUMBER B-14** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 11/5/18 COMPLETED 11/6/18 **GROUND ELEVATION** 539.2 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS AND** MATERIAL DESCRIPTION **REMARKS** (CL-ML) Silty Clay, dark brown to brown, firm to stiff, moist to very moist, organic, with some small to medium sized sub-rounded gravel and chalk in fractures/joints 98 CL-ML 5 532.8 50 ST1 (CL-ML) Silty Clay, orange-brown mottled brown and gray, stiff to hard, slightly moist, calcareous, weathered PP = 2.5-3.5 tsf 65 Fossil fragments and silty lenses in bedding 10-15 feet 10 58 PP = 4.5 tsf66 ML 15 PP = 3.0-4.5 tsf MC = 19% 50 DD = 104 pcfLL = 58 60 PI = 35 520.7 Fines = 65% Silty Shale, gray, hard, slightly moist, calcareous, unweathered Weathered to 20 Unweathered Fossil fragments in bedding 20-35 feet zone Silty lenses in bedding 18.5-45 feet ST4 PP = 4.5+ tsf 82 25 21 ST5 PP = 4.5+ tsf 56 30 60 Revision 0 4-D-39 May 2020 (Continued Next Page)

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ

BORING NUMBER B-14 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _City of Waco Landfill MSW-2400 PROJECT LOCATION Waco, Texas **PROJECT NUMBER** 16216088.00 SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY DEPTH (ft) U.S.C.S. **TESTS** AND REMARKS MATERIAL DESCRIPTION 35 Silty Shale, gray, hard, slightly moist, calcareous, unweathered PP = 4.5+ tsf MC = 15% 17 ST6 LL = 58 Silty lenses in bedding 18.5-45 feet (continued) 70 PI = 39 Fines = 94% 40 64 45 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 13 PP = 4.5+ tsf 58 50 60 55 21 PP = 4.5 + tsf80 Discipline License # 60 5-13-2020 PP = 4.5+ tsf 60 65 474.2 Bottom of borehole at 65.0 feet. 21 ST9 Revision 0 4-D-40 May 2020

SCS ENGINEERS **BORING NUMBER B-15** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 10/26/18 **COMPLETED** <u>10/26/18</u> **GROUND ELEVATION** 563.35 ft HOLE SIZE 7.25 inches **DRILLING CONTRACTOR** West Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS AND** MATERIAL DESCRIPTION **REMARKS** (CL-ML) Silty Clay, dark brown to brown with orange-brown staining, firm to stiff, moist, with trace of white gravel, organics in top 1-2 feet CL-96 ML 5 558.4 (CL-ML) Silty Clay, orange-brown mottled brown and gray, stiff to hard, slightly moist, with weathered shale GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 63 ST1 PP = 4.0-4.5 + tsf76 ML 10 553.4 Silty Shale, orange-brown mottled brown and gray, hard, slightly moist Silty lenses in interbeds 10-15 feet 63 PP = 4.5 + tsf46 15 Crystalline lenses in interbeds 15-25 feet 75 PP = 4.5+ tsf 83 20 75 ST4 PP = 4.5+ tsf 89 25 538.4 25.0 Silty Shale, brown and gray stained orange-brown, hard, slightly moist, with crystalline lenses in interbeds, weathered 75 ST5 PP = 4.5 + tsf72 30 Weathered to 531.9 83 Unweathered Silty Shale, gray, hard, slightly moist, calcareous zone PP = 4.5 + tsf100 Revision 0 May 2020 4-1)-41 (Continued Next Page)

BORING NUMBER B-15 1901 Central Drive STE 550 PAGE 2 OF 2 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS** AND REMARKS MATERIAL DESCRIPTION 35 Silty Shale, gray, hard, slightly moist, calcareous 38 PP = 4.5 + tsf100 40 84 45 Minor shell fragments 45-50 feet GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\S\ITE 50 WACO.GPJ 25 ST8 PP = 4.5+ tsf 100 50 100 55 PP = 4.5+ tsf MC = 11% 25 DD = 116 pcf 100 LL = 57 PI = 37 Fines = 91% 60 James Lawrence 100 Discipline License # 65 29 ST10 PP = 4.5+ tsf 100 5-13-2020 493.4 Bottom of borehole at 70.0 feet. Revision 0 4-D-42 May 2020

SCS ENGINEERS **BORING NUMBER B-16** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas **COMPLETED** _10/4/18 **GROUND ELEVATION** 560.25 ft HOLE SIZE 8.25 inches DATE STARTED 10/4/18 **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _---LOGGED BY T. Derstine CHECKED BY J. Lawrence AT END OF DRILLING _---**NOTES** AFTER DRILLING ---SAMPLE TYPE/NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY DEPTH (ft) U.S.C.S. **REMARKS** MATERIAL DESCRIPTION (CL) Clay, dark gray, slightly moist, hard, non-calcareous to slightly calcareous, with trace of sub-rounded small gravel CL Organic from 0-1.5 feet 80 556.3 (CL-ML) Silty Clay, olive green/ mustard brown, slightly moist, hard, very 5 calcareous Color change to yellow-brown at 6 feet with chalk/limestone in joints and GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 25 trace of sub-rounded to angular gravel ML PP = 4.5 + tsf50 10 10.0 550.3 Shaley Clay, yellow to orange brown, slightly moist to dry, hard, PP = 4.5 + tsfMC = 19% calcareous, weathered 54 DD = 105 pcfChalk/limestone intrusions 10-15 feet 50 LL = 78 PI = 53Fines = 91% Tan to orange-brown at 15-20 feet 15 54 PP = 4.5 + tsf50 20 Orange-brown mottled brown 20-25 feet 25 ST4 PP = 4.5 + tsf53 25 PP = 4.5 + tsfMC = 15% 54 ST5 DD = 116 pcf LL = 60 60 PI = 38Fines = 77% 30 Orange-brown staining in joints 30-34.5 feet 29 PP = 4.5 + tsf60 Weathered to

4-D-43

Revision 0

525.3

PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00 PROJECT LOCATION Waco, Texas

	PROJI	ECT NUM	IBER	16216088	.00			PROJECT LOCATION Waco, Texas
	S DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
					Unweathered zone			Silty Clay Shale, dark gray, hard, dry, calcareous, unweathered
Γ		ST7	33					Orange-brown staining in joints 35-45 feet
Γ		017	60		PP = 4.5+ tsf			
			00					
Ī	40							
Γ		ST8	29					
			60		PP = 4.5+ tsf			
L	45							
L								
GP.								
ACC -			50		PP = 4.5+ tsf			
50 \								
SISITE	50					-		
ECT					PP = 4.5+ tsf MC = 17%			
PRO		ST9	25		DD = 115 pcf			
EN P			60		LL = 64			
-E					PI = 43 Fines = 94%			
BENT	55				Filles – 94%			
SINE								
N N								
			69					
								Shells in interbeds 60 feet
RSI	60	SPT1	22	24.50				61.0 499.3
3SU			_33_	21-50				Bottom of borehole at 61.0 feet.
51 - C								
9 15:6								
- 2/4/1								
GDT								THE OF THE PROPERTY OF THE PRO
LAB.								
SD Q.								former & tawrince
TS T								James Lawrence
5								Discipline
WELI								License #
/ TP /								11-541-696
L BH,								VALUE OF SECTION OF THE PROPERTY OF THE PROPER
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ								5-13-2020
E L		Revisio	n O					4-D-44 May 2020



May 2020

SCS ENGINEERS **BORING NUMBER B-17** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 10/8/18 **COMPLETED** 10/9/18 **GROUND ELEVATION** 546.75 ft HOLE SIZE 7.25 inches **DRILLING CONTRACTOR** West Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY V. Wooters CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS AND** MATERIAL DESCRIPTION **REMARKS** 546.3 0.5 Limestone, white, hard, dry (CL) Clay, dark gray, slightly moist, hard, with sub-angular gravel <1/8-2" 40 CL 5 541.8 (CL) Clay, yellow-brown mottled gray, slightly moist, hard ST1 40 PP = 4.5 + tsf10 CL 80 PP = 4.5 + tsf15 531.8 (CL) Shaley Clay, tan to gray mottled orange, slightly moist to dry, hard, calcareous, PP = 4.5+ tsf weathered MC = 19%ST3 DD = 106 pcfColor change to tan to brown mottled orange at 20 feet 60 LL = 66 Mineral deposits in fractures 20-22 feet PI = 41Fines = 91% 20 ST4 40 PP = 4.5 + tsfCL 25 PP = 4.5 + tsfST5 40 LL = 67PI = 2330 515.8 Silty Clay Shale, dark gray, hard, dry, calcareous, weathered PP = 4.5+ tsf 100 33.0 513.8 Weathered to Unweathered zone May 2020 Revision 0 4-D-45 (Continued Next Page)

BORING NUMBER B-17 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS** AND REMARKS MATERIAL DESCRIPTION 35 Silty Clay Shale, dark gray, hard, dry, calcareous, unweathered ST7 60 PP = 4.5 + tsf40 ST8 60 PP = 4.5+ tsf 45 PP = 4.5 + tsfMC = 15% GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ ST9 DD = 120 pcf 60 LL = 60 PI = 41 Fines = 83% 50 ST10 100 PP = 4.5 + tsf55 ST11 100 PP = 4.5 + tsfLimestone/chalk in fractures and joints 60-65 feet. Weathered zones throughout from 60-71 feet. (continued) 60 ST12 100 PP = 0-4.5 + tsfJames Lawrence 65 Discipline License # 100 PP = 0-4.5 + tsf70 5-13-2020 475.8 Bottom of borehole at 71.0 feet. Revision 0 4-D-46 May 2020

1901 Bedf	S ENGIN Central Di ord, Texas phone: 81	rive ST 76021	E 550				WELL NUMB	ER B-18 (PZ-18) PAGE 1 OF 2	
CLIE	ENT City of	of Wad	:0				PROJECT NAME City of Waco Landfill MSW-	2400	
	-						· · · · · · · · · · · · · · · · · · ·		
							GROUND ELEVATION 534.75 ft HOLE SIZE 8.25 inches		
			TOR BEST Drilli						
			Continuous Fligh				AT TIME OF DRILLING No Groundwa	ater	
						BY J. Lawrence			
	ES						AFTER DRILLING No Groundwater		
O DEPTH	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION	WELL DIAGRAM	
-	-	88		CL- ML		moist, orgar	y Clay Topsoil, dark brown, soft to firm, nic 532 y Clay, brown, firm to stiff, moist, with traces nedium gravel and chalk in fractures/joints	2.1	
50 WACO.GPJ	ST1	25 100	PP = 4.5+ tsf	CL- ML		6.8 (CL-ML) Silt	nedium gravel and chalk in fractures/joints 528 y Clay, orange-brown mottled gray, hard, st, calcareous	3.0	
BENTLEY/GINT/PROJECTS/SITE 50 WACO.GPJ	- ST2	25 77	PP = 4.5+ tsf MC = 19% DD = 105 pcf LL = 66 PI = 45 Fines = 92% Weathered to Unweathered	CL- ML		14.5	in bedding 10-14.5 feet	0.3	
S/PUBLIC/DOCUMENTS/BE	ST3	17 93	zone PP = 4.5+ tsf			unweathered Slight orang			
- 2/4/19 15:51 - C:\USER! 	_ ST4	21 78	PP = 4.5+ tsf						
GINT STD US LAB.GDT	ST5	25 80	PP = 4.5+ tsf						
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C:\USERS\PUBLICDOCUMENTS\ 29	Revisio	70 on 0					in bedding 30-35 feet -47 (Continued Next Page)	May 2020	
		-					(Continued Next Page)	,	

WELL NUMBER B-18 (PZ-18) PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021

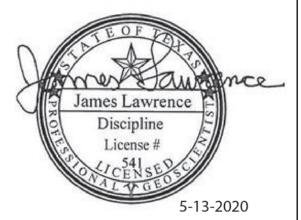
Telephone: 817-571-2288

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00 PROJECT LOCATION Waco, Texas

Ļ			,	102 10000.00		_	FROJECT EOCATION _Waco, Texas	
	0EPTH (#)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
-		OTO	21				Silty Shale, gray, hard, slightly moist, calcareous, unweathered	
		ST6	80	PP = 4.5+ tsf				
-	- ₋							
					_			
-			76					
	45			PP = 4.5+ tsf	_			
20.GPJ		ST7	21	MC = 13% DD = 109 pcf				
≡ 50 WA	-		76	LL = 57 PI = 38				
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\G\INT\PROJECTS\S\ITE 50 WACO.GPJ	50	-		Fines = 90%				
\PROJE			80	PP = 4.5+ tsf				
EYGINT	 		00	11 - 4.51 (3)				
S/BENTL	55				_		56.0 478.	0
JMENTS		ST8	17				Bottom of borehole at 56.0 feet.	0
IC/DOCI	ı							
3S/PUBL								
C:\USEF								
9 15:51 -								
T - 2/4/19							EOF	
LAB.GD								
STD US							mest	autorne
L - GINT							James Lawi Disciplin	
P / WEL							License +	
AL BH / ī							ONAL TO G	
GENER,		Revisio	. n. C				4-D-48	5-13-2020 May 2020



May 2020 Revision 0 4-D-48

190 Bed	CS ENGI 01 Central I dford, Texa ephone: 8	Orive Si s 7602	TE 550 1				BORING NUMBER B-19 PAGE 1 OF 3
	IENT <u>City</u>		co _16216088.00				PROJECT NAME City of Waco Landfill MSW-2400 PROJECT LOCATION Waco, Texas
DA	TE START	ED _10	0/30/18	COMP	LETE	D 10/30/18	
DR	RILLING CO	NTRAC	CTOR West Drillin	g			GROUND WATER LEVELS:
DR	RILLING ME	THOD	Continuous Flight	Auge	r		AT TIME OF DRILLING No Groundwater
LO	GGED BY	V. Wo	ooters	CHEC	KED E	3Y J. Lawrence	AT END OF DRILLING No Groundwater
NC	OTES						AFTER DRILLING No Groundwater
ОЕРТН	0 4	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC		MATERIAL DESCRIPTION
-	-	100		CL- ML		4.0	ty Clay, dark brown, soft, moist, calcareous 558.1
5	5					(CL-ML) Si	ty Clay, gray/tan mottled orange, hard, slightly moist, calcareous
	ST	100	PP = 4.5+ tsf			Chalk in fra	ctures/joints 4-20 feet
BENTLEY/GINTYPROJECTS/SITE 50 WACO.GPJ	ST.	50	PP = 0-4.5+ tsf LL = 60 PI = 38			Very weath	ered zones 15-20 feet
S/PUBLIC/DOCUMENTS/I	ST	100	PP = 4.5+ tsf	CL- ML			
- 2/4/19 15:51 - C:\USER	ST.	100	PP = 4.5+ tsf				
GINT STD US LAB.GDT	ST	100	PP = 0-4.5+ tsf				
NERAL BH / TP / WELL	ST	100	PP = 0-4.5+ tsf				
<u>ප් 3</u>	6 Revis	on 0	1		WW	<u>4-</u> [0-49 (Continued Next Page) May 2020

BORING NUMBER B-19 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 **CLIENT** City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS** AND MATERIAL DESCRIPTION **REMARKS** 35 (CL-ML) Silty Clay, gray/tan mottled orange, hard, slightly moist, calcareous ST7 CL-100 PP = 0-4.5 + tsfML 40 522.1 (CL) Clay, dark gray with orange to tan mottling, dry, hard, calcareous, with soft weathered shale zones ST8 100 PP = 0-4.5 + tsfCL 45 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 100 513.1 49.0 Silty Clay Shale, dark gray, hard, dry, calcareous, with chalk in joints/fractures, 50 weathered PP = 4.5 + tsfMC = 14% ST9 DD = 117 pcf 100 LL = 63 53.0 509.1 PI = 44 Silty Clay Shale, dark gray, hard, dry, calcareous, unweathered Fines = 91% Chalk in fractures/joints 53-65 feet Weathered to 55 Unweathered Intermittent weathered zones from 50-87 feet zone 100 60 100 PP = 0-4.5 + tsf65 100 70 PP = 0-4.5 + tsfMC = 15%ST11 100 LL = 57 PI = 38 Fines = 95% May 2020 4-D-50 Revision 0 (Continued Next Page)

PAGE 3 OF 3

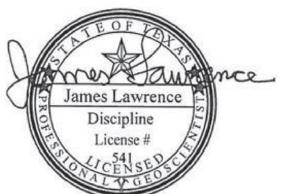
1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00 PROJECT LOCATION Waco, Texas

	DEPTH (ff)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION
							Silty Clay Shale, dark gr Chalk in fractures/joints	ay, hard, dry, calcareous, unweathered 53-65 feet
	80		100				Intermittent weathered z	ones from 50-87 feet (continued)
-	 85	ST12	100	PP = 0-4.5+ tsf				
Ę.			100	PP = 4.5+ tsf			87.0	475.1
WACO.G		ST13					07.0	Bottom of borehole at 87.0 feet.
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ								James Lawrence Discipline License #
GE		Revisio	n O				4-D-51	5-13-2020 May 2020



May 2020

	ENGI						WELL NU	IMBE	R B-20 (PZ-20)
	Central Di ord, Texas								PAGE 1 OF 2
	hone: 817								
C. 15	NT O'E	£\^/-					DDO IECT NAME ON STATES IN 199	MOW O	20
1	NT City o						PROJECT NAME _City of Waco Landfill	MSW-240	JU
			16216088.00	00:		0/00/40	PROJECT LOCATION Waco, Texas		
1			/29/18					HOLE S	IZE 7.25 inches
1			TOR West Drilli	_			-		
			Continuous Fligh				AT TIME OF DRILLING No Gro		
		V. Wo	oters	CHEC	KED BY _	J. Lawrence			
NOTI	ES						▼ AFTER DRILLING 7.90 ft / Elev 5	56.20 ft	
O DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM
- 5	-	100		CL- ML	5.0	(CL-ML) Sil <1/8" pebbl	ty Clay, gray mottled tan, hard, dry, with es and chalk in fractures/joints, calcareous	559.1	
						(CL-ML) Sil	ty Clay, tan/gray mottled orange, hard, dry,	000.1	
<u></u>	ST1					calcareous			
00	311	60	PP = 4.5+ tsf			√ <1/8" pebbl	es 5-10 feet		
 - 	1					_	nts/fractures 5-10 feet		
10	1					J			
				_					
10 15 15 15 15 15 15 15	ST2	50	PP = 4.5+ tsf						
15	1								
SIBEL						Very uncon	solidated/weathered 15-35 feet		
20 25 25 25 25 25 25 25 25 25 25 25 25 25	CTO								
<u></u>	ST3	50	PP = 0 tsf						
	1			CI					
20 2				CL- ML					
	OT :								
-	ST4	50	PP = 0 tsf						
<u>-</u>									
						N 41: 1 - 1	ita 24 25 faat		
25						ivlineral dep	posits 24-25 feet		
<u> </u>	-								
<u>i</u>	ST5	50	PP = 0 tsf						
-			5 (0)						
<u>-</u>	-								
30_									
<u></u>									
<u>-</u>	ST6	E0.	DD = 0 +=+						
<u>.</u>	\Box	50	PP = 0 tsf						
<u>i</u> -	-								
35	Revisio	n O			35.0) Δ-Γ)-52 (Continued Next Page)	529.1	May 2020
		•				, ,	- – (Continuea Next Page)		

WELL NUMBER B-20 (PZ-20) 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY DEPTH (ft) U.S.C.S. **TESTS** AND MATERIAL DESCRIPTION WELL DIAGRAM **REMARKS** 35 (CL) Clay, dark gray with orange/tan mottling, hard, dry, calcareous, with weathered shale ST7 Mineral deposits in fractures 25-35 feet 100 PP = 4.5 + tsfCL 40 ST8 100 PP = 4.5 + tsf43.0 521.1 Silty Clay Shale, dark gray, hard, dry, calcareous, weathered Weathered to 45 Unweathered zone PP = 4.5+ tsf GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ ST9 47.0 517.1 MC = 13% Silty Clay Shale, dark gray, hard, dry, calcareous, 100 DD = 116 pcf LL = 59 unweathered PI = 36 Orange-brown oxidation staining 50-55 feet Fines = 95% 50 Chalk/limestone in fractures 50-55 feet 100 55 PP = 4.5 + tsfMC = 15% No oxidation staining beginning at 57.5 feet DD = 118 pcf ST10 100 LL = 58 PI = 37 Fines = 96% 60 100 PP = 4.5 + tsf65 James Lawrence Discipline ST11 License # 70 5-13-2020 491.1 Bottom of borehole at 73.0 feet.

SCS ENGINEERS **BORING NUMBER B-21** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 10/29/18 **COMPLETED** 10/29/18 **GROUND ELEVATION** 538.75 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS AND** MATERIAL DESCRIPTION **REMARKS** (CL-ML) Silty Clay, dark brown to brown, firm, moist, organic, with traces of small CLgravel and shells ML 536.5 66 (CL-ML) Silty Clay, orange-brown mottled brown and gray, hard, slightly moist, calcareous Shell fragments 2.3-15 feet 5 Mineral deposits in fractures 5-10 feet 29 PP = 4.5 + tsf88 10 25 PP = 4.5 + tsf80 CL-ML 15 PP = 4.5 + tsf33 MC = 19% 43 LL = 69 PI = 44Fines = 97% 20 29 ST4 PP = 4.5 + tsf56 Weathered to 513.9 25 Unweathered Silty Shale, gray, slightly moist to moist, hard, calcareous zone Orange-brown staining in fractures 24.9-35 feet 21 ST5 PP = 4.5 + tsfShell fragments 30-35 feet 89 30 PP = 4.5 + tsfMC = 15% 21 ST₆ DD = 118 pcf 100 LL = 57 PI = 39Fines = 94% Revision 0 4-D-54 May 2020 (Continued Next Page)

PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

PROJECT NUMBER _ 16216088.00

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT LOCATION Waco, Texas

0EPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
						Silty Shale, gray, slightly moist to moist, hard, calcareous
 						Fossil remnants 35-45 feet
+ +		90				1 occili reminante de 16 feet
+ +		90				
I -						
40						
L			PP = 4.5+ tsf			
	ST7	17	MC = 14%			
	017					
F -		98	LL = 61			
 			PI = 40			
45			Fines = 88%			45.0 493.8
ı						Pottom of boroholo at 45 0 foot

Bottom of borehole at 45.0 feet.



May 2020

SCS ENGINEERS **BORING NUMBER B-22** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 12/18/18 **COMPLETED** 12/19/18 **GROUND ELEVATION** 555.5 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY DEPTH (ft) U.S.C.S. **TESTS** AND MATERIAL DESCRIPTION **REMARKS** (MH) Clayey Silt, brown, soft, moist, with some subrounded gravel and MH 554.0 (CL-ML) Silty Clay, brown, soft to firm, moist, with subrounded gravel and 46 roots CL-ML 5 550.6 (CL-ML) Silty Clay, brown-gray stained orange-brown, firm, moist, with white chalky material and silty micaceous lenses, calcareous 9-16-22 83 (38)PP = 3.5-4.5 tsf 10 Stiff to hard 10-34.7 feet 38 ST2 No white chalky material 10-34.7 feet PP = 4.0-4.5 tsf 61 15 50 ST3 15-26-29 100 (55)PP = 4.0 tsf 20 ML 17 48 PP = 4.0 tsf25 18-24-35 Minor crystalline pockets 27-34.7 feet 100 (59)86 PP = 4.0 tsf30 29 PP = 4.5 + tsfST6 MC = 20%70 LL = 74PI = 47520.8 Fines = 84% Revision 0 4-D-56 May 2020 (Continued Next Page)

BORING NUMBER B-22 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 **CLIENT** City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas SAMPLE TYPE/NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY DEPTH (ft) U.S.C.S. **TESTS** AND MATERIAL DESCRIPTION **REMARKS** 35 Shale Marl, dark gray with orange-brown staining in joints, stiff to hard, slightly moist, with silty to very fine sand micaceous lenses and fossil 25 21-27-50 ST7 remnants, calcareous 100 (77)100 PP = 4.5 + tsfSPT4 Transition zone (continued) Weathered to 38.5 517.0 Unweathered Shale Marl, dark gray, hard, slightly moist, with silty micaceous lenses and fossil remnants, calcareous, unweathered zone 40 21 ST8 100 PP = 4.5 + tsf45 PP = 4.5 + tsf17 50 ST9 MC = 17%100 SPT5 LL = 64 PI = 39Fines = 92% 50 100 55 17 ST10 76 PP = 4.5 + tsf60 76 65 90 70 80 Revision 0 4-D-57 May 2020

PAGE 3 OF 3

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00

PROJECT LOCATION Waco, Texas

PROJE	ECT NUM	IBER	16216088	.00			PROJECT LOCATION Waco, Texas	
DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	
		80					Shale Marl, dark gray, hard, slightly moist, with silty micaceous lenses and fossil remnants, calcareous, unweathered (continued) 80.0	475.5
- 30			I	l			Pottom of harabala at 90.0 fact	7/3.3

Bottom of borehole at 80.0 feet.



Revision 0 4-D-58 May 2020

SCS ENGINEERS **BORING NUMBER B-23** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 10/5/18 **COMPLETED** <u>10/5/18</u> GROUND ELEVATION 540.1 ft HOLE SIZE 8.25 inches DRILLING CONTRACTOR BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--_ LOGGED BY _T. Derstine CHECKED BY _J. Lawrence AT END OF DRILLING _---NOTES AFTER DRILLING ---SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS** AND MATERIAL DESCRIPTION REMARKS 0 (CL-ML) Silty Clay, dark gray, slightly moist to moist, stiff, with some gravel, non-calcareous Some fossil/shell fragments 5 CL-ML 28 PP = 3.0-4.0 tsf 49 Color change to orange/brown mottled tan/brown and slightly moist to dry with calcareous material in joints at 10 ft 10 530.1 10.0 (CL-ML) Silty Clay, orange-brown mottled tan and gray, stiff to hard, slightly moist to PP = 2.0-2.75 tsf MC = 20%dry, calcareous 36 DD = 108 pcf Chalk in joints 10-20 feet 49 LL = 73 PI = 52Fines = 98% 15 Shells in bedding 15-20 feet 36 PP = 4.0-4.5+ tsf 46 20 24 ST4 CL-PP = 4.5 + tsf52 ML 25 24 ST5 PP = 4.5 + tsf55 30 Sandy lenses 30-38 feet PP = 4.5+ tsf MC = 18% 28 ST₆ DD = 108 pcf LL = 74 PI = 51 Fines = 85%

BORING NUMBER B-23 1901 Central Drive STE 550 PAGE 2 OF 2 Bedford, Texas 76021 Telephone: 817-571-2288 **CLIENT** City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS** AND MATERIAL DESCRIPTION **REMARKS** 35 PP = 4.5+ tsf MC = 20% 24 ML ST7 DD = 101 pcf LL = 77

interbeds

45.0

28 ST9

80

12

96

ST8

40

45

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ

PI = 55

Fines = 89% Weathered to Unweathered

zone PP = 4.5 + tsf

MC = 15%

LL = 70 PI = 50

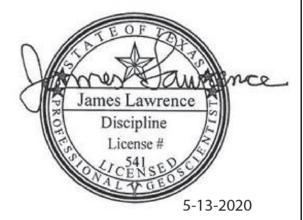
Fines = 96%

Bottom of borehole at 45.7 feet.

Silty Clay Shale, dry, very hard, calcareous, unweathered, with sandy lenses in

502.1

495.1



May 2020 Revision 0 4-D-60

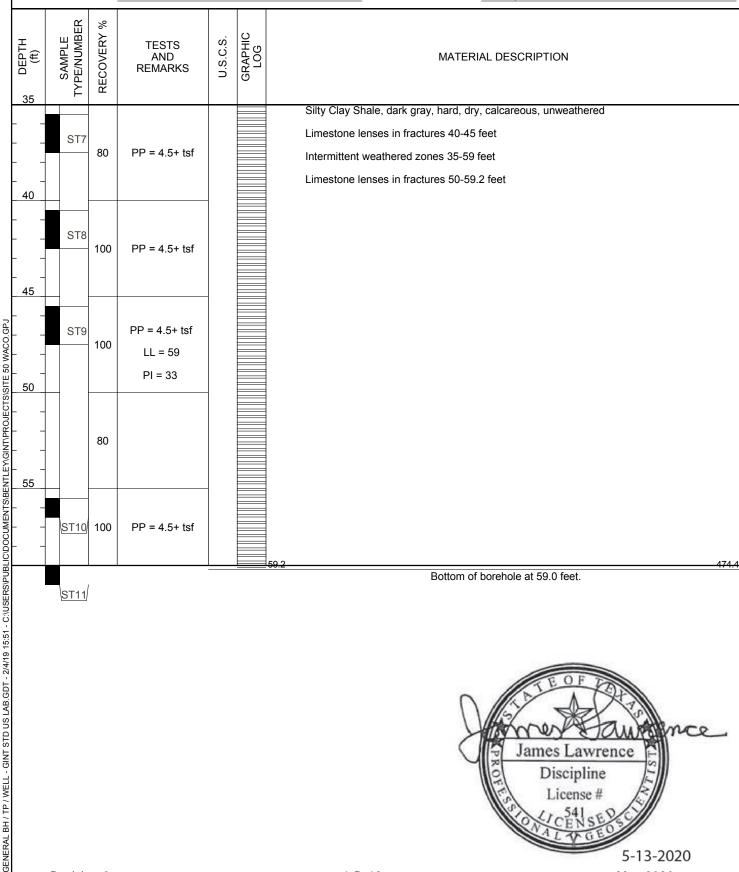
SCS ENGINEERS **BORING NUMBER B-24** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 10/11/18 **COMPLETED** 10/11/18 **GROUND ELEVATION** 533.62 ft HOLE SIZE 7.25 inches **DRILLING CONTRACTOR** West Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY V. Wooters CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY DEPTH (ft) U.S.C.S. **TESTS AND** MATERIAL DESCRIPTION **REMARKS** (CH) Clay, dark gray, hard, dry, non-calcareous, with sub-angular calcareous Color change to light grayand slightly moist at 5 feet 100 5 PP = 3-4.5 + tsfMC = 15%526.6 ST₁ DD = 112 pcf (CL-ML) Silty Clay, orange-tan mottled gray, dry, hard, with chalk/limestone in joints 80 LL = 51 and sand in fractures, slightly calcareous, weathered/crumbled PI = 33 Sub-angular calcareous pebbles 7-10 feet Fines = 73% 10 40 PP = 3.0 tsf15 PP = 2.0-4.5 + tsfCL-MC = 21%ML ST3 DD = 99 pcf60 LL = 74PI = 52Fines = 98% 20 ST4 100 PP = 3.0-4.5 + tsf25 508.6 PP = 2.0 tsf (CL) Shaley Clay, dark gray with brown staining, soft, dry, calcareous, very weathered MC = 19% ST5 DD = 103 pcfCL 80 LL = 69 PI = 44Fines = 89% 30 503.6 Silty Clay Shale, dark gray, hard, dry, calcareous, unweathered Intermittent weathered zones 35-59 feet PP = 4.5 + tsfWeathered to 80 Unweathered zone Revision 0 May 2020 4-1)-61 (Continued Next Page)

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

CLIENT City of Waco

PROJECT NAME _City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00 PROJECT LOCATION Waco, Texas





SCS ENGINEERS **BORING NUMBER B-25** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 10/11/18 **COMPLETED** 10/11/18 **GROUND ELEVATION** 533.25 ft HOLE SIZE 7.25 inches **DRILLING CONTRACTOR** West Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY V. Wooters **CHECKED BY** J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS AND** MATERIAL DESCRIPTION **REMARKS** (CL-ML) Silty Clay, dark gray, soft to hard, slightly moist to dry, calcareous, with chalk in joints Color change to light gray 4-5 feet CL-100 ML 5 528.3 (CL-ML) Silty Clay, orange/gray/tan mottled, hard, slightly moist to dry, calcareous, with chalk in joints and sub-rounded pebbles 1/8" BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C:\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ ST₁ PP = 4.5+ tsf 80 10 James Lawrence PP = 3.0-4.5 + tsfDiscipline CL-ML License # 15 No pebbles 15-20 feet ST3 Silty Sand lenses in fractures 15-23 feet PP = 3.0-4.5 + tsf5-13-2020 20 ST4 100 PP = 1.0-3.0 tsf 510.3 (CL) Shaley Clay, dark gray, medium hard to soft, dry, calcareous, weathered CL 25 508.3 Silty Clay Shale, dark gray, hard, dry, calcareous, unweathered Intermittent weathered zones 25-33 feet PP = 1.0-3.0 tsf ST5 Weathered to 100 Unweathered zone 30 100 PP = 1.0-3.0 tsf 500.3 GENERAL Bottom of borehole at 33.0 feet. Revision 0 May 2020 4-D-63

SCS ENGINEERS **BORING NUMBER B-26** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 11/18/18 **COMPLETED** 11/18/18 **GROUND ELEVATION** 530.45 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Millbrand CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater TYPE/NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY DEPTH (ft) SAMPLE U.S.C.S. **TESTS** AND MATERIAL DESCRIPTION **REMARKS** Top Soil, black, soft, moist, with roots and small gravel 529.1 (CL-ML) Silty Clay, llight brown, hard, slightly moist, with small round to sub-rounded gravel up to 1/4", slightly calcareous 36 CL-ML 5 5.0 525.5 (CL-ML) Silty Clay, tan to light brown mottled orange and gray, very hard, dry, slightly calcareous 14-25-35 83 (60)PP = 4.5 + tsf93 10 CI Orange staining 10-15 feet ML 35 ST2 37 PP = 4.5 + tsf15 515.5 (CL-ML) Silty Clay, tan/brown with orange staining, hard to very hard, 18-26-37 35 calcareous ST3 100 (63)CL-PP = 3.0-4.5 + tsf75 SPT2 ML Color change to dark gray at 20 feet 20 20.0 510.5 (CL-ML) Silty Clay, dark gray to gray with orange staining, very soft to very hard, dry, slightly to moderately calcareous 28 ST4 Transition zone into weathered shale 51 PP = 0.5-4.5 + tsfCL-ML 25 Weathered to 26.0 504.5 Unweathered 28-50 Clay (Shale), dark gray, very soft to very hard, dry, with fossil remnants, 33 zone slightly calcareous, unweathered PP = 1.5-4.5+ tsf 63 SPT3 Trace of orange staining 25-30 feet 30 26 ST6 47 PP = 2.5-4.0 tsf May 2020 Revision 0 4-1)-64 (Continued Next Page)

PAGE 2 OF 2

494.5

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

PROJECT NUMBER 16216088.00

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

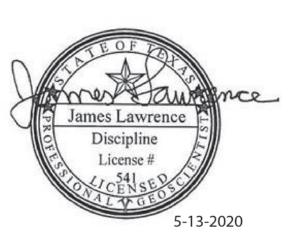
PROJECT LOCATION Waco, Texas

36.0

DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	
35							

MATERIAL DESCRIPTION

Bottom of borehole at 36.0 feet.



May 2020

	1901 C Bedford	entral Dr d, Texas one: 817	ive S ⁻ 7602	TE 550 1					BORING NUMBER B-2 PAGE 1 O				
	PROJE	T City of	IBER	16216088	.00 COMPLETE	=D 1*	1/14/19	3	PROJECT NAME _City of Waco Landfill MSW-2400 PROJECT LOCATION _Waco, Texas GROUND ELEVATION _546.65 ft HOLE SIZE _8.25 inches				
				CTOR BES			1/ 1-7/ 10						
					s Flight Auger				AT TIME OF DRILLING No Groundwater				
	LOGGI	ED BY	T. Dei	rstine	CHECKED	BY _J	. Lawr	ence	AT END OF DRILLING No Groundwater				
	NOTES	S							AFTER DRILLING No Groundwater				
	о ОЕРТН (#)	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION				
						МН			(MH) Clayey Silt, dark brown, soft to firm, very moist, organic				
						IVIII	Ш	2.5		544.2			
	 5		90						(MH) Clayey Silt, brown, stiff to hard, moist to slightly moist, with white chalk and fossil fragments, calcareous				
ſ		ST1	33			MH	Ш						
30.GP		311	40		PP = 4.5+ tsf								
) WAC			40		11 - 4.51 (3)		Ш						
ITE 50	10						Ш	10.0		E26 -			
S/BENTLEY/GINT/PROJECTS/SITE 50 WACO.GPJ	10	ST2	50 100 60	18-34-44 (78)	PP = 4.5+ tsf	CL- ML		10.0	(CL-ML) Silty Clay, orange-brown mottled brown and gray, hard, slightly moist, calcareous	536.7			
VTLE)	15							15.0		531.7			
TS\BE!	10							10.0	Silty Shale, orange-brown mottled brown and light gray, hard, slightly moist, calcareous, weathered	331.7			
JMEN		ST3	38						White crystalline lenses in interbeds 17.7-21.4 feet				
DOCL		SPT2	72 60	49-50	PP = 4.5+ tsf				Write Gystainte letises in interbeds 17.7-21.4 feet				
BLIC	└ -												
S\PU	20												
USEF		ST4	29										
1 - C:\		314	78	25-36-50	PP = 4.5+ tsf								
3 15:5	├ -	SPT3	93	(86)	11 - 4.51 (3)								
2/4/19	 25								Orange-brown and crystalline in interbeds 25-29 feet				
3DT -	23			00.07.40	PP = 4.5+ tsf								
LAB.		ST5	21 100	26-27-40 (67)	MC = 18% DD = 108 pcf								
D US		SPT4	68		LL = 68 PI = 47								
NT ST					Fines = 87%			29.0		517.7			
L - GI	30				Weathered to				Silty Shale, gray, hard, slightly moist, calcareous, micaceous, unweathered				
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENT		005	53	26-50	Unweathered zone				Orange-brown staining in joints/bedding 29-40 feet				
/ TP,		SS5	_13	<u> </u>	DD 45 : 1								
¹L BH		SPT6	80		PP = 4.5+ tsf				Occasional fossil fragments 33-38 feet				
:NER/	-								Fossil fragments 40.8-53 feet				
ਲ	35	Revisio	n 0					4	-D-66 (Continued Next Page) May 2020				

PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

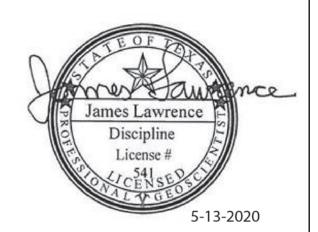
CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER <u>16216088.00</u>

PROJECT LOCATION Waco, Texas

обратн (#)	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
40 45 50 50	ST7 SPT6	100	50	PP = 4.5+ tsf MC = 15% DD = 118 pcf LL = 61 PI = 40 Fines = 97%			Silty Shale, gray, hard, slightly moist, calcareous, micaceous, unweathered Orange-brown staining in joints/bedding 29-40 feet Occasional fossil fragments 33-38 feet Fossil fragments 40.8-53 feet (continued)
	SPT7			PP = 4.5+ tsf			53.0 493.7
غِ ا							Bottom of borehole at 53.0 feet.



Revision 0 4-D-67 May 2020

SCS ENGINEERS **BORING NUMBER B-28** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 10/11/18 **COMPLETED** 10/11/18 **GROUND ELEVATION** 529.6 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine **CHECKED BY** J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS AND** MATERIAL DESCRIPTION REMARKS (CL-ML) Silty Clay, gray, soft to firm, moist, organic, with traces of small to large gravel and chalk material CL-98 ML 5 524.6 (CL-ML) Silty Clay, orange-brown mottled gray and brown, very hard, slightly moist, with some weathered shale, weathered GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 21 ST1 Chalky material interbedded 5-10 feet PP = 4.5 + tsf51 Sub-rounded, small to large gravel 5-6 feet Shell fragments 10-15 feet 10 54 PP = 4.5 + tsf64 15 ML Crystalline/mineral deposits 15-25 feet 33 PP = 4.5 + tsf100 20 25 ST4 PP = 4.5 + tsf100 25 504.6 Silty Shale, orange-brown mottled brown and gray, very hard, slightly moist, with shell fragments, weathered 29 ST5 PP = 4.5 + tsf100 28.0 501.6 Weathered to Silty Clay Shale, gray to dark gray, very hard, slightly moist to dry, calcareous, Unweathered unweathered zone 30 Mineral deposits 28-30 feet Shell fragments 30-35 feet Orange-brown staining 28-35 feet 13 PP = 4.5 + tsf100 Revision 0 May 2020 4-1)-68 (Continued Next Page)

PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

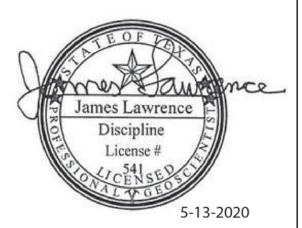
CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00

PROJECT LOCATION Waco, Texas

	ECT NOW	IDEK	16216088.00			PROJECT LOCATION Waco, Texas
DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
	CT7	21				Silty Clay Shale, gray to dark gray, very hard, slightly moist to dry, calcareous, unweathered
	ST7	66	PP = 4.5+ tsf			Mineral deposits 28-30 feet Shell fragments 30-35 feet Orange-brown staining 28-35 feet <i>(continued)</i>
40						
		58				
45						
CO.GPJ	ST8	21	PP = 4.5+ tsf			
TE 50 WA		71				
DECTS/SIT						
INT\PRO		66				
						55.0 474.6
AENTS/BI						Bottom of borehole at 55.0 feet.
CIDOCUI						
S/PUBLIC						
- C:\USER						
19 15:51 -						
GENERAL BH / TP / WELL - GINT STD US LAB GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLE\Y\GINT\PROJECTS\SITE 50 WACO.GPJ G						James Lawrence Discipline License # Licen
OEN CEN	Revisio	n O				5-13-2020 4-D-69 May 2020



	Central D						BORING NUMBER B-29
Bedfo	ord, Texas phone: 81	7602	1				PAGE 1 OF 2
	ENT City of						PROJECT NAME City of Waco Landfill MSW-2400
	-		16216088.	00			PROJECT LOCATION _ Waco, Texas
				COMPLETE	ED 11	1/16/10	
- 1			CONTINUES				
- 1				s Flight Auger	D V 1		AT TIME OF DRILLING No Groundwater
- 1				CHECKED	BA 7	. Lawr	
NOT	ES						AFTER DRILLING No Groundwater
O DEPTH (#)	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
-	-				МН		(MH) Clayey Silt, dark brown, soft, moist, with organics 2.0 538.
-		73			CL- ML		(CL-ML) Silty Clay, brown to yellow-brown, hard to stiff, slightly moist to moist, with traces of sub-rounded gravel
_ 5							5.0 535.
.GPJ	ST1	25 89	10-16-21 (37)				(CL-ML) Silty Clay (Weathered Shale/Marl), orange-brown stained gray and brown, hard to stiff, slightly moist, with white chalky material, calcareous, weathered
0 WACO	SPT1	67		PP = 4.5+ tsf			Traces of gravel 5-15 feet
JECTS/SITE 5	- ST2	25	-				
rleygint/pro.	- 512	40		PP = 4.5+ tsf			
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C:\USERS\PUBLIC\DOCUMENT\PIBBENTLE\NG\NT\PROJECTS\SITE 50 WACO.GPJ 2	SPT2	94	10-24-36 (60)	PP = 4.5+ tsf	CL-		Black iron staining and limey lenses 15-25 feet
S:\USERS\PUB	- ST4	21	-				Color transitioning into mostly gray at 20 feet
4/19 15:51 - (50	-	PP = 4.5+ tsf			
AB.GDT - 2	SPT3	78	25-50	Weathered to Unweathered zone PP = 4.5+ tsf			25.0 515. Shale Marl, gray with some orange-brown staining, very hard, slightrly moist, calcareous, weathered 513.
NSI -	ST5	13 92		MC = 16% DD = 113 pcf			Crystalline material in spots 25-26 feet
GINT STD - 30	- 313	52		LL = 60 PI = 39 Fines = 95%			Silty Clay Shale Marl, gray with some orange-brown staining, very hard, slightrly moist, calcareous, weathered
/ WEL	_	13					Orange-brown limey/micaceous lenses 30-45 feet
TP.	ST6			55 / - · -			Fossil remnants 25-45 feet
AL BH	-	92		PP = 4.5+ tsf			
- RE	4						
ਲ 35	Revision	on 0					4-D-70 (Continued Next Page) May 2020

PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

CLIENT City of Waco

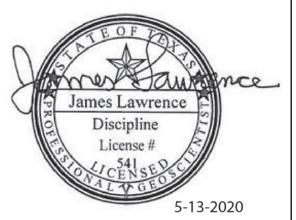
PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00

PROJECT LOCATION Waco, Texas

HL(#) SPT4 28 8 50 PP = 4.5+ tsf MC = 11% DD = 114 pcf LL = 51 PI = 34 Fines = 90% A50 A50 A50 A50 A50 A50 A50 A								
SPT4 28 8 50 MC = 11% DD = 114 pcf LL = 51 Pl = 34 Fines = 90% Fines = 90% Solution and the state of the stat		SAMPLE TYPE/NUMBER		BLOW COUNTS (N VALUE)	AND	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
	40		72	50	MC = 11% DD = 114 pcf LL = 51 PI = 34			Slightrly moist, calcareous, weathered Orange-brown limey/micaceous lenses 30-45 feet Fossil remnants 25-45 feet (continued)

Bottom of borehole at 45.0 feet.



May 2020

SCS ENGINEERS **BORING NUMBER B-30** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** _16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 11/17/18 **COMPLETED** <u>11/18/18</u> **GROUND ELEVATION** 543.05 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine CHECKED BY J. Lawrence AT END OF DRILLING --- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater TYPE/NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY DEPTH (ft) SAMPLE U.S.C.S. **TESTS** MATERIAL DESCRIPTION Top Soil, dark brown to black, very soft, with organic material and silt 11.11 2.0 541.1 (CL-ML) Silty Clay, gray, medium to very hard, slightly moist, with some 86 round to sub-rounded pebles and chalky white material ML 5 538.1 (CL-ML) Silty Clay, gray mottled orange and brown, moderately hard, 48 slightly moist, with some round to sub-rounded pebbles up to 1/2" and 8-12-16 BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C:\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ white chalky material, calcareous 80 (28)PP = 3.0-4.5 + tsfML 96 10 10.0 533.1 (CL-ML) Silty Clay, orange-brown mottled gray and orange, medium soft, 35 ST2 slightly moist, with white chalky material, calcareous Minor pebbles less than 1/8" 10-15 feet 53 PP = 2.0 tsf15 PP = 0-3.0 tsfNo pebbles or chalky white material 15-20 feet 15-25-37 23 MC = 18% 100 (62)Turning gray 15-20 feet DD = 115 pcf CL-SPT2 LL = 61 ML PI = 41Fines = 90% 20 Crystalline deposits and very hard 20-25 feet 18 ST4 36 PP = 4.5 + tsf25 518.1 25.0 (CL-ML) Silty Clay, light brown/orange to gray, medium hard to very hard, dry, calcareous, weathered 18-31-39 19 100 (70)Red-brown staining along fractures, medium soft to hard, and crystalline 58 PP = 2.0-4.5 + tsfSPT deposits 30-35 feet 30 CL-ML 45 PP = 1.5-3.5 tsf ST6 MC = 18% 78 LL = 62PI = 41Fines = 94%

(Continued Next Page)

Revision 0

PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00 PROJECT LOCATION Waco, Texas

	35 DEPTH	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
	 40	ST7	25 55 100	31-50	PP = 1.5-4.5+ tsf	CL- ML		37.3 505.8 Silty Clay Shale Marl, gray to dark gray, very hard, dry, with orange-brown staining, calcareous unweathered Less orange staining 40-45 feet
	 45	ST8	15 72		PP = 4.5+ tsf			
TE 50 WACO.GPJ		ST9	20 36 100	50	PP = 3.0-4.5 tsf			Some orange mottling and hard to very hard 45-48 feet 48.0 Bottom of borehole at 48.0 feet.
_EY\GINT\PROJECTS\SI								
3LIC/DOCUMENTS/BENT								
9 15:51 - C:\USERS\PUE								
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.:USERS!PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ								James Lawrence Discipline License #
GENERA		Revisio	n O					5-13-2020 4-D-73 May 2020



May 2020

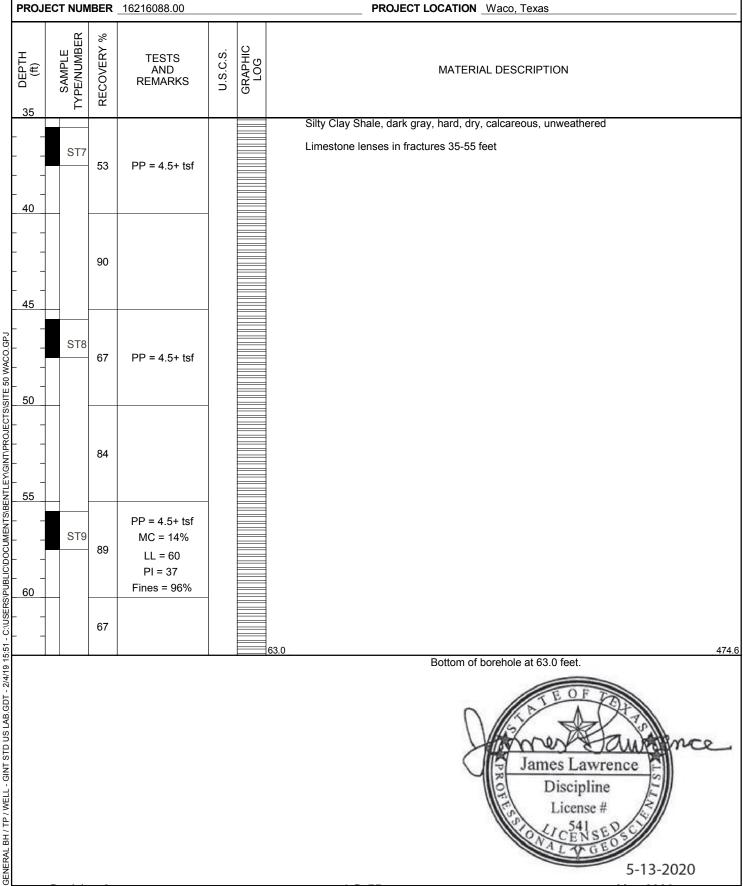
SCS ENGINEERS **BORING NUMBER B-31** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 10/8/18 **COMPLETED** 10/9/18 **GROUND ELEVATION** 537.55 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine **CHECKED BY** J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS AND** MATERIAL DESCRIPTION **REMARKS** (CL-ML) Silty Clay, gray to dark gray, slightly moist to dry, stiff to hard, with trace of gravel, calcareous Organic rich 0-2 feet 100 Color change to orange-brown mottled yellow-brown and chalk/limestone in joints 7.5-11.5 feet 5 CL-ML GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ ST₁ 84 PP = 4.5 + tsf10 526.1 (CL-ML) Silty Clay, orange/brown/gray mottled brown, hard, slightly moist to dry, calcareous, with traces of sub-rounded gravel 85 PP = 4.5 + tsf15 PP = 4.5 + tsfST3 85 LL = 66 CL-ML PI = 3920 Shell fragments at 20 feet ST4 PP = 4.0-4.5 + tsf64 25 512.6 Silty Clay Shale, dark gray, hard, dry, calcareous, unweathered Orange-brown staining in fractures 25-30 feet PP = 4.5 + tsfST5 Weathered to 80 Unweathered zone 30 PP = 4.0 tsf MC = 18% DD = 103 pcf 87 LL = 74 PI = 52Limestone lenses in fractures 35-55 feet Fines = 90%Revision 0 4-D-74 May 2020 (Continued Next Page)

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

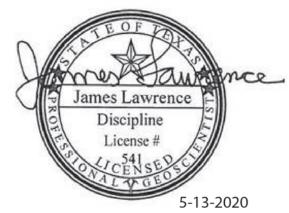
CLIENT City of Waco

PROJECT NAME _City of Waco Landfill MSW-2400

PROJECT LOCATION Waco, Texas



Bottom of borehole at 63.0 feet.



May 2020 Revision 0 4-D-75

SCS ENGINEERS **BORING NUMBER B-32** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas **COMPLETED** 10/12/18 DATE STARTED 10/11/18 **GROUND ELEVATION** 526.3 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine **CHECKED BY** J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS AND** MATERIAL DESCRIPTION **REMARKS** MH 1 0.5 (MH) Clayey Silt, brown, slightly moist to moist, soft to hard, organic (CL-ML) Silty Clay, orange-brown mottled brown and gray, slightly moist to dry, hard, 525.8 calcareous, with weathered shale Traces of small sub-rounded gravel 2.5-5 feet Chalk in joints 5-10 feet 5 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C:\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 50 PP = 4.5 + tsf50 10 25 CL-PP = 4.5 + tsf56 ML James Lawrence 15 Discipline License # 25 PP = 4.5 + tsf47 5-13-2020 20 29 ST4 PP = 4.5 + tsf58 Weathered to 501.8 Unweathered 25 Silty Clay Shale, dark gray to gray, very hard, slightly moist, with orange-brown zone staining in joints, weathered 25 ST5 PP = 4.5 + tsf68 29.0 497.3 Silty Clay Shale, dark gray to gray, very hard, slightly moist, calcareous, with lighter 30 colored material, unweathered 100 PP = 4.5 + tsf25 494.3 Bottom of borehole at 32.0 feet.

	S ENGI 1 Central D						WELL NUMBER B-33 (PZ-33) PAGE 1 OF 2
Bed	Iford, Texa	s 7602	1				PAGE 1 OF 2
CLI	ENT City	of Wa	CO				PROJECT NAME City of Waco Landfill MSW-2400
PR	OJECT NU	MBER	16216088				PROJECT LOCATION Waco, Texas
DA	TE START	ED <u>1</u> 1	1/19/18	COMPLETE	ED _11	1/20/18	GROUND ELEVATION 539.4 ft HOLE SIZE 8.25 inches
DR	ILLING CO	NTRAC	CTOR BES	T Drilling			GROUND WATER LEVELS:
DR	ILLING ME	THOD	Continuou	s Flight Auger			AT TIME OF DRILLING No Groundwater
LO	GGED BY	T. De	rstine	CHECKED	BY J	. Lawre	ence AT END OF DRILLING No Groundwater
NO	TES						AFTER DRILLING No Groundwater
O DEPTH	0, ₽	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION WELL DIAGRAM
						1 7 1 1 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	Clayey Silt Topsoil, dark brown, soft to firm, moist, with roots and organics
-	-	60					(CL-ML) Silty Clay, orange-brown mottled brown/tan, hard, moist to slightly moist, with white chalky material, calcareous
5	1						Silty/micaceous interbeds 5-15 feet
.GPJ	ST	33 89	13-29-37				
WACO	SPT	100	(55)	PP = 4.5+ tsf	CL-		
TE 50	_				ML		
)	+					
ONEC	ST	33 67	22-50				
AT/PR	SPT	_	22 00	PP = 4.5+ tsf			
NGIN							
E 15	5]						15.0 524.4
TS/BE		21					(CL-ML) Silty Clay, orange-brown mottled brown and light gray, hard, slightly moist,
AE L	ST:	3 21					with black iron staining, fossil remnants, and silty/micaceous interbeds, calcareous
1000	_	89		PP = 4.5+ tsf			
BLIC	4						Weathered shale marl transition zone and mostly gray color at 25 feet
20			=		_		
USER	- ST	21			CL-		
GENERAL BH / TP / WELL - GINT STD US LAB GDT - 2/4/19 15:51 - C:\USERS\PUBLIC\DOCUMENT\S\BENTLE\MG\INT\PROJECTS\SITE 50 WACO.GPJ 10	- 314	49	-	PP = 4.5+ tsf	ML		
9 15:5	-	73		11 - 7.01 (3)			
25	, -						
-TOS			1		1		
LAB.(ST	25 94	20-40-50 (90)				
SD Q	SPT	_	(55)	PP = 4.5+ tsf	L		28.0 511.4
TST				Weathered to Unweathered	CL-		(CL-ML) Silty Clay Shale Marl, gray, hard, slightly moist, calcareous, unweathered
5 30]	zone	ML		30.0
WELL		1-	1				Orange-brown staining at 28.2 and 29.7 feet Shale Marl, gray, very hard, slightly moist,
<u> </u>	ST	f 17					with fossil remnants, calcareous,
HH/		100		PP = 4.5+ tsf			unweathered
ERAL							
35	5	00.0					4 0.77
	Revis	UIIU					4-D-77 (Continued Next Page) May 2020

WELL NUMBER B-33 (PZ-33) PAGE 2 OF 2

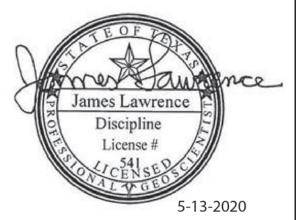
1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00 PROJECT LOCATION Waco, Texas

	1 1100		.DL.	10210000	.00			PROJECT LOCATION _waco, rexas	
	0EPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
	 40	ST7	17 28 100	50	PP = 4.5+ tsf			Shale Marl, gray, very hard, slightly moist, with fossil remnants, calcareous, unweathered (continued)	
	 45		74						
S\SITE 50 WACO.GPJ	 50	ST8	21 28 90	50	PP = 4.5+ tsf				
3ENTLEY\GINT\PROJECT	 - 55	-	76					55.0 484.4 Bottom of borehole at 55.0 feet.	
8:51 - C:\USERS\PUBLIC\DOCUMENTS\E								Bottom of borefiole at 55.0 feet.	
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C:\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ								James Lawr Discipline License #	2
GE		Revisio	n O					4-D-78	May 2020



Revision 0 May 2020 4-D-78

SCS ENGINEERS **BORING NUMBER B-34** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 PROJECT NUMBER _ 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 11/17/18 **COMPLETED** 11/17/18 **GROUND ELEVATION** 535.65 ft **HOLE SIZE** 8.25 inches DRILLING CONTRACTOR BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Millbrand CHECKED BY J. Lawrence AT END OF DRILLING --- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater TYPE/NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY DEPTH (ft) SAMPLE U.S.C.S. **TESTS** AND MATERIAL DESCRIPTION **REMARKS** Topsoil, dark brown to black, very soft, with roots, organic material, and 11.11 2.0 533.7 (CL-ML) Silty Clay, light brown mottled white, very hard, dry, with some 50 chalky material, calcareous ML 5 530.7 5.0 (CL-ML) Silty Clay, brown-orange, very hard, dry to slightly moist, with 14-22-34 some sub-round to round pebbles, calcareous 23 ST1 BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 83 (56)SPT 20 PP = 4.0-4.5 + tsfML 10 525.7 10.0 (CL-ML) Silty Clay, light brown to white mottled gray, medium soft to medium hard, dry, with some orange staining and chalky white material, PP = 0.5-3.0 tsf calcareous 28 MC = 14%CL-32 ML LL = 57 PI = 38Fines = 82% 15 520.7 15.0 (CL-ML) Silty Clay, light brown to orange mottled gray, medium hard, dry, calcareous 75 Less chalky white material throughout CI -13-20-29 PP = 2.0-3.0 tsf 60 Transition zone ML (49)133 20 515.7 PP = 3.0-4.5 + tsfClayey Shale, gray with orange-brown staining, moderately hard to very hard, dry, calcareous, weathered MC = 16% 15 ST4 DD = 111 pcf 31 LL = 63 PI = 43Fines = 95% 25 26.0 509.7 15 24-50 Weathered to Clayey Shale, light gray with some orange-brown, very hard, dry, with 33 Unweathered some crystalline mineral deposits, calcareous zone 100 SPT3 PP = 4.5+ tsf 30 30.0 505.7 Shale Marl, dark gray with very little orange staining, very hard, dry, with minor fossil fragments, slightly calcareous 15 PP = 4.5 + tsf100

4-D-79

GENERAL

Revision 0

PAGE 2 OF 2

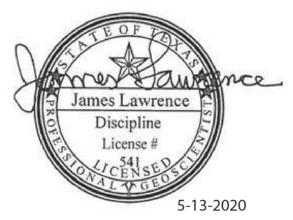
1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

CLIENT City of Waco

PROJECT NAME _ City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00 PROJECT LOCATION Waco, Texas

DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	
							Shale Marl, dark gray with very little orange staining, very hard, dry, with minor fossil fragments, slightly calcareous (continued)	
	ST7	15 33	50					
-	SPT4	92		PP = 4.5+ tsf				
_ 40		100		PP = 4.5+ tsf				
				11 - 4.5* (5)			41.0	494.7
	ST8	50					Bottom of borehole at 41.0 feet.	



Revision 0 4-D-80 May 2020

SCS ENGINEERS **BORING NUMBER B-35** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 12/12/18 **COMPLETED** <u>12/12/18</u> **GROUND ELEVATION** 553.3 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY DEPTH (ft) U.S.C.S. **TESTS** AND MATERIAL DESCRIPTION **REMARKS** Clayey Silt (top 0.5') to Silty Clay, brown, soft to firm, moist to very moist, with roots and organics 1.1/ 2.0 551.3 (CL-ML) Silty Clay, brown, stiff, moist, with traces of sub-rounded gravel 100 and roots CL-ML 5 547.8 (CL-ML) Silty Clay, orange-brown stained gray and brown, stiff, moist, 15-18-18 ST1 weathered 78 (36)CL-PP = 4.5 tsfWhite chalky zone 6.5-7 feet ML Sandy zone (gray to brown) at 9 feet White chalky material 9-10 feet 10 10.0 543.3 Silty Clay Shale Marl, orange-brown mottled gray and brown, stiff to hard, slightly moist to moist, calcareous, weathered 38 ST2 Traces of white gravel sized nodules 10-13.5 feet 85 PP = 4.5 tsfGray silty lenses 15-34.8 feet 15 33 19-24-34 ST3 100 (58)PP = 4.5 tsf 85 20 29 ST4 46 PP = 3.0-4.5 tsf25 21-36-40 (76)117 100 PP = 4.5 tsf SPT3 30 21 ST6 56 PP = 4.5-4.5 + tsfWeathered to Revision 0 4-D-81 May 2020 (Continued Next Page)

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ

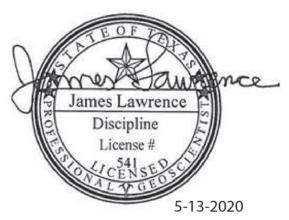
PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJ	ECT NUM	BER	16216088	.00			PROJECT LOCATION Waco, Texas
25 DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
	SPT4	28	50	Unweathered zone			Silty Shale Marl, gray, hard, slightly moist, calcareous, unweathered
	SP14	28 13 90		PP = 4.5+ tsf PP = 4.5+ tsf			Orange-brown stained zone 37.5-38 feet
	017			11 1.0 101			
40							
 		76					Trace of fossil remnants and silty/limey lenses 40-59 feet (continued)
45				DD 45:44			
	ST8	17 28	50	PP = 4.5+ tsf MC = 13%			
	SPT5	70		DD = 109 pcf LL = 54			
_				PI = 33			
50				Fines = 75%			
 55		73					
 		108					
							Bottom of borehole at 59.0 feet.
50 55							James Lawrence Discipline License #
							5-13-2020



May 2020 4-D-82 Revision 0

SCS ENGINEERS **BORING NUMBER B-36** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 1/8/19 COMPLETED 1/9/19 **GROUND ELEVATION** 532.5 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater **LOGGED BY** T. Derstine CHECKED BY J. Lawrence AT END OF DRILLING --- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater TYPE/NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY DEPTH (ft) SAMPLE U.S.C.S. **REMARKS** MATERIAL DESCRIPTION MH 0.5 532.0 (MH) Clayey Silt, brown, soft, moist, with roots and organics (CL-ML) Silty Clay, brown grading to light gray, firm to stiff, moist, with organics in top layer and trace of subrounded gravel in bottom layer 100 CL-ML 5 527.5 5.0 (CL-ML) Silty Clay, light gray, stiff, slightly moist to moist, with some orange-brown staining, white chalky material, and some gravel, 58 calcareous 10-14-19 PP = 2.0 tsf 94 (33)100 Color change to orange-brown mottled gray and brown at 7.5 feet 10 CI ML PP = 4.5 tsf 50 ST2 100 15 Silty Clay Shale Marl, orange-brown stained gray and brown, stiff to hard, PP = 4.0 tsfslightly moist, with very fine sandy laminate layers 15-24-31 29 ST3 MC = 18% 94 (55)LL = 56 SPT2 PI = 35Fines = 91%20 25 PP = 4.0 tsfST4 40 25 Crystalline material in joints at 25 feet 7-15-50 PP = 3.5 tsf(65)94 71 SPT3 Color change to mostly dark gray at 27 feet 30 PP = 4.5 tsfMC = 17%DD = 115 pcf 25 ST6 LL = 64 PI = 39 68 Fines = 93% Weathered to 498.5 34.0 Unweathered zone Revision 0 4-D-83

BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ

PAGE 2 OF 2

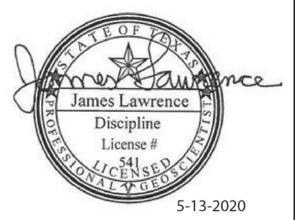
1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER _ 16216088.00 PROJECT LOCATION Waco, Texas

FROSE	ECT NOW	IDLIN	16216088.	00			PROJECT LOCATION Waco, Texas
(#) (#)	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
							Shale Marl, dark gray, hard, slightly moist, calcareous, unweathered
	ST7	17 _50	35-50	PP = 4.5 tsf			Occasional orange-brown staining 34-40 feet
	SPT4	54					
40							
	ST8	21		PP = 4.5 tsf			Silty/limey laminate layers 42-58 feet (continued)
		44					
45							
	0.70	25	00.50				
5 -	ST9	25 50	33-50	PP = 4.5 tsf			
-	SPT5	100					
50							
30							
		100					
55							
	CT10	21 28	50	PP = 4.5 tsf			
	ST10	60					58.0 474.
	SPT6		1				Bottom of borehole at 58.0 feet.
55							James Lawrence Discipline License #
							5-13-2020



May 2020

SCS ENGINEERS **BORING NUMBER B-37** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 12/6/18 **COMPLETED** <u>12/11/18</u> **GROUND ELEVATION** 526.9 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater **LOGGED BY** T. Derstine CHECKED BY J. Lawrence AT END OF DRILLING --- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. SAMPLE **TESTS AND** MATERIAL DESCRIPTION **REMARKS** (ML) Silt, gray, soft, moist, with a trace of clay and roots/organics MI 525.9 (CL-ML) Silty Clay, light gray, firm to stiff, slightly moist to moist, with white chalky material in areas, trace of gravel, and roots 86 CL-ML 5 521.9 (CL-ML) Silty Clay, light gray to brown, stiff, slightly moist to moist, with white chalky areas and trace of sub-rounded gravel CL-56 ML 10 516.9 CL-(CL-ML) Sandy Silty Clay, light brown to tan, firm, slightly moist to moist, trace of 515.9 ML (CL-ML) Silty Clay, orange-brown mottled gray and brown, hard, slightly moist to moist, with white chalky material in joints/bedding, calcareous, weathered 90 15 90 ML 20 90 503.4 Shale Marl (Silty Clay), gray with trace of orange-brown staining, hard, slightly moist, calcareous, weathered 25 Weathered to 26.0 Transition zone 500.9 Unweathered Shale Marl (Silty Clay), gray, hard, slightly moist, with fossil remnants, calcareous, zone unweathered 98 30 84 May 2020 Revision 0 4-D-85 (Continued Next Page)

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GP\

PAGE 2 OF 2

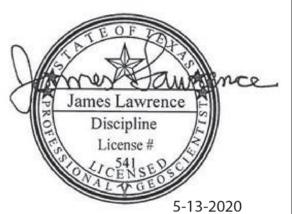
1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00 PROJECT LOCATION Waco, Texas

L		-01 11011		102 10000.00	_		FROJECT LOCATION _Waco, Texas	
	(#) (#)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	
- -	40		96				Shale Marl (Silty Clay), gray, hard, slightly moist, with fossil remnants, calcareous, unweathered (continued)	
-	 45		90					
S\SITE 50 WACO.GPJ	50		100		-			
OJECT			100				52.0	474.9
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ							James Lawrence Discipline License #	-1
GENER		Revisio	n û				5-13-2020 4-D-86 May 2020	



SCS ENGINEERS **BORING NUMBER B-38** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 12/4/18 **COMPLETED** <u>12/5/18</u> **GROUND ELEVATION** 529.85 ft **HOLE SIZE** 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater **LOGGED BY** T. Derstine CHECKED BY J. Lawrence AT END OF DRILLING --- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater TYPE/NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY DEPTH (ft) SAMPLE U.S.C.S. **TESTS** AND MATERIAL DESCRIPTION **REMARKS** ML(ML) Silt, brown, dry to slightly moist, soft 529.2 0.7 (CL-ML) Silty Clay, dark brown to brown, firm to hard with depth, slightly moist to moist, with roots/organics and trace gravel 66 CL-ML 5 524.9 5.0 (CL-ML) Silty Clay, light gray with orange-brown staining, slightly moist, firm to stiff, with white chalky material and trace sub-rounded gravel 15-25-25 94 (50)PP = 2.0-3.5 tsf 63 ML 10 10.0 519.9 Sandy Clay, brown, firm to stiff, slightly moist, with trace of white chalky spots and trace sub-rounded gravel at top, calcareous Fossil remnants 15-17 ft 36 15 17.0 512.9 (CL-ML) Silty Clay, brown, stiff, slightly moist, with trace of white chalky 22 material and gravel, calcareous CL-ML 20 509.9 Silty Clay Shale Marl, brown and gray, stiff, slightly moist to moist, with orange-brown staining and trace fossil remnants, calcareous, weathered 40 25 Weathered to 27.0 502.9 Unweathered Shale Marl (Silty Clay), gray, hard, slightly moist to moist, with fossil 66 zone remnants, calcareous Orange-brown staining 28-28.2 feet 30 48 Revision 0 4-1)-87 May 2020 (Continued Next Page)

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C:\USERS\PUBLIC\DOCUMENTS\BENTLEY\G\NT\PROJECTS\S\ITE 50 WACO.GPJ

PAGE 2 OF 2

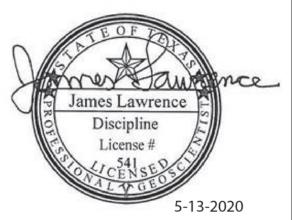
1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJ	ECT NUM	IBER	16216088	.00			PROJECT LOCATION Waco, Texas
OEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
							Shale Marl (Silty Clay), gray, hard, slightly moist to moist, with fossil
							remnants, calcareous
		54					
-							
40							Light gray limey lenses 40-55 feet (continued)
-							
-		66					
-							
45							
45							
<u>-</u>							
		60					
50							
5 50							
		44					
<u></u>							
50							
55							55.0 474.9 Rottom of borehole at 55.0 feet

Bottom of borehole at 55.0 feet.



May 2020 Revision 0 4-D-88

1901 Bedfo	S ENGIN Central Dr ord, Texas phone: 817	ive S1 76021	TE 550				BORING NUMBER B-39 PAGE 1 OF 2
	ENT <u>City o</u>		16216088.00				PROJECT NAME City of Waco Landfill MSW-2400 PROJECT LOCATION Waco, Texas
DAT	E STARTE	D 12	/5/18	СОМР	LETE	D 12/6/18	GROUND ELEVATION 522.95 ft HOLE SIZE 8.25 inches
DRIL	LING CON	TRAC	TOR BEST Dril	ling			GROUND WATER LEVELS:
DRIL	LING MET	HOD	Continuous Fligh	ht Auge	r		AT TIME OF DRILLING No Groundwater
LOG	GED BY	T. Der	stine	CHEC	KED E	J. Lawrence	AT END OF DRILLING No Groundwater
NOT	ES						AFTER DRILLING No Groundwater
O DEPTH	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION
-	-			ML		(CL-ML) Sil	ark brown to brown, soft, moist, with a trace of clay and roots ty Clay, brown to gray, firm to stiff, slightly moist to moist, with trace s, fossil remnants, and white chalky material
F	-	84				Color chang	ge to orange-brown mottled gray and brown at 5 feet
-	-			CL-		Sandy from	5-7 feet
5				_ ML			
TSISITE 50 WACO.GPJ	- - -	100			_	8.6 (CL-ML) Sil trace of whi	514 ty Clay, orange-brown mottled gray and brown, hard, slightly moist, with te chalky material and gravel, calcareous
ABENTLEYGINT/PROJECTS/SITE 50 WACO.GPJ	- - -	60					
SCIPPING OF THE STATE OF THE ST	- - -	76		CL- ML			
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\ 0.0000000000000000000000000000000000	- - -	52					
INT STD US LAB.GD	- - - -	70				29.0 Shala Mad	mostly grov with groups brown staining bard slightly maint with trops
30				4		Snale Marl, chalky white	mostly gray with orange-brown staining, hard, slightly moist, with trace e material, fossil remnants, and limey lenses, calcareous
SENERAL BH / TP / WEI	- - - -	66					cone from weathered to unweathered
<u>შ 35</u>	Revisio	n 0				- 4-€	0-89 (Continued Next Page) May 2020

PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021

Telephone: 817-571-2288

 CLIENT
 City of Waco
 PROJECT NAME
 City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00 PROJECT LOCATION Waco, Texas

35 DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	
 40		100	Weathered to Unweathered zone			Shale Marl, mostly gray with orange-brown staining, hard, slightly moist, with trace chalky white material, fossil remnants, and limey lenses, calcareous Transition zone from weathered to unweathered (continued) Shale Marl, gray, hard, slightly moist, with limey lenses, calcareous, unweathered	485.0
 45		80					
WACO.GPJ		100				48.0 Rottom of horehole at 48.0 feet	475.0

Bottom of borehole at 48.0 feet.



Revision 0 4-D-90 May 2020

SCS ENGINEERS **BORING NUMBER B-40** 1901 Central Drive STE 550 PAGE 1 OF 1 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas **COMPLETED** 12/5/18 **GROUND ELEVATION** 522.8 ft DATE STARTED 12/5/18 HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine **CHECKED BY** J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. **TESTS AND** MATERIAL DESCRIPTION **REMARKS** (CL-ML) Silty Clay, brown, firm to stiff, slightly moist to moist, with trace sub-rounded gravel, fossil remnants, roots Sandy at 5 feet 40 CL-ML 5 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GP. 515.8 (CL-ML) Silty Clay, orange-brown mottled brown and gray, stiff, slightly moist to 100 moist, with white chalky material/gravel and fossil remnants, calcareous Crystalline pockets 10-19 feet 10 88 CL-James Lawrence ML Discipline 15 76 5-13-2020 503.8 (CL-ML) Silty Clay, gray with trace of orange-brown staining, hard, slightly moist, 20 with fossil remnants, calcareous, unweathered Transition zone CL-54 ML 25 Weathered to 496.8 Unweathered (CL-ML) Shale Marl, gray, hard, slightly moist, with fossil remnants, calcareous, 100 zone CLunweathered ML 494.8 Bottom of borehole at 28.0 feet.

1901 Cer Bedford, Telephon	Texas 76 ie: 817-	e STE 550 6021 571-2288	0					WELL NUI	MBEK	B-41 (PZ-41 PAGE 1 OF
CLIENT	-						PROJECT NAME City		ISW-2400	
		SER _1621					PROJECT LOCATION _			
						12/18/18			HOLE SIZE	8.25 inches
			BEST Drilli							
				CHEC	KED BY	J. Lawrence				
NOTES							AFTER DRILLING	No Groundwa	ater	
O DEPTH (ft)			TESTS AND EMARKS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTI	ON		WELL DIAGRAM
-		72		CL- ML		moist to ver roots/organi	y Clay, dark brown to gray y moist, with a trace of gra cs	, soft to stiff, vel and	700.0	
5 10		44		CL- ML		orange-brov large sub-ro	y Clay, gray grading to bro n stained, stiff, moist, with unded gravel and white ch e to orange-brown stained	trace of small to alky material	530.0	
15		34			1	brown and o	y Clay Shale Marl, orange ray, stiff to hard, moist, wi enses in bedding, calcareo	th white	523.0	
20		82		CL-						
25		44		ML						
- - - -		54			2	29.0 Shale Marl.	dark gray with orange-bro	wn stainining in	506.0	
30		56				joints, hard, unweathere	slightly moist to moist, cal			
25										
35 R	evision	0				4-D	-92 (Continued Next Page	1	IV	ay 2020

WELL NUMBER B-41 (PZ-41) PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021

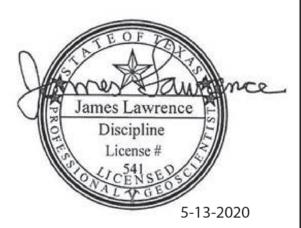
Telephone: 817-571-2288

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00 PROJECT LOCATION Waco, Texas

DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
 40		56				Shale Marl, dark gray with orange-brown stainining in joints, hard, slightly moist to moist, calcareous, unweathered Trace of crystalline areas 29-30 feet (continued)	
 45		100	Weathered to Unweathered zone			3.0 Shale Marl, gray to dark gray, hard, slightly moist, with lighter limey/silty lenses, fossil remnants, and crystalline areas, unweathered	2.0
CTS/SITE 50 WACO.GPJ		100					
RSIPUBLICIDOCUMENTS\BENTLEY\G\int\PROJECTS\S\ITE 50 WACO.GPJ 0		100					
SSPUBLICODOCUMEN 9 1 1 1		50					5.0
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C:\USER.						Bottom of borehole at 60.0 feet. James Law Discipli License	ne S



4-D-93 May 2020 Revision 0

SCS ENGINEERS **BORING NUMBER B-42** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 12/6/18 **COMPLETED** 12/6/18 **GROUND ELEVATION** 527 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. **TESTS AND** MATERIAL DESCRIPTION REMARKS ML 0.5 526.5 (ML) Silt, gray, soft, moist, with roots and organics (CL-ML) Silty Clay, brown-gray, firm to stiff, moist, with a trace of gravel, roots, and white spots 100 CL-ML5 522.0 (CL-ML) Silty Clay, gray, stiff, moist, with white chalky material and trace of sub-rounded gravel CL-72 ML Orange-brown staining at 9-10 feet 10 517.0 (CL-ML) Silty Clay, gray and brown with orange-brown staining, stiff to hard, slightly moist to moist, with white chalky material/spots, weathered CL-86 ML 15 512.0 (CL-ML) Silty Clay (Shale Marl), gray and brown with orange-brown staining, stiff to hard, slightly moist to moist, with white chalky material/spots, weathered 80 20 CL-ML Discipline 25

More gray 28-30 feet (transition zone)

496.0

495.0

5-13-2020

Shale Marl, gray, hard, slightly moist, with white chalky material/specs, calcareous

Bottom of borehole at 32.0 feet.

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GP.

30

80

100

Weathered to

Unweathered

zone

	ENGINI						WELL NUMBER B-43 (PZ-43)
	Enginee Central I						PAGE 1 OF 4
Ste. 5		6024					
	rd, TX 7 I T City o						PROJECT NAME City of Waco Landfill MSW-2400
				.00			PROJECT LOCATION Waco, Texas
						2/17/19	9 GROUND ELEVATION 548.86 ft HOLE SIZE 8.25 inches
1				T Drilling; West Dr			GROUND WATER LEVELS:
DRILL	ING ME	THOD	Continuo	us Flight Auger			AT TIME OF DRILLING No Groundwater
LOGG	ED BY	T. De	erstine; A. Bo	oudreaux CHECK	(ED B	Y J. L.	
NOTE	s						AFTER DRILLING
O DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION WELL DIAGRAM
					MH		(MH) Clayey Silt, dark brown, soft, very moist, with trace of gravel and organics
		47			CL- ML		(CL-ML) Silty Clay, dark brown, hard, moist, with trace of gravel and organics 5.0 543.9
		00	1-0				(CL-ML) Silty Clay, orange-brown mottled gray and brown, stiff to hard, slightly moist to
	ST1	29 93	15-27-50 (77)				moist, with white chalky material in
	SPT1	67		PP = 4.5 tsf	CL- ML		interbeds, calcareous
10							10.0 538.9
00 WACO.GFJ	ST2	29 28		PP = 4.5 tsf MC = 18% DD = 111 pcf LL = 60			(CL-ML) Silty Clay (weathered shale/marl), orange-brown stained light gray and brown, stiff to hard, slightly moist, calcareous, weathered
				PI = 40			White chalky material in interbeds 10-16 feet
$\frac{9}{5}$ 15				Fines = 95%			Black iron staining in joints/interbeds 20-24
KOUE(25	21-39-50				feet a feet
	ST3	25 93	(89)				Weathered to unweathered transition at 25 feet
5 -	SPT2	67		PP = 4.5 tsf	CL- ML		
] - -							
20							
20	ST4	25					
<u>- - </u>	514		_	DD = 45: 1-1			
<u>-</u>		80		PP = 4.5+ tsf			
25							
· 23 _							25.0 523.9 (CL-ML) Silty Clay, (shale/marl) gray with
- LAB:GD1	ST5	17 72	26-50	PP = 4.5+ tsf MC = 16%			some orange-brown staining, hard, calcareous, with white fossil remnants
	SPT3	$\overline{}$		DD = 117 pcf			School South Mills 1886 Formation
	29			LL = 61 PI = 42	CL- ML		
30				Fines = 94%	IVIL		
, well							
<u>}</u>	ST6	21		Weathered to			32.0
		60	1	Unweathered zone			
26 - 26 - 26 - 26 - 26 - 26 - 26 - 26 -				PP = 4.5+ tsf			
35							
	Revisio	วท บิ				·	4-D-95 (Continued Next Page) May 2020

SCS ENGINEERS

SCS Engineers 1901 Central Dr Ste. 550 Bedford, TX 76021

WELL NUMBER B-43 (PZ-43) PAGE 2 OF 4

	T City o			00			PROJECT LOCATION Wass Taylor	-2400
KOJE	1	IBEK	16216088	00	1		PROJECT LOCATION Waco, Texas	
(#) (#)	SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
-	ST7	19					Silty Shale Marl, gray, hard, slightly moist, calcareous, unweathered	
_	317	50					Occasional orange-brown staining and fossil remnants in beds 32-43 feet	
-								
40		47					White crystalline material in bedding/joints at 35 feet	
	ST8	17 80		PP = 4.5+ tsf			Micaceous interbeds and traces of fossil remnants 45-70 feet	
-		00		PP = 4.5+ (SI				
45								
-	ST9	21 28	50	PP = 4.5+ tsf MC = 16%				
-	SPT4			DD = 108 pcf LL = 63 PI = 40				
50				Fines = 95%				
-								
-		60						
55		47	50					
	ST10	17 22 43	50	PP = 4.5+ tsf				
+	SPT5	43		FF = 4.5+ (SI				
60								
-		87						
65								
Ŧ	ST11	17						
	3.11	67		PP = 4.5+ tsf				
]								
70	\dashv			DD = 45: 1-1	-			
-		02		PP = 4.5+ tsf LL = 60				
-		83		PI = 40 MC = 15%				
75 	Revisio	n 0		Fines = 91%			75.0 4: 4-D-96 (Continued Next Page)	73.9 May 2020

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SCS Engineers 1901 Central Dr Ste. 550

WELL NUMBER B-43 (PZ-43)
PAGE 3 OF 4

Bedford, TX 76021 CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00						PROJECT LOCATION Waco, Texas			
SAMPLE TYPE/NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM		
- - - -	100					Shale with minor, very fine sand to silt. Dark gray, very hard, moist, laminated Few, small fossils			
	100					Becoming harder with depth Fewer laminations with depth 80-85' very small mica flakes			
85 - - - - 90	100					85-95' some fossils			
95	100								
	85								
105	90								
110	100								
	100					Large bivalve fossil @ 110' Shale with minor, very fine sand. Dark gray, very hard, moist, trace lamination			

SCS ENGINEERS

SCS Engineers 1901 Central Dr Ste. 550 Bedford, TX 76021 WELL NUMBER B-43 (PZ-43)
PAGE 4 OF 4

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

	NUMBER	16216088	.00		PROJECT LOCATION _Waco, Texas				
OEPTH (ft) (ft) SAMPLE					GRAPHIC LOG	MATERIAL DESCRIPTION WELL DIAGRAM			
	100		LL = 68 PI = 46 MC = 12%			Shale with minor, very fine sand to silt. Dark gray, very hard, moist, laminated			
120	80		Fines = 81%	-		Becoming harder with depth			
125	75			_		Trace sands transitioning to no sands below 125'			
130	70			-		Scarce laminations			
135				_		Featureless			
140	95			_		James Lawrence Discipline			
145	100					Discipline License # 5-13-2020			
- - -	20		LL = 75 PI = 50 MC = 15% Fines = 99%			Shale. Dark gray, very hard, moist, no lamination 150.0 398.9			

SCS ENGINEERS **BORING NUMBER B-44** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 10/10/18 **COMPLETED** 10/10/18 **GROUND ELEVATION** 551.2 ft HOLE SIZE 7.25 inches **DRILLING CONTRACTOR** West Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY V. Wooters CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY DEPTH (ft) U.S.C.S. **TESTS AND** MATERIAL DESCRIPTION **REMARKS** (CL) Clay, dark brown to black, hard, moist, non-calcareous Calcareous 4-5 feet. 100 CL 5 546.2 (CL-ML) Silty Clay, orange-tan mottled gray, hard, slightly moist, with ST1 chalk/limestone deposits in joints and fractures, calcareous 100 PP = 3.75-4.5+ tsf 10 PP = 4.5 + tsfST2 MC = 20%DD = 108 pcf80 LL = 71 PI = 49 Fines = 91% 15 No chalk/limestone in fractures 15-25 feet ST3 Minor sand and silt in fractures (gray) 15-39.5 feet PP = 4.5+ tsf 20 MLPP = 4.5 + tsfST4 MC = 21%DD = 105 pcf 60 LL = 79 PI = 55 Fines = 84% 25 ST5 50 PP = 3.0-4.5 + tsf30 PP = 3.0-4.5+ tsf ST6 MC = 25%DD = 97 pcf 60 LL = 72 PI = 51 Fines = 97%

(Continued Next Page)

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:52 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ

Revision 0

BORING NUMBER B-44 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 **CLIENT** City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. **TESTS** AND MATERIAL DESCRIPTION **REMARKS** 35 (CL-ML) Silty Clay, orange-tan mottled gray, hard, slightly moist, with chalk/limestone deposits in joints and fractures, calcareous ST7 100 PP = 3.0-4.5 + tsfML No chalk/limestone in fractures 15-25 feet Weathered to Minor sand and silt in fractures (gray) 15-39.5 feet (continued) 511.7 Unweathered 40 Shaley Clay, dark gray, hard, dry, slightly calcareous, weathered zone 510.2 ST8 Silty Clay Shale, dark gray, hard, dry, calcareous, with limestone intrusions in fractures 100 PP = 4.5 + tsf45 ST9 90 PP = 4.5+ tsf 50 PP = 4.5+ tsf 100 LL = 60 PI = 38 55 No limestone intrusions in fractures 55-76 feet 100 60 ST11 100 PP = 4.5 + tsf65 Interbedded heavily weathered zones 65-76 feet 100 70 ST12 100 PP = 4.5+ tsf Revision 0 4-D-100 May 2020 (Continued Next Page)

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:52 - C:\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ

BORING NUMBER B-44 1901 Central Drive STE 550 PAGE 3 OF 3 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. **TESTS** AND REMARKS MATERIAL DESCRIPTION

Bottom of borehole at 76.0 feet.

76.0



May 2020

475.2

Revision 0

4-D-101

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:52 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ

75

100

1		ENGII Central Di							BORING NUMBER B	
	Bedfo	rd, Texas hone: 81	76021	1					PAGE 1 C	JF 2
									DDO IFOT NAME O'R of Many Landfill MOW 0400	
		NT City o								
				16216088.00						
)/31/18						
				Continuous Fligh						
				Continuous Fligh			N 11		AT TIME OF DRILLING No Groundwater	
		S		ooters	CHEC	KED E	J. L	<u>-awrence</u>	AT END OF DRILLING No Groundwater AFTER DRILLING No Groundwater	
ŀ	NOTE			Ī	1				AFTER DRILLING NO GIOUNUWALEI	
	o DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS	U.S.C.S.	GRAPHIC LOG			MATERIAL DESCRIPTION	
-	 		100		CL- ML		4.0		ty Clay, dark brown, medium hard, moist, slightly calcareous, organic	541.5
	5							(CL-ML) Si calcareous	ty Clay, orange/tan mottled gray hard, slightly moist to dry, slightly	
SISITE 50 WACO.GPJ	 - 10	ST1	50	PP = 0-4.5+ tsf					d weathered zones 5-26 feet	
ENTLEY/GINT\PROJECT8	 - 15	ST2	50	PP = 0-4.5+ tsf	CL-					
SIPUBLICIDOCUMENTSIB	 - 20	ST3	100	PP = 0-4.5+ tsf	ML					
2/4/19 15:52 - C:\USER	 	ST4	100	PP = 0-4.5+ tsf						
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:52 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\G\NT\PROJECTS\SITE 50 WACO.GPJ		ST5	100	Weathered to Unweathered zone PP = 0-4.5+ tsf MC = 21% DD = 107 pcf LL = 66 PI = 46 Fines = 90%	CL		26.0	weathered	Clay, dark gray with orange/tan mottling, dry, hard, calcareous, with shale hale, dark gray, hard, dry, slightly calcareous, weathered	519.5 517.5
GENERAL BH / TP / WELL	 - 35	ST6	100	PP = 4.5+ tsf				4 -	102	
		Revisio	πU					4-D	-102 (Continued Next Page) May 2020	

PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00 PROJECT LOCATION Waco, Texas

	35 DEPTH (ft)	SAMPLE TYPE/NUMBER	RECOVERY %	TESTS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	
	40		100				Silty Clay Shale, dark gray, hard, dry, slightly calcareous, weathered (continued)	
	- - - 45	ST7,	100	PP = 4.5+ tsf MC = 15% LL = 58 PI = 38 Fines = 92%				
DJECTS\SITE 50 WACO.GPJ	50		100	PP = 4.5+ tsf				
DECTS		ST8					51.0 Bottom of borehole at 51.0 feet.	494.5

Bottom of borehole at 51.0 feet.



4-D-103 May 2020 Revision 0

58 CL-ML Silty Clay, orange-brown mottled brown, stiff to hard, slightly moist, with some gravel 50 CL-ML Silty Clay, orange-brown mottled brown, stiff to hard, slightly moist, with some gravel 55 CL-ML Silty Clay, orange-brown mottled brown, hard, slightly moist, calcareous, with chalk in joints and fossil fragments CL-ML Silty Clay, orange-brown mottled brown, hard, slightly moist, calcareous, with chalk in joints and fossil fragments		1901 C Bedford	ENGII Central D d, Texas one: 81	rive S ⁻ 7602	TE 550 1					BORING NUMBER B-46 PAGE 1 OF 2	
DRILLING METHOD Continuous Flight August CheckEd By J Lawrence NOTES CHECKED BY J Lawrence NOTES CHECKED BY J Lawrence AT END OF DRILLING No Groundwater AT END OF DRILLING No Groundwater AT END OF DRILLING No Groundwater			-							-	_
DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING No Groundwater AT FIND OF DRILLING No Groundwater		DATE	STARTE	D 11	/1/18	СОМР	LETE	D _11/	1/18	GROUND ELEVATION 559.25 ft HOLE SIZE 8.25 inches	
CL-MIL Sity Clay, orange-brown mottled brown, hard, slightly moist, calcareous, weathered ST2 29 PP = 4.5+ tsf ST3 33 PP = 4.5+ tsf ST4 33 PP = 4.5+ tsf ST5 33 PP = 4.5+ tsf More moist and softer 25-35 feet More moist and softer 25-35 feet		DRILL	ING CON	NTRAC	TOR BEST Drill	ing				GROUND WATER LEVELS:	
NOTES AFTER DRILLING — No Groundwater TESTS SAMPOND ALL BEST SAMPOND ALL BEST SAMPOND AND AND AND AND AND AND AND AND AND A		DRILL	ING MET	HOD	Continuous Fligh	nt Auge	r			AT TIME OF DRILLING No Groundwater	
MATERIAL DESCRIPTION Material Description Material Description Material Description		LOGG	ED BY	T. Der	rstine	CHEC	KED E	3Y <u>J.</u>	Lawrence	AT END OF DRILLING No Groundwater	
MH III 1.0 (Alth) Clayer, Slit, brown, soft to firm, moist, organic, with a trace of gravel and white change material (CL-ML) Slity Clay, orange-brown mottled brown, sliff to hard, slightly moist, with some gravel (CL-ML) Slity Clay, orange-brown mottled brown, hard, slightly moist, calcareous, with chalk in joints and fosall fragments ST1 33 (CL-ML) Slity Clay, orange-brown mottled brown, hard, slightly moist, calcareous, with chalk in joints and fosall fragments ST2 29 (CL-ML) Slity Clay, orange-brown mottled brown, hard, slightly moist, calcareous, weathered Chalk in joints 10-11.5 feet SSIty Shale, orange-brown mottled brown and gray, hard, slightly moist, calcareous, weathered Chalk in joints 10-11.5 feet SSIty lenses and crystalline deposits in interbeds 15-35 feet More moist and softer 25-35 feet More moist and softer 25-35 feet		NOTES	s							AFTER DRILLING No Groundwater	_
MH III 10 (MH) Clayey Slit, brown, soft to firm, moist, organic, with a trace of gravel and white challenges and control of the control of th			SAMPLE TYPE/NUMBER		AND	U.S.C.S.	GRAPHIC LOG			MATERIAL DESCRIPTION	
Silly Shale, orange-brown mottled brown, sliff to hard, slightly moist, with some gravel (CL-ML) Silty Clay, orange-brown mottled brown, hard, slightly moist, calcareous, with chalk in joints and fossil fragments (CL-ML) Silty Clay, orange-brown mottled brown, hard, slightly moist, calcareous, with chalk in joints and fossil fragments (CL-ML) Silty Clay, orange-brown mottled brown, hard, slightly moist, calcareous, with chalk in joints and fossil fragments (CL-ML) Silty Clay, orange-brown mottled brown, hard, slightly moist, calcareous, with chalk in joints and fossil fragments (CL-ML) Silty Clay, orange-brown mottled brown, hard, slightly moist, calcareous, with chalk in joints and fossil fragments (CL-ML) Silty Clay, orange-brown mottled brown, hard, slightly moist, calcareous, weathered Chalk in joints 10-11.5 feet (CL-ML) Silty Clay, orange-brown mottled brown, hard, slightly moist, calcareous, weathered Chalk in joints 10-11.5 feet (CL-ML) Silty Clay, orange-brown mottled brown, hard, slightly moist, calcareous, weathered Chalk in joints 10-11.5 feet (CL-ML) Silty Clay, orange-brown mottled brown, hard, slightly moist, calcareous, weathered Chalk in joints 10-11.5 feet (CL-ML) Silty Clay, orange-brown mottled brown, hard, slightly moist, calcareous, weathered Chalk in joints 10-11.5 feet (CL-ML) Silty Clay, orange-brown mottled brown, hard, slightly moist, calcareous, weathered Chalk in joints 10-11.5 feet (CL-ML) Silty Clay, orange-brown mottled brown, hard, slightly moist, calcareous, weathered Chalk in joints 10-11.5 feet (CL-ML) Silty Clay, orange-brown mottled brown, hard, slightly moist, calcareous, weathered Chalk in joints 10-11.5 feet (CL-ML) Silty Clay, orange-brown mottled brown, hard, slightly moist, calcareous, weathered (CLay) Silty Clay, orange-brown mottled brown and gray, hard, slightly moist, calcareous, weathered (CLay) Silty Clay, orange-brown mottled brown and gray, hard, slightly moist, calcareous, weathered (CLay) Silty Clay, orange-brown mottled brown and gr	Ī					МН	Ш	1.0			3.3
ST1 33 PP = 4.5+ tsf ID	-	 		58					(CL-ML) Sil	ty Clay, orange-brown mottled brown, stiff to hard, slightly moist, with	
ST3 33 PP = 4.5+ tsf 100	30.GPJ	5 	ST1		PP = 4.5+ tef	CL-		5.0	(CL-ML) Sil with chalk in	ty Clay, orange-brown mottled brown, hard, slightly moist, calcareous,	<u>1.3</u>
ST3 33 PP = 4.5+ tsf 100	S\SITE 50 WAC	 10		76	11 - 4.51 (5)	ML		10.0	Silty Shale	orange brown mottled brown and gray, hard, slightly moist, calcareous	9.3
ST3 33 PP = 4.5+ tsf 100	ECT								-	orange-brown motified brown and gray, maid, silgnity moist, calcareous,	
ST3 33 PP = 4.5+ tsf 100	PRO		ST2	29	DD 45.44					nts 10-11 5 feet	
ST3 33 PP = 4.5+ tsf 100	ENTLEYIGINT	 15		100	PP = 4.5+ tst						
	MTS/B								Only lenses	and drystalline deposits in interbeds 15-55 feet	
	UME		ST3	33							
	SIPUBLICIDOC	 20		100	PP = 4.5+ tsf						
	D:\USERS	_	ST4	33							
	5:52 - (014		PP = 4.5+ tsf						
	119 15										
	- 2/4,	25									
	GDT.								More moist	and softer 25-35 feet	
	SLAB		ST5	33							
	Ď L	_		71	PP = 3.0 tsf						
	NT S										
	L- G	30	_								
	WEL										
	/TP/		ST6	38							
	LBH	_		61	PP = 1.0-4.0 tsf	·					
	ERA										
	BE	35	Revision	on ()					4-D	-104 (Continued Mayt Rose) May 2020	_

BORING NUMBER B-46 1901 Central Drive STE 550 PAGE 2 OF 2 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS** AND REMARKS MATERIAL DESCRIPTION 35 33 ST7 PP = 3.0-4.5 tsf 71 40 40.0 519.3 Silty Shale, gray, hard, slightly moist, calcareous, with silty lenses in interbeds 21 PP = 4.5 + tsfST8 Weathered to Traces of orange-brown staining 40-65 feet 96 Unweathered zone 45 PP = 4.5 + tsfShell/fossil fragments 45-65 feet MC = 13% GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:52 - C:\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\S\ITE 50 WACO.GPJ 21 ST9 DD = 110 pcf 96 LL = 62 PL = 41 Fines = 94% 50 74 55 25 James Lawrence ST10 PP = 4.5 + tsf95 Discipline License # 60 PP = 4.5+ tsf 5-13-2020 80 65 Bottom of borehole at 65.4 feet. 17 ST11 Revision 0 4-D-105 May 2020

SCS ENGINEERS WELL NUMBER B-47 (PZ-47) 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 **CLIENT** City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 10/11/18 **COMPLETED** 10/12/18 **GROUND ELEVATION** 532.4 ft HOLE SIZE 7.25 inches **DRILLING CONTRACTOR** West Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY V. Wooters CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater SAMPLE TYPE/NUMBER GRAPHIC LOG RECOVERY DEPTH (ft) U.S.C.S. **REMARKS** MATERIAL DESCRIPTION WELL DIAGRAM ML 0.5 531.9 (ML) Silt, dark brown, soft, moist (CL) Clay, light gray, hard, dry, calcareous, with chalk in fractures 100 CL 5 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:52 - C;UVSERS/PUBLIC/DOCUMENTS/BENTLE?\GINT\PROJECTS\SITE 50 WACO.GPJ ST1 7.0 525.4 PP = 4.5 + tsf(CL-ML) Silty Clay, orange-tan mottled gray, hard, dry, 100 calcareous, with chalk in fractures/joints Trace of sub-angular gravel 1/8" at 7-10 feet 10 PP = 4.5 + tsf40 15 CL. ST3 PP = 4.5 + tsfML 80 20 ST4 PP = 4.5 + tsf80 25 27.0 505.4 ST5 PP = 4.5 + tsf(CL) Clay, gray with orange-brown mottling, hard, slighty 100 moist to dry, calcareous, with weathered shale, weathered 30 CL 80 Weathered to Unweathered zone 4-D-106(Continued Next Page) May 2020 Revision 0

WELL NUMBER B-47 (PZ-47) PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

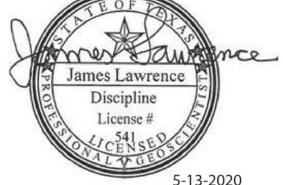
PROJECT NUMBER 16216088.00

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT LOCATION Waco, Texas

FROJE	-01 14014	IDEN .	102 10000.00			PROJECT LOCATION Waco, Texas	
(ft) 22	SAMPLE TYPE/NUMBER	RECOVERY %	REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM
 40		100				Silty Clay Shale, dark gray, hard, dry, calcareous, unweathered Limestone lenses in fractures 38-57 (continued)	
 45		80					
 - 50	ST6	80	PP = 4.5+ tsf				
 55		80					
	ST7	100	PP = 4.5+ tsf			57.0 475.4	
50						James Lawro Discipline License #	
	Revisio	n O				4-D-107	5-13-2020 May 2020



May 2020 Revision 0 4-D-107

APPENDIX III-4.E STATE WELL REPORTS



STATE OF TEXAS WELL REPORT for Tracking #508684

Latitude:

Longitude:

Elevation:

Owner Well #: Owner: PZ-1 The City of Waco

Address: 401 Franklin Avenue Grid #: 39-17-5

Waco, TX 76701

Well Location: intersection of Happy Swaner Ln &

TK Pkwv 939

Axtell, TX 76701

31° 42' 16.86" N

096° 55' 59.13" W

552 ft. above sea level

Well County: McLennan

Type of Work: New Well Proposed Use: **PIEZOMETER**

Drilling Start Date: 10/4/2018 Drilling End Date: 10/4/2018

Diameter (in.) Top Depth (ft.) Bottom Depth (ft.) Borehole: 8.25 0 39.47

Drilling Method: Hollow Stem Auger

Filter Packed Borehole Completion:

Top Depth (ft.) Bottom Depth (ft.) Filter Material Size Filter Pack Intervals: 16 39.47 Sand 20/40

Top Depth (ft.) Bottom Depth (ft.) Description (number of sacks & material) Annular Seal Data: 0 13 Cement 1 Bags/Sacks 13 16 Bentonite 1 Bags/Sacks

Seal Method: Tremie Distance to Property Line (ft.): No Data

Sealed By: Driller Distance to Septic Field or other

concentrated contamination (ft.): No Data

Distance to Septic Tank (ft.): No Data

Method of Verification: No Data

Surface Completion: Surface Slab Installed Surface Completion by Driller

Water Level: No Data

Packers: No Data

Type of Pump: No Data

Well Tests: No Test Data Specified Water Quality:

Strata Depth (ft.)	Water Type
No Data	No Data

Chemical Analysis Made: No

Did the driller knowingly penetrate any strata which

contained injurious constituents?: No

Certification Data: The driller certified that the driller drilled this well (or the well was drilled under the

driller's direct supervision) and that each and all of the statements herein are true and correct. The driller understood that failure to complete the required items will result in

the report(s) being returned for completion and resubmittal.

Company Information: BEST DRILLING SERVICES, INC.

P.O. BOX 845

FRIENDSWOOD, TX 77549

Driller Name: L. Bruce Milton License Number: 4926

Comments: No Data

Lithology: DESCRIPTION & COLOR OF FORMATION MATERIAL

Casing: BLANK PIPE & WELL SCREEN DATA

Top (ft.)	Bottom (ft.)	Description				
0	2	SILTY CLAY, drk. brown				
2	15	SILTY CLAY, red/orange to brown				
15	28	SILTY CLAY shale, orange- brown mottled brown				
28	39.47	SILTY CLAY shale, gray to drk. gray				

Dla (in.)	Туре	Material	Sch./Gage	Top (ft.)	Bottom (ft.)
2	Riser	New Plastic (PVC)	40	0	19.19
2	Screen	New Plastic (PVC)	40 0.010	19.19	38.13
2	END CAP	New Plastic (PVC)	40	38.86	39.47

IMPORTANT NOTICE FOR PERSONS HAVING WELLS DRILLED CONCERNING CONFIDENTIALITY

TEX. OCC. CODE Title 12, Chapter 1901.251, authorizes the owner (owner or the person for whom the well was drilled) to keep information in Well Reports confidential. The Department shall hold the contents of the well log confidential and not a matter of public record if it receives, by certified mail, a written request to do so from the owner.

Please include the report's Tracking Number on your written request.

Texas Department of Licensing and Regulation P.O. Box 12157 Austin, TX 78711 (512) 334-5540

STATE OF TEXAS WELL REPORT for Tracking #508363

Owner Well #: Owner: PZ-3 The City of Waco

Address: 401 Franklin Avenue Grid #: 39-17-5

Waco, TX 76701

Well Location: intersection of Happy Swaner Ln &

TK Pkwv 939

Axtell, TX 76701

Longitude: 096° 55' 43.84" W

Latitude:

Elevation: 541 ft. above sea level

31° 41' 54.3" N

Well County: McLennan

Type of Work: **New Well** Proposed Use: **PIEZOMETER**

Drilling Start Date: 10/10/2018 Drilling End Date: 10/10/2018

Bottom Depth (ft.) Diameter (in.) Top Depth (ft.) Borehole: 8.25 0 45

Drilling Method: Hollow Stem Auger

Filter Packed Borehole Completion:

Top Depth (ft.) Bottom Depth (ft.) Filter Material Size Filter Pack Intervals: 21.5 45 Sand 20/40

Top Depth (ft.) Bottom Depth (ft.) Description (number of sacks & material) Annular Seal Data: 0 17.5 Cement 1 Bags/Sacks 17.5 21.5 Bentonite 1 Bags/Sacks

Seal Method: Tremie Distance to Property Line (ft.): No Data

Sealed By: Driller Distance to Septic Field or other

concentrated contamination (ft.): No Data

Distance to Septic Tank (ft.): No Data

Method of Verification: No Data

Surface Completion: Surface Slab Installed Surface Completion by Driller

Water Level: No Data

Packers: No Data

Type of Pump: No Data

Well Tests: No Test Data Specified

Submitted on: 4/12/2019

Water Quality:

Strata Depth (ft.)	Water Type
No Data	No Data

Chemical Analysis Made: No

Did the driller knowingly penetrate any strata which contained injurious constituents?: **No**

Certification Data: The driller certified that the driller drilled this well (or the well was drilled under the

driller's direct supervision) and that each and all of the statements herein are true and correct. The driller understood that failure to complete the required items will result in

the report(s) being returned for completion and resubmittal.

Company Information: BEST DRILLING SERVICES, INC.

P.O. BOX 845

FRIENDSWOOD, TX 77549

Driller Name: L. BRUCE MILTON License Number: 4926

Comments: No Data

Lithology: DESCRIPTION & COLOR OF FORMATION MATERIAL

Top (ft.)	Bottom (ft.)	Description
0	2	Topsoil
2	8	CLAY, brown to red/brown
8	20	CLAY, mottled red/gray/brown
20	22.6	SAND, brown
22.6	22.8	SILTY CLAY, drk. brown
22.8	27	SILTY CLAY, orange-brown mottled brown
27	39	SILTY CLAY, shale, gray with orange-brown staining
39	45	SILTY CLAY, shale, drk. gray

Casing: BLANK PIPE & WELL SCREEN DATA

Dla (in.)	Туре	Material	Sch./Gage	Top (ft.)	Bottom (ft.)
2	Riser	New Plastic (PVC)	40	0	24.53
2	Screen	New Plastic (PVC)	40 0.010	24.53	44.53
2	END CAP	New Plastic (PVC)	40	44.53	44.76

IMPORTANT NOTICE FOR PERSONS HAVING WELLS DRILLED CONCERNING CONFIDENTIALITY

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Please include the report's Tracking Number on your written request.

Texas Department of Licensing and Regulation P.O. Box 12157 Austin, TX 78711 (512) 334-5540

STATE OF TEXAS WELL REPORT for Tracking #508360

Latitude:

Owner: Owner Well #: PZ-8 The City of Waco

Address: 401 Franklin Avenue Grid #: 39-17-5

Waco, TX 76701

Well Location: intersection of Happy Swaner Ln &

TK Pkwv 939

Axtell, TX 76701

Longitude:

Elevation: 550 ft. above sea level

31° 42' 11.59" N

096° 55' 12.21" W

Well County: Limestone

Type of Work: New Well Proposed Use: **PIEZOMETER**

Drilling Start Date: 11/27/2018 Drilling End Date: 11/28/2018

Bottom Depth (ft.) Diameter (in.) Top Depth (ft.) Borehole: 8.25 0 **75**

Drilling Method: Hollow Stem Auger

Filter Packed Borehole Completion:

Top Depth (ft.) Bottom Depth (ft.) Filter Material Size Filter Pack Intervals: 52.7 75 Sand 20/40

Top Depth (ft.) Bottom Depth (ft.) Description (number of sacks & material) Annular Seal Data: 0 48.7 Cement 2 Bags/Sacks 48.7 52.7 Bentonite 1 Bags/Sacks

Seal Method: Tremie Distance to Property Line (ft.): No Data

Sealed By: Driller Distance to Septic Field or other

concentrated contamination (ft.): No Data

Distance to Septic Tank (ft.): No Data

Method of Verification: No Data

Surface Completion: Surface Slab Installed Surface Completion by Driller

Water Level: No Data

Packers: No Data

Type of Pump: No Data

Well Tests: No Test Data Specified Water Quality:

Strata Depth (ft.)	Water Type
No Data	No Data

Chemical Analysis Made: No

Did the driller knowingly penetrate any strata which contained injurious constituents?: **No**

Certification Data: The driller certified that the driller drilled this well (or the well was drilled under the

driller's direct supervision) and that each and all of the statements herein are true and correct. The driller understood that failure to complete the required items will result in

the report(s) being returned for completion and resubmittal.

Company Information: BEST DRILLING SERVICES, INC.

P.O. BOX 845

FRIENDSWOOD, TX 77549

Driller Name: L. BRUCE MILTON License Number: 4926

Comments: No Data

Lithology: DESCRIPTION & COLOR OF FORMATION MATERIAL

Casing: BLANK PIPE & WELL SCREEN DATA

Top (ft.)	Bottom (ft.)	Description
0	1.5	CLAYEY SILT, drk. brown
1.5	10	SILTY CLAY, gray to It. gray
10	20	SILTY CLAY, orange-brown
20	43.8	SILTY CLAY (weathered shale marl), orange-brown
43.8	75	SILTY CLAY Shale Marl, gray

Dla (in.)	Туре	Material	Sch./Gage	Top (ft.)	Bottom (ft.)
2	Riser	New Plastic (PVC)	40	0	54.47
2	Riser	New Plastic (PVC)	40 0.010	54.47	74.47
2	Bottom Cap	New Plastic (PVC)	40	74.47	74.7

IMPORTANT NOTICE FOR PERSONS HAVING WELLS DRILLED CONCERNING CONFIDENTIALITY

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Please include the report's Tracking Number on your written request.

Texas Department of Licensing and Regulation P.O. Box 12157 Austin, TX 78711 (512) 334-5540

STATE OF TEXAS WELL REPORT for Tracking #508367

Latitude:

31° 42' 10.46" N

Owner: Owner Well #: PZ-9 The City of Waco

Address: 401 Franklin Avenue Grid #: 39-17-5

Waco, TX 76701

Well Location: intersection of Happy Swaner Ln &

TK Pkwv 939

Axtell, TX 76701

Longitude: 096° 55' 37.43" W

Elevation: 535 ft. above sea level Well County: Limestone

Type of Work: New Well Proposed Use: **PIEZOMETER**

Drilling Start Date: 10/9/2018 Drilling End Date: 10/10/2018

Bottom Depth (ft.) Diameter (in.) Top Depth (ft.) Borehole: 8.25 0 40

Drilling Method: Hollow Stem Auger

Filter Packed Borehole Completion:

Top Depth (ft.) Bottom Depth (ft.) Filter Material Size Filter Pack Intervals: 15.9 38.48 Sand 20/40

Top Depth (ft.) Bottom Depth (ft.) Description (number of sacks & material) Annular Seal Data: 0 10.8 Cement 1 Bags/Sacks 10.8 15.9 Bentonite 1 Bags/Sacks

Seal Method: Tremie Distance to Property Line (ft.): No Data

Sealed By: Driller Distance to Septic Field or other

concentrated contamination (ft.): No Data

Distance to Septic Tank (ft.): No Data

Method of Verification: No Data

Surface Completion: **Surface Slab Installed Surface Completion by Driller**

Water Level: No Data

Packers: No Data

Type of Pump: No Data

Well Tests: No Test Data Specified

> Well Report Tracking Number 508367 4-F-8 Submitted on: 4/12/2019

Strata Depth (ft.) Water Type Water Quality: No Data No Data

Chemical Analysis Made: No

Did the driller knowingly penetrate any strata which

contained injurious constituents?: No

Certification Data: The driller certified that the driller drilled this well (or the well was drilled under the

driller's direct supervision) and that each and all of the statements herein are true and correct. The driller understood that failure to complete the required items will result in

the report(s) being returned for completion and resubmittal.

Company Information: **BEST DRILLING SERVICES, INC.**

P.O. BOX 845

FRIENDSWOOD, TX 77549

Driller Name: L. BRUCE MILTON License Number: 4926

Comments: No Data

4/12/201R & 25/25 185 PM

Lithology: DESCRIPTION & COLOR OF FORMATION MATERIAL

Casing: BLANK PIPE & WELL SCREEN DATA

Top (ft.)	Bottom (ft.)	Description
0	5	SILTY CLAY, drk. brown to gray
5	10	SILTY CLAY, It. gray/tan
10	28.5	SILTY CLAY shale gray and orange-brown
28.5	40	SILTY CLAY shale

Dla (in.)	Type	Material	Sch./Gage	Top (ft.)	Bottom (ft.)
2	Riser	New Plastic (PVC)	40	0	18.28
2	Screen	New Plastic (PVC)	40 0.010	18.28	38.28
2	END CAP	New Plastic (PVC)	40	38.28	38.48

IMPORTANT NOTICE FOR PERSONS HAVING WELLS DRILLED CONCERNING CONFIDENTIALITY

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Please include the report's Tracking Number on your written request.

Texas Department of Licensing and Regulation P.O. Box 12157 Austin, TX 78711 (512) 334-5540

Well Report Tracking Number 508367

Submitted on: 4/12/2019

STATE OF TEXAS WELL REPORT for Tracking #509203

Owner Well #: Owner: **PZ-18** The City of Waco

Address: 401 Franklin Avenue Grid #: 39-17-5

Waco, TX 76701

Well Location: intersection of Happy Swaner Ln &

TK Pkwy 939

Axtell, TX 76701

Longitude:

Latitude:

31° 42' 28.96" N

096° 55' 26.98" W

Elevation: 535 ft. above sea level

Well County: Limestone

Type of Work: New Well Proposed Use: **PIEZOMETER**

Drilling Start Date: 10/29/2018 Drilling End Date: 10/30/2018

Bottom Depth (ft.) Diameter (in.) Top Depth (ft.) Borehole: 8.25 0 56

Drilling Method: Hollow Stem Auger

Filter Packed Borehole Completion:

Filter Pack Intervals:

Top Depth (ft.)	Bottom Depth (ft.)	Filter Material	Size
22.8	56	Sand	20/40

Annular Seal Data:

Top Depth (ft.)	Bottom Depth (ft.)	Description (number of sacks & material)
0	19	Cement 1 Bags/Sacks
19	22.8	Bentonite 1 Bags/Sacks

Seal Method: Tremie Distance to Property Line (ft.): No Data

Sealed By: Driller Distance to Septic Field or other

concentrated contamination (ft.): No Data

Distance to Septic Tank (ft.): No Data

Method of Verification: No Data

Surface Completion: **Surface Slab Installed Surface Completion by Driller**

Water Level: No Data

Packers: No Data

No Data Type of Pump:

Well Tests: No Test Data Specified

> Well Report Tracking Number 509203 4-F-10 Submitted on: 4/23/2019

Water Quality:

Strata Depth (ft.)	Water Type
No Data	No Data

Chemical Analysis Made: No

Did the driller knowingly penetrate any strata which contained injurious constituents?: **No**

Certification Data: The driller certified that the driller drilled this well (or the well was drilled under the

driller's direct supervision) and that each and all of the statements herein are true and correct. The driller understood that failure to complete the required items will result in

the report(s) being returned for completion and resubmittal.

Company Information: BEST DRILLING SERVICES, INC.

P.O. BOX 845

FRIENDSWOOD, TX 77549

Driller Name: L. Bruce Milton License Number: 4926

Comments: Hole backfilled 56' - 45.5'

Lithology: DESCRIPTION & COLOR OF FORMATION MATERIAL

Casing: BLANK PIPE & WELL SCREEN DATA

Top (ft.)	Bottom (ft.)	Description
0	2.7	SANDY CLAY, topsoil, drk. brown
2.7	6.8	SILTY CLAY, It. gray
6.8	14.5	SILTY CLAY, orange brown
14.5	30	SILTY SILT, gray
30	56	SILTY shale, gray
56	60	SILTY SILT, gray

Dla (in.)	Туре	Material	Sch./Gage	Top (ft.)	Bottom (ft.)
2	Riser	New Plastic (PVC)	40	0	25.18
2	Screen	New Plastic (PVC)	40 0.010	25.18	44.13
2	END CAP	New Plastic (PVC)	40	44.13	45.5

IMPORTANT NOTICE FOR PERSONS HAVING WELLS DRILLED CONCERNING CONFIDENTIALITY

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Please include the report's Tracking Number on your written request.

Texas Department of Licensing and Regulation P.O. Box 12157 Austin, TX 78711 (512) 334-5540

STATE OF TEXAS WELL REPORT for Tracking #500910

Owner:

City of Waco

Owner Well #:

B-20

Address:

721 N. 4th Street Waco, TX 76701

Grid #:

39-17-2

Well Location:

Southeast corner of TK Pkwy and

Latitude:

31° 42' 34,93" N

HWy 31

Longitude:

096° 55' 14.49" W

Well County:

Axtell, TX 76673

Elevation:

No Data

Limestone

Piezometer

Type of Work:

New Well

Proposed Use:

Drilling Start Date: 10/29/2018

Drilling End Date: 10/29/2018

Borehole:

Diameter (in.)	Top Depth (ft.)	Bottom Depth (ft.)
7.25	0	73

Drilling Method:

Hollow Stem Auger

Borehole Completion:

Open Hole

Annular Seal Data:

Top Depth (ft.)	Bottom Depth (ft.)	Description (number of sacks & material)
0	3	Cement 2 Bags/Sacks
3	42	Bentonite 15 Bags/Sacks
42	64	Sand 10 Bags/Sacks
64	73	backfill cuttings

Seal Method: Gravity

Distance to Property Line (ft.): No Data

Sealed By: Driller

Distance to Septic Field or other

concentrated contamination (ft.): No Data

Distance to Septic Tank (ft.): No Data

Method of Verification: No Data

Surface Completion:

Surface Slab Installed

Surface Completion by Driller

Water Level:

No Data

Packers:

No Data

Type of Pump:

No Data

Well Tests:

No Test Data Specified

1/17/2019 1:26:21 PM

Well Report Tracking Number 500910 Submitted on: 1/17/2019 4-F-12

Page 1 of 3

Revision 0

	Strata Depth (ft.)	Water Type	
Water Quality:	No Data	No Data	Wilder Control

Chemical Analysis Made: No

Did the driller knowingly penetrate any strata which

contained injurious constituents?:

The driller did certify that while drilling, deepening or otherwise altering the above described well, injurious water or constituents was encountered and the landowner or person having the well drilled was informed that such well must be completed or plugged in such a manner as to avoid injury or pollution.

Certification Data:

The driller certified that the driller drilled this well (or the well was drilled under the driller's direct supervision) and that each and all of the statements herein are true and correct. The driller understood that failure to complete the required items will result in the report(s) being returned for completion and resubmittal.

Company Information:

WEST Drilling

101 Industrial Drive Waxahachie, TX 75165

Driller Name:

Ricardo Garcia

License Number:

54637

Apprentice Name:

Joseph Garcia

Apprentice Number:

No

59885

Comments:

No Data

Lithology: DESCRIPTION & COLOR OF FORMATION MATERIAL

Casing: BLANK PIPE & WELL SCREEN DATA

Top (ft.)	Bottom (ft.)	Description	No. of the last	Dla (in.)	Туре	Material	Sch./Gage	Top (ft.)	Bottom (ft.)	
0	7.5	Silty Clay gray	1	2	Riser	New Plastic	40	3	44	20
7.5	35	Silty Clay tan gray		-	TRISCI	(PVC)		_		
35	47	Shaley Clay dark gray		2	Screen	New Plastic (PVC)	0.010	44	64	
47	73	Silty Clay Shale dark gray								

IMPORTANT NOTICE FOR PERSONS HAVING WELLS DRILLED CONCERNING CONFIDENTIALITY

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Please include the report's Tracking Number on your written request.

Texas Department of Licensing and Regulation P.O. Box 12157 Austin, TX 78711 (512) 334-5540

STATE OF TEXAS WELL REPORT for Tracking #509216

Latitude:

Owner: Owner Well #: **PZ-33** The City of Waco

Address: 401 Franklin Avenue Grid #: 39-17-5

Waco, TX 76701

Well Location: intersection of Happy Swaner Ln &

TK Pkwv 939

Axtell, TX 76701

Longitude: 096° 55' 14.54" W

Elevation: 539 ft. above sea level

31° 42' 00" N

Well County: Limestone

Type of Work: New Well Proposed Use: **PIEZOMETER**

Drilling Start Date: 11/19/2018 Drilling End Date: 11/20/2018

Bottom Depth (ft.) Diameter (in.) Top Depth (ft.) Borehole: 8.25 0 55

Drilling Method: Hollow Stem Auger

Filter Packed Borehole Completion:

Top Depth (ft.) Bottom Depth (ft.) Filter Material Size Filter Pack Intervals: 33 55 Sand 20/40

Top Depth (ft.) Bottom Depth (ft.) Description (number of sacks & material) Annular Seal Data: 0 30 Cement 1 Bags/Sacks 30 33 Bentonite 1 Bags/Sacks

Seal Method: Tremie Distance to Property Line (ft.): No Data

Sealed By: Driller Distance to Septic Field or other

concentrated contamination (ft.): No Data

Distance to Septic Tank (ft.): No Data

Method of Verification: No Data

Surface Completion: **Surface Slab Installed Surface Completion by Driller**

Water Level: No Data

Packers: No Data

Type of Pump: No Data

Well Tests: No Test Data Specified

Well Report Tracking Number 509216

May 2020 9ge 1 of 2 4-F-14 Submitted on: 4/23/2019

Water Quality:

Strata Depth (ft.)	Water Type
No Data	No Data

Chemical Analysis Made: No

Did the driller knowingly penetrate any strata which

contained injurious constituents?: No

Certification Data: The driller certified that the driller drilled this well (or the well was drilled under the

driller's direct supervision) and that each and all of the statements herein are true and correct. The driller understood that failure to complete the required items will result in

the report(s) being returned for completion and resubmittal.

Company Information: BEST DRILLING SERVICES, INC.

P.O. BOX 845

FRIENDSWOOD, TX 77549

Driller Name: L. Bruce Milton License Number: 4926

Comments: No Data

Lithology: DESCRIPTION & COLOR OF FORMATION MATERIAL

Casing: BLANK PIPE & WELL SCREEN DATA

Top (ft.)	Bottom (ft.)	Description
1	1.5	CLAYEY SILT topsoil
1.5	28	SILTY CLAY, brown to tan
28	55	SILTY CLAY, shale, gray

Dla (in.)	Туре	Material	Sch./Gage	Top (ft.)	Bottom (ft.)
2	Riser	New Plastic (PVC)	40	0	34.63
2	Screen	New Plastic (PVC)	40 0.010	34.63	54.63
2	END CAP	New Plastic (PVC)	40	54.63	54.9

IMPORTANT NOTICE FOR PERSONS HAVING WELLS DRILLED CONCERNING CONFIDENTIALITY

TEX. OCC. CODE Title 12, Chapter 1901.251, authorizes the owner (owner or the person for whom the well was drilled) to keep information in Well Reports confidential. The Department shall hold the contents of the well log confidential and not a matter of public record if it receives, by certified mail, a written request to do so from the owner.

Please include the report's Tracking Number on your written request.

Texas Department of Licensing and Regulation P.O. Box 12157 Austin, TX 78711 (512) 334-5540

Well Report Tracking Number 509216

4-E-15 Submitted on: 4/23/2019

STATE OF TEXAS WELL REPORT for Tracking #508364

Owner: Owner Well #: PZ-41 The City of Waco

Address: 401 Franklin Avenue Grid #: 39-17-6

Waco, TX 76701

Well Location: intersection of Happy Swaner Ln &

TK Pkwv 939

Axtell, TX 76701

Longitude: 096° 54' 58.94" W

Latitude:

31° 42' 10.8" N

Elevation: 535 ft. above sea level Well County: Limestone

Type of Work: New Well Proposed Use: **PIEZOMETER**

Drilling Start Date: 12/17/2018 Drilling End Date: 12/18/2018

Bottom Depth (ft.) Diameter (in.) Top Depth (ft.) Borehole: 8.25 0 60

Drilling Method: Hollow Stem Auger

Filter Packed Borehole Completion:

Top Depth (ft.) Bottom Depth (ft.) Filter Material Size Filter Pack Intervals: 24 48.77 Sand 20/40

Top Depth (ft.) Bottom Depth (ft.) Description (number of sacks & material) Annular Seal Data: 0 22 Cement 1 Bags/Sacks 22 24 Bentonite 1 Bags/Sacks

Seal Method: Tremie Distance to Property Line (ft.): No Data

Sealed By: Driller Distance to Septic Field or other

concentrated contamination (ft.): No Data

Distance to Septic Tank (ft.): No Data

Method of Verification: No Data

Surface Completion: **Surface Slab Installed Surface Completion by Driller**

Water Level: No Data

Packers: No Data

Type of Pump: No Data

Well Tests: No Test Data Specified

Well Report Tracking Number 508364

May 2020ge 1 of 2 4-F-16 Submitted on: 4/12/2019

Water Quality:

Strata Depth (ft.)	Water Type
No Data	No Data

Chemical Analysis Made: No

Did the driller knowingly penetrate any strata which contained injurious constituents?: **No**

Certification Data: The driller certified that the driller drilled this well (or the well was drilled under the

driller's direct supervision) and that each and all of the statements herein are true and correct. The driller understood that failure to complete the required items will result in

the report(s) being returned for completion and resubmittal.

Company Information: BEST DRILLING SERVICES, INC.

P.O. BOX 845

FRIENDSWOOD, TX 77549

Driller Name: L. BRUCE MILTON License Number: 4926

Comments: Hole Backfilled from 60' - 48.77 with native material

Lithology: DESCRIPTION & COLOR OF FORMATION MATERIAL

Top (ft.) Bottom (ft.) Description SILTY CLAY, drk. brown to 0 5 SILTY CLAY, gray grading to 5 12 brown and orange-brown SILTY CLAY shale marl, 12 29 orange-brown stained brown and gray Shale Marl, drk. gray with orange-brown staining in 29 43 joints 43 60 Shale Marl, gray to drk. gray

Casing: BLANK PIPE & WELL SCREEN DATA

Dla (in.)	Туре	Material	Sch./Gage	Top (ft.)	Bottom (ft.)
2	Riser	New Plastic (PVC)	40	0	28.58
2	Screen	New Plastic (PVC)	40 0.010	28.58	48.58
2	END CAP	New Plastic (PVC)	40	48.58	48.77

IMPORTANT NOTICE FOR PERSONS HAVING WELLS DRILLED CONCERNING CONFIDENTIALITY

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Please include the report's Tracking Number on your written request.

Texas Department of Licensing and Regulation P.O. Box 12157 Austin, TX 78711 (512) 334-5540

Well Report Tracking Number 508364

STATE OF TEXAS WELL REPORT for Tracking #508365

Latitude:

Owner: Owner Well #: **PZ-43** The City of Waco

Address: 401 Franklin Avenue Grid #: 39-17-5

Waco, TX 76701

Well Location: intersection of Happy Swaner Ln &

TK Pkwv 939

Axtell, TX 76701

Longitude: 096° 55' 01.03" W

Elevation: 549 ft. above sea level

31° 42' 20.55" N

Well County: Limestone

Type of Work: New Well Proposed Use: **PIEZOMETER**

Drilling Start Date: 11/15/2018 Drilling End Date: 11/16/2018

Bottom Depth (ft.) Diameter (in.) Top Depth (ft.) Borehole: 8.25 0 **75**

Drilling Method: Hollow Stem Auger

Filter Packed Borehole Completion:

Top Depth (ft.) Bottom Depth (ft.) Filter Material Size Filter Pack Intervals: 24 48.45 Sand 20/40

Top Depth (ft.) Bottom Depth (ft.) Description (number of sacks & material) Annular Seal Data: 0 22 Cement 1 Bags/Sacks 22 24 Bentonite 1 Bags/Sacks

Seal Method: Tremie Distance to Property Line (ft.): No Data

Sealed By: Driller Distance to Septic Field or other

concentrated contamination (ft.): No Data

Distance to Septic Tank (ft.): No Data

Method of Verification: No Data

Surface Completion: **Surface Slab Installed Surface Completion by Driller**

Water Level: No Data

Packers: No Data

Type of Pump: No Data

Well Tests: No Test Data Specified

> Well Report Tracking Number 508365 4-F-18 Submitted on: 4/12/2019

Water Quality:

Strata Depth (ft.)	Water Type
No Data	No Data

Chemical Analysis Made: No

Did the driller knowingly penetrate any strata which contained injurious constituents?: **No**

Certification Data: The driller certified that the driller drilled this well (or the well was drilled under the

driller's direct supervision) and that each and all of the statements herein are true and correct. The driller understood that failure to complete the required items will result in

the report(s) being returned for completion and resubmittal.

Company Information: BEST DRILLING SERVICES, INC.

P.O. BOX 845

FRIENDSWOOD, TX 77549

Driller Name: L. BRUCE MILTON License Number: 4926

Comments: Hole backfilled with native material from 75' - 48.45'

Lithology: DESCRIPTION & COLOR OF FORMATION MATERIAL

Casing: BLANK PIPE & WELL SCREEN DATA

Top (ft.)	Bottom (ft.)	Description
0	1	CLAYEY SILT, drk. brown
1	5	SILTY CLAY, drk. brown
5	10	SILTY CLAY, orange-brown
10	25	SILTY CLAY (weathered shale/marl) orange-brown
25	32	SILTY CLAY (shale/marl) gray
32	75	SILTY shale marl, gray
32	75	SILT I Shale man, gray

Dla (in.)	Туре	Material	Sch./Gage	Top (ft.)	Bottom (ft.)
2	Riser	New Plastic (PVC)	40	0	28.2
2	Screen	New Plastic (PVC)	40 0.010	28.2	48.2
2	END CAP	New Plastic (PVC)	40	48.2	48.45

IMPORTANT NOTICE FOR PERSONS HAVING WELLS DRILLED CONCERNING CONFIDENTIALITY

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Please include the report's Tracking Number on your written request.

Texas Department of Licensing and Regulation P.O. Box 12157 Austin, TX 78711 (512) 334-5540

STATE OF TEXAS WELL REPORT for Tracking #500935

Owner:

City of Waco

Owner Well #:

PZ-47

Address:

721 N. 4th Street

Grid #:

39-17-5

Waco, TX 76701

Latitude:

31° 42' 02.16" N

Well Location:

Southeast corner of TK Pkwy and

Longitude:

096° 55' 28.39" W

HWy 31

Axtell, TX 76673

Elevation:

No Data

Well County:

Limestone

Type of Work: New Well

Proposed Use:

Piezometer

Drilling Start Date: 10/29/2018

Drilling End Date: 10/29/2018

Borehole:

Diameter (in.)	Top Depth (ft.)	Bottom Depth (ft.)	
7.25	0	57.4	

Drilling Method:

Hollow Stem Auger

Borehole Completion:

Open Hole

Annular Seal Data:

Top Depth (ft.)	Bottom Depth (ft.)	Description (number of sacks & material)
0	3.5	Cement 2 Bags/Sacks
3.5	8	Bentonite 2 Bags/Sacks
8	30	Sand 10 Bags/Sacks
30	57	Bentonite 14 Bags/Sacks

Seal Method: Gravity

Distance to Property Line (ft.): No Data

Sealed By: Driller

Distance to Septic Field or other

concentrated contamination (ft.): No Data

Distance to Septic Tank (ft.): No Data

Method of Verification: No Data

Surface Completion:

Surface Slab Installed

Surface Completion by Driller

Water Level:

No Data

Packers:

No Data

Type of Pump:

No Data

Well Tests:

No Test Data Specified

1/17/2019 1:25:57 PM

Well Report Tracking Number 500935 Submitted on: 1/17/2019

Page 1 of 3

Revision 0

4-E-20

May 2020

Water Quality:

Strata Depth (ft.)	Water Type	
No Data	No Data	4

Chemical Analysis Made:

Did the driller knowingly penetrate any strata which

contained injurious constituents?:

The driller did certify that while drilling, deepening or otherwise altering the above described well, injurious water or constituents was encountered and the landowner or person having the well drilled was informed that such well must be completed or plugged in such a manner as to avoid injury or pollution.

Certification Data:

The driller certified that the driller drilled this well (or the well was drilled under the driller's direct supervision) and that each and all of the statements herein are true and correct. The driller understood that failure to complete the required items will result in the report(s) being returned for completion and resubmittal.

Company Information:

WEST Drilling

101 Industrial Drive Waxahachie, TX 75165

Driller Name:

Ricardo Garcia

License Number:

No

No

54637

Apprentice Name:

Joseph Garcia

Apprentice Number:

59885

Comments:

No Data

Lithology: DESCRIPTION & COLOR OF FORMATION MATERIAL

Casing: BLANK PIPE & WELL SCREEN DATA

Top (ft.)	Bottom (ft.)	Description	Dla (in.)	Туре	Material	Sch./Gage	Top (ft.)	Bottom (ft.)
0	7	Clay light gray	2	Riser	New Plastic	40	0	10
7	27	Silty Clay tan gray	N. Douglasses	Kisei	(PVC)			
27	33	Shaley Clay gray	2	Screen	New Plastic (PVC)	0.010	10	30
33	57.4	Silty Clay Shale dark gray						

IMPORTANT NOTICE FOR PERSONS HAVING WELLS DRILLED CONCERNING CONFIDENTIALITY

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Texas Department of Licensing and Regulation P.O. Box 12157 Austin, TX 78711 (512) 334-5540

APPENDIX III-4.F GEOTECHNICAL INVESTIGATION REPORTS





Site 50

Summary of Laboratory Test Results

Boring	Sample Depth			% Passing on	% Retained on				
Number	(ft)	LL ⁽¹⁾	PI ⁽²⁾	#200 Sieve	#4 Sieve	MC ⁽³⁾	USCS ⁽⁴⁾	GSA ⁽⁵⁾	Description
A-1	10 to 12	83	58	97	0	31	CH		FAT CLAY; tan and light gray
	12 to 14			93	0			✓	FAT CLAY; tan and light gray
	14 to 16	89	63	98	0	30	CH		FAT CLAY; tan and gray
	18 to 20	79	56	80	13	22	CH		FAT CLAY; reddish brown, with gravel and trace sand
	30 to 35	66	43	84	2	14			SHALE; dark gray, with sand lens
	40 to 45	73	52	91	0	14			SHALE; dark gray, calcareous
	60 to 65	72	52	90	1	18		✓	SHALE; dark gray
A-2	10 to 12	71	51	90	1	20	СН		FAT CLAY; tan and brown, calcareous
	16 to 18	69	48	82	0	18	CH	✓	FAT CLAY; tan and light gray, iron staining, with sand
	30 to 32	74	52	84	3	21	CH	✓	FAT CLAY; tan and gray, with sand
	45 to 50	56	36	91	0	13		✓	SHALE; dark gray
A-4	10 to 12	75	51	95	0	21	CH		FAT CLAY; tan and brown, calcareous
	22 to 24	74	53	94	1	21	CH	✓	FAT CLAY; tan and gray, iron staining
	31 to 36	55	37	91	0	13		✓	SHALE; dark gray
	46 to 51	62	44	97	0	13			SHALE; dark gray
	86 to 91	74	53	77	9	14			SHALE; dark gray, with sand lens
A-5	12 to 14	62	41	75	4	16	CH		FAT CLAY; tan and light gray, with sand
	22 to 24	66	46	76	8	18	CH	✓	FAT CLAY; tan, calcareous, with sand
	30 to 35	63	42	96	1	17			SHALE; dark gray

⁽¹⁾Liquid Limit

Office: (254) 235 - 1048

4-F-2

⁽²⁾Plasticity Index

⁽³⁾ Moisture Content

⁽⁴⁾Unified Soil Classification System

⁽⁵⁾ Grain Size Analysis - Detailed Grain Size Analysis Results are recorded on the following pages. Gradation Curves are included.



Site 50, Part 2, West

Summary of Laboratory Test Results

Boring	Sample							Dry Unit	Qu Strength		
Number	Depth (ft)	LL ⁽¹⁾	PI ⁽²⁾	% Fines*	% Sand**	% Gravel***	MC ⁽³⁾	Weight (pcf)		USCS ⁽⁴⁾	Description
B-1	15-20	75	53	93	5	2	23			СН	FAT CLAY; tan and brown, with iron stains
	35-38	69	45	97	3	0	19			СН	FAT CLAY; dark gray
B-3	25-30	60	36	93	7	0	18				FAT CLAY; tan and light gray
	40-45	63	43	96	4	0	16				FAT CLAY; dark gray
B-8	10-12										Bulk Sample, Proctor
B-9	5-7	53	35	75	23	2	15			СН	FAT CLAY; light gray, with sand
	20-22	67	47	91	6	3	20	105	12.32		FAT CLAY; tan and light gray
	35-37	62	42	89	8	3	15	116		СН	FAT CLAY; dark gray
B-16	10-12	78	53	91	9	0	19	105		CH	FAT CLAY; tan and gray, with iron stains
	10-12										Bulk Sample, Proctor
	25-27	60	38	77	18	5	15	116	17.76	CH	FAT CLAY; tan, with sand
	50-52	64	43	94	6	0	17	115		CH	FAT CLAY; dark gray
B-17	15-17	66	41	91	9	0	19	106	8.09	CH	FAT CLAY; tan and light gray
	25-27										Sample sent to TRI, also receiving advanced geotechnical testing
	45-47	60	41	83	17	0	15	120	23.36	CH	FAT CLAY; gray, with sand
B-19	10-12										Bulk Sample, Proctor
B-23	10-12	73	52	98	2	0	20	108		CH	FAT CLAY; tan and light gray
	10-12										Bulk Sample, Proctor
	30-32	74	51	85	12	3	18	108		CH	FAT CLAY; tan and gray, with sand
	35-37	77	55	89	11	0	20	101	Not testable	CH	FAT CLAY; gray, with iron stains
	40-42	70	50	96	4	0	15			CH	FAT CLAY; dark gray
B-24	5-7	51	33	73	24	3	15	112	14.94	CH	FAT CLAY; light gray, with sand
	15-17	74	52	98	2	0	21	99	7.94	CH	FAT CLAY; tan and gray
	25-27	69	44	89	11	0	19	103		CH	FAT CLAY; brown and light gray
	45-47										Sample sent to TRI, also receiving advanced geotechnical testing
B-31	15-17										Sample sent to TRI, also receiving advanced geotechnical testing
	30-32	74	52	90	7	3	18	103	5.37	CH	FAT CLAY; dark gray
	55-57	60	37	96	3	1	14			CH	FAT CLAY; dark gray
B-44	10-12	71	49	91	6	3	20	108		CH	FAT CLAY; tan and light gray
	20-22	79	55	84	11	5	21	105		CH	FAT CLAY; tan, with sand
	30-32	72	51	97	3	0	25	97	4.44	CH	FAT CLAY; tan and light gray
	50-52										Sample sent to TRI, also receiving advanced geotechnical testing

⁽¹⁾Liquid Limit

12/24/2018

Revision 0 4-F-3 May 2020

⁽²⁾Plasticity Index

⁽³⁾ Moisture Content

⁽⁴⁾Unified Soil Classification System

^{* %} Fines is defined as the fraction of the total sample passing the #200 Sieve

^{** %} Sand is defined as the fraction of the total sample passing the #4 Sieve and retained on the #200 Sieve

^{*** %} Gravel is defined as the fraction of the total sample retained on the #4 Sieve



Site 50, Part 2, East

Summary of Laboratory Test Results

Boring	Sample							Dry Unit	Qu Strength			
Number	Depth (ft)	LL ⁽¹⁾	PI ⁽²⁾	% Fines*	% Sand**	% Gravel***	MC ⁽³⁾	Weight (pcf)	(tsf)	USCS ⁽⁴⁾	Description	
B-8	40-42	58	38	92	8	0	16	106	4.02	СН	SHALY FAT CLAY; tan, with iron stains	
	50-52	58	37	97	2	1	14	116	Not testable	СН	SHALY FAT CLAY; dark gray	
B-11	20-22	75	49	89	10	1	21	95		СН	FAT CLAY; tan and gray, with calcareous fragments	
	45-47	55	33	86	14	0	13	120		СН	FAT CLAY; dark brown, with iron stains	
B-13	35-37	66	43	94	6	0	20	109		СН	FAT CLAY; tan, with iron stains	
	45-47	51	33	95	5	0	15	112	Not testable	СН	SHALY FAT CLAY; dark gray	
B-14	15-17	58	35	65	30	5	19	104		СН	SANDY FAT CLAY; tan and gray, with iron stains	
	35-37	58	39	94	5	1	15			СН	FAT CLAY; dark gray	
B-15	55-57	57	37	91	7	2	11	116	1.61	СН	FAT CLAY; brown and dark gray	
B-18	10-12	66	45	92	7	1	19	105	4.26	СН	FAT CLAY; tan and brown, with iron stains	
	45-47	57	38	90	10	0	13	109	3.59	СН	FAT CLAY; dark gray, with iron stains	
B-19	50-52	63	44	91	7	2	14	117		СН	SHALY FAT CLAY; tan and gray, with iron stains	
	50-51	60	39	85			13				Sample sent to TRI, also receiving advanced geotechnical testing	
	70-72	57	38	95	5	0	15	115	16.29	СН	SHALY FAT CLAY; gray and dark brown	
B-20	45-47	59	36	95	5	0	13	116	18.68	СН	SHALY FAT CLAY; gray and dark brown	
	55-57	58	37	96	3	1	15	118	16.82		SHALY FAT CLAY; gray and dark brown	
B-21	15-17	69	44	97	3	0	19			СН	FAT CLAY; tan and gray, with iron stains	
	30-32						19	108	10.49	СН	SHALY FAT CLAY; dark brown	
	30-32	57	39	94	6	0	15			СН	FAT CLAY; gray	
	40-42	61	40	88	8	4	14			СН	SHALY FAT CLAY; gray	
B-27	25-27	68	47	87	10	3	18	108		СН	FAT CLAY; tan and gray, with calcareous fragments	
	40-42	61	40	97	3	0	15	118		CH	SHALY FAT CLAY; gray	
B-29	25-27	60	39	95	4	1	16	113		СН	FAT CLAY; dark gray	
	35-37	51	34	90	10	0	11	114			FAT CLAY; dark gray	
B-30	15-17	61	41	90	6	4	18	115		СН	FAT CLAY; tan, with iron stains	
	30-32	62	41	94	6	0	18			СН	FAT CLAY; tan and gray, with a silty seam	
B-34	10-12	57	38	82	17	1	14			СН	FAT CLAY; tan, with calcareous fragments	
	20-22	63	43	95	5	0	16	111		СН	FAT CLAY; tan and gray, with calcareous fragments and iron stains	
B-35	45-47	54	33	75	17	8	13	109		СН	SHALY FAT CLAY; gray, with sand	
B-43	10-12	60	40	95	5	0	18	111	7.12	СН	FAT CLAY; tan, with iron stains	
	25-27	61	42	94	5	1	16	117	Not testable	СН	FAT CLAY; tan, with calcareous fragments	
	45-47	63	40	95	5	0	16	108		СН	SHALY FAT CLAY; gray	
B-45	25-27	66	46	90	8	2	21	107	6.21	СН	FAT CLAY; brown and gray, with calcareous fragments and iron stains	
	40-42	58	38	92	8	0	15			СН	SHALY FAT CLAY; gray	
B-46	45-47	62	41	94	6	0	13	110	Not testable	СН	SHALY FAT CLAY; gray	

⁽¹⁾Liquid Limit

02/15/2019

⁽²⁾Plasticity Index

⁽³⁾ Moisture Content

⁽⁴⁾Unified Soil Classification System

^{* %} Fines is defined as the fraction of the total sample passing the #200 Sieve

^{** %} Sand is defined as the fraction of the total sample passing the #4 Sieve and retained on the #200 Sieve

^{*** %} Gravel is defined as the fraction of the total sample retained on the #4 Sieve

[&]quot;Not testable" indicates that the sample was fractured or otherwise compromised for quality strength tests



Site 50, Part 2, Data Set 4

Summary of Laboratory Test Results

Boring	Sample							Dry Unit		
Number	Depth (ft)	LL ⁽¹⁾	PI ⁽²⁾	% Fines*	% Sand**	% Gravel***	MC ⁽³⁾	Weight (pcf)	USCS ⁽⁴⁾	Description
B-10	10-12	65	41	90	7	3	19		СН	FAT CLAY; tan and gray, with iron stains and limestone fragments
	25-27	54	33	94	6	0	15	108	СН	FAT CLAY; tan and brown, with iron stains and limestone fragments
	40-42	59	39	92	7	1	14		СН	FAT CLAY; dark brown
B-22	30-32	74	47	84	8	8	20		СН	FAT CLAY; tan and gray, with gravel and iron stains
	45-47	64	39	92	7	1	17		СН	FAT CLAY; dark brown, with iron stains
B-36	15-17	56	35	91	8	1	18		СН	FAT CLAY; tan and gray, with iron stains
	30-32	64	39	93	7	0	17	115	СН	FAT CLAY; tan and brown, with iron stains

⁽¹⁾Liquid Limit

2/21/2019

⁽²⁾Plasticity Index

⁽³⁾ Moisture Content

⁽⁴⁾Unified Soil Classification System

^{* %} Fines is defined as the fraction of the total sample passing the #200 Sieve

^{** %} Sand is defined as the fraction of the total sample passing the #4 Sieve and retained on the #200 Sieve

^{*** %} Gravel is defined as the fraction of the total sample retained on the #4 Sieve

[&]quot;Not testable" indicates that the sample was fractured or otherwise compromised for quality strength tests



Site 50, Part 2, Data Set 4

Summary of Laboratory Test Results

Boring	Sample							Dry Unit		
Number	Depth (ft)	LL ⁽¹⁾	PI ⁽²⁾	% Fines*	% Sand**	% Gravel***	MC ⁽³⁾	Weight (pcf)	USCS ⁽⁴⁾	Description
B-9	57	63	41	99	1	0	15		CH	SHALY FAT CLAY; gray
B-9	78	64	42	93	4	3	14		СН	SHALY FAT CLAY; gray
B-9	106	73	51	97	3	0	15		СН	SHALY FAT CLAY; gray
B-9	132	74	49	89	11	0	16		СН	SHALY FAT CLAY; gray
B-43	74	60	40	91	8	1	15		СН	SHALY FAT CLAY; gray
B-43	119	68	46	81	9	10	12		СН	SHALY FAT CLAY; gray, with gravel
B-43	146	75	50	99	1	0	15		СН	SHALY FAT CLAY; gray

⁽¹⁾Liquid Limit

3/5/2020

⁽²⁾Plasticity Index

⁽³⁾ Moisture Content

⁽⁴⁾Unified Soil Classification System

^{* %} Fines is defined as the fraction of the total sample passing the #200 Sieve

^{** %} Sand is defined as the fraction of the total sample passing the #4 Sieve and retained on the #200 Sieve

^{*** %} Gravel is defined as the fraction of the total sample retained on the #4 Sieve



Job Number	W18-006						
Client	SCS Engine	SCS Engineers/City of Waco					
Job Description	Site 50						
Core ID	A-1						
Top Depth	12'						
Bottom Depth	14'						
	D (mm)	Sieve #	% Finer				
	63	2.5"	100.00				
	19	3/4"	100.00				
	9.5	3/8"	100.00				
	4.75	4	100.00				
	2	2 10					
 	0.85						
l õ	0.425	94.74					
<u> </u>	0.25	60	94.49				
<u>X</u>	0.15	100	94.41				
S	0.075	200	93.44				
Grain Size Data	0.0000						
<u>a</u> :	0.0000						
	0.0000						
0	0.0000						
	0.0000						
	0.0000						
	0.0000						
	0.0000						
	0.0000	_					

Maximum Particle Size	
4.75 mm	

Dispersing Agent
(NaPO3)6 @ 40 g/L

Soak Time in Dispersing Agent	
24 hrs	

Dispersing Device
Apparatus A, ASTM D-422

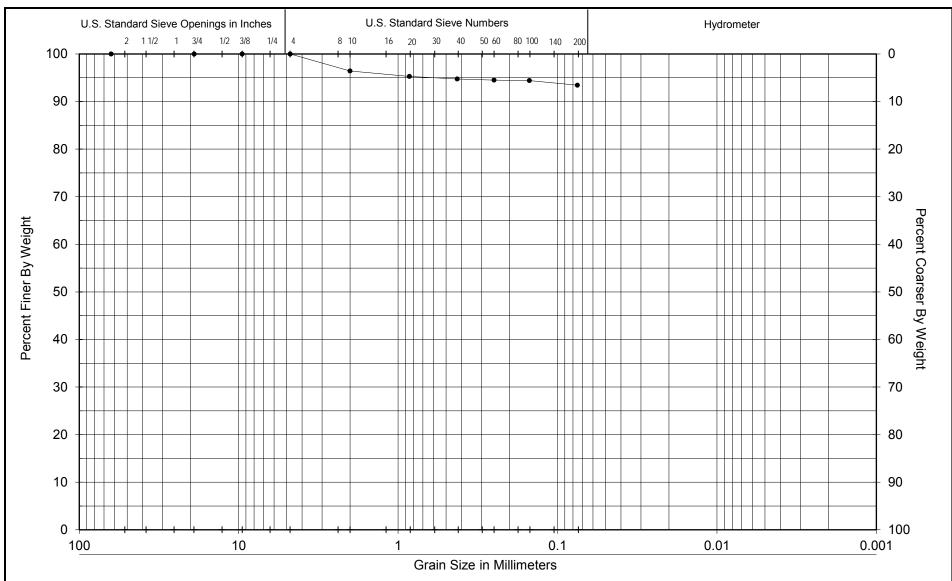
Dispersing Period	
1 min	

% Gravel	> 2 mm	3.58
% Sand	0.075 - 2 mm	2.98
% Silt	0.002 - 0.075 mm	
% Clay	< 0.002 mm	

Hydrometer Type
151H

% Passing #10 96.42 % Passing #200 93.44

% Pass 2μ





GRADATION CURVE

W18-006 Core ID A-1

SCS Engineers/City of Waco Depth 12' to 14'

Site 50



Job Number	W18-006		
Client	SCS Engineers/City of Waco		
Job Description	Site 50		
Core ID	A-1		
Top Depth	60'		
Bottom Depth	65'		
	D (mm)	Sieve #	% Finer
	63	2.5"	
	19	3/4"	
	9.5	3/8"	
	4.75	4	89.53
Grain Size Data	2	10	82.28
	0.85	20	77.42
Ö	0.425	40	75.08
<u> </u>	0.25	60	74.08
<u>Ž</u>	0.15	100	73.51
S	0.075	200	69.37
_	0.0414		60.96
<u>.e</u>	0.0297		58.31
	0.0189		56.98
0	0.0111		53.01
	0.0079	_	50.36
	0.0056		49.03
	0.0029		38.43
	0.0013		29.15
	0.0006		21.20

Maximum Particle Size	
not recorded	

Dispersing Agent
(NaPO3)6 @ 40 g/L

Soak Time in Dispersing Agent	
24 hrs	

Dispersing Device		
Apparatus A, ASTM D-422		

Dispersing Period	
1 min	

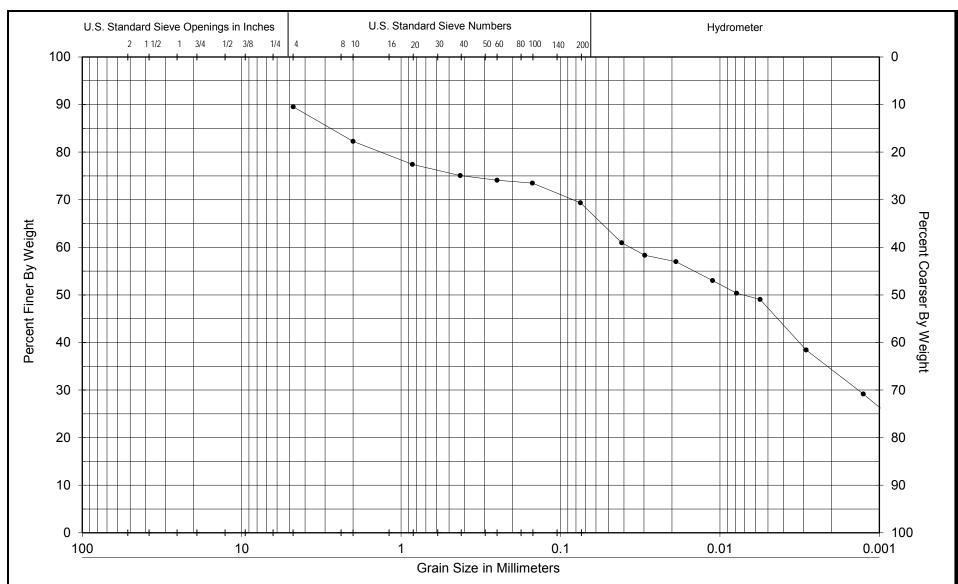
% Gravel	> 2 mm	17.72
% Sand	0.075 - 2 mm	12.91
% Silt	0.002 - 0.075 mm	37.72
% Clay	< 0.002 mm	31.64

Hydrometer Type
151H

% Passing #10 82.28 % Passing #200 69.37 % Pass 2μ 31.64

Comments:

A large piece of Shaly material did not disaggregate during the sieve analysis of this sample. It contributed to a disproportionate mass to be retained on the No. 4 sieve. The size and mass of the shale piece was not recorded. However, another sample from the same depth was wet sieved on the No. 200 sieve later. At that time, 90% of the sample passed the No. 200 sieve and 1% was retained on the No. 4 sieve.





GRADATION CURVE

W18-006 Core ID A-1

SCS Engineers/City of Waco Depth 60' to 65'

Site 50



Job Number	W18-006		
Client	SCS Engineers/City of Waco		
Job Description	Site 50		
Core ID	A-2		
Top Depth	16'		
Bottom Depth	18'		
	D (mm)	Sieve #	% Finer
	63	2.5"	100.00
	19	3/4"	100.00
	9.5	3/8"	100.00
	4.75	4	100.00
	2	10	91.44
#	0.85	20	87.21
l ö	0.425	40	85.55
<u> </u>	0.25	60	84.91
Ň	0.15	100	84.59
S	0.075	200	82.20
Grain Size Data	0.0377		76.35
<u>a</u> :	0.0271		73.72
	0.0174		71.09
0	0.0102		67.14
	0.0073		64.50
	0.0052		61.87
	0.0027		55.29
	0.0012		47.39
	0.0006		39.49

Maximum Particle Size	
4.75 mm	

Dispersing Agent
(NaPO3)6 @ 40 g/L

Soak Time in Dispersing Agent
24 hrs

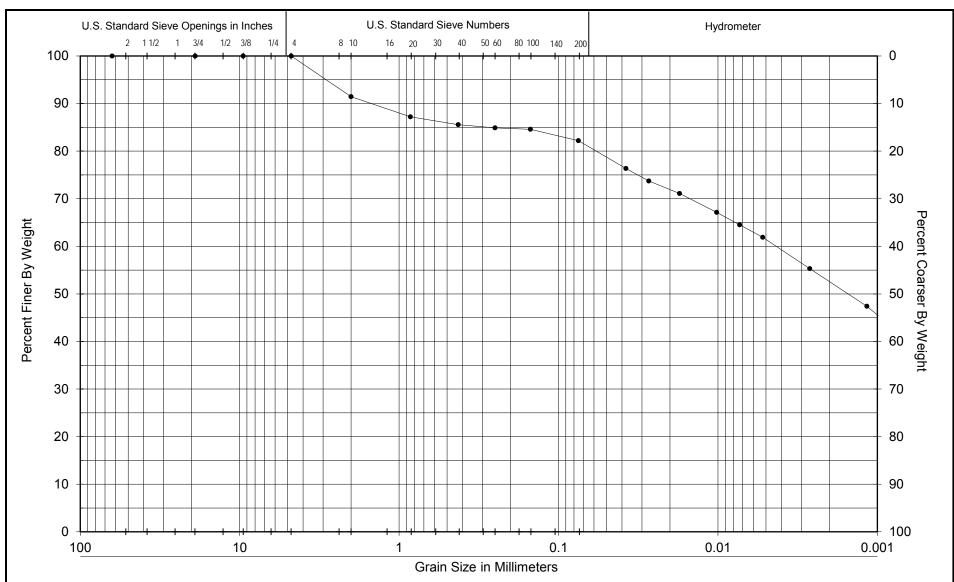
Dispersing Device
Apparatus A, ASTM D-422

Dispersing Period
1 min

% Gravel	> 2 mm	8.56
% Sand	0.075 - 2 mm	9.24
% Silt	0.002 - 0.075 mm	31.96
% Clay	< 0.002 mm	50.24

Hydrometer Type
151H

% Passing #10 91.44 % Passing #200 82.20 % Pass 2μ 50.24





GRADATION CURVE

W18-006 Core ID A-2

SCS Engineers/City of Waco Depth 16' to 18'

Site 50



Job Number	W18-006		
Client	SCS Engine	ers/City of	Waco
Job Description	Site 50		
Core ID	A-2		
Top Depth	30'		
Bottom Depth	32'		
	D (mm)	Sieve #	% Finer
	63	2.5"	
	19	3/4"	
	9.5	3/8"	
	4.75	4	95.00
Grain Size Data	2	10	92.36
	0.85	20	88.59
l ö	0.425	40	87.11
	0.25	60	86.53
Ň	0.15	100	86.25
S	0.075	200	84.12
_	0.0000		
<u>.</u>	0.0000		
	0.0000		
0	0.0000		
	0.0000		
	0.0000		
	0.0000		
	0.0000		
	0.0000	_	

Maximum Particle Size
not recorded

Dispersing Agent
(NaPO3)6 @ 40 g/L

Soak Time in Dispersing Agent	
24 hrs	

Dispersing Device
Apparatus A, ASTM D-422

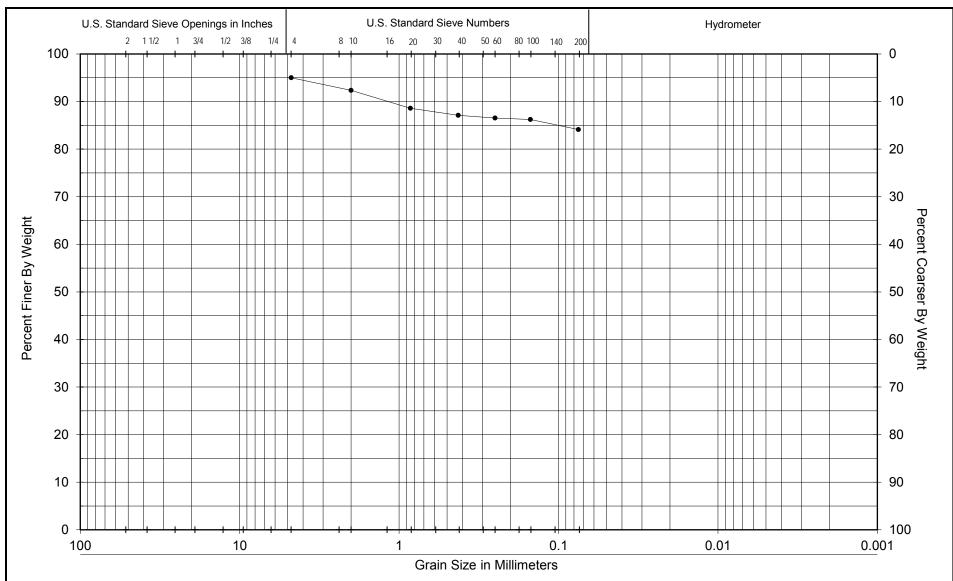
Dispersing Period	
1 min	

% Gravel	> 2 mm	7.64
% Sand	0.075 - 2 mm	8.24
% Silt	0.002 - 0.075 mm	
% Clay	< 0.002 mm	

Hydrometer Type
151H

% Passing #10 92.36 % Passing #200 84.12

% Pass 2μ





GRADATION CURVE

W18-006 Core ID A-2

SCS Engineers/City of Waco Depth 30' to 32'

Site 50



Job Number	W18-006		
Client	SCS Engineers/City of Waco		
Job Description	Site 50		
•			
Core ID	A-2 45'		
Top Depth	_		
Bottom Depth	50'	"	
	D (mm)	Sieve #	% Finer
	63	2.5"	100.00
	19	3/4"	100.00
	9.5	3/8"	100.00
	4.75	4	100.00
_ m	2	10	98.95
#	0.85	20	94.95
Data	0.425	40	93.35
<u></u>	0.25	60	92.86
Ň	0.15	100	92.65
N S	0.075	200	90.73
Grain Size	0.0384		86.17
<u>a</u> :	0.0280		80.02
	0.0181		75.40
9	0.0106		70.78
	0.0077		64.63
	0.0055		63.09
	0.0028		52.32
	0.0012		36.93
	0.0006		24.62

Maximum Particle Size	
4.75 mm	

Dispersing Agent
(NaPO3)6 @ 40 g/L

Soak Time in Dispersing Agent	
24 hrs	

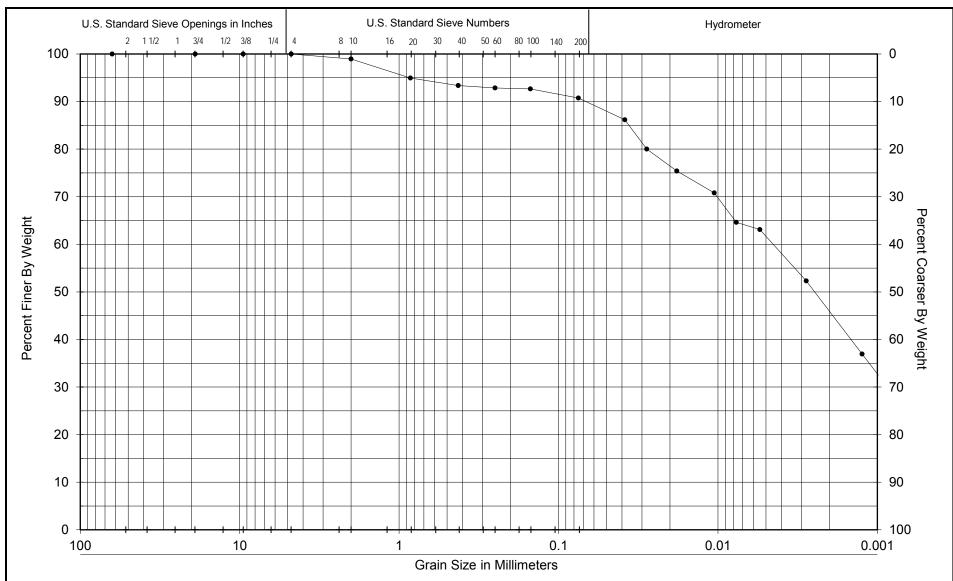
Dispersing Device		
Apparatus A, ASTM D-422		

Dispersing Period	
1 min	

% Gravel	> 2 mm	1.05
% Sand	0.075 - 2 mm	8.22
% Silt	0.002 - 0.075 mm	48.67
% Clay	< 0.002 mm	42.06

Hydrometer Type
151H

% Passing #10 98.95 % Passing #200 90.73 % Pass 2μ 42.06





GRADATION CURVE

W18-006 Core ID A-2

SCS Engineers/City of Waco Depth 45' to 50'

Site 50



Job Number	W18-006		
Client	SCS Engineers/City of Waco		
Job Description	Site 50		
Core ID	A-4		
	A-4 22'		
Top Depth			
Bottom Depth	24'	<u> </u>	0. =
	D (mm)	Sieve #	% Finer
	63	2.5"	
	19	3/4"	
	9.5	3/8"	
	4.75	4	99.00
l a	2	10	96.62
#	0.85	20	95.99
Data	0.425	40	95.53
<u> </u>	0.25	60	95.27
Ň	0.15	100	95.04
Si Si	0.075	200	93.65
Grain Size	0.0373		91.35
<u> </u>	0.0266		89.78
<u></u>	0.0169		88.20
l G	0.0100		83.48
	0.0072		80.33
	0.0052		77.18
	0.0026		69.30
	0.0011		59.85
	0.0006		50.40

Maximum Particle Size	
not recorded	

Dispersing Agent
(NaPO3)6 @ 40 g/L

Soak Time in Dispersing Agent	
24 hrs	

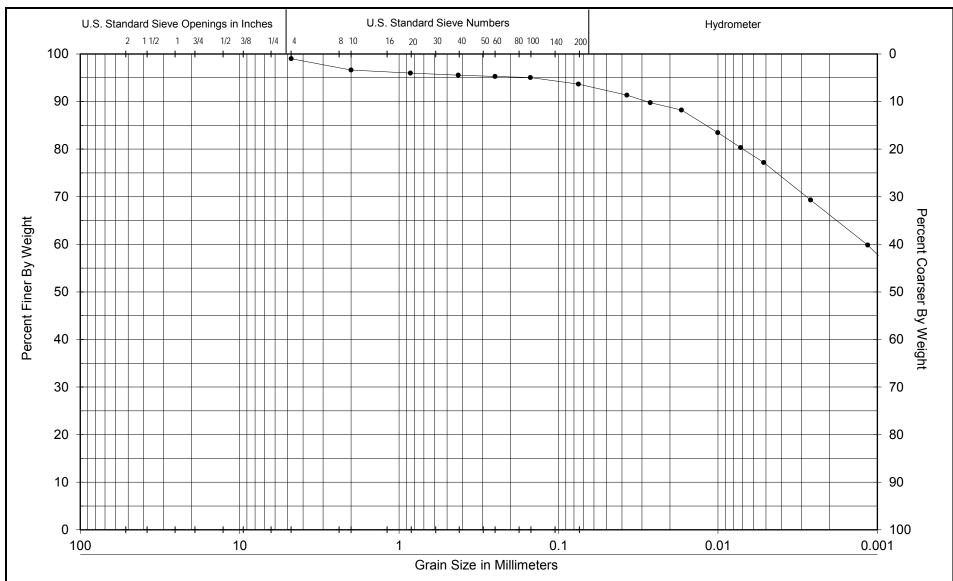
Dispersing Device
Apparatus A, ASTM D-422

Dispersing Period	
1 min	

% Gravel	> 2 mm	3.38
% Sand	0.075 - 2 mm	2.97
% Silt	0.002 - 0.075 mm	33.32
% Clay	< 0.002 mm	60.33

Hydrometer Type
151H

% Passing #10 96.62 % Passing #200 93.65 % Pass 2μ 60.33





GRADATION CURVE

W18-006 Core ID A-4

SCS Engineers/City of Waco Depth 22' to 24'

Site 50



Job Number	W18-006		
Client	SCS Engine	ers/City of	Waco
Job Description	Site 50		
Core ID	A-4		
Top Depth	31'		
Bottom Depth	36'		
	D (mm)	Sieve #	% Finer
	63	2.5"	100.00
	19	3/4"	100.00
	9.5	3/8"	100.00
Grain Size Data	4.75	4	100.00
	2	10	99.73
	0.85	20	98.46
	0.425	40	97.57
<u></u>	0.25	60	97.04
Size	0.15	100	96.65
	0.075	200	91.32
_	0.0434		58.91
<u>a</u> :	0.0314		52.54
	0.0203		46.17
9	0.0118		44.58
	0.0084		41.39
	0.0061		39.80
	0.0030		35.03
	0.0013		27.06
	0.0007		20.70

Maximum Particle Size	
4.75 mm	

Dispersing Agent
(NaPO3)6 @ 40 g/L

Soak Time in Dispersing Agent
24 hrs

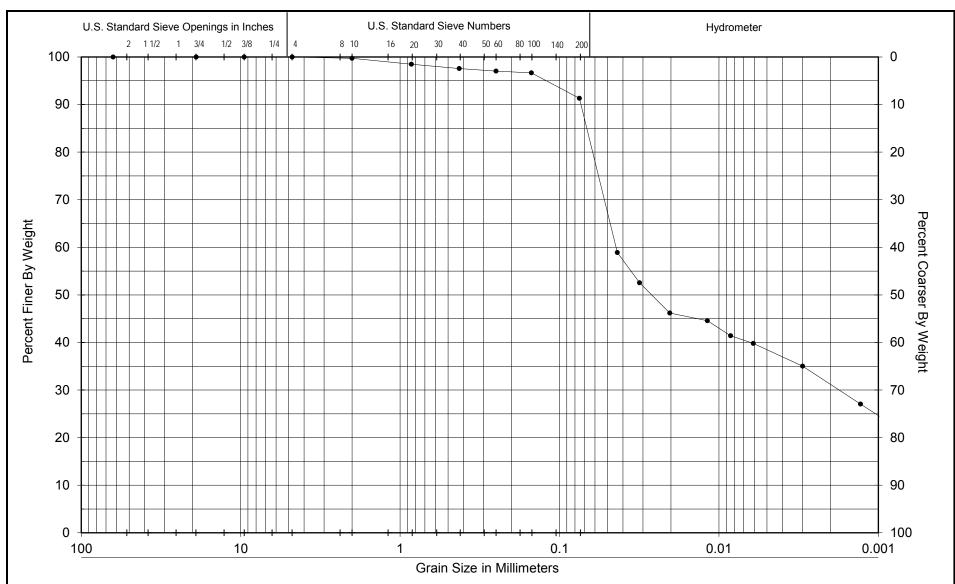
Dispersing Device
Apparatus A, ASTM D-422

Dispersing Period	
1 min	

% Gravel	> 2 mm	0.27
% Sand	0.075 - 2 mm	8.42
% Silt	0.002 - 0.075 mm	63.82
% Clay	< 0.002 mm	27.49

Hydrometer Type
151H

% Passing #10 99.73 % Passing #200 91.32 % Pass 2μ 27.49





GRADATION CURVE

W18-006 Core ID A-4

SCS Engineers/City of Waco Depth 31' to 36'

Site 50



Job Number	W18-006		
Client	SCS Engineers/City of Waco		
Job Description	Site 50		
Core ID	A-5		
Top Depth	22'		
Bottom Depth	24'		
	D (mm)	Sieve #	% Finer
	63	2.5"	
	19	3/4"	
	9.5	3/8"	
	4.75	4	91.00
	2	10	90.38
)	0.85	20	86.70
l ö	0.425	40	84.81
<u></u>	0.25	60	83.99
<u> </u>	0.15	100	83.31
S	0.075	200	75.81
Grain Size Data	0.0414		70.06
<u></u>	0.0299		65.29
	0.0192		62.10
0	0.0111		60.51
	0.0080		57.33
	0.0057		55.73
	0.0029		47.77
	0.0012		38.22
	0.0007		11.15

Maximum Particle Size	
not recorded	

Dispersing Agent
(NaPO3)6 @ 40 g/L

Soak Time in Dispersing Agent	
24 hrs	

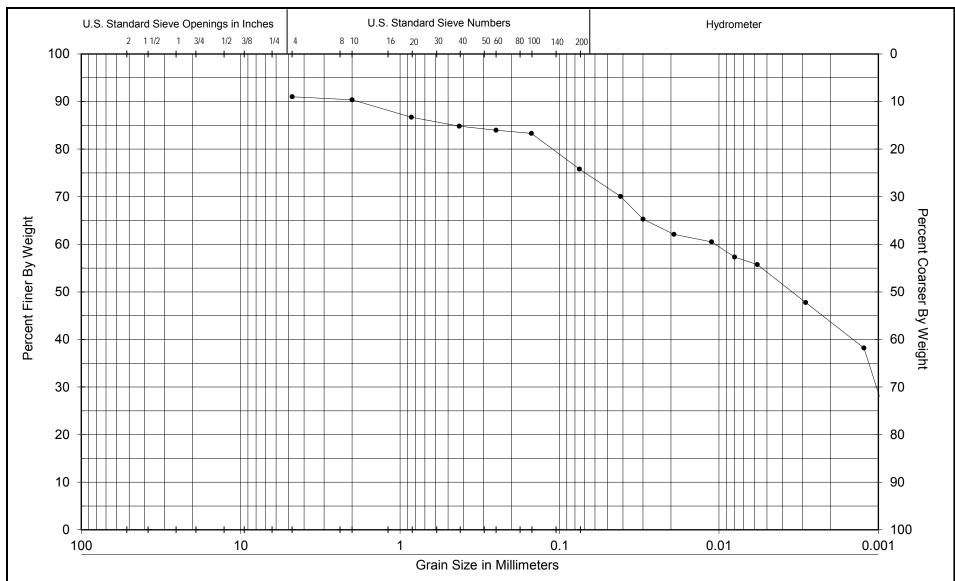
Dispersing Device	
Apparatus A, ASTM D-422	

Dispersing Period	
1 min	

% Gravel	> 2 mm	9.62
% Sand	0.075 - 2 mm	14.57
% Silt	0.002 - 0.075 mm	51.48
% Clay	< 0.002 mm	24.33

Hydrometer Type
151H

% Passing #10 90.38 % Passing #200 75.81 % Pass 2μ 24.33





GRADATION CURVE

W18-006 Core ID A-5

SCS Engineers/City of Waco Depth 22' to 24'

Site 50



2000 South 15th Street, Waco, Texas 76706 Ph: 254/235-1048 www.LFEctx.com

To: SCS Project No.: W18-068

Project: Site 50

Date: 12/28/2018 **Lab ID No.:** 9162

Material Description: Gray and Reddish-Brown Fat Clay

B-16, 10.0' - 12.0'

Sampled By: SCS

Test Performed By: PR

Test Method: ASTM D 698, Method A

Estimated Spec. Gravity: 2.70

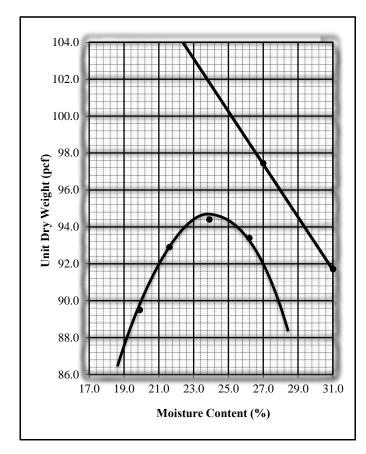
Unit Dry Wgt.

Moisture (%)	lbs/cu ft
19.9	89.5
21.6	92.9
23.9	94.4
26.2	93.4

Atterberg Limit

(ASTMD 4318-98 Wet Method)

Liquid Limit: 83
Plasticity Index: 58
Passing #200 Sieve (%): 94



Optimum Moisture (%): 23.8 Maximum Density (PCF): 94.8



2000 South 15th Street, Waco, Texas 76706 Ph: 254/235-1048 www.LFEctx.com

To: SCS

Project No.: W18-068

Project: Site 50

Date: 12/28/2018 **Lab ID No.:** 9163

Material Description: Tan and Greenish-Gray Fat Clay

B-23, 10.0' - 12.0'

Sampled By: SCS

Test Performed By: PR

Test Method: ASTM D 698, Method A

Estimated Spec. Gravity: 2.70

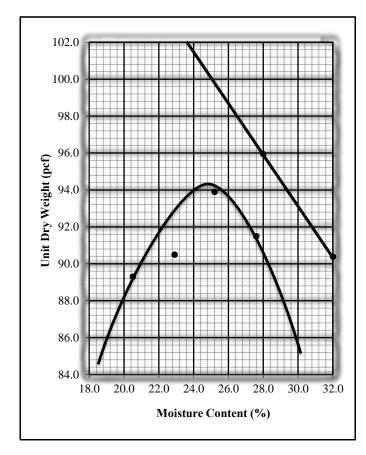
Unit Dry Wgt.

Moisture (%)	lbs/cu ft
20.5	89.3
22.9	90.5
25.2	93.9
27.6	91.5

Atterberg Limit

(ASTMD 4318-98 Wet Method)

Liquid Limit: 70
Plasticity Index: 50
Passing #200 Sieve (%): 95



Optimum Moisture (%): 24.9 Maximum Density (PCF): 94.4



2000 South 15th Street, Waco, Texas 76706 Ph: 254/235-1048 www.LFEctx.com

To: SCS

Project No.: W18-068

Project: Site 50

Date: 12/28/2018 **Lab ID No.:** 9164

Material Description: Gray Fat Clay with Sand

B-8, 10.0' - 12.0'

Sampled By: SCS

Test Performed By: PR

Test Method: ASTM D 698, Method A

Estimated Spec. Gravity: 2.70

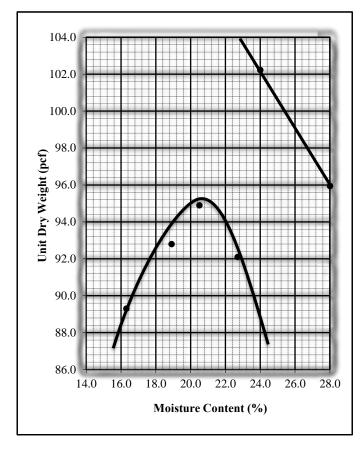
Unit Dry Wgt.

Moisture (%)	<u>lbs/cu ft</u>
16.3	89.3
18.9	92.8
20.5	94.9
22.7	92.1

Atterberg Limit

(ASTMD 4318-98 Wet Method)

Liquid Limit: 67
Plasticity Index: 50
Passing #200 Sieve (%): 85



Optimum Moisture (%): 20.6 Maximum Density (PCF): 95.3



2000 South 15th Street, Waco, Texas 76706 Ph: 254/235-1048 www.LFEctx.com

To: SCS

Project No.: W18-068

Project: Site 50

Date: 12/28/2018 **Lab ID No.:** 9165

Material Description: Gray Fat Clay

B-19, 10.0' - 12.0'

Sampled By: SCS

Test Performed By: PR

Test Method: ASTM D 698, Method A

Estimated Spec. Gravity: 2.70

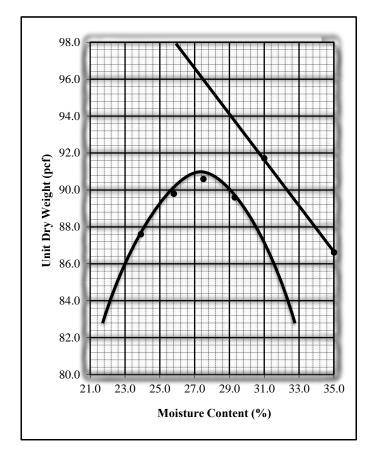
Unit Dry Wgt.

Moisture (%)	lbs/cu ft
23.9	87.6
25.8	89.8
27.5	90.6
29.3	89.6

Atterberg Limit

(ASTMD 4318-98 Wet Method)

Liquid Limit: 83
Plasticity Index: 59
Passing #200 Sieve (%): 92



Optimum Moisture (%): 27.2 Maximum Density (PCF): 90.9

Geotechnical, Environmental, Construction Materials Testing

February 8, 2019 TEAM Project No. 192022 Report No. 1

SCS Engineers 1901 Central Drive Suite 550 Bedford, Texas 76021

Attn: Ms. Basak Gulec, P.E.

Re: Geotechnical Laboratory Testing

Waco Landfill

Dear Ms. Gulec:

Submitted here is our report of laboratory testing services completed on four (4) bulk soil samples received at our materials testing laboratory in Arlington, Texas on January 31, 2019 for the above referenced project.

The samples were tested for Proctor (ASTM D-698A), Grain Size Analysis (ASTM D-422), Atterberg Limits (ASTM D-4318), and Permeability (USACE EM 1110-2-1906, Appendix VII). The results of those tests are presented on the attached proctor curves and laboratory permeability worksheets.

We appreciate the opportunity to be of assistance to you with this project. Should you have any questions, or if we may be of further assistance, please call.

Sincerely,

TEAM Consultants, Inc.

Jason Young, G Staff Geologist

SUMMARY OF LABORATORY TEST RESULTS

SCS Engineers, Waco Landfill

				n Size An STM D-4	,			erg Limits D-4318)		ity Relationship D-698)		Permeability Te (EM 1110-2-190	
Sample	Unified Classification System		Fraction	n Passin	ng Sieve	;	Liquid	Plasticity	Optimum Moisture	Max Unit Weight	Moisture Content	Dry Density	Falling Head Permeability
Identification	(ASTM D-2487)	1"	#4	#10	#40	#200	Limit	Index	(%)	(PCF)	(%)	(pcf)	K (cm/sec)
B-8 10-12'	СН	100	99.5	98.5	97.8	86.1	70	44	23.6	97.9	23.5	92.9	2.23E-08
B-16 10-12'	СН	100	99.7	99.0	98.2	90.6	71	45	24.0	97.6	23.9	92.6	1.94E-08
B-19 10-12'	СН	100	99.3	98.9	98.3	93.0	81	53	26.6	93.9	26.5	88.9	2.05E-08
B-23 10-12'	СН	100	99.4	98.3	96.7	91.6	77	49	25.1	96.0	25.0	91.2	2.69E-08

4087 Shilling Way Dallas, Texas 75237 Phone: (214) 33I-4395 Fax: (214) 33I-4458 3101 Pleasant Valley Lane, Suite IOI Arlington, Texas 76015 Phone: (817) 467-5500 Fax: (817) 468-9920

To: SCS Engineers Project: Waco Landfill

Test Method: ASTM-D-698

Job No.: 192022

Date: 2/4/19

Sample: B-8 10-12'

Proctor No. 848

Description: Tan and light gray fat clay (CH)

 Mold:
 1/30 cu. ft.

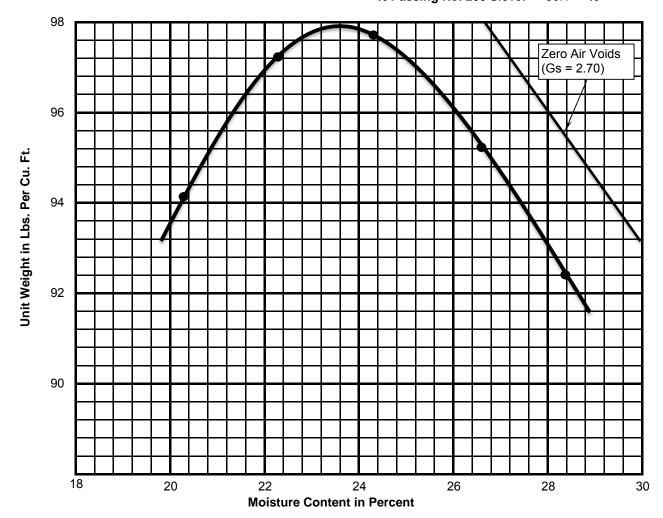
 Hammer:
 5.5#
 Liquid Limit:
 70

 Drop:
 12"
 Plasticity Index:
 44

 Blows:
 25
 Optimum Moisture:
 23.6

Blows: 25 Optimum Moisture: 23.6 %
Layers: 3 Max. Unit Dry Weight: 97.9 Lbs./Cu. Ft.

% Passing No. 200 Sieve: 86.1 %



OPTIMUM MOISTURE TEST

TEAM Consultants, Inc.

foront foung

TEAM Consultants, Inc.

4087 Shilling Way Dallas, Texas 75237 Phone: (214) 33I-4395 Fax: (214) 33I-4458 3101 Pleasant Valley Lane, Suite IOI Arlington, Texas 76015 Phone: (817) 467-5500 Fax: (817) 468-9920

To: SCS Engineers Project: Waco Landfill

Job No.: 192022

Date: 2/4/19

Sample: B-16 10-12'

Proctor No. 849

Description: Tan and light gray fat clay (CH)

Mold: 1/30 cu. ft.
Hammer: 5.5#
Prop: 12"

Test Method: ASTM-D-698

 Drop:
 12"

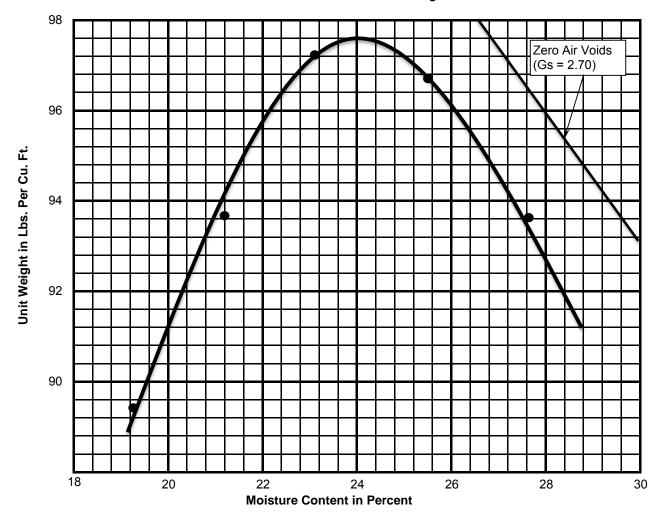
 Blows:
 25

 Layers:
 3

Liquid Limit: 71
Plasticity Index: 45
Optimum Moisture: 24.0

Max. Unit Dry Weight: 97.6 Lbs./Cu. Ft.

% Passing No. 200 Sieve: 90.6 %



OPTIMUM MOISTURE TEST

TEAM Consultants, Inc.

forost foung

4087 Shilling Way Dallas, Texas 75237 Phone: (214) 33I-4395 Fax: (214) 33I-4458 3101 Pleasant Valley Lane, Suite IOI Arlington, Texas 76015 Phone: (817) 467-5500 Fax: (817) 468-9920

To: SCS Engineers Project: Waco Landfill

Job No.: 192022

Date: 2/4/19

Sample: B-19 10-12'

Proctor No. 850

Description: Tan and light gray fat clay (CH)

Test Method: ASTM-D-698 Mold: 1/30 cu. ft. Hammer: 5.5#

Liquid Limit: 81
Plasticity Index: 53

 Hammer:
 5.5#

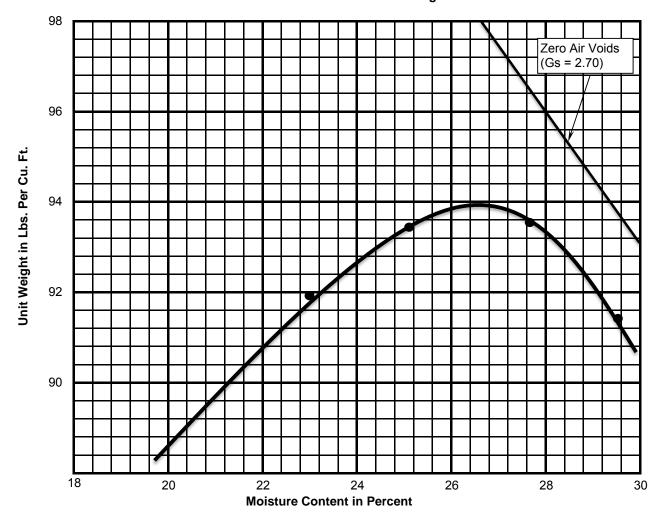
 Drop:
 12"

 Blows:
 25

 Layers:
 3

Optimum Moisture: 26.6 %
Max. Unit Dry Weight: 93.9 Lbs./Cu. Ft.

% Passing No. 200 Sieve: 93.0 %



OPTIMUM MOISTURE TEST

TEAM Consultants, Inc.

foront foung

TEAM Consultants, Inc.

4087 Shilling Way Dallas, Texas 75237 Phone: (214) 33I-4395 Fax: (214) 33I-4458 3101 Pleasant Valley Lane, Suite IOI Arlington, Texas 76015 Phone: (817) 467-5500 Fax: (817) 468-9920

To: SCS Engineers Project: Waco Landfill

Job No.: 192022

Date: 2/4/19

Sample: B-23 10-12'

Proctor No. 851

Description: Tan and light gray fat clay (CH)

Test Method: ASTM-D-698 Mold: 1/30 cu. ft. Hammer: 5.5#

Liquid Limit: 77
Plasticity Index: 49
Optimum Moisture: 25.1

 Drop:
 12"

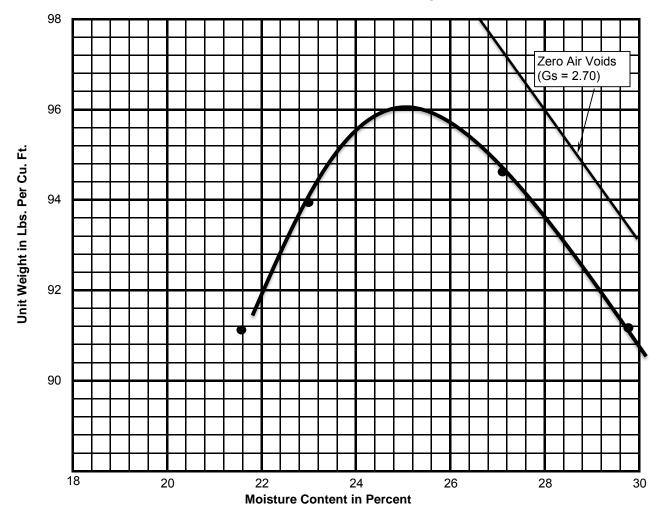
 Blows:
 25

 Layers:
 3

Optimum Moisture: 25.1 %

Max. Unit Dry Weight: 96.0 Lbs./Cu. Ft.

% Passing No. 200 Sieve: 91.6 **%**



OPTIMUM MOISTURE TEST

TEAM Consultants, Inc.

foront foung

TEAM Consultants, Inc.

PERMEABILITY TEST
EM 1110-2-1906 30 NOV 70)

(EM 1110-2-1906 30 NOV 70)								
Project: SC	S Waco Landfill		Project No.:	192022	Date:2/6/2019			
Sample No:	B-8 10-12'			Date	Sampled: n/a			
Material Description:		Tai	n and light gray	fat clay (CH)				
		·						
SAMPLE ME	EASUREMENTS			MOISTURE CO	NTENT			
Wet weight sample+ring:	320.6	g	Tare No.:		664			
Ring weight:	211.4	g	Wet weight+tar	e:	186.3 g			
Wet weight of sample:	109.2	g	Dry weight+tare	171.0 g				
Diameter:	6.35	cm	Tare weight:		105.9 g			
Area:	31.67	cm ²	Dry weight of sa	Ory weight of sample: 65.1				
Thickness:	1.877	cm	Weight of mois	ture:	15.3 g			
Unit dry weight:		pcf	Percent moistu	re:	23.5 %			
		_						
		PERMEAE	BILITY DATA					
Date & Time	Elapsed Time	Burre	tte Readings	Per	Permeability (k)			
	(t) sec	(H ₀) cm	(H ₁) cm	Single	Cumulative			
2/7/19 06:45 AM		44.6						
2/7/19 07:30 AM	2,700		44.1	2.05E-08				
2/7/19 09:30 AM	7,200		43.0	1.72E-08				
2/7/19 11:55 AM	8,700		41.4	2.14E-08				
2/7/19 02:40 PM	9,900		39.2	2.71E-08				
	28,500				2.23E-08			
Tube No.:								
Remarks: A temperate as this test was performed maintained at or slightly a	•			Tested by:	Jason Young			
				,	<u> </u>			
				Computed by:	Jason Young			
			Checked by:	James Hutt				

PERMEABILITY TEST
EM 1110-2-1906 30 NOV 70)

(EM 1110-2-1906 30 NOV 70)								
Project: SC	CS Waco Landfill		Project No.:	192022	Date: _	2/6/2019		
Sample No:	B-16 10-12'	_		Date	Sampled:	n/a		
Material Description:		Tar	n and light gray	fat clay (CH)	_			
SAMPLE ME	EASUREMENTS			MOISTURE CO	ONTENT			
Wet weight sample+ring:	320.6	g	Tare No.:		470			
Ring weight:	211.4			re:		g		
Wet weight of sample:	109.2	g	Dry weight+tare	e:	246.6	g		
Diameter:	6.35				146.9	g		
Area:			Dry weight of sample:			g		
Thickness:		cm	Weight of moisture:		23.8	g		
Unit dry weight:		pcf	Percent moistu	re:	23.9	%		
		PERMEAB	BILITY DATA					
Date & Time	Elapsed Time	Burre	tte Readings	Pe	Permeability (k)			
	(t) sec	(H ₀) cm	(H ₁) cm	Single	Cı	umulative		
2/7/19 07:30 AM		47.9						
2/7/19 09:30 AM	7,200		46.7	1.73E-08				
2/7/19 11:55 AM	8,700		45.1	1.97E-08				
2/7/19 02:40 PM	9,900		43.0	2.37E-08				
2/7/19 05:15 PM	9,300		41.7	1.62E-08				
	35,100				1.9	94E-08		
Tube No.:								
Remarks: A temperate as this test was performed maintained at or slightly a	•			-				
				Tested by:	Jason Yo	ung		
				Computed by:	Jason Yo	oung		
Checked by: James Hutt								

PERMEABILITY TEST

(EM 1110-2-1906 30 NOV 70)								
Project: SC			Project No.:					
Sample No:					Sampled: n/a			
Material Description:		Та	n and light gray fa	at clay (CH)				
SAMDI E MI	EASUREMENTS			MOISTURE CON	NTENT			
Wet weight sample+ring:		g	Tare No.:	WOISTONE CON				
Ring weight:	·	<u> </u>		:				
<u></u>	107.1	<u> </u>			-			
Diameter:		cm		136.0 g				
Area:		cm ²		ry weight of sample: 79.2				
Thickness:		cm	Weight of moistu	ıre:	21.0 g			
Unit dry weight:	88.9	pcf	Percent moisture	e:	26.5 %			
		PERMEAE	BILITY DATA	_				
Date & Time	·		tte Readings		neability (k)			
	(t) sec	(H ₀) cm	(H ₁) cm	Single	Cumulative			
2/7/19 06:45 AM		44.5						
2/7/19 07:30 AM	2,700		44.0	2.06E-08				
2/7/19 09:30 AM	7,200		42.6	2.21E-08				
2/7/19 11:55 AM	8,700		41.1	2.02E-08				
2/7/19 02:40 PM	9,900		39.5	1.97E-08	0.055.00			
	28,500				2.05E-08			
Tube No.:								
Remarks: A temperate as this test was performed maintained at or slightly a	•							
				Tested by:	Jason Young			
				Computed by:	Jason Young			
			(Checked by:	James Hutt			

PERMEABILITY TEST	
EM 1110-2-1906 30 NOV 70)

(EM 1110-2-1906 30 NOV 70)							
Project: SC	CS Waco Landfill		Project No ·	192022	Date [.]	2/6/2019	
Sample No:					Sampled:		
Material Description:		 Ta	—— n and light gray		_		
Material Description.		ı a	ir and light gray	Tat Clay (OTT)			
SAMPLE MI	EASUREMENTS			MOISTURE CO	NTENT		
Wet weight sample+ring:	319.9	<u>g</u>	Tare No.:		678		
Ring weight:	211.4	g		re:		g	
Wet weight of sample:	108.5	g	Dry weight+tare	e:	215.6	g	
Diameter:	6.35	cm	Tare weight: _		127.1	g	
Area:		cm ²	<u></u>	ample:		g	
Thickness:		cm		ture:		g	
Unit dry weight:		pcf		ire:		%	
		-					
		PERMEA	BILITY DATA				
Date & Time	Elapsed Time	Burre	tte Readings	Per	Permeability (k)		
	(t) sec	(H ₀) cm	n (H ₁) cm	Single	Cı	umulative	
2/7/19 06:45 AM		46.4					
2/7/19 07:30 AM	2,700		45.8	2.37E-08			
2/7/19 09:30 AM	7,200		44.1	2.58E-08			
2/7/19 11:55 AM	8,700		41.8	3.03E-08			
2/7/19 02:40 PM	9,900		39.7	2.56E-08			
	28,500				2.6	69E-08	
Tube No.: Area of Tube: Confining Load: 0.	5 0829 cm ² 625 tsf			$K = \left\lfloor \frac{axL}{Axt} \right\rfloor$ $K = 2.69$	$\frac{\left x\ln\left \frac{H_0}{H_1}\right xR_T\right }{9E-08}$	cm/sec	
Remarks: A temperate as this test was performed maintained at or slightly a	•	,					
				Tested by:	Jason Yo	ung	
				Computed by:	Jason Yc	oung	
				Checked by:	James F	lutt	

Client: Langerman Foster Engineering

Project: Site 50 Part 2 Sample: B-24 (45-46)

43240.1

Specimens							
Identification	1	2	3	4			
Depth/Elev. (ft)	-	-	-	-			
Eff. Consol. Stress (psi)	20.0	50.0	100.0	-			
Initial Specimen Properties							
Avg. Diameter (in)	1.47	1.49	1.51	-			
Avg. Height (in)	3.16	3.03	2.90	-			
Avg. Water Content (%)	18.2	-	1	-			
Bulk Density (pcf)	115.9	117.8	120.5	-			
Dry Density (pcf)	98.0	-	-	-			
Saturation (%)	67.4	-	-	-			
Void Ratio, n	0.74	0.71	0.67	-			
Total Back-Pressure (psi)	79.1	79.1	79.1	-			
B-Value, End of Saturation	0.97	-	-	-			
Note - A specific gravity of 2.73 was assumed for mass/volume calculations							

Test Setup				
Specimen Condition	Undisturbed / Intact			
Specimen Preparation	Trimmed			
Mounting Method	Wet			
Consolidation	Isotropic			

Test Method: ASTM D4767 Mod

Post-Consolidation / Pre-Shear					
Void Ratio		0.74	0.71	0.67	-

Shear / Post-Shear					
Rate of Strain (%/hr) 0.50 0.50 -					
Avg. Water Content (%)	-	-	22.4	-	

Note - A specific gravity of 2.73 was assumed for mass/volume calculations.

	At I	ailure						
Failure Criterion: Peak Principal Stress	Difference, $(\sigma_1' - \sigma_3')_{max}$ Ratio, $(\sigma_1' / \sigma_3')_{max}$							
Axial Strain at Failure (%), $\epsilon_{a,f}$	-	-	-	-	2.4	1.8	1.6	-
Minor Effective Stress (psi), σ ₃ ' _f	-	-	-	-	4.0	14.4	35.5	-
Principal Stress Difference (psi), (σ ₁ -σ ₃) _f	-	-	-	-	42.1	82.8	124.6	-
Pore Water Pressure, $\Delta u_f(psi)$	-	-	-	-	15.9	35.3	64.3	-
Major Effective Stress (psi), σ ₁ ' _f	-	-	-	-	46.1	97.2	160.1	-
Secant Friction Angle (degrees)	-	-	-	-	57.2	47.8	39.6	-
Effective Friction Angle (degrees)	- 34.0							
Effective Cohesion (psi)	- 10.0							

Note: Multi-stage testing was performed for this sample. The first two stages were terminated in accordance with stress path tangency and/or peak principal stress ratio. The presented M-C parameters are based on a linear regression in modified stress space, across all assigned effective consolidation stresses. This fit does not purported to capture typical curvature of envelopes that may, in particular, be observed across broader range in effective stresses. Please note that the stresses associated with peak principal stress ratio are presented in tabular form on the first page of the report. There are alternate interpretations to this failure criterion including but not limited to peak principal stress difference and strain compatibility.

Jeffrey A. Kuhn , Ph.D., P.E., 1/2/2019

Analysis & Quality Review/Date

1 of 6

Client: Langerman Foster Engineering TRI Log #: 43240.1

Project: Site 50 Part 2 Test Method: ASTM D4767 Mod

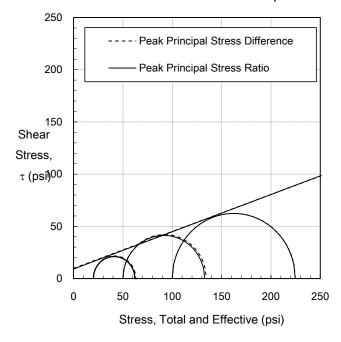
Sample: B-24 (45-46)

R / "Total Stress" Envelope					
Failure Criterion: Peak Principal Stress Difference, $(\sigma_1' - \sigma_3')_{max}$ Ratio, $(\sigma_1'/\sigma_3')_{max}$					
Friction Angle (deg) ϕ_R		19.5	19.6		
Cohesion (psi)	c _R	9.7	9.1		

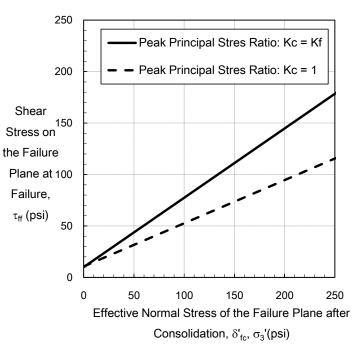
Kc = Kf Envelope, Effective Stress Envelope (Duncan et al. 1990)					
Failure Criterion: Peak Principal Stress Difference, $(\sigma_1' - \sigma_3')_{max}$ Ratio, $(\sigma_1' / \sigma_3')_{max}$					
Effective Friction Angle (deg)	φ'	33.9	34.0		
Effective Cohesion (psi) c' 10.1 10.0					

Kc = 1 (τ_{ff} vs σ'_{fc}) Enelope, Total Stress Envelope (Duncan et al. 1990)					
Failure Criterion: Peak Principal Stress Difference, $(\sigma_1' - \sigma_3')_{max}$ Ratio, $(\sigma_1'/\sigma_3')_{max}$					
Friction Angle (deg) d _{Kc=1}		22.5	22.8		
Cohesion (psi)					

R / "Total Stress" Envelope



Three-Stage Rapid Drawdown Envelopes



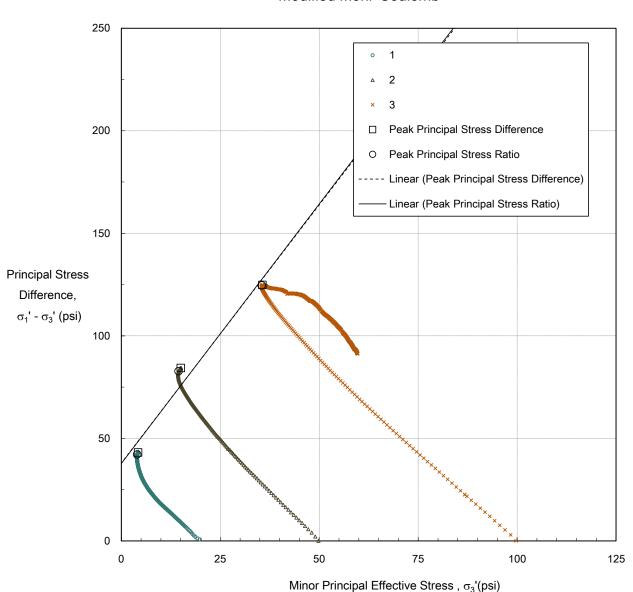
2 of 6

Client: Langerman Foster Engineering

TRI Log #: 43240.1

Project: Site 50 Part 2 Sample: B-24 (45-46) Test Method: ASTM D4767 Mod

Modified Mohr-Coulomb



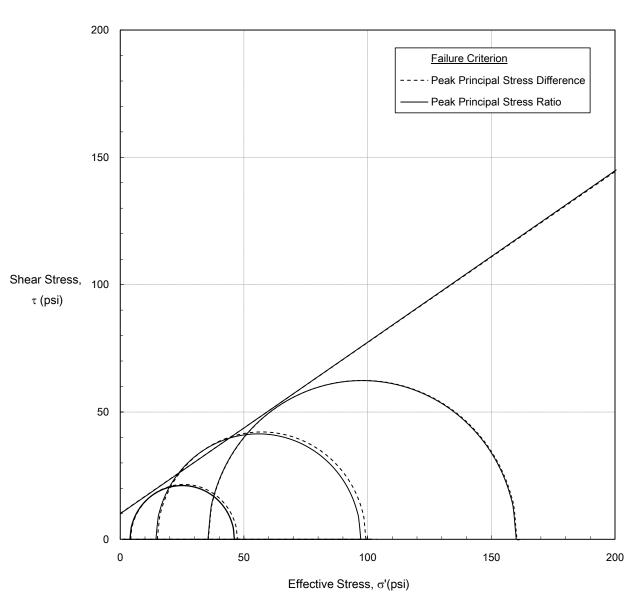
Failure Criterion: Peak Principal Stress	Difference, $(\sigma_1'-\sigma_3')_{max}$	Ratio, $(\sigma_1'/\sigma_3')_{max}$	
Effective Friction Angle (deg)	-	34.0	
Effective Cohesion (psi)	of 6 -	10.0	

Client: Langerman Foster Engineering

TRI Log #: 43240.1

Project: Site 50 Part 2 Sample: B-24 (45-46) Test Method: ASTM D4767 Mod

Mohr-Coulomb



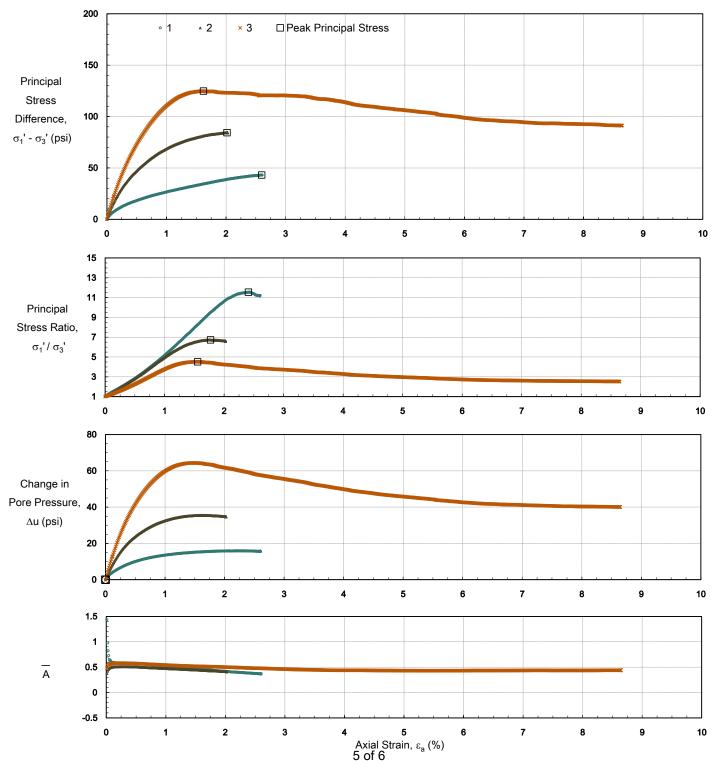
Failure Criterion: Peak Principal Stress	Difference, $(\sigma_1'-\sigma_3')_{max}$	Ratio, $(\sigma_1'/\sigma_3')_{max}$
Effective Friction Angle (deg)	-	34.0
Effective Cohesion (psi)	of 6	10.0

Client: Langerman Foster Engineering

Revision 0

43240.1 Project: Site 50 Part 2 Test Method: ASTM D4767 Mod

Sample: B-24 (45-46)



Client: Langerman Foster Engineering

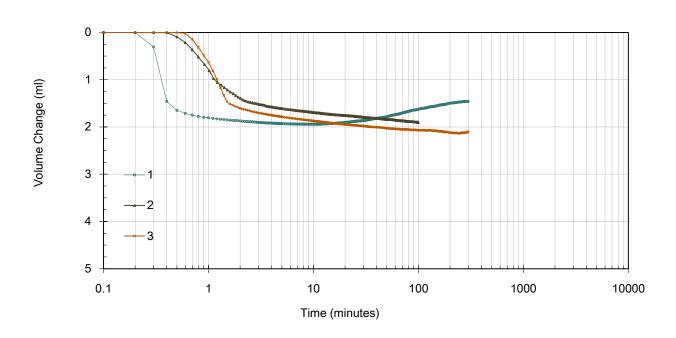
Project: Site 50 Part 2

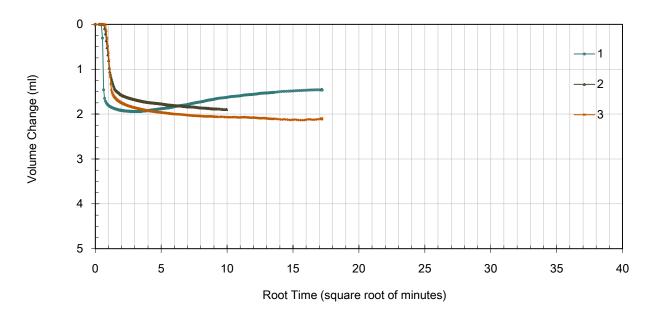
Sample: B-24 (45-46)

TRI Log #: 43240.1

Test Method: ASTM D4767 Mod

Consolidation





6 of 6

AUSTIN, TX - USA | ANAHEIM, CA - USA | ANDERSON, SC - USA | GOLD COAST - AUSTRALIA | SUZHOU - CHINA

Consolidated-Undrained Triaxial Compression

Client: Langerman Foster Engineering

TRI Log #: 43240.2

Test Method: ASTM D4767

Project: Site 50 Part 2 Sample: B-17 (25-26)

Sp	ecimens							
Identification	1	2	3	4				
Depth/Elev. (ft)	-	-	-	-				
Eff. Consol. Stress (psi)	20.0	-	100.0	-				
Initial Spe	Initial Specimen Properties							
Avg. Diameter (in)	1.45	-	1.39	-				
Avg. Height (in)	3.22	-	3.32	-				
Avg. Water Content (%)	18.5	-	18.5	-				
Bulk Density (pcf)	124.8	-	132.2	-				
Dry Density (pcf)	105.3	-	111.6	-				
Saturation (%)	81.8	-	95.9	-				
Void Ratio, n	0.62	-	0.53	-				
Total Back-Pressure (psi)	80.0		37.6	-				
B-Value, End of Saturation	0.96	-	0.95	-				

Test Setup					
Specimen Condition Undisturbed / Intact					
Specimen Preparation	Trimmed				
Mounting Method	Wet				
Consolidation	Isotropic				

Post-Consolidation / Pre-Shear						
Void Ratio	0.62	ı	0.53	-		

Shear / Post-Shear					
Rate of Strain (%/hr)	1.00	-	0.25	-	
Avg. Water Content (%)	23.4	-	22.5	1	

Note - A specific gravity of 2.73 was assumed for mass/volume calculations.

	At F	ailure						
Failure Criterion: Peak Principal Stress	Di	Difference, (σ ₁ '-σ ₃ ') _{max}				Ratio, $(\sigma_1'/\sigma_3')_{max}$		
Axial Strain at Failure (%), $\epsilon_{a,f}$	14.8	-	6.2	-	2.2	-	4.7	-
Minor Effective Stress (psi), σ ₃ ' _f	18.0	-	88.0	-	10.3	-	83.4	-
Principal Stress Difference (psi), (σ ₁ -σ ₃) _f	33.8	-	144.5	-	23.2	-	141.8	-
Pore Water Pressure, Δu_f (psi)	2.1	-	12.1	-	9.7	-	16.6	-
Major Effective Stress (psi), σ ₁ ' _f	51.8	-	232.5	-	33.5	-	225.2	-
Secant Friction Angle (degrees)	28.9	-	26.8	-	32.0	-	27.4	-
Effective Friction Angle (degrees)		26.2			26.6			
Effective Cohesion (psi)		1.6				2	2.0	

Note: The presented M-C parameters are based on a linear regression in modified stress space, across all assigned effective consolidation stresses. This fit does not purported to capture typical curvature of envelopes that may, in particular, be observed across broader range in effective stresses. Please note that the stresses associated with peak principal stress ratio and peak principal stress difference are presented in tabular form on the first page of the report. There are alternate interpretations to theses two failure criterion including but not limited to strain compatibility and post-peak.

Jeffrey A. Kuhn , Ph.D., P.E., 1/2/2019

Analysis & Quality Review/Date

1 of 6

Client: Langerman Foster Engineering TRI Log #: 43240.2

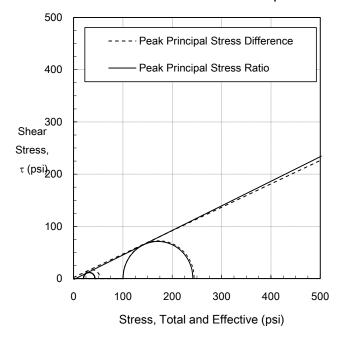
Project: Site 50 Part 2 Test Method: ASTM D4767 Sample: B-17 (25-26)

R / "Total Stress" Envelope							
Failure Criterion: Peak Principal Stress		Difference, $(\sigma_1'-\sigma_3')_{max}$	Ratio, $(\sigma_1'/\sigma_3')_{max}$				
Friction Angle (deg) ϕ_R		24.1	25.2				
Cohesion (psi)	c _R	2.0	-2.0				

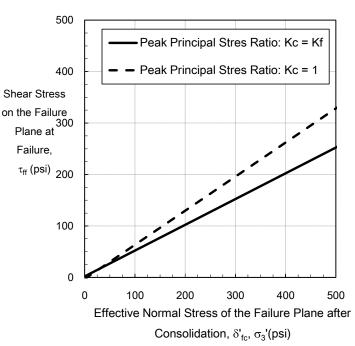
Kc = Kf Envelope, Effective Stress Envelope (Duncan et al. 1990)							
Failure Criterion: Peak Principal Stress		Difference, $(\sigma_1'-\sigma_3')_{max}$	Ratio, $(\sigma_1'/\sigma_3')_{max}$				
Effective Friction Angle (deg)	φ'	26.2	26.6				
Effective Cohesion (psi)	c'	1.6	2.0				

Kc = 1 (τ_{ff} vs σ'_{fc}) Enelope, Total Stress Envelope (Duncan et al. 1990)						
Failure Criterion: Peak Principal Stres	S	Difference, $(\sigma_1'-\sigma_3')_{max}$	Ratio, $(\sigma_1'/\sigma_3')_{max}$			
Friction Angle (deg) d _{Kc=1}		31.8	33.5			
Cohesion (psi) ψ _{Kc=1}		2.8	-2.9			

R / "Total Stress" Envelope



Three-Stage Rapid Drawdown Envelopes



2 of 6

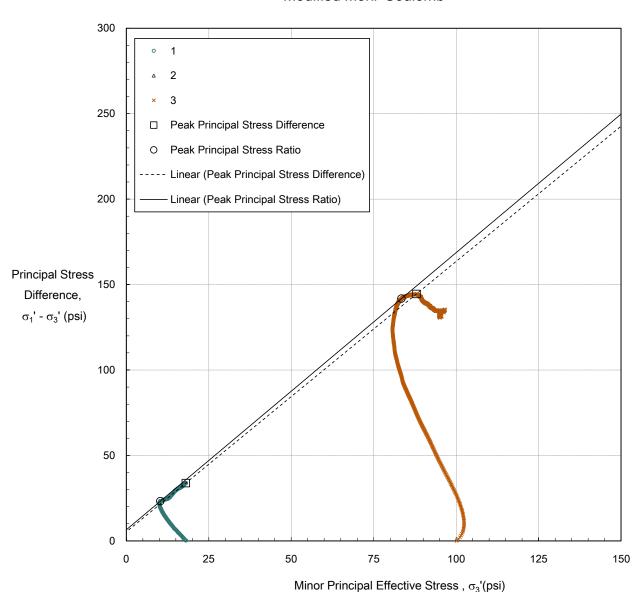
Client: Langerman Foster Engineering

TRI Log #: 43240.2

Test Method: ASTM D4767

Project: Site 50 Part 2 Sample: B-17 (25-26)

Modified Mohr-Coulomb



Failure Criterion: Peak Principal Stress	Difference, $(\sigma_1'-\sigma_3')_{max}$	Ratio, $(\sigma_1'/\sigma_3')_{max}$
Effective Friction Angle (deg)	26.2	26.6
Effective Cohesion (psi)	of 6 1.6	2.0

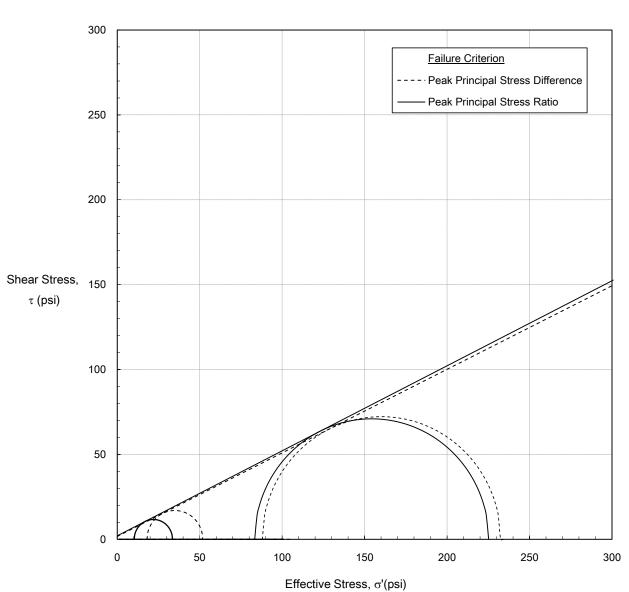
Client: Langerman Foster Engineering

TRI Log #: 43240.2

Test Method: ASTM D4767

Project: Site 50 Part 2 Sample: B-17 (25-26)

Mohr-Coulomb

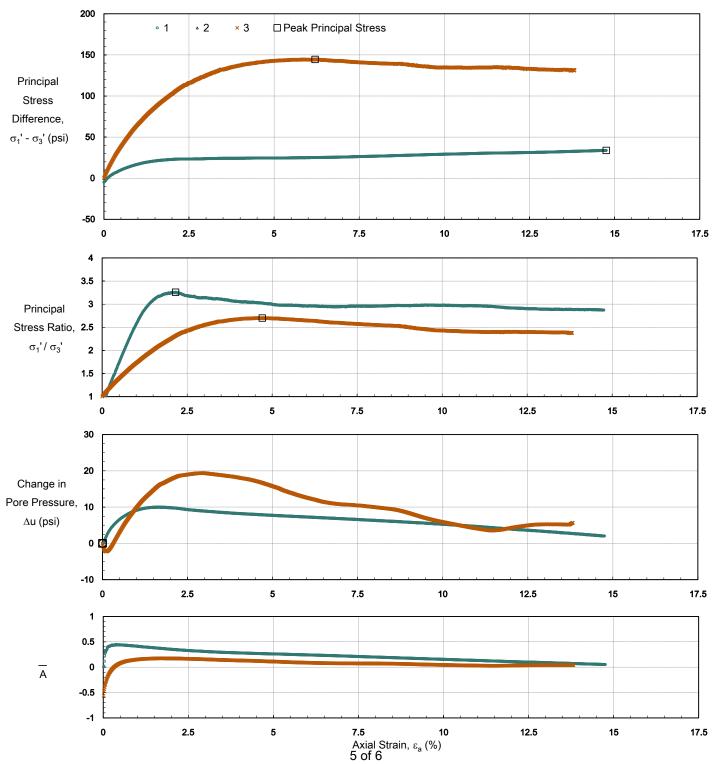


Failure Criterion: Peak Principal Stress	Difference, $(\sigma_1'-\sigma_3')_{max}$	Ratio, $(\sigma_1'/\sigma_3')_{max}$	
Effective Friction Angle (deg)	26.2	26.6	
Effective Cohesion (psi)	of 6 1.6	2.0	

Client: Langerman Foster Engineering

TRI Log #: 43240.2 Project: Site 50 Part 2 Test Method: ASTM D4767

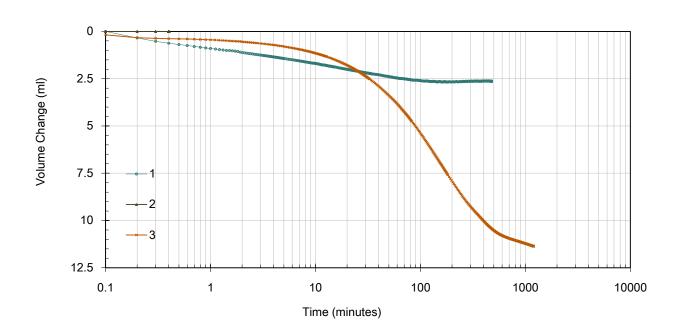
Sample: B-17 (25-26)

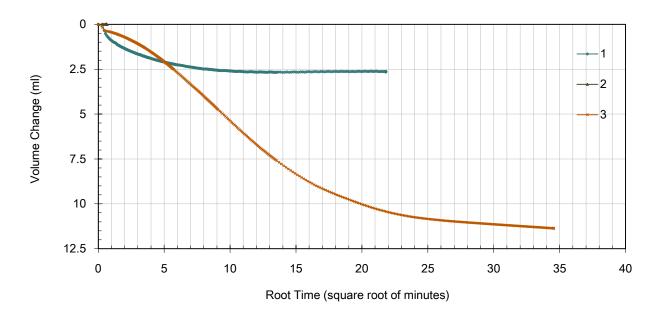


Client: Langerman Foster Engineering

Project: Site 50 Part 2 Sample: B-17 (25-26) TRI Log #: 43240.2 Test Method: ASTM D4767

Consolidation





6 of 6

AUSTIN, TX - USA | ANAHEIM, CA - USA | ANDERSON, SC - USA | GOLD COAST - AUSTRALIA | SUZHOU - CHINA

Consolidated-Undrained Triaxial Compression

Client: Langerman Foster Engineering

TRI Log #: 43240.3 Project: Site 50 Part 2 Test Method: ASTM D4767

Sample: B-31 (15-15.9)

Specimens							
Identification	1	2	3	4			
Depth/Elev. (ft)	-	-	-	-			
Eff. Consol. Stress (psi)	20.0	-	100.0	-			
Initial Specimen Properties							
Avg. Diameter (in)	1.41	-	1.45	-			
Avg. Height (in)	2.94	-	3.24	-			
Avg. Water Content (%)	19.2	-	24.9	-			
Bulk Density (pcf)	140.5	-	119.9	-			
Dry Density (pcf)	117.8	-	96.0	-			
Saturation (%)	117.7	-	87.8	-			
Void Ratio, n	0.45	-	0.77	-			
Total Back-Pressure (psi)	79.1	-	79.6	-			
B-Value, End of Saturation	0.99	-	0.95	-			

Test Setup					
Undisturbed / Intact					
Trimmed					
Wet					
Isotropic					

Post-Consolidation / Pre-Shear						
Void Ratio		0.44	ı	0.77	-	

Shear / Post-Shear						
Rate of Strain (%/hr) 0.50 - 0.50 -						
Avg. Water Content (%)	26.8	-	24.9	-		

Note - A specific gravity of 2.73 was assumed for mass/volume calculations.

	At I	Failure						
Failure Criterion: Peak Principal Stress	Di	Difference, $(\sigma_1'-\sigma_3')_{max}$				Ratio, $(\sigma_1'/\sigma_3')_{max}$		
Axial Strain at Failure (%), $\epsilon_{a,f}$	16.7	-	2.4	-	11.9	-	2.3	-
Minor Effective Stress (psi), σ ₃ ' _f	9.6	-	47.6	-	9.2	-	47.6	-
Principal Stress Difference (psi), (σ ₁ -σ ₃) _f	32.4	-	91.3	-	31.4	-	91.3	-
Pore Water Pressure, Δu _f (psi)	9.2	-	52.6	-	9.6	-	52.7	-
Major Effective Stress (psi), σ ₁ ' _f	42.0	-	138.9	-	40.6	-	138.8	-
Secant Friction Angle (degrees)	38.9	-	29.3	-	39.0	-	29.3	-
Effective Friction Angle (degrees)		25.9			26.0			
Effective Cohesion (psi)		5	.5			5	.3	

Note: The presented M-C parameters are based on a linear regression in modified stress space, across all assigned effective consolidation stresses. This fit does not purported to capture typical curvature of envelopes that may, in particular, be observed across broader range in effective stresses. Please note that the stresses associated with peak principal stress ratio and peak principal stress difference are presented in tabular form on the first page of the report. There are alternate interpretations to theses two failure criterion including but not limited to strain compatibility and post-peak.

Jeffrey A. Kuhn , Ph.D., P.E., 1/2/2019

Analysis & Quality Review/Date

1 of 6

Client: Langerman Foster Engineering TRI Log #: 43240.3

Project: Site 50 Part 2 Test Method: ASTM D4767

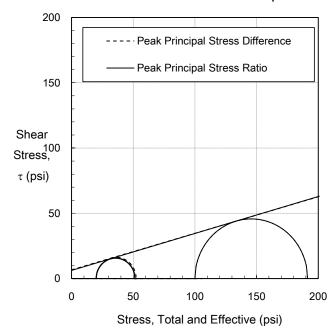
Sample: B-31 (15-15.9)

R / "Total Stress" Envelope					
Failure Criterion: Peak Principal Stress Difference, $(\sigma_1'-\sigma_3')_{max}$ Ratio, $(\sigma_1'/\sigma_3')_{max}$					
Friction Angle (deg) ϕ_R		15.6	15.8		
Cohesion (psi)	c_R	6.7	6.2		

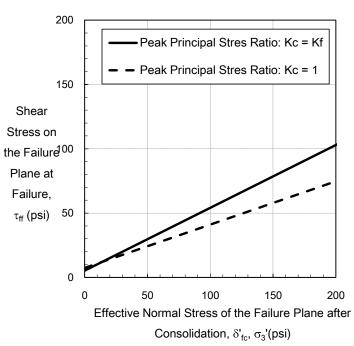
Kc = Kf Envelope, Effective Stress Envelope (Duncan et al. 1990)					
Failure Criterion: Peak Principal Stress Difference, $(\sigma_1' - \sigma_3')_{max}$ Ratio, $(\sigma_1' / \sigma_3')_{max}$					
Effective Friction Angle (deg)		25.9	26.0		
Effective Cohesion (psi)	c'	5.5	5.3		

Kc = 1 (τ_{ff} vs σ'_{fc}) Enelope, Total Stress Envelope (Duncan et al. 1990)						
Failure Criterion: Peak Principal Stress Difference, $(\sigma_1' - \sigma_3')_{max}$ Ratio, $(\sigma_1' / \sigma_3')_{max}$						
Friction Angle (deg) d _{Kc=1}		18.3	18.6			
Cohesion (psi)						

R / "Total Stress" Envelope



Three-Stage Rapid Drawdown Envelopes



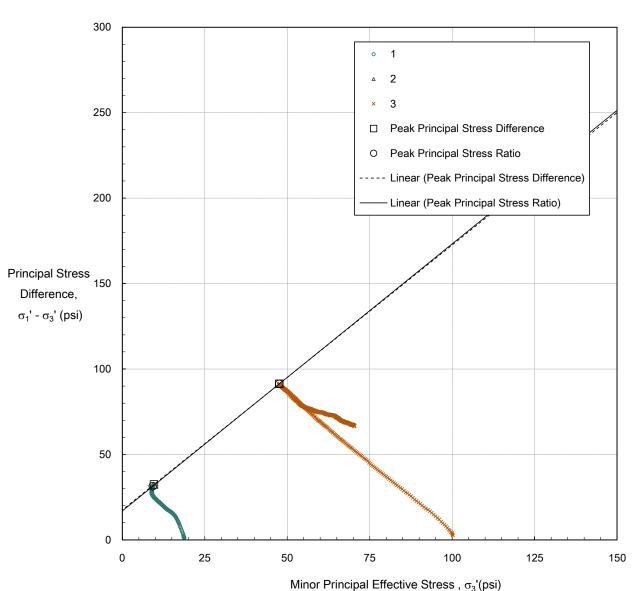
2 of 6

Client: Langerman Foster Engineering

TRI Log #: 43240.3 Project: Site 50 Part 2 Test Method: ASTM D4767

Sample: B-31 (15-15.9)

Modified Mohr-Coulomb



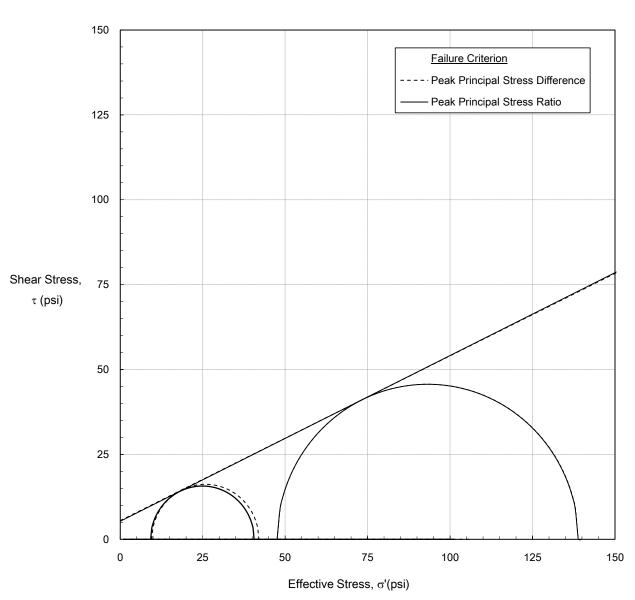
Failure Criterion: Peak Principal Stress	Difference, $(\sigma_1'-\sigma_3')_{max}$	Ratio, $(\sigma_1'/\sigma_3')_{max}$
Effective Friction Angle (deg)	25.9	26.0
Effective Cohesion (psi)	of 6 5.5	5.3

Client: Langerman Foster Engineering

TRI Log #: 43240.3 Test Method: ASTM D4767

Project: Site 50 Part 2 Sample: B-31 (15-15.9)

Mohr-Coulomb



Failure Criterion: Peak Principal Stress	Difference, $(\sigma_1'-\sigma_3')_{max}$	Ratio, $(\sigma_1'/\sigma_3')_{max}$
Effective Friction Angle (deg)	25.9	26.0
Effective Cohesion (psi)	of 6 5.5	5.3

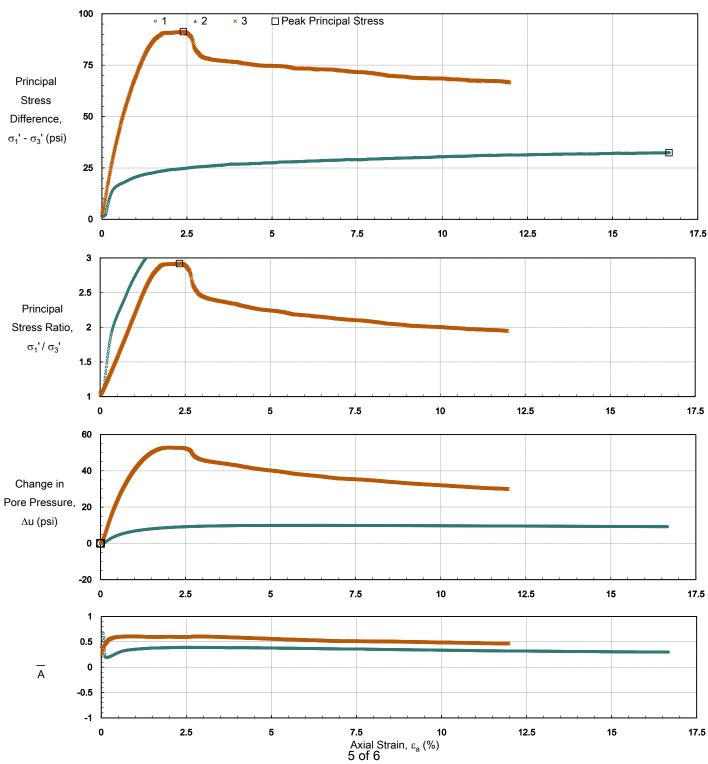
Client: Langerman Foster Engineering

Revision 0

Project: Site 50 Part 2

Sample: B-31 (15-15.9)

eering TRI Log #: 43240.3 Test Method: ASTM D4767



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May 2020

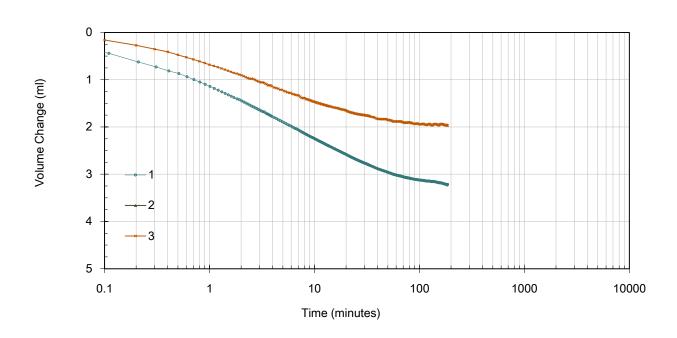
Client: Langerman Foster Engineering

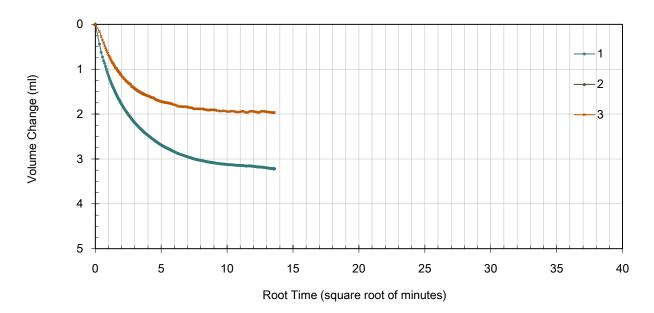
Revision 0

Project: Site 50 Part 2 Sample: B-31 (15-15.9) TRI Log #: 43240.3 Test Method: ASTM D4767

May 2020

Consolidation





6 of 6

AUSTIN, TX - USA | ANAHEIM, CA - USA | ANDERSON, SC - USA | GOLD COAST - AUSTRALIA | SUZHOU - CHINA

Consolidated-Undrained Triaxial Compression

Client: Langerman Foster Engineering

TRI Log #: 43240.4

Test Method: ASTM D4767

Project: Site 50 Part 2 Sample: B-44 (50-51.5)

Sp	ecimens			
Identification	1	2	3	4
Depth/Elev. (ft)	-	-	ı	1
Eff. Consol. Stress (psi)	20.0	-	100.0	ı
Initial Spe	cimen Pro	operties		
Avg. Diameter (in)	1.53	-	1.43	-
Avg. Height (in)	3.28	-	3.31	-
Avg. Water Content (%)	18.3	-	15.3	ı
Bulk Density (pcf)	123.9	-	140.5	-
Dry Density (pcf)	104.7	-	121.8	-
Saturation (%)	79.7	-	105.2	-
Void Ratio, n	0.63	-	0.40	-
Total Back-Pressure (psi)	79.3	-	83.8	-
B-Value, End of Saturation	0.98	-	0.99	•

st Setup
Undisturbed / Intact
Trimmed
Wet
Isotropic

Post-Consolidation / Pre-Shear					
Void Ratio		0.63	ı	0.40	ı

Shear / Post-Shear						
Rate of Strain (%/hr) 0.50 - 0.50 -						
Avg. Water Content (%)	22.5	-	19.9	1		

Note - A specific gravity of 2.73 was assumed for mass/volume calculations.

	At I	ailure						
Failure Criterion: Peak Principal Stress	Di	Difference, $(\sigma_1'-\sigma_3')_{max}$			Ratio, $(\sigma_1'/\sigma_3')_{max}$			
Axial Strain at Failure (%), $\epsilon_{a,f}$	14.3	-	11.6	-	3.3	-	7.2	-
Minor Effective Stress (psi), σ ₃ ' _f	25.3	-	76.5	-	18.8	-	72.9	-
Principal Stress Difference (psi), (σ ₁ -σ ₃) _f	26.8	-	78.2	-	23.3	-	76.4	-
Pore Water Pressure, Δu _f (psi)	-5.4	1	23.7	-	1.1	-	27.4	-
Major Effective Stress (psi), σ ₁ ' _f	52.1	-	154.7	-	42.1	-	149.3	-
Secant Friction Angle (degrees)	20.2	1	19.8	1	22.5	-	20.1	-
Effective Friction Angle (degrees)		19.6 19.2			•			
Effective Cohesion (psi)		0.5 1.7						

Note: The presented M-C parameters are based on a linear regression in modified stress space, across all assigned effective consolidation stresses. This fit does not purported to capture typical curvature of envelopes that may, in particular, be observed across broader range in effective stresses. Please note that the stresses associated with peak principal stress ratio and peak principal stress difference are presented in tabular form on the first page of the report. There are alternate interpretations to theses two failure criterion including but not limited to strain compatibility and post-peak.

Jeffrey A. Kuhn, Ph.D., P.E., 1/2/2019

Analysis & Quality Review/Date

1 of 6

Client: Langerman Foster Engineering TRI Log #: 43240.4

Project: Site 50 Part 2 Test Method: ASTM D4767

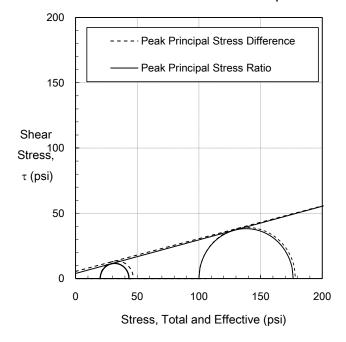
Sample: B-44 (50-51.5)

R / "Total Stress" Envelope					
Failure Criterion: Peak Principal Stress		Difference, $(\sigma_1'-\sigma_3')_{max}$	Ratio, $(\sigma_1'/\sigma_3')_{max}$		
Friction Angle (deg)	φ _R	14.1	14.4		
Cohesion (psi)	c_R	5.4	3.9		

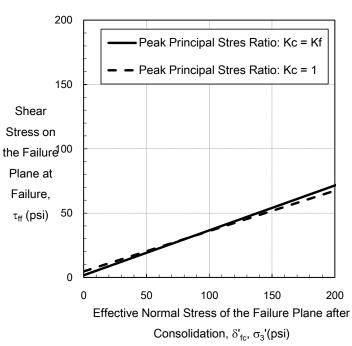
Kc = Kf Envelope, Effective Stress Envelope (Duncan et al. 1990)					
Failure Criterion: Peak Principal Stress		Difference, $(\sigma_1'-\sigma_3')_{max}$	Ratio, $(\sigma_1'/\sigma_3')_{max}$		
Effective Friction Angle (deg)	φ'	19.6	19.2		
Effective Cohesion (psi)	c'	0.5	1.7		

Kc = 1 ($\tau_{\rm ff}$ vs $\sigma'_{\rm fc}$) Enelope, Total Stress Envelope (Duncan et al. 1990)					
Failure Criterion: Peak Principal Stress		Difference, $(\sigma_1'-\sigma_3')_{max}$	Ratio, $(\sigma_1'/\sigma_3')_{max}$		
Friction Angle (deg)	d _{Kc=1}	16.9	17.4		
Cohesion (psi)	Ψ _{Kc=1}	6.6	4.7		

R / "Total Stress" Envelope



Three-Stage Rapid Drawdown Envelopes



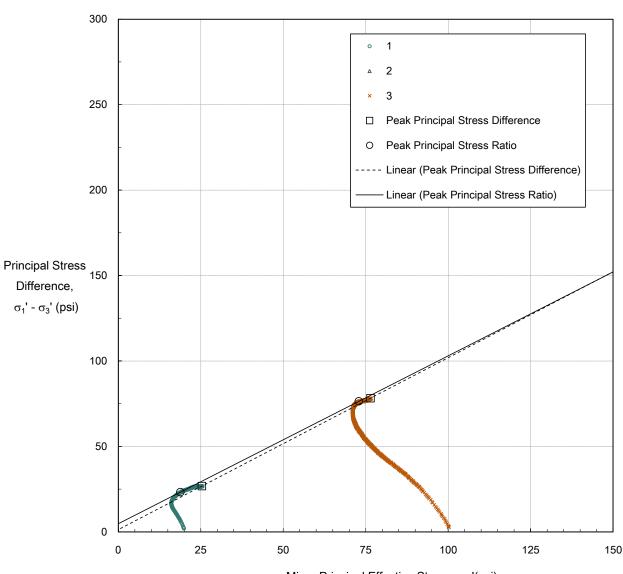
2 of 6

Client: Langerman Foster Engineering

TRI Log #: 43240.4

Project: Site 50 Part 2 Sample: B-44 (50-51.5) Test Method: ASTM D4767

Modified Mohr-Coulomb



Minor Principal Effective Stress , σ_3 '(psi)

Failure Criterion: Peak Principal Stress	Difference, $(\sigma_1'-\sigma_3')_{max}$	Ratio, $(\sigma_1'/\sigma_3')_{max}$
Effective Friction Angle (deg)	19.6	19.2
Effective Cohesion (psi)	of 6 0.5	1.7

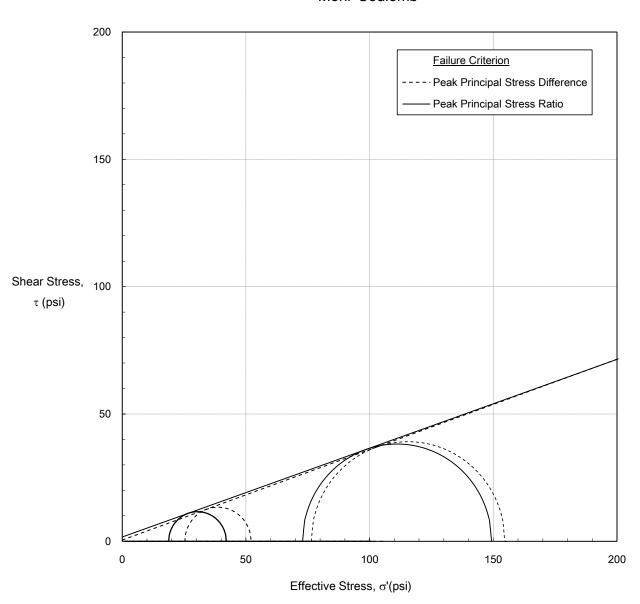
Client: Langerman Foster Engineering

TRI Log #: 43240.4

Test Method: ASTM D4767

Project: Site 50 Part 2 Sample: B-44 (50-51.5)

Mohr-Coulomb



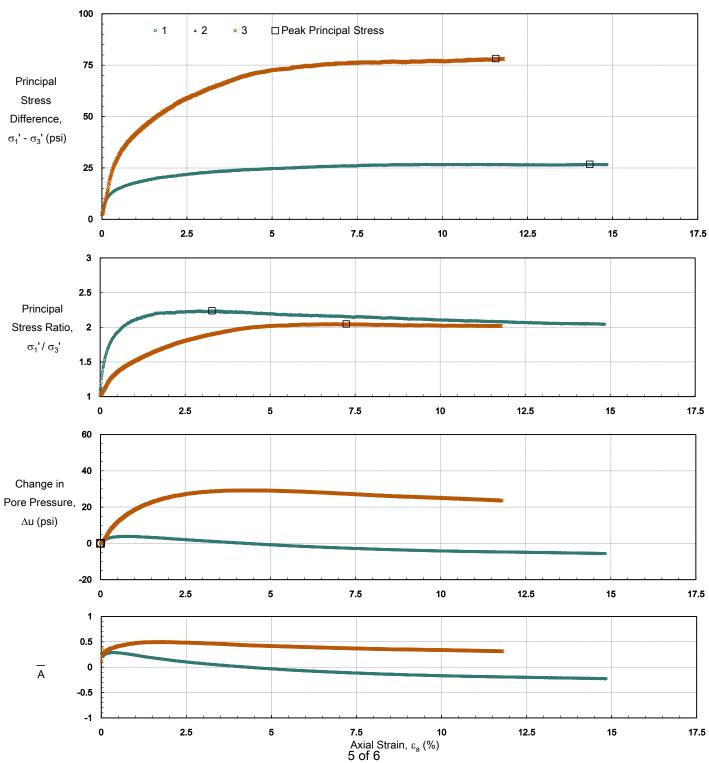
Failure Criterion: Peak Principal Stress	Difference, $(\sigma_1'-\sigma_3')_{max}$	Ratio, $(\sigma_1'/\sigma_3')_{max}$
Effective Friction Angle (deg)	19.6	19.2
Effective Cohesion (psi)	of 6 0.5	1.7

Client: Langerman Foster Engineering

Revision 0

TRI Log #: 43240.4 Project: Site 50 Part 2 Test Method: ASTM D4767

Sample: B-44 (50-51.5)



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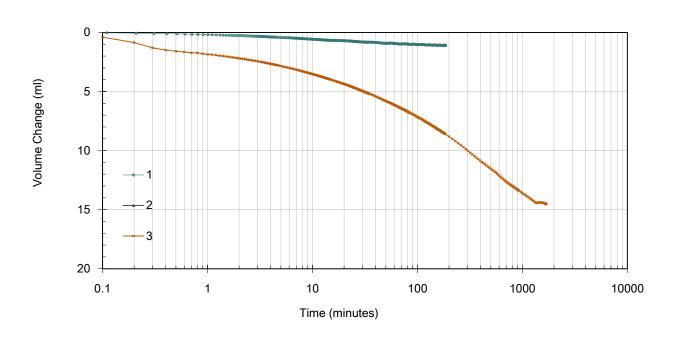
May 2020

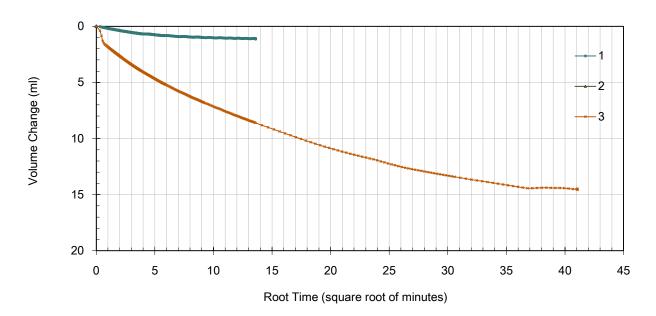
Client: Langerman Foster Engineering

TRI Log #: 43240.4 Project: Site 50 Part 2 Test Method: ASTM D4767

Sample: B-44 (50-51.5)

Consolidation





6 of 6

AUSTIN, TX - USA | ANAHEIM, CA - USA | ANDERSON, SC - USA | GOLD COAST - AUSTRALIA | SUZHOU - CHINA

Consolidated-Undrained Triaxial Compression

Client: Langerman Foster Engineering

Project: Site 50 Part 2

Sample: B-19(50-51)

Total Back-Pressure (psi)

B-Value, End of Saturation

	Specimens				
Identification	1	2	3	4	Specimen
Depth/Elev. (ft)	-	-	-	-	Specimen
Eff. Consol. Stress (psi)	20.0	-	100.0	-	Specimen
Initial Sp	ecimen Pro	operties	•	•	Specimen
Avg. Diameter (in)	1.47	-	1.53	-	Mounting N
Avg. Height (in)	3.31	-	3.27	-	Consolidat
Avg. Water Content (%)	14.3	-	15.3	-	
Bulk Density (pcf)	131.1	-	125.0	-	
Dry Density (pcf)	114.7	-	108.5	-	Void Ratio
Saturation (%)	80.6	-	73.0	-	
Void Ratio, n	0.49	_	0.57	_	

80.5

0.98

Test Setup				
Specimen Condition	Undisturbed / Intact			
Specimen Preparation	Trimmed			
Mounting Method	Wet			
Consolidation	Isotropic			

TRI Log #:

44112.1

Test Method: ASTM D4767

Post-Consolidation / Pre-Shear						
Void Ratio	0.49	ı	0.57	ı		

Shear / Post-Shear				
Rate of Strain (%/hr)	1.00	-	1.00	1
Avg. Water Content (%)	20.7	1	18.4	-

0.98 Note - A specific gravity of 2.73 was assumed for mass/volume calculations.

79.5

	At F	ailure						
Failure Criterion: Peak Principal Stress	Di	fference	, (σ ₁ '-σ ₃ ') _m	nax		Ratio, (σ ₁ '/σ ₃ ') _{max}	
Axial Strain at Failure (%), $\epsilon_{a,f}$	12.8	-	5.0	-	3.7	-	3.4	-
Minor Effective Stress (psi), σ ₃ ' _f	16.9	-	59.7	-	10.3	-	54.7	-
Principal Stress Difference (psi), (σ ₁ -σ ₃) _f	45.9	-	104.6	-	37.3	-	101.8	-
Pore Water Pressure, Δu_f (psi)	3.4	-	40.4	-	9.8	-	45.3	-
Major Effective Stress (psi), σ ₁ ' _f	62.8	-	164.3	-	47.6	-	156.5	-
Secant Friction Angle (degrees)	35.2	-	27.8	-	40.0	-	28.8	-
Effective Friction Angle (degrees)		24.0		24.9				
Effective Cohesion (psi)		7	.4	•		7	'.1	

Note: The presented M-C parameters are based on a linear regression in modified stress space, across all assigned effective consolidation stresses. This fit does not purported to capture typical curvature of envelopes that may, in particular, be observed across broader range in effective stresses. Please note that the stresses associated with peak principal stress ratio and peak principal stress difference are presented in tabular form on the first page of the report. There are alternate interpretations to theses two failure criterion including but not limited to strain compatibility and post-peak.

Jeffrey A. Kuhn, Ph.D., P.E., 2/1/2019

Analysis & Quality Review/Date

1 of 6

Client: Langerman Foster Engineering TRI Log #: 44112.1

Project: Site 50 Part 2 Test Method: ASTM D4767

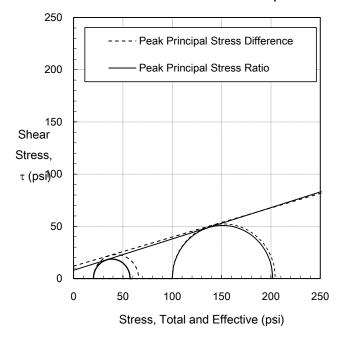
Sample: B-19(50-51)

R / "Total Stress" Envelope					
Failure Criterion: Peak Principal Stress Difference, $(\sigma_1' - \sigma_3')_{max}$ Ratio, $(\sigma_1' / \sigma_3')_{max}$					
Friction Angle (deg)	φ _R	15.6	16.7		
Cohesion (psi)	c_R	11.9	7.9		

Kc = Kf Envelope, Effective Stress Envelope (Duncan et al. 1990)					
Failure Criterion: Peak Principal Stres	Ratio, $(\sigma_1'/\sigma_3')_{max}$				
Effective Friction Angle (deg)	φ'	24.0	24.9		
Effective Cohesion (psi) c' 7.4 7.1					

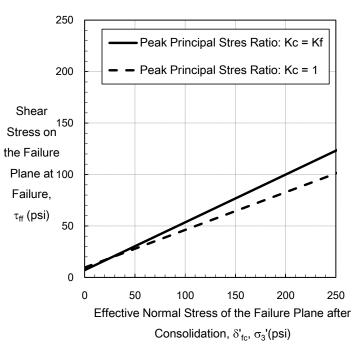
Kc = 1 ($\tau_{\rm ff}$ vs $\sigma'_{\rm fc}$) Enelope, Total Stress Envelope (Duncan et al. 1990)					
Failure Criterion: Peak Principal Stress Difference, $(\sigma_1' - \sigma_3')_{max}$ Ratio, $(\sigma_1'/\sigma_3')_{max}$					
Friction Angle (deg)	d _{Kc=1}	18.5	20.1		
Cohesion (psi) $\psi_{Kc=1}$ 14.3 9.6					

R / "Total Stress" Envelope



Revision 0

Three-Stage Rapid Drawdown Envelopes



May 2020

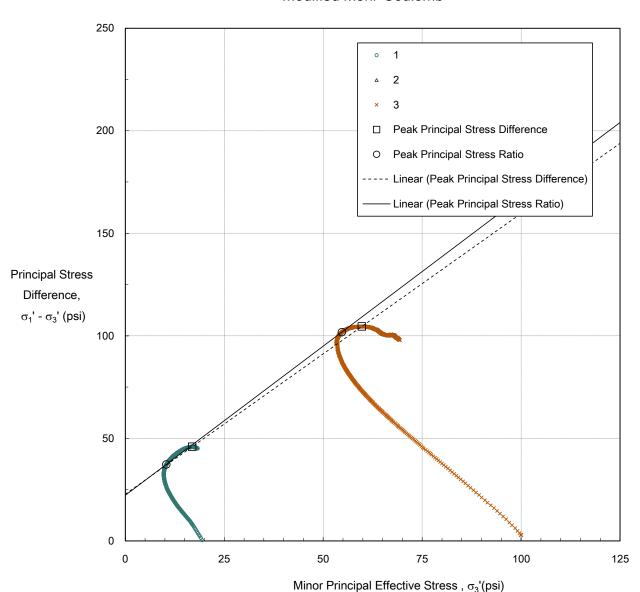
2 of 6

Client: Langerman Foster Engineering

TRI Log #: 44112.1 Project: Site 50 Part 2 Test Method: ASTM D4767

Sample: B-19(50-51)

Modified Mohr-Coulomb



Failure Criterion: Peak Principal Stress	Difference, $(\sigma_1'-\sigma_3')_{max}$	Ratio, $(\sigma_1'/\sigma_3')_{max}$
Effective Friction Angle (deg)	24.0	24.9
Effective Cohesion (psi)	of 6 7.4	7.1

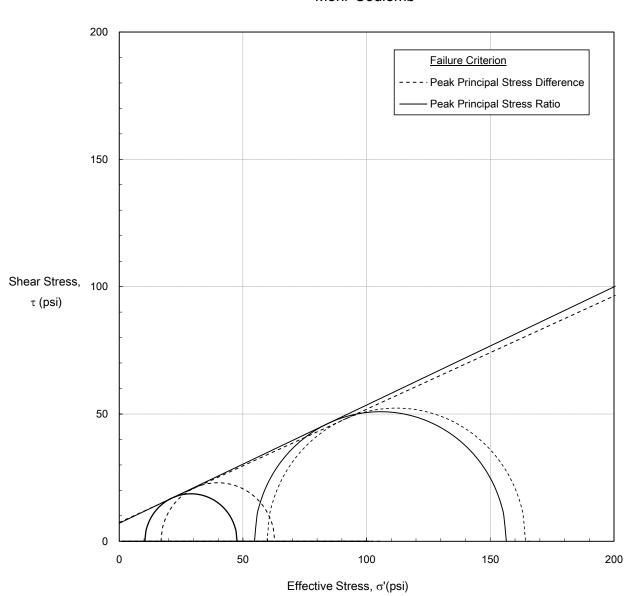
Client: Langerman Foster Engineering

TRI Log #: 44

44112.1

Project: Site 50 Part 2 Sample: B-19(50-51) Test Method: ASTM D4767

Mohr-Coulomb



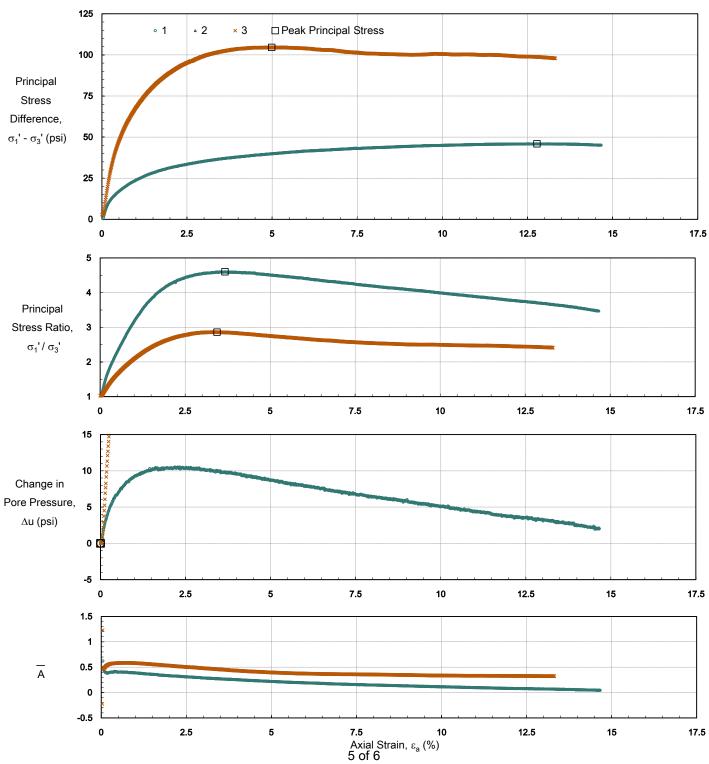
Failure Criterion: Peak Principal Stress	Difference, $(\sigma_1'-\sigma_3')_{max}$	Ratio, $(\sigma_1'/\sigma_3')_{max}$
Effective Friction Angle (deg)	24.0	24.9
Effective Cohesion (psi)	of 6 7.4	7.1

Client: Langerman Foster Engineering

Revision 0

TRI Log #: 44112.1 Project: Site 50 Part 2 Test Method: ASTM D4767

Sample: B-19(50-51)



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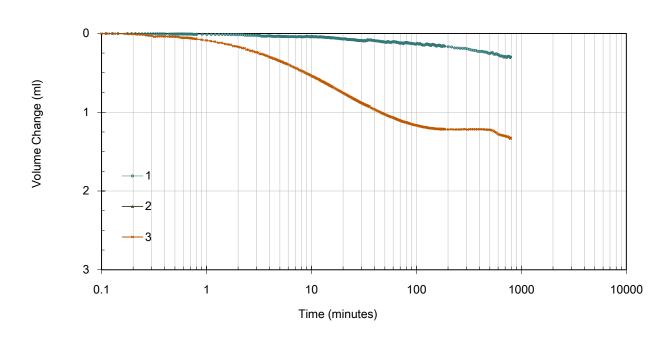
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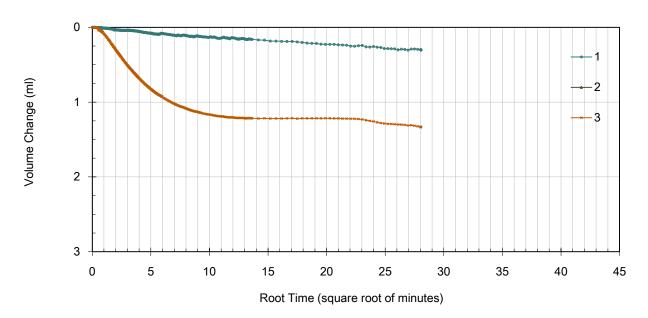
Client: Langerman Foster Engineering

TRI Log #: 44112.1 Project: Site 50 Part 2 Test Method: ASTM D4767

Sample: B-19(50-51)

Consolidation





6 of 6

AUSTIN, TX - USA | ANAHEIM, CA - USA | ANDERSON, SC - USA | GOLD COAST - AUSTRALIA | SUZHOU - CHINA

Client: Langerman Foster Engineering

Project: Site 50 Part 2

Jeffrey A. Kuhn, Ph.D., P.E., 1/2/2019

TRI Log #:

Quality Review/Date

43240

COC Line #	Sample Identification	Atterberg Limits			
		Liquid Limit	Plastic Limit	Plasticity Index	
-	Test Method	ASTM D4318, Method A: Multipoint			
1	B-24 (45-46)	59	26	33	
2	B-17 (25-26)	67	23	44	
3	B-31 (15-15.9)	66	27	39	
4	B-44 (50-51.5)	60	25	35	

Note: NL = No Liquid Limit; NP = No Plastic Limit

AUSTIN, TX - USA | ANAHEIM, CA - USA | ANDERSON, SC - USA | GOLD COAST - AUSTRALIA | SUZHOU - CHINA

Client: Langerman Foster Engineering TRI Log #: 44112

Project: Site 50 Part 2

Jeffrey A. Kuhn, Ph.D., P.E., 2/1/2019

Quality Review/Date

COC Line #	Sample Identification	Fines (%)	Moisture Content (%)	Atterberg Limits		
				Liquid Limit	Plastic Limit	Plasticity Index
-	Test Method	ASTM D1140	ASTM D2216	ASTM D4318, Method A : Multipoint		
1	B-19(50-51)	85.2	13.3	60	21	39

Note: NL = No Liquid Limit; NP = No Plastic Limit

APPENDIX III-4.G

VIBRATING WIRE PIEZOMETER MANUAL AND CALIBRATION FORMS



GEOKON_®

48 Spencer Street
Lebanon, NH 03766, USA
Tel: 603·448·1562
Fax: 603·448·3216
Email: geokon@geokon.com
http://www.geokon.com

Instruction Manual

Model 4500 series

Vibrating Wire Piezometer



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TABLE of CONTENTS

1. THEORY OF OPERATION	t
2. QUICK START INSTRUCTIONS	2
3. PRIOR TO INSTALLATION	3
3.1 SATURATING FILTER TIPS 3.1.1 Saturating Low Air Entry (Standard) Filters 3.1.2 Saturating High Air Entry Ceramic Filters 3.1.3 Saturating Model 4500C Filter Tips 3.2 ESTABLISHING AN INITIAL ZERO READING 3.2.1 Recommended Method for Establishing an Initial Zero Reading 3.2.2 Alternative Method One 3.2.3 Alternative Method Two 3.2.4 Alternative Method Three 3.3 CHECKING THE PIEZOMETER PERFORMANCE	
4. INSTALLATION	
4.1 Installation in Standpipes or Wells 4.2 Installation in Boreholes. 4.3 Installation in Fills and Embankments 4.4 Installation by Pushing or Driving into Soft Soils 4.5 Model 4500H and Model 4500HH Transducer 4.6 Splicing and Junction Boxes 4.7 Lightning Protection 4.8 Freezing Protection	
5. TAKING READINGS	18
5.1 GK-404 READOUT BOX. 5.1.1 Operating the GK-404. 5.2 GK-405 READOUT BOX. 5.2.1 Connecting Sensors with a 10-pin Bulkhead. 5.2.2 Connecting Sensors with Bare Leads. 5.2.3 Operating the GK-405. 5.3 GK-403 READOUT BOX (OBSOLETE MODEL). 5.3.1 Connecting Sensors with a 10-pin Bulkhead. 5.3.2 Connecting Sensors with Bare Leads. 5.3.3 Operating the GK-403. 5.4 MEASURING TEMPERATURES.	
6. DATA REDUCTION	21
6.1 PRESSURE CALCULATION	22 23 24
7. TROUBLESHOOTING	26
APPENDIX A. SPECIFICATIONS	28
A.1 4500 SERIES SPECIFICATIONS	28
APPENDIX B. THERMISTOR TEMPERATURE DERIVATION	29
APPENDIX C. HIGH TEMPERATURE THERMISTOR LINEARIZATIONERROR DEFINED. APPENDIX D. IMPROVING THE ACCURACY OF THE CALCULATED PRESSURE.	

APPENDIX E. TYPICAL CALIBRATION REPORT	32
APPENDIX F. MODEL 4500AR PIEZOMETER	
APPENDIX G. PIEZOMETER PRESSURE AND WATER LEVEL	34
FIGURES	
FIGURES	
FIGURE 1 - MODEL 4500S VIBRATING WIRE PIEZOMETER	1
FIGURE 2 - 4500C SATURATION	
FIGURE 3 - TYPICAL LEVEL MONITORING INSTALLATION	
FIGURE 4 - TYPICAL BOREHOLE INSTALLATIONS	11
FIGURE 5 - HIGH AIR ENTRY FILTER	13
FIGURE 6 - LOW AIR ENTRY FILTERS ONLY	13
FIGURE 7 - TYPICAL SOFT SOILS INSTALLATION	
FIGURE 8 - TYPICAL MULTI-PIEZOMETER INSTALLATION	16
FIGURE 9 - RECOMMENDED LIGHTNING PROTECTION SCHEME	
FIGURE 10 - LEMO CONNECTOR TO GK-404	18
FIGURE 11 - LIVE READINGS - RAW READINGS	19
FIGURE 12 - VENTED PIEZOMETERS	24
FIGURE 13 - TYPICAL CALIBRATION REPORT	
FIGURE 14 - 4500AR PIEZOMETER	33
TABLES	
TABLE 1 - CEMENT/BENTONITE/WATER RATIOS	12
TABLE 2 - ENGINEERING UNITS MULTIPLICATION FACTORS	22
TABLE 3 - SAMPLE RESISTANCE	
TABLE 4 - RESISTANCE WORK SHEET.	
TABLE 5 - VIBRATING WIRE PIEZOMETER SPECIFICATIONS	
TABLE 6 - STANDARD PIEZOMETER WIRING	
TABLE 7 - THERMISTOR RESISTANCE VERSUS TEMPERATURE	
TABLE 8 - THERMISTOR RESISTANCE VERSUS TEMPERATURE FOR HIGH TEMPERATURE MODELS I	
NOT DEFINED. TABLE 9 - 4500AR WIRING CHART	33
EQUATIONS	
EQUATION 1 - DIGITS CALCULATION	21
EQUATION 2 - CONVERT DIGITS TO PRESSURE	21
EQUATION 3 - TEMPERATURE CORRECTION	22
EQUATION 4 - BAROMETRIC CORRECTION	23
EQUATION 5 - CORRECTED PRESSURE CALCULATION	24
EOUATION 6 - RESISTANCE TO TEMPERATURE	29
EQUATION 7 - HIGH TEMPERATURE RESISTANCE TO TEMPERATUREERROR! BOOK	MARK NOT DEFINED.
EQUATION 8 - SECOND ORDER POLYNOMIAL EXPRESSION	31
EQUATION 9 - LINEARITY CALCULATION	31
The state of the s	

1. THEORY OF OPERATION

Geokon model 4500 Vibrating Wire Piezometers are intended primarily for long-term measurements of fluid depths and pore pressures in standpipes, boreholes, embankments, pipelines, and pressure vessels. Several different models are available to suit a variety of Geotechnical applications. Calibration data is supplied with each piezometer.

All Geokon vibrating wire piezometers utilize a sensitive stainless steel diaphragm (with the exception of model 4500C, which employs bellows) to which a vibrating wire element is connected. During use, changing pressures on the diaphragm cause it to deflect. This deflection is measured as a change in tension and frequency of vibration of the vibrating wire element. The square of the vibration frequency is directly proportional to the pressure applied to the diaphragm. A filter is used to keep out solid particles and prevent damage to the sensitive diaphragm. Standard filters are 50-micron stainless steel. High air entry value filters are available upon request.

Two coils, one with a magnet insert, the other with a pole piece insert, are installed near the vibrating wire. In use, a pulse of varying frequency (swept frequency) is applied to these coils, causing the wire to vibrate primarily at its resonant frequency. When the excitation ends, the wire continues to vibrate. During vibration, a sinusoidal signal is induced in the coils and transmitted to the readout box where it is conditioned and displayed.

Portable readout units are available to provide the excitation, signal conditioning, and readout of the instrument. Datalogger systems, which allow remote, unattended data collection of multiple sensors, are also available. Contact Geokon for additional information.

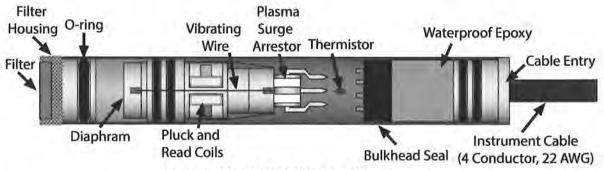


Figure 1 - Model 4500S Vibrating Wire Piezometer

All exposed components are made of corrosion resistant stainless steel. If proper installation techniques are used, the device should have an unlimited life.

In salt water, it may be necessary to use special materials for the diaphragm and housing. The 4500TI series piezometers are constructed from titanium and are specifically designed to be used in this type of environment.

2. QUICK START INSTRUCTIONS

For those familiar with Geotechnical instrumentation and its installation, the following quick start instructions may be used. For more detailed instructions see Section 3.

- Prior to installation, allow the piezometer to come to thermal equilibrium for a minimum of 15 minutes. (Alternatively, if the instrument is attached to a readout box, wait until the piezometer reading has stabilized.)
- Record the piezometer reading, barometric pressure, and temperature while the piezometer is experiencing zero (atmospheric) pressure. This is what is known as the "initial zero" reading.
- Verify that the initial zero reading for the piezometer is compatible with the factory supplied zero reading on the calibration report.
- 4) Carefully measure and mark the cable where it will lie at the top of the borehole, well, or standpipe, once the piezometer has reached the desired depth. (The piezo diaphragm lies 3/4 of an inch above the tip of the piezometer.)
- 5) Saturate the piezometer filter. (See Section 3.1) Warning! Do not allow the piezometer to freeze once the filter stone has been saturated!
- 6) For installation in standpipes or wells, see Section 4.1, for boreholes Section 4.2, and for fills and embankments Section 4.3.

3. PRIOR TO INSTALLATION

3.1 Saturating Filter Tips

Warning! Do not allow the piezometer to freeze once the filter stone has been saturated! See Section 4.8 for information about protecting the piezometer from freezing.

Most filter tips can be removed for saturation and then reassembled. To maintain saturation, the unit should be kept underwater until installation. If the piezometer is used in a standpipe where it will be raised and lowered frequently, the filter housing may loosen over time, and a permanent filter assembly may be required. The removable filter may be fixed permanently by prick punching the piezometer tube approximately 1/16" to 1/8" behind the filter assembly joint.

Salts in the water can be deposited into the filter stone causing it to become clogged if it is allowed to dry out completely. Filter stones may be replaced with screens for standpipe installations. Screens available from Geokon are less likely than standard filters to collect salt and become clogged.

3.1.1 Saturating Low Air Entry (Standard) Filters

For accurate results, total saturation of the filter is necessary. As the piezometer is lowered into the water, water is forced into the filter, compressing the air in the space between the filter stone and the pressure sensitive diaphragm. After a period, this air will dissolve into the water, filling the filter and the space above it entirely with water.

To speed up the saturation process, remove the filter from the piezometer by carefully twisting and pulling on the filter housing assembly (or unscrewing the point of the piezometer for model 4500DP). Hold the piezometer with the filter facing up and fill the space above the diaphragm with water. Slowly replace the filter housing, allowing the water to squeeze through the filter stone as it is installed. For piezometers with a range of less than 10 psi, take readings with a readout box while reinstalling the filter housing to ensure the piezometer is not overranged.

3.1.2 Saturating High Air Entry Ceramic Filters

Because of the high air entry characteristics of the ceramic filter, de-airing is particularly important. Different air entry values require different saturation procedures.

3.1.2.1 One Bar Filters

- Remove the filter from the piezometer by carefully twisting and pulling on the filter housing assembly.
- Boil the filter assembly in de-aired water.
- 3) Reassemble the piezometer under the surface of a container of de-aired water. Use a readout box while installing the filter to monitor the diaphragm pressure. If the piezometer begins to overrange, allow the pressure to dissipate before pushing further.
- 4) Be sure that no air is trapped in the transducer cavity.

3.1.2.2 Two Bar and Higher Filters

The proper procedure for de-airing and saturating these filters is somewhat complex; therefore, it is recommended that saturation be done at the factory by Geokon. If saturation must be done in the field, carefully follow the instructions below:

- Place the assembled piezometer, filter down, in a vacuum chamber that has an inlet port at the bottom for de-aired water.
- Close off the water inlet and evacuate the chamber. The transducer should be monitored while the chamber is being evacuated.
- When maximum vacuum has been achieved, allow de-aired water to enter the chamber until it reaches an elevation a few inches above the piezometer filter.
- 4) Close off the inlet port.
- 5) Release the vacuum.
- 6) Observe the transducer output. It may take up to 24 hours for the filter to completely saturate and the pressure to rise to zero.
- 7) After saturation, the transducer should be kept in a container of de-aired water until installation. If de-aired at the factory a special cap is applied to the piezometer to maintain saturation.

3.1.3 Saturating Model 4500C Filter Tipe

WARNING! The filter housing is not removable on the 4500C. Any attempt to remove the filter stone or the housing will destroy the transducer!

If the pressure to be measured is less than 5 psi the filter stone must be saturated. A hand operated vacuum pump and short length of half inch surgical tubing is required. Hand pumps and tubing are available from the factory. (A hand pump that has been used successfully is the MityvacII® by Lincoln Industries Corp. of St. Louis, MO.)

The saturation procedure is as follows:

- 1) Attach the tube to the transducer as shown in Figure 2.
- 2) Fill the tubing with approximately two inches (five centimeters) of water.
- Attach the other end of the tube to the hand vacuum pump.

4) While holding the transducer so that the water rests on the filter, but does not enter the pump, squeeze the hand pump to initiate a vacuum inside the tubing. This will draw the air out of the filter and the area behind it, replacing it with water. A vacuum of 20 to 25" Hg. (50 to 65 cm Hg.) is enough for proper air evacuation.

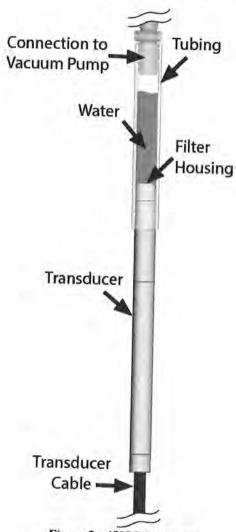


Figure 2 - 4500C Saturation

3.2 Establishing an Initial Zero Reading

Vibrating Wire Piezometers differ from other types of pressure sensors in that they indicate a reading when no pressure is exerted on the sensor. It is imperative that an accurate initial zero reading be obtained for each piezometer, as this reading will be used for all subsequent data reduction.

Generally, the initial zero reading is obtained by reading the instrument prior to installation. There are several different ways of taking an initial zero reading. The essential element in all methods is that the piezometer needs to thermally stabilize in a constant temperature environment while the pressure on the piezometer is barometric only. Because of the way the piezometer is constructed, it usually takes 15 to 20 minutes for the temperature of all the different elements to equalize.

A question may arise as to what to do with the filter stone while taking zero readings. If a standard stainless steel filter is being used, it will not matter if the filter stone is saturated or not. However, if the piezometer is equipped with a ceramic high air entry filter stone, then it must be saturated while taking the zero readings.

It will be necessary to measure the barometric pressure only if the piezometer is unvented and it will be installed in a location that is subject to barometric pressure changes that would require correction, such as in an open well. A piezometer sealed in place at depth could be recording pressures in groundwater that is not hydraulically connected to the atmosphere, for which barometric pressure compensation would be inappropriate. See Section 6.3 for more information on Barometric corrections.

Calibration data is supplied with each gauge, a factory zero reading taken at a specific temperature and absolute barometric pressure is included. (See Appendix E for a sample calibration report.) Zero readings at the site should coincide with the factory readings within 50 digits, after barometric and temperature corrections are made. Barometric pressures change with elevation at a rate of approximately 3.45 kPa (½ psi) per 300 meters (1,000 ft.). The factory elevation is +580 feet. All stated barometric readings represent absolute pressure uncorrected for height above sea level. A thermistor is included inside the body of the piezometer for the measurement of temperature.

NOTE REGARDING THE 4500C: The construction of this very slender vibrating wire transducer requires a miniaturization of the internal parts, which consequently are somewhat delicate. Handle the transducer with care during the installation procedure. Despite taking every precaution to ensure that the transducer arrives unharmed, it is possible for the zero to shift during shipment due to rough handling. However, tests have shown that though the zero may shift, the calibration factors do not change. Therefore, it is doubly important that an initial no load zero reading be taken prior to installation.

3.2.1 Recommended Method for Establishing an Initial Zero Reading

- Saturate the filter stone per Section 3.1. Warning! Do not allow the piezometer to freeze once the filter stone has been saturated!
- Replace the filter stone.
- 3) Hang the piezometer in the borehole at a point just above the water.
- 4) Wait until the piezometer reading has stopped changing.
- 5) Take the zero and temperature readings.

3.2.2 Alternative Method One

- 1) Place the piezometer under water in a bucket.
- 2) Allow 15 to 20 minutes for the temperature of the unit to stabilize.
- Use the instrument cable to lift the piezometer out of the water. Do not handle the piezometer housing; body heat from the hands could cause temperature transients.
- 4) Immediately take a zero and temperature reading.

3.2.3 Alternative Method Two

- 1) Allow 15 to 20 minutes for the temperature of the unit to stabilize.
- Lift the piezometer into the air by the cable only. Do not handle the piezometer housing; body heat from the hand could cause temperature transients.
- 3) Take a zero and temperature reading. (If this method is chosen, be sure that the piezometer is protected from sunlight or sudden changes of temperature. Wrapping it in some insulating material is recommended.)

3.2.4 Alternative Method Three

- 1) Lower the piezometer to a known depth marked on the piezometer cable. (The diaphragm inside the piezometer is located approximately 3/4" (15 mm) from the tip.)
- 2) Use a dip meter to accurately measure the depth to the water surface.
- After temperature stabilization, read the piezometer pressure.
- 4) Using the factory calibration constants and a knowledge of the pressure of the water column above the piezometer (height times density), calculate the equivalent zero pressure reading if linear regression is used, or the factor C if the second order polynomial is used.

3.3 Checking the Piezometer Performance

If a rough check of the piezometer performance is needed, the following procedure is recommended:

- 1) Lower the piezometer to a point near the bottom of a water-filled borehole, or below the surface of a body of water.
- 2) Allow 15 to 20 minutes for the piezometer to come to thermal equilibrium.
- 3) Using a readout box, record the reading at the current depth.
- 4) Raise the piezometer by a measured increment.
- 5) Record the reading on the readout box at the new depth.
- 6) Using the factory calibration factor, calculate the change in water depth.
- Compare the calculated change in depth with the measured depth increment. The two values should be roughly the same.

Alternative method using a dip meter:

- 1) Lower the piezometer tip to a measured depth below the water surface.
- 2) Allow 15 to 20 minutes for the piezometer to come to thermal equilibrium.
- 3) Using a readout box, record the reading at that level.
- 4) Calculate the elevation of the water surface using the given calibration factor.
- 5) Compare the calculated elevation to the elevation measured using the dip meter.

A couple of things that can affect this checking procedure:

- If the density of the water is not one gram/cubic centimeter.
- If the water is saline or turbid.
- The water level inside the borehole may vary during the test. This is due to the displacement of water caused by the cable as it is raised and lowered in the borehole. The smaller the borehole is, the greater the displacement will be. For example, a Model 4500S-50KPA piezometer lowered 50 feet below the water column in a one-inch (0.875-inch ID) standpipe will displace the water level by more than four feet.

4. INSTALLATION

4.1 Installation in Standpipes or Wells

- 1) Saturate the filter stone and establish an initial zero reading by following the steps outlined in Section 3.1 and Section 3.2. (Warning! Do not allow the piezometer to freeze once the filter stone has been saturated!)
- 2) Mark the cable where the top of the well or standpipe will reside once the piezometer has reached the desired depth. (The piezometer diaphragm is located 3/4 of an inch above the tip of the piezometer.)
- 3) Lower the piezometer into the standpipe/well.
- 4) Be sure the cable is securely fastened to prevent the piezometer from sliding further into the well and causing an error in the readings.

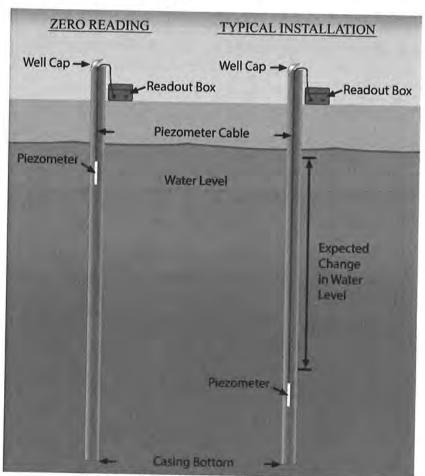


Figure 3 - Typical Level Monitoring Installation

It is not recommended that piezometers be installed in wells or standpipes where an electrical pump or cable is nearby. Electrical interference from these sources can cause unstable readings. If unavoidable, it is recommended that the piezometer be placed inside a piece of steel pipe. In situations where packers are used in standpipes, special care should be taken to avoid cutting the cable jacket with the packer, as this could introduce a possible pressure leak in the cable.

4.2 Installation in Boreholes

Geokon piezometers can be installed in cased or uncased boreholes, in either single or multiple piezometer configurations. If pore pressures in a particular zone are to be monitored, careful attention must be paid to the borehole sealing technique.

The borehole should extend 6 to 12 inches below the proposed piezometer location. Boreholes should be drilled without using drilling mud, or by using a material that degrades rapidly with time, such as Revert™. Wash the borehole clean of drill cuttings. Backfill the borehole with clean fine sand to a point six inches below the desired piezometer tip location. The piezometer can then be lowered into position. (Preferably, the piezometer will be encapsulated in a canvas bag containing clean, saturated sand.) While holding the instrument in position, (a mark on the cable is helpful) fill the borehole with clean fine sand to a point six inches above the piezometer.

Three different methods of isolating the zone to be monitored are detailed below.

Installation A:

Immediately above the area filled with clean fine sand, known as the "collection zone", the borehole should be sealed by an impermeable bentonite cement grout mix, or with alternating layers of bentonite and sand backfill, tamped in place for approximately one foot, followed by common backfill. (See Figure 4.)

If multiple piezometers are to be used in a single hole, the bentonite and sand should be tamped in place below and above the upper piezometers, as well as at interval between the piezometer zones. When using tamping tools special care should be taken to ensure that the piezometer cable jackets are not cut during installation, as this could introduce a possible pressure leak in the cable.

Installation B:

The borehole is filled from the "collection zone" upwards with an impermeable bentonite grout. (See Figure 4.)

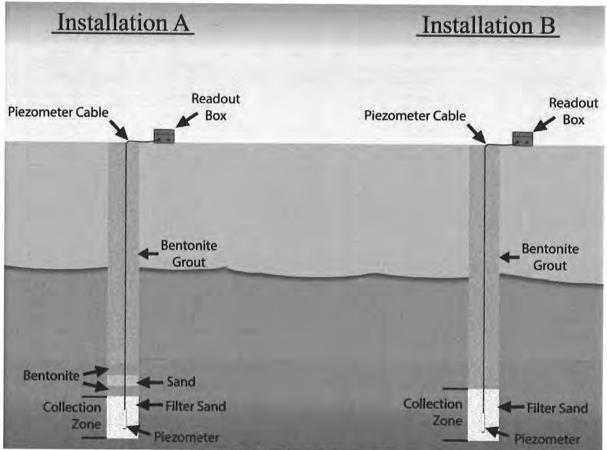


Figure 4 - Typical Borehole Installations

Installation C:

It should be noted that since the vibrating wire piezometer is essentially a no flow instrument, collection zones of appreciable size are not required. The piezometer can be placed directly in contact with most materials, provided that the fines are not able to migrate through the filter. The latest thinking is that it is not necessary to provide sand zones and that the piezometer can be grouted directly into the borehole using a bentonite cement grout only. However, good results have been obtained by placing the piezometer inside a canvas bag filled with sand before grouting.

The general rule for installing piezometers in this way is to use a bentonite grout that mimics the strength of the surrounding soil. The emphasis should be on controlling the water to cement ratio. This is accomplished by *mixing the cement with the water first*. The most effective way of mixing the two substances is to use a drill rig pump to circulate the mix in a 50 to 200-gallon barrel or tub.

Any kind of bentonite powder combined with Type I or Type II Portland cement can be used to make drilling mud. The exact amount of bentonite needed will vary somewhat. Table 1 shows two possible mixes for strengths of 50 psi and 4 psi.

	50 PSI Grout for Medium to Hard Soils		4 PSI Grout for Soft Soils		
	Amount	Ratio by Weight	I	Amount	Ratio by Weight
Water	30 gallons	2.5	75 gallons		6.6
Portland Cement	94 lb. (one sack)	1	94 lb. (one sack)		1
Bentonite	25 lb. (as required)	0.3	39 lb. (as required)		0.4
Note:	is about 50 psi, simila	similar to very stiff to hard mix		The 28-day st mix is ab- similar to ve	out 4 psi,

Table 1 - Cement/Bentonite/Water ratios

Add the measured amount of clean water to the barrel then gradually add the cement in the correct weight ratio. Slowly add the bentonite powder so that clumps do not form. Keep adding bentonite until the watery mix turns to an oily/slimy consistency. Let the grout thicken for 5 to 10 minutes. Add more bentonite as required until it is a smooth, thick cream, similar to pancake batter. It is now as heavy as it is feasible to pump.

When pumping grout (unless the tremie pipe is to be left in place,) withdraw the tremie pipe after each batch, by an amount corresponding to the grout level in the borehole.

CAUTION! If the grout is pumped into the hole, rather than tremie piped, there is a danger that the piezometer will be overranged and damaged. Pumping directly into the bottom of the borehole should be avoided. It is good practice to read the piezometer while pumping.

For more details on grouting, refer to "Piezometers in Fully Grouted Boreholes" by Mikkelson and Green, FMGM proceedings Oslo 2003. Copies are available from Geokon.

4.3 Installation in Fills and Embankments

Geokon piezometers are normally supplied with direct burial cable suitable for placement in fills such as highway embankments and dams, both in the core and in the surrounding materials.

For installations in non-cohesive fill materials, the piezometer may be placed directly in the fill, or, if large aggregate sizes are present, in a saturated sand pocket in the fill. If installed in large aggregate, additional measures may be necessary to protect the cable from damage.

In fills such as impervious dam cores, where subatmospheric pore water pressure may need to be measured, (as opposed to the pore air pressure,) a ceramic tip with a high air entry value is often used. This type of filter should be carefully placed in direct contact with the compacted fill material. (See Figure 5).

Cables are normally installed inside shallow trenches with the fill material consisting of smaller size aggregate. This fill is carefully hand compacted around the cable. Bentonite plugs are placed at regular intervals to prevent migration of water along the cable path. In high traffic areas and in materials that exhibit pronounced "weaving", heavy-duty armored cable should be used.

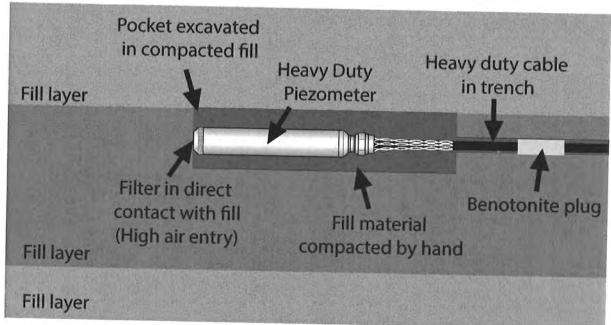


Figure 5 - High Air Entry Filter

In partially saturated fills (if only the pore air pressure is to be measured,) the standard tip is satisfactory. It should be noted that the standard coarse tip (low air entry) measures the air pressure when there is a difference between the pore air pressure and the pore water pressure. The difference between these two pressures is due to the capillary suction in the soil. The consensus is that the difference is normally of no consequence to embankment stability.

The coarse tip filter is suitable for most routine measurements. Both the installation shown in Figure 5 and the installation shown in Figure 6 may be used with the standard piezometer filter.

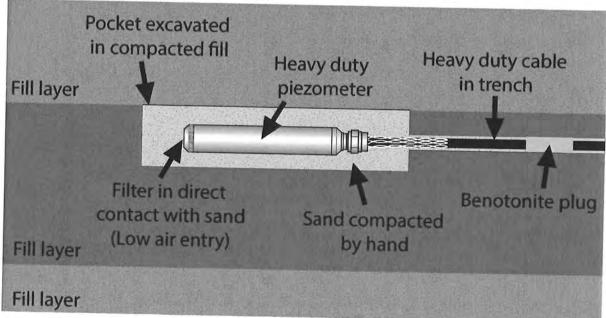


Figure 6 - Low Air Entry Filters ONLY

4.4 Installation by Pushing or Driving into Soft Soils

The Model 4500DP piezometer is designed to be pushed into soft soils. In soft soils, it can be difficult to keep a borehole open. The 4500DP may eliminate the need for a borehole altogether. The unit is connected directly to the drill rod (AW, EW, or other) and pressed into the ground, either by hand or by means of the hydraulics on the rig. (See Figure 7.) The units can also be driven into the soil, but there is a possibility that the driving forces may shift the zero reading.

The ground conditions need to be relatively soft for the 4500DP to be effective. Soft soils (like clays or silts) with SPT blow counts under 10 are ideal. In stiffer soils, it is possible to drill a hole and then push the 4500DP only a few feet below the bottom of the hole, but if the soil is too stiff, the sensor may overrange or break.

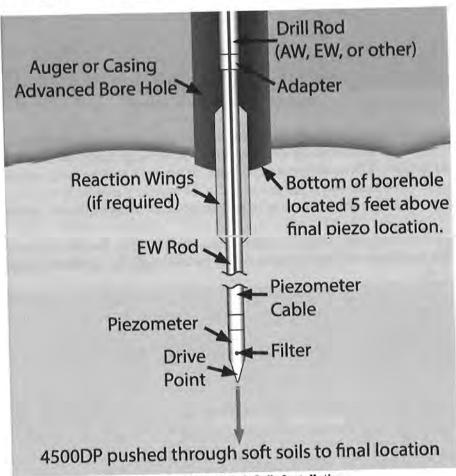


Figure 7 - Typical Soft Soils Installation

The piezometer should be connected to a readout box and monitored during the installation process. If pressures reach or exceed the calibrated range, the installation should be stopped. Allow the pressure to dissipate before continuing.

The drill rod can be left in place or it can be removed. If it is to be removed, a special five-foot section of EW (or AW) rod with reaction wings and a left-hand thread are attached directly to the piezometer tip. This section is detached from the rest of the drill string by rotating the string clockwise. The reaction wings prevent the EW rod from turning. A LH/RH adapter is available from Geokon. This adapter is retrieved along with the drill string.

4.5 Model 4500H and Model 4500HH Transducer

When connecting the Model 4500H transducer to external fittings, the fitting should be tightened into the 1/4-18 NPT female port by placing a wrench on the flats provided on the transducer housing. Avoid tightening onto a closed system; the process of tightening the fittings could overrange and permanently damage the transducer. If in doubt, attach the gauge leads to a readout box and take readings while tightening. For an easier and more positive connection to the transducer, PTFE (plumber's) tape on the threads is recommended. The maximum pressure for the 4500H is 3 MPa.

Geokon's Model 4500HH is designed for high-pressure environments. This model uses a 7/16-20, 60-degree, female, medium pressure fitting. The maximum pressure for the 4500HH is 75 MPa.

CAUTION! All high-pressure sensors are potentially dangerous. Care must be taken not to overrange them beyond their calibrated range. Sensors are tested to 150% of their range to provide a factor of safety.

4.6 Splicing and Junction Boxes

Because the vibrating wire output signal is a frequency rather than a current or voltage, variations in cable resistance have little effect on gauge readings. Therefore, splicing of cables has no effect, and in some cases may in fact be beneficial. For example, if multiple piezometers are installed in a borehole, and the distance from the borehole to the terminal box or datalogger is great, a splice (or junction box) could be made to connect the individual cables to a single multiconductor cable. (See Figure 8.) This multi-conductor cable would then be run to the readout station. For these types of installations, it is recommended that the piezometer be supplied with enough cable to reach the installation depth, plus extra cable to pass through drilling equipment (rods, casing, etc.).

Cable used for making splices should be a high-quality twisted pair type, with 100% shielding and an integral shield drain wire. When splicing, it is very important that the shield drain wires be spliced together. Splice kits recommended by Geokon incorporate casts that are placed around the splice and then filled with epoxy to waterproof the connections. When properly made, this type of splice is equal or superior to the cable in strength and electrical properties. Contact Geokon for splicing materials and additional cable splicing instructions.

Junction boxes and terminal boxes are available from Geokon for all types of applications. In addition, portable readouts and dataloggers are also available. Contact Geokon for specific application information.

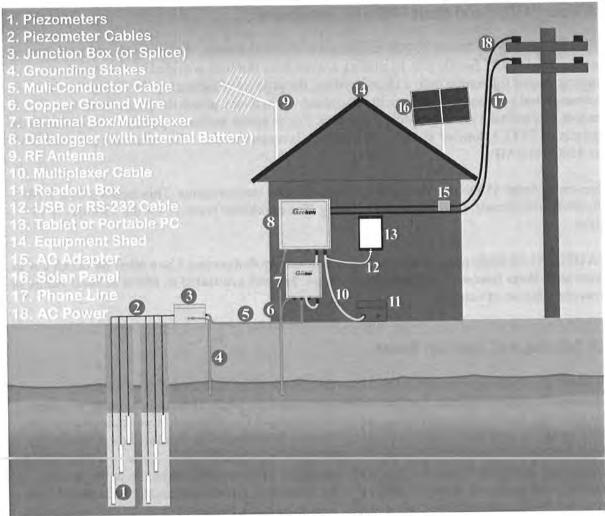


Figure 8 - Typical Multi-Piezometer Installation

4.7 Lightning Protection

In exposed locations, it is vital that the piezometer be protected against lightning strikes. A tripolar plasma surge arrestor, which protects against voltage spikes across the input leads, is built into the body of the piezometer. (See Figure 1.)

Additional lightning protection measures available include:

- Placing a Lightning Arrestor Board (LAB-3), in line with the cable, as close as possible to
 the installed piezometer. (See Figure 9.) These units utilize surge arrestors and transzorbs to
 further protect the piezometer. This is the recommended method of lightning protection.
- Terminal boxes available from Geokon can be ordered with lightning protection built in. The
 terminal board used to make the gauge connections has provision for the installation of
 plasma surge arrestors. Lightning Arrestor Boards (LAB-3) can also be incorporated into the
 terminal box. The terminal box must be connected to an earth ground for these levels of
 protection to be effective.

If the instruments will be read manually with a portable readout (no terminal box), a simple
way to help protect against lightning damage is to connect the cable leads to a good earth
ground when not in use. This will help shunt transients induced in the cable to ground, away
from the instrument.

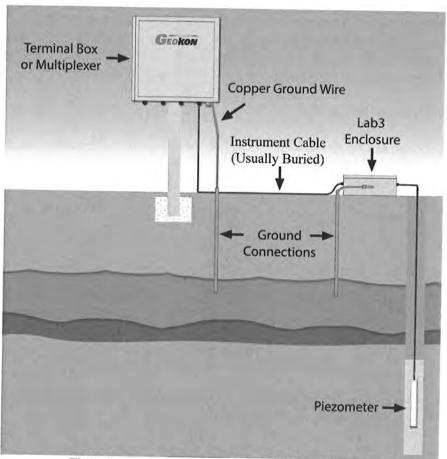


Figure 9 - Recommended Lightning Protection Scheme

4.8 Freezing Protection

If the water around the piezometer freezes this could damage the piezometer diaphragm causing a large shift in the zero pressure reading. If the piezometer is to be used in locations that are subject to freezing, Geokon can provide a special modification that will protect the piezometer diaphragm.

5. TAKING READINGS

5.1 GK-404 Readout Box

The Model GK-404 Vibrating Wire Readout is a portable, low-power, handheld unit that can run continuously for more than 20 hours on two AA batteries. It is designed for the readout of all Geokon vibrating wire gauges and transducers; and is capable of displaying the reading in either digits, frequency (Hz), period (μs), or microstrain (με). The GK-404 also displays the temperature of the transducer (embedded thermistor) with a resolution of 0.1 °C.

5.1.1 Operating the GK-404

Before use, attach the flying leads to the GK-404 by aligning the red circle on the silver Lemo connector of the flying leads with the red line on the top of the GK-404 (Figure 10). Insert the Lemo connector into the GK-404 until it locks into place.



Figure 10 - Lemo Connector to GK-404

Connect each of the clips on the leads to the matching colors of the sensor conductors, with blue representing the shield (bare).

To turn the GK-404 on, press the "ON/OFF" button on the front panel of the unit. The initial startup screen will be displayed. After approximately one second, the GK-404 will start taking readings and display them based on the settings of the POS and MODE buttons.

The unit display (from left to right) is as follows:

- The current Position: Set by the POS button. Displayed as a letter A through F.
- The current Reading: Set by the MODE button. Displayed as a numeric value followed by the unit of measure.
- Temperature reading of the attached gauge in degrees Celsius.

Use the **POS** button to select position **B** and the **MODE** button to select **Dg** (digits). (Other functions can be selected as described in the GK-404 Manual.)

The GK-404 will continue to take measurements and display readings until the unit is turned off, either manually, or if enabled, by the Auto-Off timer.

If no reading displays or the reading is unstable, see Section 7 for troubleshooting. For further information, consult the GK-404 manual.

5.2 GK-405 Readout Box

The GK-405 Vibrating Wire Readout is made up of two components: The Readout Unit, consisting of a Windows Mobile handheld PC running the GK-405 Vibrating Wire Readout Application; and the GK-405 Remote Module, which is housed in a weatherproof enclosure and connects to the vibrating wire gauge to be measured. The two components communicate wirelessly. The Readout Unit can operate from the cradle of the Remote Module, or, if more convenient, can be removed and operated up to 20 meters from the Remote Module.

5.2.1 Connecting Sensors with a 10-pin Bulkhead

Align the grooves on the sensor connector (male), with the appropriate connector on the readout (female connector labeled senor or load cell). Push the connector into place, and then twist the outer ring of the male connector until it locks into place.

5.2.2 Connecting Sensors with Bare Leads

Attach the GK-403-2 flying leads to the bare leads of a Geokon vibrating wire sensor by connecting each of the clips on the leads to the matching colors of the sensor conductors, with blue representing the shield (bare).

5.2.3 Operating the GK-405

Press the button labeled "POWER ON". A blue light will begin blinking, signifying that the Remote Module is waiting to connect to the handheld unit.

Launch the GK-405 VWRA program on the handheld PC by tapping on "Start", then "Programs", then the GK-405 VWRA icon. After a few seconds, the blue light on the Remote Module should stop flashing and remain lit, indicating that the remote module has successfully paired with the handheld PC. The Live Readings Window will be displayed on the handheld PC. Figure 11 shows a typical vibrating wire piezometer output in digits and thermistor output in degrees Celsius.

If the no reading displays or the reading is unstable, see Section 7 for troubleshooting suggestions. For further information, consult the GK-405 Instruction Manual.

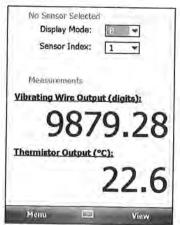


Figure 11 - Live Readings - Raw Readings

5.3 GK-403 Readout Box (Obsolete Model)

The GK-403 can store gauge readings as well as apply calibration factors to convert readings to engineering units. The following instructions explain taking gauge measurements using Modes "B" and "F".

5.3.1 Connecting Sensors with a 10-pin Bulkhead

Align the grooves on the sensor connector (male), with the appropriate connector on the readout (female connector labeled senor or load cell). Push the connector into place, and then twist the outer ring of the male connector until it locks into place.

5.3.2 Connecting Sensors with Bare Leads

Attach the GK-403-2 flying leads to the bare leads of a Geokon vibrating wire sensor by connecting each of the clips on the leads to the matching colors of the sensor conductors, with blue representing the shield (bare).

5.3.3 Operating the GK-403

- 1) Turn the display selector to position "B" (or "F").
- 2) Turn the unit on.
- 3) The readout will display the vibrating wire output in digits (see Equation 1 in Section 6). The last digit may change one or two digits while reading.
- The thermistor reading will be displayed above the gauge reading in degrees centigrade.
- 5) Press the "Store" button to record the value displayed.

If the no reading displays or the reading is unstable, see Section 7 for troubleshooting suggestions. The unit will automatically turn off after approximately two minutes to conserve power. Consult the GK-403 Instruction Manual for additional information.

5.4 Measuring Temperatures

All vibrating wire piezometers are equipped with a thermistor, which gives a varying resistance output as the temperature changes. The white and green leads of the instrument cable are normally connected to the internal thermistor. Geokon readout boxes will read the thermistor and display the temperature in degrees C. (High temperature versions use a different thermistor, which must be read using an ohmmeter.)

To read temperatures using an ohmmeter:

- Connect an ohmmeter to the green and white thermistor leads coming from the piezometer. Since the resistance changes with temperature are large, the effect of cable resistance is usually insignificant. For long cables a correction can be applied, equal to approximately 14.7 Ω per one thousand feet (48.5Ω per km). Multiply this factor by two to account for both directions.
- 2) Look up the temperature for the measured resistance in Appendix B, Table 7. For high temperature models, use Appendix C, Table 8.

6. DATA REDUCTION

6.1 Pressure Calculation

The digits displayed by the Geokon Models GK-403, GK-404, and GK-405 Readout Boxes on channel B are based on the equation:

Digits =
$$\left(\frac{1}{\text{Period}}\right)^2 \times 10^{-3} \text{ or Digits} = \frac{\text{Hz}^2}{1000}$$

Equation 1 - Digits Calculation

Note that in the above equation, the period is in seconds; Geokon readout boxes display microseconds. For example, a piezometer reading of 8000 digits corresponds to a period of 354 μ s and a frequency of 2828 Hz.

Digits are directly proportional to the applied pressure, as can be seen by the following equation:

Pressure =

(Current Reading - Initial Zero Reading) × Linear Calibration Factor

Ot

$$P = (R_1 - R_0) \times G$$

Equation 2 - Convert Digits to Pressure

Since the linearity of most sensors is within $\pm 0.2\%$ F.S., the errors associated with nonlinearity are of minor consequence. However, for those situations requiring the highest degree of accuracy, it may be desirable to use a second order polynomial to get a better fit of the data points. The use of a second order polynomial is explained in Appendix D.

The instrument's calibration report (a typical example of which is shown in Appendix E,) shows the data from which the linear gauge factor and the second order polynomial coefficients are derived. Columns on the right show the size of the error incurred by assuming a linear coefficient and the improvement that can be expected by going to a second order polynomial. In many cases, the difference is minor. The calibration report gives the pressure in certain engineering units. These can be converted to other engineering units using the multiplication factors shown in Table 2.

From → To ↓	psi	"н ₂ о	'н ₂ о	mm H ₂ 0	m H ₂ 0	"HG	mm HG	atm	mbar	bar	kPa	MPa
psi	-1	.036127	.43275	.0014223	1.4223	.49116	.019337	14.696	.014503	14.5039	.14503	145.03
"H ₂ O	27.730	1	12	.039372	39.372	13.596	,53525	406.78	.40147	401.47	4.0147	4016.1
'H ₂ O	2.3108	.08333	1	.003281	3.281	1.133	.044604	33.8983	.033456	33,4558	.3346	334.6
mm H ₂ 0	704.32	25.399	304.788	ı	1000	345.32	13,595	10332	10.197	10197	101.97	101970
m H ₂ 0	.70432	.025399	.304788	.001	1	.34532	.013595	10.332	.010197	10.197	.10197	101.97
"HG	2.036		.882624	7 10 10 10	2.8959	1	.03937	29.920	.029529	29.529	.2953	295.3
mm HG			22.4196	-	73.558	25.4	1	760	.75008	750.08	7.5008	7500.8
atm	.06805	0.150.07.10		.0000968		.03342	.001315	1	.000986	.98692	.009869	9.869
mbar	68.947		29.8896	1020	98.068	33.863	1.3332	1013.2	1	1000	10	10000
bar	.068947		_	.0000981	.098068	.033863	.001333	1.0132	.001	1 -	.01	10
kPa	6.8947	-		.0098068		3.3863	.13332		.1	100	1	1000
MPa	1,60,50,40,7	1000		.0000098	_		.000133	.101320	.0001	.1	.001	1

Table 2 - Engineering Units Multiplication Factors

(Note: Due to changes in specific gravity with temperature, the factors for mercury and water in the above table are approximate.)

6.2 Temperature Correction

The materials used in the construction of Geokon's vibrating wire piezometers have been carefully selected to minimize thermal effects; however, most units still have a slight temperature coefficient. Consult the calibration report supplied with the instrument to obtain the coefficient for the individual piezometer.

Since piezometers are normally installed in a tranquil and constant temperature environment, corrections are normally not required. If this is not the case for the selected installation, corrections can be made using the internal thermistor for temperature measurement. See Section 5.4 for instructions regarding obtaining the piezometer temperature.

The temperature correction equation is as follows:

Temperature Correction =

(Current Temperature - Initial Zero Temperature) × Thermal Factor

Or

$$P_T = (T_1 - T_0) \times K$$

Equation 3 - Temperature Correction

The calculated correction would then be added to the pressure calculated using Equation 2. If the engineering units were converted, remember to apply the same conversion to the calculated temperature correction.

For example, if the initial temperature was 22 °C, and the current temperature is 15 °C, and the thermal factor (K on the calibration report,) is +0.1319 kPa per °C rise. The temperature correction is +0.1319(15-22) = -0.92 kPa. Refer to the calibration report provided with the instrument for the thermal factor.

6.3 Barometric Correction (required only on unvented transducers)

Since the standard piezometer is hermetically sealed, it responds to changes in atmospheric pressure. Corrections may be necessary, particularly for the sensitive, low-pressure models. For example, a barometric pressure change from 29 to 31 inches of mercury would result in approximately one PSI of error (or ≈ 2.3 feet if monitoring water level in a well). It is advisable to read and record the barometric pressure every time the piezometer is read. Having an onsite barometer also allows the monitoring of barometric changes to judge what extent they may be affecting the reading. A separate pressure transducer (piezometer), kept out of the water, may also be used for this purpose.

The barometric correction equation is as follows:

Barometric Correction =

(Current Barometer - Initial Zero Barometer) × Conversion Factor

Or

$$P_B = (S_1 - S_0) \times F$$

Equation 4 - Barometric Correction

The calculated barometric correction is subtracted from the pressure calculated using Equation 2. If the engineering units were converted, remember to apply the same conversion to the calculated barometric correction.

Barometric pressure is usually recorded in inches of mercury. The conversion factor for inches of mercury to PSI is 0.491, and from inches of mercury to kPa is 3.386. Table 2 in Section 6.1 lists other common conversion factors.

The user should be cautioned that this correction scheme assumes ideal conditions. In reality, conditions are not always ideal. For example, if the well is sealed, barometric effects at the piezometer level may be minimal or attenuated from the actual changes at the surface. Thus, errors may result from applying a correction that is not required. In these cases, Geokon recommends independently recording the barometric pressure changes and correlating them with the observed pressure changes to arrive at a correction factor.

An alternative to making barometric corrections is to use piezometers that are vented to the atmosphere (see Section 6.4). However, vented piezometers only make sense if the piezo is in an open well or standpipe and the user is only interested in the water level. If the piezo is buried it is not certain that the full effect of the barometric change will be felt immediately at the instrument and is more likely to be attenuated and delayed, in which case a vented piezo would automatically apply a correction that is too large and too soon.

Equation 5 shows the pressure calculation with temperature and barometric correction applied.

$$P_{corrected} = (R_1 - R_0)G + (T_1 - T_0)K - (S_1 - S_0)F$$

Equation 5 - Corrected Pressure Calculation

6.4 Model 4500SV, Vented Piezometers



Figure 12 - Vented Piezometers

The Model 4500SV vented piezometer is designed to eliminate the effect of barometric pressure changes on water level measurements in wells, reservoirs, and boreholes that are connected directly to the atmosphere. They are not to be used where pore water pressures are being measured.

The space inside the transducer is not hermetically sealed and evacuated, as it is in the standard 4500 model piezometer, instead, it is connected via a tube (integral within the cable) to the atmosphere. A chamber containing desiccant capsules is attached to the outer end of this tube to prevent moisture from entering the transducer cavity. Vented piezometers require more maintenance then unvented types, since there is always the danger that moisture may find its way inside the transducer and ruin it.

Installation of the piezometer is accomplished simply by lowering it to the desired level in the well, reservoir, or borehole. The piezometer can be placed inside a canvas bag filled with sand, if so desired.

The desiccant capsule chamber needs to be positioned in some kind of housing to keep it dry. Geokon can provide suitable housings on request.

To keep the desiccant fresh during storage and transportation, the end of the desiccant chamber is closed off by means of a seal screw before being shipped from the factory. THIS SEAL SCREW MUST BE REMOVED BEFORE THE PIEZOMETER IS PUT INTO SERVICE!

The desiccant capsules are blue when fresh. They will gradually turn pink as they absorb moisture. When they have turned light pink in color, they should be replaced. Contact Geokon for replacement capsules.

6.5 Environmental Factors

Since the purpose of the piezometer installation is to monitor site conditions, factors that may affect these conditions should always be observed and recorded. Seemingly minor effects may have a real influence on the behavior of the structure being monitored and may give an early indication of potential problems. Some of these factors include, but are not limited to, blasting, rainfall, tidal levels, traffic, temperature and barometric changes, weather conditions, changes in personnel, nearby construction activities, excavation and fill level sequences, seasonal changes, etc.

7. TROUBLESHOOTING

Maintenance and troubleshooting of vibrating wire piezometers is confined to periodic checks of cable connections and maintenance of terminals. The transducers themselves are sealed and are not user serviceable. Gauges should not be opened in the field.

Should difficulties arise, consult the following list of problems and possible solutions. For additional troubleshooting and support, contact Geokon.

Symptom: Thermistor resistance is too high

✓ It is likely that there is an open circuit. Check all connections, terminals, and plugs. If a cut is located in the cable, splice according to instructions in Section 4.6.

Symptom: Thermistor resistance is too low

- ✓ It is likely that there is a short. Check all connections, terminals, and plugs. If a short is located in the cable, splice according to instructions in Section 4.6.
- ✓ Water may have penetrated the interior of the piezometer. There is no remedial action.

Symptom: Piezometer reading unstable

- ✓ Make sure the shield drain wire is connected to the blue clip on the flying leads. (Green for the GK-401.)
- ✓ Isolate the readout from the ground by placing it on a piece of wood or another insulator.
- ✓ Check for sources of nearby electrical noise such as motors, generators, antennas, or electrical cables. Move the piezometer cable away from these sources if possible. Contact the factory for available filtering and shielding equipment.
- ✓ The Piezometer may have been damaged by overranging or shock. Inspect the diaphragm and housing for damage.
- ✓ The body of the Piezometer may be shorted to the shield. Check the resistance between the shield drain wire and the Piezometer housing. If the resistance is very low, the gauge conductors may be shorted.

Symptom: Piezometer fails to give a reading

- ✓ Check the readout with another gauge to ensure it is functioning properly.
- ✓ The Piezometer may have been overranged or shocked. Inspect the diaphragm and housing for damage.
- ✓ Check the resistance of the cable by connecting an ohmmeter to the sensor leads. Table 3 shows the expected resistance for the various wire combinations; Table 4 is provided for the customer to fill in the actual resistance found. Cable resistance is approximately 14.7Ω per 1000 feet (48.5Ω per km). Multiply this factor by two to account for both directions. If the resistance is very high or infinite, the cable is probably broken or cut. If the resistance is very low, the gauge conductors may be shorted. If a cut or a short is located in the cable, splice according to instructions in Section 4.6.

	Vibrating W	/ire Sensor Lea	d Grid - SAMP	LE VALUES	
	Red	Black	White	Green	Shield
Red	N/A	≅180Ω	infinite	infinite	infinite
Black	≅180Ω	N/A	infinite	infinite	infinite
White	infinite	infinite	N/A	3000Ω at 25°C	infinite
Green	infinite	infinite	3000Ω at 25°C	N/A	infinite
Shield	infinite	infinite	infinite	infinite	N/A

Table 3 - Sample Resistance

	Vibrating W	ire Sensor Lead	Grid - SENSO	R NAME/##:	
	Red	Black	White	Green	Shield
Red					
Black		7			
White					
Green					
Shield					

Table 4 - Resistance Work Sheet

APPENDIX A. SPECIFICATIONS

A.1 4500 Series Specifications

Model	4500S	4500AL1	4500AR	4500B	4500C	4500DP	4580
Model Available Ranges ² (psi)	0-50 0-100 0-150 0-250 0-500 0-750 0-1000 0-1500 0-3000 0-5000 0-10000 0-15000	0-10 0-25		0-50 0-100 0-250	0-50 0-100 0-250	0-10 0-25 0-50 0-150 0-250 0-500 0-750 0-1000 0-3000 0-5000 0-10000	0-1 0-5
Resolution		0.025% F.S.	0.025% F.S.	0.025% F.S.	0.05% F.S.	0.025% F.S.	0.01% F.S.
Linearity ³				< 0.5% F.S	S		
Accuracy ⁴				0.1% F.S			
Overrange				1.5 × Rated Pro			0.0050/
Thermal Coefficient	<0.025% F.S./°C	<0.1% F.S./°C	<0.05% F.S./°C	<0.025% F.S./°C	<0.05% F.S./°C	<0.025% F.S./°C	<0.025% F.S./°C
Femperature Range				-20 °C to +8	0 °C		
Frequency Range				1400-3500		1 200	1.68
OD	.75" 19.05 mm	1" 25.40 mm	.75" 19.05 mm	.687" 17.45 mm	.437" 11.10 mm	1.3" 33,3 mm	1.5" 38.10 mm
Length	5.25" 133 mm	5.25" 133 mm	10" 254 mm	5.25" 133 mm	6.5" 165 mm	7.36" 187 mm	6.5" 165 mm

Table 5 - Vibrating Wire Piezometer Specifications

Notes:

Accuracy of Geokon test apparatus: 0.1%

Contact Geokon for specific application information.

Accuracy of test apparatus: 0.05%

² Other ranges available upon request.

³ 0.1% F.S. linearity available upon request.

⁴ Derived using second order polynomial.

A.2 Thermistor (See Appendix B. also)

Range: -80 to +150 °C Accuracy: ±0.5 °C

A.3 Standard Piezometer Wiring

Pin	Function	Wire Color
A	Vibrating Wire Gauge +	Red
A	Vibrating Wire Gauge -	Black
C	Thermistor	White
D	Thermistor	Green
E	Cable Shield	Shield
F-K	Not Used	

Table 6 - Standard Piezometer Wiring

APPENDIX B. THERMISTOR TEMPERATURE DERIVATION

Thermistor Type: YSI 44005, Dale #1C3001-B3, Alpha #13A3001-B3 Resistance to Temperature Equation:

$$T = \frac{1}{A + B(LnR) + C(LnR)^3} - 273.15 \text{ °C}$$

Equation 6 - Resistance to Temperature

Where:

T = Temperature in °C.

LnR = Natural Log of Thermistor Resistance

 $A = 1.4051 \times 10^{-3}$

 $\mathbf{B} = 2.369 \times 10^{-4}$

 $C = 1.019 \times 10^{-7}$

Note: Coefficients calculated over the -50 to +150° C. span.

Ohms	Temp	Ohms	Temp	Ohms	Temp	Ohms	Temp	T Ohms	Tr.
201.1K	-50	16.60K	-10	2417	+30	525.4		Ohms	Tem
187.3K	-49	15.72K	-9	2317	31		+70	153.2	+110
174.5K	-48	14.90K	-8	2221	32	507.8	71	149.0	111
162.7K	-47	14.12K	-7	2130	33	490.9	72	145.0	112
151.7K	-46	13.39K	-6	2042		474.7	73	141.1	113
141.6K	-45	12.70K	-5	1959	34 35	459.0	74	137.2	114
132.2K	-44	12.05K	-4	1880	36	444.0	75	133.6	115
123.5K	-43	11.44K	-3	1805		429.5	76	130.0	116
115.4K	-42	10.86K	-2	1733	37	415.6	77	126.5	117
107.9K	-41	10.31K	-1	1664	38	402,2	78	123,2	118
101.0K	-40	9796	0	1598	40	389.3	79	119,9	119
94.48K	-39	9310	+1	1535	41	376.9	80	116.8	120
88.46K	-38	8851	2	1475		364.9	81	113.8	121
82.87K	-37	8417	3		42	353.4	82	110.8	122
77.66K	-36	8006	4	1418	43	342.2	83	107.9	123
72.81K	-35	7618	5	1363	44	331.5	84	105.2	124
68.30K	-34	7252	6	1310	45	321.2	85	102.5	125
64.09K	-33	6905	7	1260	46	311.3	86	99.9	126
60.17K	-32	6576	8	1212	47	301.7	87	97.3	127
56.51K	-31	6265	9	1167	48	292.4	88	94.9	128
53.10K	-30	5971	10	1123	49	283.5	89	92.5	129
49.91K	-29	5692	11	1081	50	274.9	90	90.2	130
46.94K	-28	5427	12	1040	51	266.6	91	87.9	131
44.16K	-27	5177		1002	52	258.6	92	85.7	132
41.56K	-26	The second second	13	965.0	53	250.9	93	83.6	133
39.13K	-25	4939	14	929.6	54	243.4	94	81.6	134
36.86K	-24	4714	15	895.8	55	236.2	95	79.6	135
34.73K	-23	4500	16	863.3	56	229.3	96	77.6	136
32.74K	-23	4297	17	832.2	57	222.6	97	75.8	137
30.87K	-21	4105	18	802,3	58	216,1	98	73.9	138
29.13K	-20	3922	19	773.7	59	209.8	99	72.2	139
27.49K	-19	3748	20	746.3	60	203.8	100	70.4	140
25.95K	-18	3583	21	719.9	61	197.9	101	68.8	141
24.51K	-17	3426	22	694.7	62	192.2	102	67.1	142
23.16K		3277	23	670.4	63	186.8	103	65.5	143
21.89K	-16	3135	24	647.1	64	181.5	104	64.0	144
	-15	3000	25	624.7	65	176.4	105	62.5	145
20.70K	-14	2872	26	603.3	66	171.4	106	61.1	146
19.58K	-13	2750	27	582.6	67	166.7	107	59.6	147
18.52K	-12	2633	28	562.8	68	162.0	108	58.3	148
17.53K	-11	2523	29	543.7	69	157.6	109	56.8	149
	T	able 7 - The	ermistor F	Resistance V	Vereue To	mmanature		55.6	150

APPENDIX C. HIGH TEMPERATURE THERMISTOR LINEARIZATION

Resistance to Temperature Equation for US Sensor 103JL1A:

$$T = \frac{1}{A + B(LnR) + C(LnR)^3 + D(LnR)^5} -273.15 \text{ °C}$$

Equation 7 - High Temperature Resistance to Temperature

Where:

T = Temperature in °C.

LnR = Natural Log of Thermistor Resistance.

 $A = 1.127670 \times 10^{-3}$

 $B = 2.344442 \times 10^{-4}$

 $C = 8.476921 \times 10^{-8}$

 $D = 1.175122 \times 10^{-11}$

Note: Coefficients optimized for a curve "J" Thermistor over the temperature range of 0°C to

250°C	Temp	Ohms	Temp	Ohms	Temp	Ohms	Temp	Ohms	Temp	Ohms	Temp	Ohms	Temp	Ohms	Temp
Ohms	0	7,402	32	2,157	64	763.5	96	316.6	128	148.4	160	76.5	192	42.8	224
32,650		7,402	33	2,083	65	741.2	97	308.7	129	145.1	161	75.0	193	42.1	225
31,029	1		34	2,003	66	719.6	98	301.0	130	142.0	162	73.6	194	41.4	226
29,498	2	6,808	35	1,942	67	698.7	99	293.5	131	138.9	163	72,2	195	40.7	227
28,052	3	6,531		1,876	68	678.6	100	286.3	132	135.9	164	70.8	196	40.0	228
26,685	4	6,267	36 37	1,813	69	659.1	101	279.2	133	133.0	165	69.5	197	39.3	229
25,392	5	6,015	38	1,752	70	640.3	102	272.4	134	130.1	166	68.2	198	38.7	230
24,170	6	5,775		1,693	71	622.2	103	203.6	135	127.3	167	66.0	100	38.0	231
23,013	7	5,545	39	1,637	72	604.6	104	259.3	136	124.6	168	65.7	200	37.4	232
21,918	8	5,326	40	1,582	73	587.6	105	253.1	137	122.0	169	64.4	201	36.8	233
20,882	9	5,117	41	1,530	74	571.2	106	247.0	138	119.4	170	63.3	202	36.2	234
19,901	10	4,917	42	1,480	75	555.3	107	241.1	139	116.9	171	62.1	203	35.6	235
18,971	11	4,725	43	1,480	76	539.9	108	235.3	140	114.5	172	61.0	204	35:1	236
18,090	-	4,543	44		77	525.0	109	229.7	141	112.1	173	59,9	205	34.5	237
17,255	-	4,368	45	1,385	78	510.6	110	224.3	142	109.8	174	58.8	206	33.9	238
16,463	-	4,201	46		79	496.7	111	219.0	143	107.5	175	57.7	207	33.4	239
15,712		4,041	47	1,297	80	483.2	112	213 9	144	105.3	176	56.7	208	32.9	240
14,999		3,888	48	1,255	81	470.1	113	208.9	145	103.2	177	55.7	209	32.3	241
14,323	***************	3,742	49	1,215	82	457.5	114	204.1	146	101.1	178	54.7	210	31.8	242
13,681		3,602	50	1,177	83	445.3	115	199.4	147	99.0	179	53.7	211	31.3	243
13,072		3,468	51	1,140	84	433.4	+	194.8	148	97.0	180	52.7	212	30.8	244
12,493	-	3,340	52	1,104	85	421.9	117	190.3	149	95.1	181	51.8	213	30.4	245
11,942		3,217		1,070		410.8	118	186.1	150	93.2	182	50.9	214	29.9	246
11,419		3,099	-	1,037		400.0		181.9	151	91.3	183	50.0	215	29.4	247
10,922		2,986		1,005		389.6	-	177.7	152	89.5	184	49.1	216	29.0	248
10,450		2,878		973.8		379.4		173.7		87.7	185	48.3	217	28.5	249
10,00		2,774		944.1		369.6		169.8			186	47.4	218	28.1	250
9,572		2,675		915.5				166.0				46.6			
9,165		2,579		887.8		360.1						45.8			
8,777		2,488		861.2		350.9						45.0			
8,408				835.4		341.9									
8,05	7 30	2,316		810.6		333.2						43.5			
7.72	2 31	2,235	63	786.6	95	324.8	127	151,	135	10.0	171	1.6216	1 -40		

Table 8 - Thermistor Resistance versus Temperature for High Temperature Models

APPENDIX D. IMPROVING THE ACCURACY OF THE CALCULATED PRESSURE

Most vibrating wire pressure transducers are sufficiently linear (± 0.2 % F.S.) that the use of the linear calibration factor satisfies normal requirements. However, it should be noted that the accuracy of the calibration data, which is dictated by the accuracy of the calibration apparatus, is always ± 0.1 % F.S.

This level of accuracy can be recaptured, even where the transducer is nonlinear, using a second order polynomial expression, which gives a better fit to the data then does a straight line.

The polynomial expression has the form:

Pressure =
$$AR^2 + BR + C$$

Equation 8 - Second Order Polynomial Expression

Where:

R is the reading (digits channel B)

A, B, and C are coefficients

Appendix E shows a typical calibration report of a transducer that has fairly normal nonlinearity. The figure under the "Linearity (%F.S.)" column is

$$\frac{\text{Calculated Pressure-True Pressure}}{\text{Full Scale Pressure}} \times 100\% = \frac{G(R_1-R_0)-P}{F.S.} \times 100\%$$

Equation 9 - Linearity Calculation

Note: The linearity is calculated using the regression zero for R₀ shown on the calibration report.

For example, when P=420 kPa, $G(R_1-R_0)=-0.1795(6749-9082)$, gives a calculated pressure of 418.8 kPa. The error is 1.2 kPa equal to 122 mm of water.

Whereas the polynomial expression gives a calculated pressure of A $(6749)^2$ + B (6749) + 1595.7 = 420.02 kPa and the actual error is only 0.02 kPa or two millimeters of water.

Note: If the polynomial equation is used it is important that the value of C be taken in the field following the procedures described in Section 3.2. The field value of C is calculated by inserting the initial field zero reading into the polynomial equation with the pressure, P, set to zero.

If the field zero reading is not available, the value of C can be calculated by using the zero pressure reading on the calibration report. In the above example the value of C would be derived from the equation: $0 = A(9074)^2 + B(9074)$ from which C = 1595.7

It should be noted that where *changes* of water levels are being monitored it makes little difference whether the linear coefficient or the polynomial expression is used.

APPENDIX E. TYPICAL CALIBRATION REPORT

	V III	rating which	ressure Trai	isouce: one					
		uraania a MD		Date of Calib	ration: Augu	st 18, 2017			
М	odel Number:	4500INS-2 MP	<u>a</u>	This calibration has been verified/validated as of 11/13/2017					
S	erial Number:	1726650		Tempe	rature: 2	2.60 °C			
Calibrati	on Instruction:	VW Pressure Trans	ducers	Barometric Pr		y Rogers			
pplied ressure (MPa)	Gage Reading 1st Cycle	Gage Reading 2nd Cycle	Average Gage Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)		
.0 .4 .8 .2 .6	8894 8158 7417 6673 5924 5172	8894 8158 7418 6673 5925 5173	8894 8158 7418 6673 5925 5173	0.004 0.399 0.797 1.197 1.599 2.004	0.19 -0.04 -0.14 -0.14 -0.03 0.18	0.000 0.400 0.800 1,200 1.600 2.000	0.00 -0.01 0.00 0.00 0.01 -0.01		
	Gage factors:		Factor (K);0.			mial equation			
	r Gage Factor	(G): -0.07794 ors: A	(psi/ digit) .: -2.838E-07 rmal Factor (K):	В:	-0.07395	C:			
	Calcu	late C by setting P	=0 and R ₁ = initial	field zero readin	ig into the palyr	nomial equation			
Calculate	d Pressures:		Polynomial, P	$(R_1 - R_0) + K(T_1 - T_1)$ = $AR_1^2 + BR_1^2$	$C + K(T_1 - T_0)$				
	*Baro	metric pressures expresse	d in MPa or psi, Barome	etric compensation is r	ot required with ven	ted transducers			
			Temperature:	22.7 °C	Baron	meter: 995.5	mbar		

Figure 13 - Typical Calibration Report

APPENDIX F. MODEL 4500AR PIEZOMETER

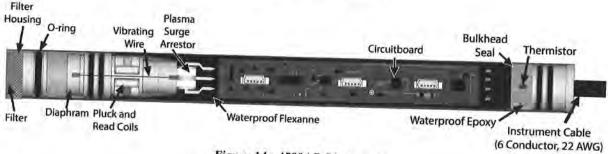


Figure 14 - 4500AR Piezometer

The Model 4500AR Piezometer is designed to be used with readout systems that can read frequency but do not have the capability to "pluck" the VW gauge. The sensor has built-in electronics that cause the gauge wire to vibrate continuously at its resonant frequency. The output from the sensor is a five-volt DC square wave at this frequency.

A DC input voltage in the range of 6 to 24 volts is required to operate the gauge. The current consumption is approximately 21 mA at 12VDC. The gauge output is independent of the input voltage.

Multiple sensors powered simultaneously can be read at quite fast rates, (up to five sensors per second,) and dynamic measurements on a single sensor can be made up to approximately 20Hz.

The gauge is installed in the field in the same way that the Model 4500 standard piezometer is installed. (See Section 3 and Section 4.)

4500AR Piezometer Wiring is shown in Table 9. The three pair cable is wired in pairs, with each pair comprising one colored and one black lead.

Wire Color	Function
Red	+6-24 VDC Power
Red's Black	Ground
White	Output
White's Black	Output Ground
Green	Thermistor +
Green's Black	Thermistor -
Bare	Shield

Table 9 - 4500AR Wiring Chart

Upon powerup the gauge will immediately start to "ring" at the resonant frequency and will continue to ring until the power is removed. Continuous operation will have no effect on the gauge life.

Note: The sensor is comprised of two transducers: the VW pressure sensor, and a thermistor for measuring temperature. The signal from the VW transducer is a high-level frequency and it will interfere with the thermistor output if left powered during the period that the thermistor is being read. If the temperature reading is important, the power to the pressure sensor should be switched off while the thermistor reading is taken.

APPENDIX G. PIEZOMETER PRESSURE AND WATER LEVEL

Frequently, when using a dip meter to check water levels in an open well, it happens that the water level, computed from a piezometer reading taken at the bottom of the well, does not agree with the water level measured directly by the dip meter. This will happen when the specific gravity of the water is not 1 gm/cc, the water is brackish or muddy, or both. It will also occur when there is a flow of water up or down the borehole. In addition, if the piezometer is removed to make room for the dip meter, the volume of the piezometer and cable displaces an equal volume of water, which can cause changes of the water level in a small diameter well.

Model Number: 4500S-350 kPa

Date of Calibration: July 12, 2019

This calibration has been verified/validated as of 07/18/2019

Serial Number: 1921455

Temperature: 23.00 °C

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 985.2 mbar

Cable Length: 70 feet

Technician: Kally Rogers

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8584	8584	8584	-0.298	-0.09	-0.085	-0.02
70.0	7873	7873	7873	70.24	0.08	70.17	0.06
140.0	7169	7169	7169	140.1	0.03	139.9	-0.03
210.0	6463	6463	6463	210.1	0.05	209.9	-0.01
279.9	5758	5759	5759	280.0	0.03	280.0	0.00
350.0	5055	5055	5055	349.8	-0.04	350.0	0.02

(kPa) Linear Gauge Factor (G): -0.09921 (kPa/digit)

Polynomial Gauge factors: A: 1.451E-07

B: -0.1012

C:

Thermal Factor (K): -0.04248 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01439 (psi/digit)

Polynomial Gauge Factors:

A: 2.105E-08

В: -0.01468

C.

Thermal Factor (K): -0.006162 (psi/°C)

Calculate C by setting P=0 and R_1 = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Factory Zero Reading: 8572 Temperature: 21.2 °C Barometer: 995 mbar

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.

GEOKON.

Vibrating Wire Pressure Transducer Calibration Report

Model Number: 4500S-350 kPa

Date of Calibration: July 12, 2019

This calibration has been verified/validated as of 07/18/2019

Serial Number: 1921444

Temperature: 23.00 °C

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Cable Length: 70 feet

Barometric Pressure: 985.2 mbar

Technician: Kally Rogers

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8701	8702	8702	0.281	0.08	0.057	0.02
70.0	8083	8083	8083	69.92	-0.02	69.90	-0.02
140.0	7462	7463	7463	139.8	-0.06	139.9	-0.03
210.0	6839	6839	6839	210.0	0.00	210.1	0.03
279.9	6217	6217	6217	280.0	0.02	280.0	0.01
350.0	5593	5594	5594	350.2	0.06	350.0	0.00

(kPa) Linear Gauge Factor (G): -0.1126 (kPa/digit)

Polynomial Gauge factors:

A: -1.371E-07

B: -0.1106

Thermal Factor (K): -0.1222 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01633 (psi/ digit)

Polynomial Gauge Factors:

A: -1.988E-08

B: -0.01605

Thermal Factor (K): -0.01773 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Factory Zero Reading: 8695 22.2 995 Temperature: Barometer:

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.

GEOKON。

VWP-\$

Vibrating Wire Pressure Transducer Calibration Report

Model Number: 4500S-350 kPa

Date of Calibration: July 12, 2019

This calibration has been verified/validated as of 07/18/2019

Serial Number: 1921438

Temperature: 23.00 °C

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 985.2 mbar

Cable Length: 70 feet

Technician: Kally Rogers

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomia (%FS)
0.0	8724	8725	8725	-0.170	-0.05	0.070	0.02
70.0	8108	8108	8108	69.84	-0.04	69.83	-0.04
140.0	7489	7489	7489	140.1	0.04	140.0	0.00
210.0	6872	6873	6873	210.1	0.05	210.0	0.01
279.9	6257	6258	6258	280.0	0.01	280.0	0.01
350.0	5643	5643	5643	349.8	-0.06	350.0	0.00

(kPa) Linear Gauge Factor (G): -0.1136 (kPa/ digit)

Polynomial Gauge factors:

A: 1.633E-07

B: -0.1159

C:

Thermal Factor (K): -0.06846 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01647 (psi/digit)

Polynomial Gauge Factors:

A: 2.368E-08

B: -0.01681

C.

Thermal Factor (K): -0.009930 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear, $P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Factory Zero Reading: 8717 Temperature: 22.2 °C Barometer: 995 mbar

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.

Vibrating Wire Pressure Transducer Calibration Report

Model Number: 4500S-350 kPa

Date of Calibration: July 12, 2019

This calibration has been verified/validated as of 07/18/2019

Serial Number: 1921442

Temperature: 23.00

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 985.2 mbar

Cable Length: 70 feet

Technician: Kally Rogers

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8697	8698	8698	0.055	0.02	0.109	0.03
70.0	8063	8063	8063	69.83	-0.04	69.77	-0.06
140.0	7424	7424	7424	140.1	0.03	140.0	0.00
210.0	6787	6787	6787	210.1	0.05	210.0	0.02
279.9	6151	6151	6151	280.1	0.04	280.0	0.02
350.0	5516	5516	5516	349.9	-0.02	350.0	-0.01

(kPa) Linear Gauge Factor (G): -0.1100 (kPa/digit)

Polynomial Gauge factors:

A: 6.915E-08

B: -0.1109

Thermal Factor (K): -0.1188 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01595 (psi/digit)

Polynomial Gauge Factors:

A: 1.003E-08

B: -0.01609

Thermal Factor (K): -0.01724 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Factory Zero Reading: 8691 Temperature: 21.9 Barometer: 995

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.



Model Number: 4500S-350 kPa

Date of Calibration: November 18, 2019

This calibration has been verified/validated as of 11/26/2019

Serial Number: 1943860

Temperature: 21.20

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 995.3 mbar

Cable Length: 160 feet

Technician:

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8924	8924	8924	0.228	0.07	-0.009	0.00
70.0	8310	8311	8311	70.05	0.01	70.03	0.01
140.0	7697	7697	7697	139.9	-0.03	140.0	0.00
210.0	7082	7082	7082	209.9	-0.03	210.0	0.00
280.0	6466	6466	6466	280.0	-0.01	280.0	-0.01
349.9	5849	5849	5849	350.2	0.07	350.0	0.00

(kPa) Linear Gauge Factor (G): -0.1138 (kPa/digit)

Polynomial Gauge factors:

A: -1.453E-07

B:___-0.1117

Thermal Factor (K): -0.1734 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01651 (psi/digit)

Polynomial Gauge Factors:

A: -2.108E-08 B: -0.01620

Thermal Factor (K): -0.02515 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear, $P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Factory Zero Reading: 8928

Temperature: 21.6 °C

The above instrument was found to be in tolerance in all operating ranges

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1

Vibrating Wire Pressure Transducer Calibration Report

Model Number: 4500S-350 kPa

Date of Calibration: July 12, 2019

This calibration has been verified/validated as of 07/18/2019

Serial Number: 1921447

Temperature: 23.00

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 985.2 mbar

Cable Length: 70 feet

Technician: Kally Rogers

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomia (%FS)
0.0	8607	8608	8608	0.060	0.02	0.045	0.01
70.0	8021	8021	8021	69.89	-0.02	69.90	-0.02
140.0	7433	7433	7433	139.9	-0.02	139.9	-0.02
210.0	6844	6845	6845	210.0	0.00	210.0	0.01
279.9	6256	6257	6257	280.0	0.01	280.0	0.02
350.0	5668	5669	5669	350.0	0.00	350.0	0.00

(kPa) Linear Gauge Factor (G): -0.1191 (kPa/digit)

Polynomial Gauge factors:

A: -1.919E-08

B: -0.1188

Thermal Factor (K): -0.08368 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01727 (psi/digit)

Polynomial Gauge Factors:

A: -2.783E-09

B: ____-0.01723

Thermal Factor (K): __-0.01214 __(psi/ °C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Factory Zero Reading:

8599

Temperature: 22.2

Barometer: 995

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.

Model Number: 4500S-350 kPa

Date of Calibration: November 18, 2019

This calibration has been verified/validated as of 11/26/2019

Serial Number: 1943862

Temperature: 21.20 °C

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 995.3 mbar

Cable Length: 150 feet

Technician:

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomia (%FS)
0.0	9088	9089	9089	-0.153	-0.04	-0.025	-0.01
70.0	8402	8402	8402	70.07	0.02	70.04	0.01
140.0	7717	7717	7717	140.1	0.05	140.0	0.02
210.0	7034	7034	7034	210.0	0.01	209.9	-0.02
280.0	6350	6350	6350	280.0	0.00	279,9	-0.01
349.9	5667	5667	5667	349.8	-0.03	350.0	0.01

(kPa) Linear Gauge Factor (G): -0.1023 (kPa/ digit)

Polynomial Gauge factors:

A: 8.587E-08 B: -0.1036

Thermal Factor (K): -0.1781 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01484 (psi/digit)

Polynomial Gauge Factors: A: 1.246E-08

B: -0.01502

Thermal Factor (K): -0.02584 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$$

Polynomial,
$$P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Factory Zero Reading: 9086 Temperature: 21.9 °C Barometer: 991.8 mbar

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.

GEOKON.

Vibrating Wire Pressure Transducer Calibration Report

Model Number: 4500S-350 kPa

Date of Calibration: July 12, 2019

This calibration has been verified/validated as of 07/18/2019

Serial Number: 1921452

Temperature: 23.00

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 985.2 mbar

Cable Length: 70 feet

Technician: Kally Rogers

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8755	8756	8756	-0.175	-0.05	-0.026	-0.01
70.0	8154	8154	8154	70.09	0.03	70.04	0.02
140.0	7555	7555	7555	140.1	0.02	139.9	-0.02
210.0	6955	6956	6956	210.1	0.04	209.9	0.00
279.9	6357	6357	6357	280.0	0.02	280.0	0.01
350.0	5759	5759	5759	349.9	-0.03	350.0	0.01

(kPa) Linear Gauge Factor (G): -0.1168 (kPa/digit)

Polynomial Gauge factors:

A: 1.392E-07

Thermal Factor (K): -0.08708 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01694 (psi/digit)

Polynomial Gauge Factors:

A: 2.019E-08

B: -0.01724

Thermal Factor (K): -0.01263 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Barometer: 995 mbar Factory Zero Reading: 8748 Temperature: 21.6

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.

GEOKON.

Vibrating Wire Pressure Transducer Calibration Report

Model Number: 4500S-350 kPa

Date of Calibration: November 18, 2019

This calibration has been verified/validated as of 11/26/2019

Serial Number: 1943861

Temperature: 21.20

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 995.3 mbar

Cable Length: 150 feet

Technician:

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	9036	9036	9036	-0.100	-0.03	-0.033	-0.01
70.0	8331	8331	8331	70.15	0.04	70.13	0.03
140.0	7631	7631	7631	139.9	-0.02	139.8	-0.04
210.0	6927	6927	6927	210.1	0.03	210.0	0.01
280.0	6225	6225	6225	280.0	0.01	280.0	0.00
349.9	5524	5524	5524	349.9	-0.02	349.9	0.00

(kPa) Linear Gauge Factor (G): -0.09965 (kPa/digit)

Polynomial Gauge factors:

A: 4.522E-08

B: -0.1003

Thermal Factor (K): -0.1721 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01445 (psi/ digit)

9040

Polynomial Gauge Factors:

A: 6.558E-09

B: -0.01455

Thermal Factor (K): -0.02497 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0) *$$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Temperature: 21.6 °C Barometer: 991.8 mbar Factory Zero Reading:

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.

Vibrating Wire Pressure Transducer Calibration Report

Model Number: 4500S-350 kPa

Date of Calibration: July 12, 2019

This calibration has been verified/validated as of 07/18/2019

Serial Number: 1921454

Temperature: 23.00

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 985.2 mbar

Cable Length: 70 feet

Technician: Kally Rogers

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8823	8823	8823	0.230	0.07	0.013	0.00
70.0	8217	8218	8218	69.99	0.00	69.96	0.00
140.0	7611	7611	7611	139.9	-0.04	139.9	-0.02
210.0	7003	7003	7003	209.9	-0.02	210.0	0.00
279.9	6394	6395	6395	280.0	0.02	280.0	0.01
350.0	5785	5785	5785	350.2	0.07	350.0	0.01

(kPa) Linear Gauge Factor (G): -0.1152 (kPa/digit)

Polynomial Gauge factors:

A: -1.308E-07

B: -0.1133

Thermal Factor (K): ___-0.1144 ___(kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01671 (psi/digit)

Polynomial Gauge Factors:

A: -1.897E-08

B: -0.01643

Thermal Factor (K): -0.01660 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Temperature: 21.7 °C Barometer: 995 mbar Factory Zero Reading: 8816

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1

Vibrating Wire Pressure Transducer Calibration Report

Model Number: 4500S-350 kPa

Date of Calibration: July 12, 2019

This calibration has been verified/validated as of 07/18/2019

Serial Number: 1921440

Temperature: 23.00

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 985.2 mbar

Cable Length: 70 feet

Technician: Karly Rogers

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8779	8780	8780	0.056	0.02	0.069	0.02
70.0	8155	8156	8156	69.82	-0.04	69.88	-0.03
140.0	7529	7530	7530	139.8	-0.05	139.9	-0.03
210.0	6902	6902	6902	210.0	0.00	210.0	0.02
279.9	6276	6276	6276	280.0	0.00	280.0	0.02
350.0	5650	5650	5650	349.9	-0.01	350.0	-0.01

(kPa) Linear Gauge Factor (G): -0.1118 (kPa/ digit)

Polynomial Gauge factors:

A: -2.715E-08

B: -0.1114

Thermal Factor (K): -0.1282 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01622 (psi/ digit)

Polynomial Gauge Factors:

A: -3.938E-09

B: -0.01616

Thermal Factor (K): -0.01860 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$$

Polynomial,
$$P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Factory Zero Reading:

The above instrument was found to be in tolerance in all operating ranges

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.

Vibrating Wire Pressure Transducer Calibration Report

Model Number: 4500S-350 kPa

Date of Calibration: July 12, 2019

Serial Number: 1921450

This calibration has been verified/validated as of 07/18/2019

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 985.2 mbar

Temperature: 23.00

Cable Length: 70 feet

Technician: Kally Rogers

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8773	8774	8774	-0.178	-0.05	-0.078	-0.02
70.0	8182	8182	8182	70.07	0.03	70.12	0.04
140.0	7594	7594	7594	139.9	-0.02	139.9	-0.01
210.0	7005	7005	7005	209.9	-0.03	209.9	-0.02
279.9	6415	6416	6416	279.9	-0.02	279.9	0.00
350.0	5825	5826	5826	350.0	-0.01	350.1	0.02

(kPa) Linear Gauge Factor (G): -0.1188 (kPa/digit)

Polynomial Gauge factors:

A: 3.602E-08

B: -0.1193

Thermal Factor (K): -0.06067 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01723 (psi/digit)

Polynomial Gauge Factors:

A: 5.224E-09

B: -0.01730

Thermal Factor (K): -0.008800 (psi/°C)

Calculate C by setting P=0 and R_1 = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Factory Zero Reading: 8766 Temperature: 21.4 °C Barometer:

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.



Model Number: 4500S-350 kPa

Date of Calibration: July 12, 2019

This calibration has been verified/validated as of 07/18/2019

Serial Number: 1921453

Temperature: 23.00

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 985.2 mbar

Cable Length: 70 feet

Technician: Kally Rogers

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8654	8655	8655	0.059	0.02	-0.014	0.00
70.0	8060	8061	8061	70.02	0.01	69.99	0.01
140.0	7466	7467	7467	140.0	0.00	140.0	0.00
210.0	6872	6873	6873	209.9	0.00	209.9	-0.01
279.9	6278	6278	6278	280.0	0.01	279.9	0.00
350.0	5682	5683	5683	350.1	0.04	350.0	0.01

(kPa) Linear Gauge Factor (G): -0.1178 (kPa/digit)

Polynomial Gauge factors:

A: -3.023E-08

B: -0.1173

Thermal Factor (K): -0.03155 (kPa/°C)

Calculate C by setting P=0 and R_1 = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01708 (psi/digit)

Polynomial Gauge Factors: A: -4.384E-09 B: -0.01702

Thermal Factor (K): -0.004576 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Factory Zero Reading: 8649 Temperature: 21.5

Barometer: 995 mbar

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.

Vibrating Wire Pressure Transducer Calibration Report

Model Number: 4500S-350 kPa

Date of Calibration: July 12, 2019

This calibration has been verified/validated as of 07/18/2019

Serial Number: 1921446

Temperature: 23.00 °C

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 985.2 mbar

Cable Length:

70 feet

Technician: Karly Rogers

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8627	8628	8628	-0.284	-0.08	0.068	0.02
70.0	8009	8009	8009	69.96	0.00	69.92	-0.02
140.0	7392	7392	7392	140.0	0.01	139.8	-0.06
210.0	6773	6773	6773	210.3	0.11	210.1	0.04
279.9	6159	6159	6159	280.1	0.04	280.0	0.03
350.0	5547	5547	5547	349.6	-0.11	349.9	-0.01

(kPa) Linear Gauge Factor (G): -0.1136 (kPa/digit)

Polynomial Gauge factors:

A: 2.621E-07

-0.1173

Thermal Factor (K): -0.1012 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01647 (psi/ digit)

8632

Polynomial Gauge Factors:

A: 3.801E-08

B: -0.01701

Thermal Factor (K): -0.01467 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Factory Zero Reading:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Temperature: 22.0

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.

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Barometer: 995

Vibrating Wire Pressure Transducer Calibration Report

Model Number: 4500S-350 kPa

Date of Calibration: July 12, 2019

This calibration has been verified/validated as of 07/18/2019

Serial Number: 1921451

Temperature: 23.00

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 985.2 mbar

Cable Length: 70 feet

Technician: Kally Rogers

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8698	8698	8698	-0.120	-0.03	0.007	0.00
70.0	8116	8116	8116	69.95	-0.01	69.97	0.00
140.0	7534	7535	7535	140.0	-0.01	139.9	-0.02
210.0	6953	6953	6953	210.0	0.00	209.9	0.00
279.9	6371	6372	6372	280.0	0.01	280.0	0.02
350.0	5791	5791	5791	349.9	-0.03	350.0	0.00

(kPa) Linear Gauge Factor (G): -0.1204 (kPa/digit)

Polynomial Gauge factors:

A: 7.521E-08

B: -0.1215

Thermal Factor (K): -0.07631 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01746 (psi/ digit)

Polynomial Gauge Factors: A: 1.091E-08 B: -0.01762

Thermal Factor (K): -0.01107 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear, $P = G(R_1 - R_1) + K(T_1 - T_0) - (S_1 - S_0)^*$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Temperature: 22.5 Factory Zero Reading: 8690 Barometer: 995 mbar

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.

GEOKON.

Vibrating Wire Pressure Transducer Calibration Report

Model Number: 4500S-350 kPa

Date of Calibration: July 12, 2019

This calibration has been verified/validated as of 07/18/2019

Serial Number: 1921439

Temperature: 23.00

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 985.2 mbar

Cable Length: 70 feet

Technician: Karly Rogers

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8636	8637	8637	-0.562	-0.16	-0.059	-0.02
70.0	7944	7945	7945	70.16	0.05	70.11	0.04
140.0	7259	7259	7259	140.2	0.07	139.9	-0.03
210.0	6574	6574	6574	210.2	0.08	209.9	-0.02
279.9	5891	5891	5891	280.0	0.02	280.0	0.01
350.0	5211	5211	5211	349.5	-0.13	350.0	0.01

(kPa) Linear Gauge Factor (G): -0.1022 (kPa/digit)

Polynomial Gauge factors:

A: 2.921E-07

B: -0.1062

Thermal Factor (K): -0.05477 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01482 (psi/digit)

Polynomial Gauge Factors:

A: 4.237E-08

B: -0.01541

Thermal Factor (K): -0.007944 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$$

Polynomial,
$$P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Factory Zero Reading: 8627 Temperature: 21.9 Barometer:

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.

Model Number; 4500S-350 kPa

Date of Calibration: November 18, 2019

This calibration has been verified/validated as of 11/26/2019

Serial Number: 1943866

Temperature: 21.20

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 995.3 mbar

Cable Length: 150 feet

Technician:

ilated sure iear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
161	-0.05	-0.054	0.02

Pressure (kPa)	Reading 1st Cycle	Reading 2nd Cycle	Gauge Reading	Pressure (Linear)	Linear (%FS)	Pressure (Polynomial)	Polynomial (%FS)
0.0	8964	8965	8965	-0.161	-0.05	-0.054	-0.02
70.0	8312	8312	8312	70.08	0.02	70.12	0.03
140.0	7663	7663	7663	139.9	-0.01	140.0	-0.01
210.0	7013	7013	7013	209.9	-0.01	209.9	-0.01
280.0	6363	6363	6363	279.9	-0.03	279.9	-0.02
349.9	5713	5713	5713	349.9	-0.02	350.0	0.01

(kPa) Linear Gauge Factor (G): -0.1077 (kPa/digit)

Polynomial Gauge factors:

A: 4.09E-08

B: -0.1083

Thermal Factor (K): -0.07397 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01561 (psi/ digit)

Polynomial Gauge Factors:

A: 5.932E-09

B: -0.01570

Thermal Factor (K): -0.01073 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Temperature: 21.9 Barometer: 991.8 mbar Factory Zero Reading: 8963

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1

Vibrating Wire Pressure Transducer Calibration Report

Model Number: 4500S-350 kPa

Date of Calibration: July 12, 2019

This calibration has been verified/validated as of 07/18/2019

Serial Number: 1921443

Temperature: 23.00

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 985.2 mbar

Cable Length: 70 feet

Gauge

Reading

Gauge

Reading

Technician: Kally Rogers

Calculated Error Calculated Error Pressure Linear Polynomial Draccura

(kPa)	1st Cycle	2nd Cycle	Reading	(Linear)	(%FS)	(Polynomial)	(%FS)
0.0	8638	8639	8639	0.287	0.08	0.073	0.02
70.0	8033	8033	8033	69.79	-0.05	69.82	-0.04
140.0	7422	7423	7423	139.9	-0.04	140.0	0.01
210.0	6813	6813	6813	209.8	-0.04	210.0	0.01
279.9	6202	6202	6202	280.0	0.00	280.0	0.01
350.0	5590	5590	5590	350.2	0.06	350.0	0.00

(kPa) Linear Gauge Factor (G): -0.1148 (kPa/digit)

Polynomial Gauge factors:

Applied

Pressure

Average

Gauge

A: -1.65E-07 B: -0.1124

Thermal Factor (K): -0.09576 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01665 (psi/digit)

Polynomial Gauge Factors:

A: -2.393E-08 B: -0.01631

Thermal Factor (K): -0.01389 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Temperature: 22.0 °C Barometer: 995 mbar Factory Zero Reading: 8631

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.



Model Number: 4500S-350 kPa

Date of Calibration: September 12, 2019

This calibration has been verified/validated as of 09/25/2019

Serial Number: 1933662

Temperature: 22.90

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 1000.4 mbar

Cable Length: 140 feet

Technician:

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8979	8979	8979	-0.113	-0.03	0.005	0.00
70.0	8360	8359	8360	69.95	-0.01	69.96	0.00
140.0	7740	7740	7740	140.0	0.02	140.0	0.00
210.0	7121	7121	7121	210.0	0.02	210.0	0.01
280.0	6503	6503	6503	279.9	-0.02	279.9	-0.02
349.9	5885	5885	5885	349.8	-0.03	349.9	0.00

(kPa) Linear Gauge Factor (G): -0.1131 (kPa/digit)

Polynomial Gauge factors:

A: 7.378E-08

Thermal Factor (K): -0.1029 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01640 (psi/ digit)

Polynomial Gauge Factors:

A: 1.07E-08

B: -0.01656

Thermal Factor (K): -0.01493 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$$

Polynomial,
$$P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Factory Zero Reading: 8996 Temperature: 23.2 Barometer: 989.9 mbar

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.

Vibrating Wire Pressure Transducer Calibration Report

Model Number: 4500S-350 kPa

Date of Calibration: July 12, 2019

This calibration has been verified/validated as of 07/18/2019

Serial Number: 1921441

Temperature: 23.00 °C

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 985.2 mbar

Cable Length: 70 feet

Technician: Kally Rogers -

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8649	8649	8649	0.000	0.00	0.075	0.02
70.0	8045	8045	8045	69.82	-0.04	69.80	-0.05
140.0	7437	7437	7437	140.1	0.03	140.0	0.01
210.0	6832	6832	6832	210.0	0.02	210.0	0.01
279.9	6227	6227	6227	280.0	0.01	280.0	0.01
350.0	5622	5622	5622	349.9	-0.02	350.0	0.00

(kPa) Linear Gauge Factor (G): -0.1156 (kPa/digit)

Polynomial Gauge factors:

A: 6.491E-08

-0.1165

Thermal Factor (K): -0.1069 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01677 (psi/ digit)

Polynomial Gauge Factors:

A: 9.414E-09

B: -0.01690

Thermal Factor (K): -0.01551 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_2) + K(T_1 - T_2) - (S_1 - S_2)^*$$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi, Barometric compensation is not required with vented transducers.

Temperature: 21.9 °C Barometer: 995 mbar Factory Zero Reading: 8642

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.

Model Number: 4500S-350 kPa

Date of Calibration: November 18, 2019

This calibration has been verified/validated as of 11/26/2019

Serial Number: 1943859

Temperature: 21.20 °C

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 995.3 mbar

Cable Length: 160 feet

Technician:

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8877	8878	8878	0.053	0.02	0.015	0.00
70.0	8217	8218	8218	69.94	-0.02	69.94	-0.02
140.0	7555	7555	7555	140.1	0.03	140.1	0.04
210.0	6896	6896	6896	209.9	-0.03	209.9	-0.02
280.0	6234	6234	6234	280.0	-0.01	280.0	-0.01
349.9	5572	5573	5573	350.0	0.01	350.0	0.00

(kPa) Linear Gauge Factor (G): -0.1059 (kPa/digit)

Polynomial Gauge factors:

A: -2.166E-08

-0.1056

Thermal Factor (K): -0.1839 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01536 (psi/digit)

Polynomial Gauge Factors:

A: -3.141E-09

B: -0.01531

Thermal Factor (K): -0.02667 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear, $P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Factory Zero Reading: 8879

Temperature:

Barometer: 991.8 mbar

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.

Model Number: 4500S-350 kPa

Date of Calibration: July 12, 2019

This calibration has been verified/validated as of 07/18/2019

Serial Number: 1921448

Temperature: 23.00

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 985.2 mbar

Cable Length: 70 feet

Technician: Kally Rogers

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8786	8787	8787	0.297	0.08	0.105	0.03
70.0	8201	8202	8202	69.86	-0.03	69.85	-0.03
140.0	7614	7614	7614	139.7	-0.07	139.8	-0.05
210.0	7023	7023	7023	210.0	0.01	210.1	0.04
279.9	6433	6434	6434	280.1	0.05	280.1	0.05
350.0	5845	5845	5845	350.1	0.03	349.9	-0.02

(kPa) Linear Gauge Factor (G): -0.1189 (kPa/digit)

Polynomial Gauge factors:

A: -1.294E-07

-0.1170

Thermal Factor (K): -0.04389 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01725 (psi/ digit)

Polynomial Gauge Factors:

A: -1.877E-08

B: -0.01697

Thermal Factor (K): -0.006366 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Factory Zero Reading: 8781 Temperature: 21.4 Barometer: 995

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.

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Vibrating Wire Pressure Transducer Calibration Report

Model Number: 4500S-350 kPa

Date of Calibration: July 12, 2019

This calibration has been verified/validated as of 07/18/2019

Serial Number: 1921449

Temperature: 23.00

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 985.2 mbar

Cable Length: 70 feet

Technician: Kally Rogers

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8723	8724	8724	0.059	0.02	0.026	0.01
70.0	8128	8128	8128	69.96	0.00	69.92	-0.02
140.0	7531	7531	7531	140.0	0.01	140.0	0.00
210.0	6935	6935	6935	210.0	0.01	209.9	0.00
279.9	6338	6339	6339	280.0	0.02	280.0	0.01
350.0	5742	5742	5742	350.0	0.02	350.0	0.01

(kPa) Linear Gauge Factor (G): -0.1174 (kPa/digit)

Polynomial Gauge factors:

A: 8.497E-09

-0.1175

Thermal Factor (K): -0.1013 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01703 (psi/digit)

Polynomial Gauge Factors:

A: 1.232E-09

B: -0.01704

Thermal Factor (K): __-0.01470 (psi/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear, $P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

Factory Zero Reading: 8718 Temperature: 21.6 Barometer: 995

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z540-1.

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Vibrating Wire Pressure Transducer Calibration Report

Model Number: 4500S-350 kPa

Date of Calibration: September 12, 2019

This calibration has been verified/validated as of 09/25/2019

Serial Number: 1933663

Temperature: 22.90 °C

Calibration Instruction: CI-Pressure Transducer 7 kPa~3 MPa

Barometric Pressure: 1000.4 mbar

Cable Length: 140 feet

Technician:

Applied Pressure (kPa)	Gauge Reading 1st Cycle	Gauge Reading 2nd Cycle	Average Gauge Reading	Calculated Pressure (Linear)	Error Linear (%FS)	Calculated Pressure (Polynomial)	Error Polynomial (%FS)
0.0	8919	8919	8919	0.109	0.03	-0.051	-0.01
70.0	8278	8278	8278	70.08	0.03	70.10	0.04
140.0	7639	7639	7639	139.8	-0.04	139.9	-0.01
210.0	6999	6999	6999	209.7	-0.08	209.8	-0.05
280.0	6354	6354	6354	280.1	0.03	280.1	0.04
349.9	5713	5713	5713	350.1	0.03	349.9	-0.01

(kPa) Linear Gauge Factor (G): -0.1092 (kPa/ digit)

Polynomial Gauge factors:

A: -1.115E-07

B: -0.1075

Thermal Factor (K): -0.1168 (kPa/°C)

Calculate C by setting P=0 and R₁ = initial field zero reading into the polynomial equation

(psi) Linear Gauge Factor (G): -0.01583 (psi/ digit)

Polynomial Gauge Factors:

A: -1.617E-08

B: -0.01560

Thermal Factor (K): -0.01694 (psi/°C)

Calculate C by setting P=0 and R_1 = initial field zero reading into the polynomial equation

Calculated Pressures:

Linear,
$$P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)^*$$

Polynomial, $P = AR_1^2 + BR_1 + C + K(T_1 - T_0) - (S_1 - S_0)^*$

*Barometric pressures expressed in kPa or psi. Barometric compensation is not required with vented transducers.

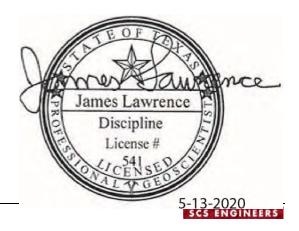
Factory Zero Reading: Temperature: 23.2 Barometer: 989.9

The above instrument was found to be in tolerance in all operating ranges.

The above named instrument has been calibrated by comparison with standards traceable to the NIST, in compliance with ANSI Z54641.

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APPENDIX III-4.H STANDPIPE PIEZOMETER COMPLETION DATA



Site Name: City of Waco Landfill

County: Mclennan Monitor Well I.D. No.: PZ-1
Date of Installation: 10/04/2018 Date of Development: 11/30/2018

Latitude: 31 42' 16.86" N Longitude: 96° 55' 59.13" W

Well Driller Name and License Number Best Drilling, Loyd Bruce Milton, License No. 4926M

Method of well development: Surge

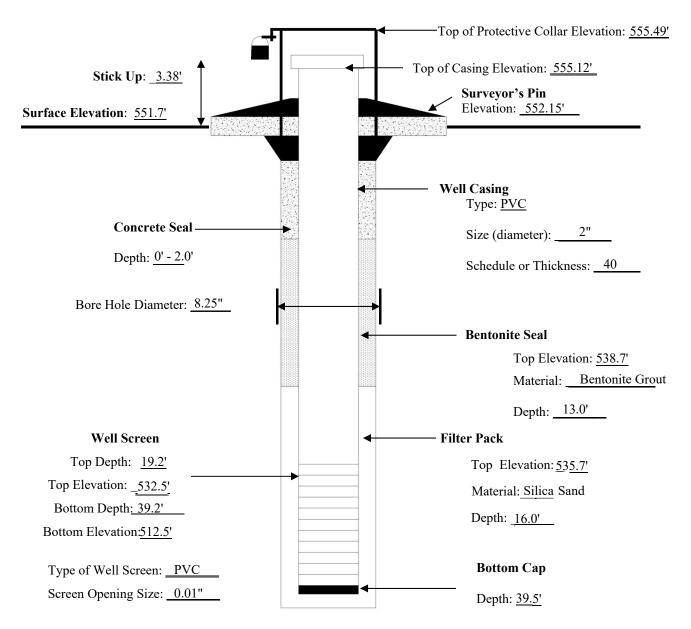
SCS Field Staff Supervising Installation: <u>Tim Derstine</u>, P.G.

Static Water Level after Well Development:

Name of Geologic Formation(s) in which Well is completed: Wolfe City Formation, Cretaceous

Type of Locking Device: Pad Lock Type of Case Protection: Aluminum

Concrete Surface Pad (with steel reinforcement) Dimensions: 2' x 2'



Site Name: <u>City of Waco Landfill</u>

County: McLennan Monitor Well I.D. No.: PZ-3
Date of Installation: 10/10/2018 Date of Development: 11/28/2018

Latitude: 31° 41′ 54.30″ N Longitude: 96° 55′ 43.84″ W

Well Driller Name and License Number Best Drilling, Loyd Bruce Milton, License No. 4926M

Method of well development: Surge

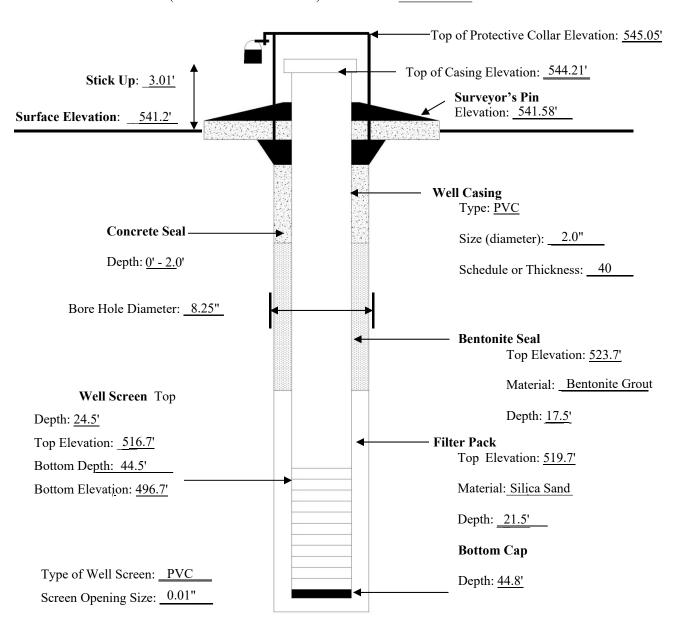
SCS Field Staff Supervising Installation: Tim Derstine, P.G.

Static Water Level after Well Development:

Name of Geologic Formation(s) in which Well is completed: Wolfe City Formation, Cretaceous

Type of Locking Device: Pad Lock Type of Case Protection: Aluminum

Concrete Surface Pad (with steel reinforcement) Dimensions: 2.0' x 2.0'



Site Name: City of Waco Landfill

County: Limestone Monitor Well I.D. No.: PZ-8

Date of Installation: 11/28/2018 Date of Development: Latitude: 31° 42' 11.59" N Longitude: 96° 55' 12.21" W

Well Driller Name and License Number Best Drilling, Loyd Bruce Milton, License No. 4926M Method of well development: ______

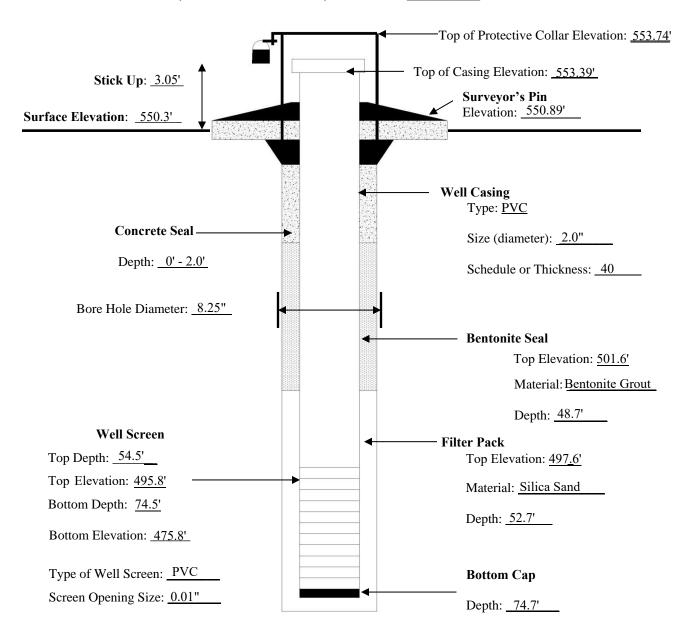
SCS Field Staff Supervising Installation: Tim Derstine, P.G.

Static Water Level after Well Development: ______

Name of Geologic Formation(s) in which Well is completed: Wolfe City Formation, Cretaceous

Type of Locking Device: Pad Lock Type of Case Protection: Aluminum

Type of Locking Device: Pad Lock Type of Case Protection: Aluminum Concrete Surface Pad (with steel reinforcement) Dimensions: 2.0' x 2.0'



Site Name: City of Waco Landfill

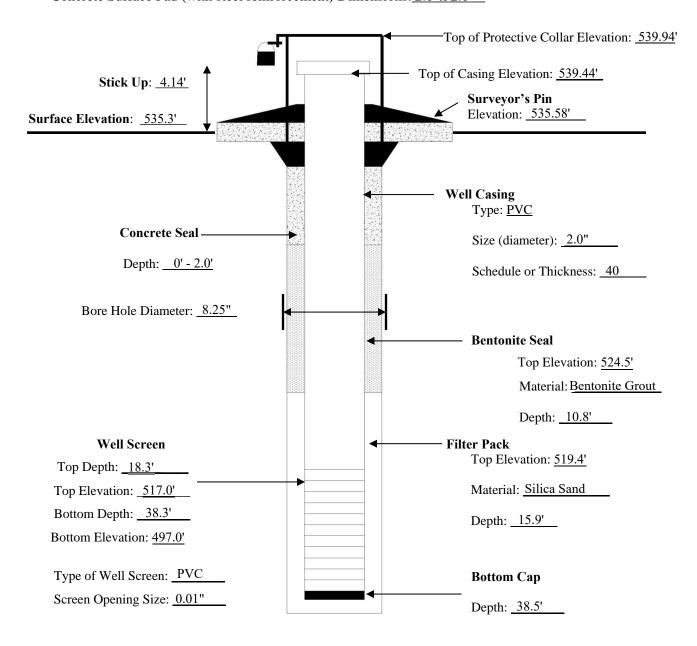
County: Limestone Monitor Well I.D. No.: PZ-9

Date of Installation: 10/10/2018 Date of Development: Latitude: 31° 42' 10.46" N Longitude: 96°55' 37.43" W

Well Driller Name and License Number Best Drilling, Loyd Bruce Milton, License No. 4926M Method of well development: SCS Field Staff Supervising Installation: Tim Derstine, P.G.

Static Water Level after Well Development: Name of Geologic Formation(s) in which Well is completed: Wolfe City Formation, Cretaceous

Type of Locking Device: Pad Lock Type of Case Protection: Aluminum Concrete Surface Pad (with steel reinforcement) Dimensions: 2.0' x 2.0'



Site Name: <u>City of Waco Landfill</u>

County: <u>Limestone</u>

Date of Installation: 10/30/2018

Monitor Well I.D. No.: <u>PZ-18</u>

Date of Development: 11/20/2018

Latitude: 31° 42' 28.96" N Longitude: 96° 55' 26.98" W

Well Driller Name and License Number Best Drilling, Loyd Bruce Milton, License No. 4926M

Method of well development: Surge

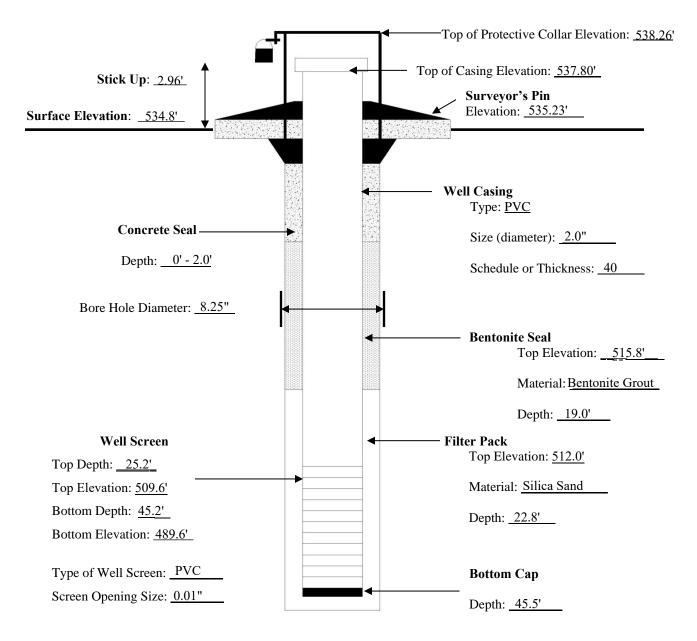
SCS Field Staff Supervising Installation: Tim Derstine, P.G.

Static Water Level after Well Development:

Name of Geologic Formation(s) in which Well is completed: Wolfe City Formation, Cretaceous

Type of Locking Device: Pad Lock Type of Case Protection: Aluminum

Concrete Surface Pad (with steel reinforcement) Dimensions: 2.0' x 2.0'



Site Name: City of Waco Landfill

County: Limestone Monitor Well I.D. No.: PZ-20
Date of Installation: 10/30/2018
Date of Development: 11/20/2018

Latitude: 31° 42' 34.93" N Easting: 96° 55' 14.45" W

Well Driller Name and License Number: West Drilling, Ricardo Garcia, License No. 54637

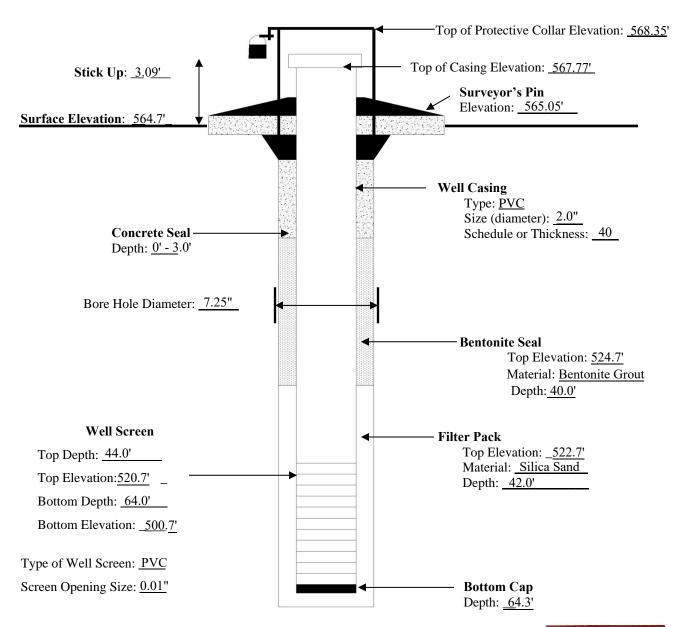
Method of well development: <u>Surge</u>

SCS Field Staff Supervising Installation: Valerie Wooters

Static Water Level after Well Development:_

Name of Geologic Formation(s) in which Well is completed: Wolfe City Formation, Cretaceous

Type of Locking Device: <u>Pad Lock</u> Type of Case Protection: <u>Aluminum</u> Concrete Surface Pad (with steel reinforcement) Dimensions: 2.0' x 2.0'



Site Name: City of Waco Landfill

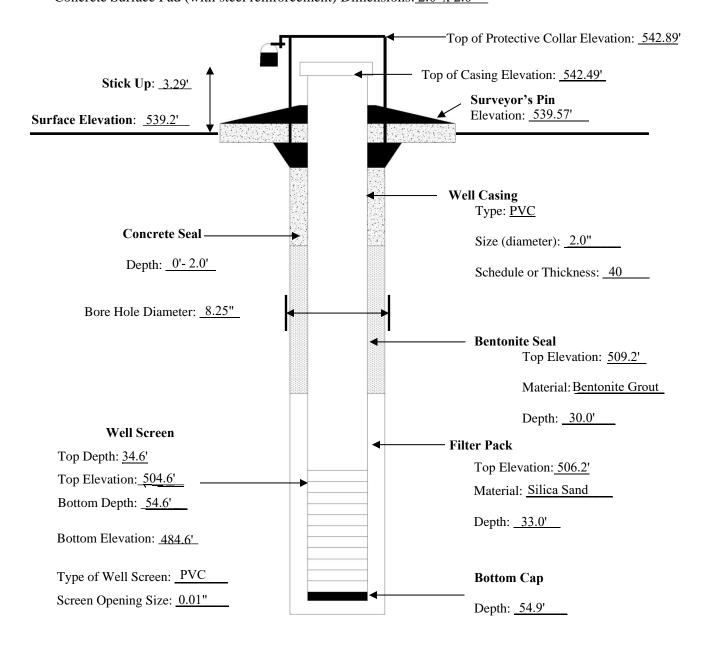
County: Limestone Monitor Well I.D. No.: PZ-33

Date of Installation: 11/20/2018 Date of Development: Latitude: 31° 42' 00.00" N Longitude: 96° 55' 14.54" W

Well Driller Name and License Number Best Drilling, Loyd Bruce Milton, License No. 4926M Method of well development: SCS Field Staff Supervising Installation: Tim Derstine, P.G.

Static Water Level after Well Development: Wolfe City Formation, Cretaceous

Type of Locking Device: Pad Lock Type of Case Protection: Aluminum Concrete Surface Pad (with steel reinforcement) Dimensions: 2.0' x 2.0'



Site Name: City of Waco Landfill

County: Limestone Monitor Well I.D. No.: PZ-41

Date of Installation: 12/18/2018 Date of Development: Latitude: 31° 42' 10.66" N Longitude: 96° 54' 59.07" W

Well Driller Name and License Number Best Drilling, Loyd Bruce Milton, License No. 4926M Method of well development: ______

SCS Field Staff Supervising Installation: Tim Derstine, P.G.

Static Water Level after Well Development: ______

Name of Geologic Formation(s) in which Well is completed: Wolfe City Formation, Cretaceous

Type of Locking Device: Pad Lock Type of Case Protection: Aluminum

Concrete Surface Pad (with steel reinforcement) Dimensions: 2.0' x 2.0'

Top of Protective Collar Elevation: <u>538.39</u>' Top of Casing Elevation: 538.04' Stick Up: <u>3.42'</u> Surveyor's Pin Elevation: <u>535.03</u> **Surface Elevation**: 534.6' **Well Casing** Type: PVC Concrete Seal -Size (diameter): 2.0" Depth: 0' - 2.0' Schedule or Thickness: 40 Bore Hole Diameter: 8.25" **Bentonite Seal** Top Elevation: 512.6' Material: Bentonite Grout Depth: 22.0' Well Screen Filter Pack Top Depth: <u>28.6'</u> Top Elevation: 510.6' Top Elevation: 506.0' Material: Silica Sand Bottom Depth: 48.6' Depth: <u>24.0'</u> Bottom Elevation: 486.0' Type of Well Screen: PVC **Bottom Cap** Screen Opening Size: 0.01" Depth: 48.8'

Site Name: City of Waco Landfill

County: Limestone Monitor Well I.D. No.: PZ-43

Date of Installation: 11/16/2018 Date of Development:

Latitude: 31° 42' 20.55" N Longitude: 96° 55' 01.03" W

Well Driller Name and License Number Best Drilling, Loyd Bruce Milton, License No. 4926M

Method of well development: ______

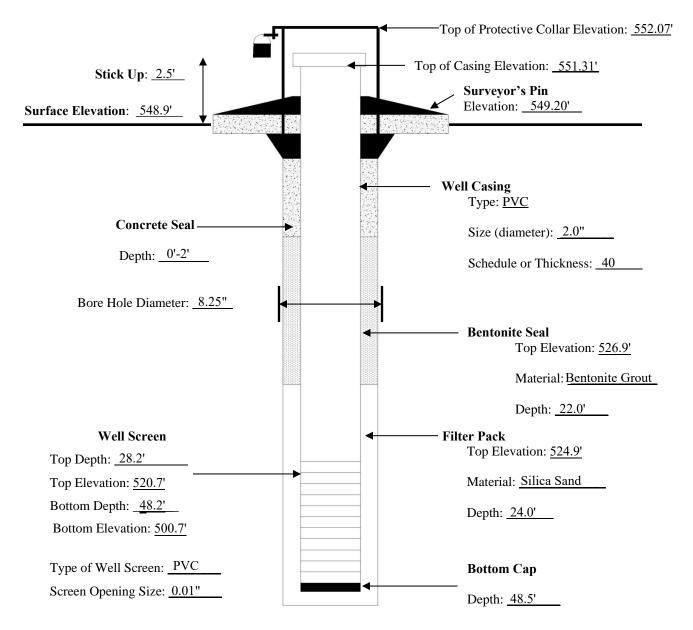
SCS Field Staff Supervising Installation: Tim Derstine, P.G.

Static Water Level after Well Development: ______

Name of Geologic Formation(s) in which Well is completed: _____ Wolfe City Formation, Cretaceous

Type of Locking Device: ____ Pad Lock ____ Type of Case Protection: Aluminum

Type of Locking Device: Pad Lock Type of Case Protection: Aluminum Concrete Surface Pad (with steel reinforcement) Dimensions: 2.0' x 2.0'



Site Name: City of Waco Landfill

County: Limestone Monitor Well I.D. No.: PZ-47

Date of Installation: 10/12/2018 Date of Development: Latitude: 31° 42' 04.15" N Longitude: 96° 55' 28.39" W

Well Driller Name and License Number West Drilling, Ricardo Garcia, License No. 54637

Method of well development: _____

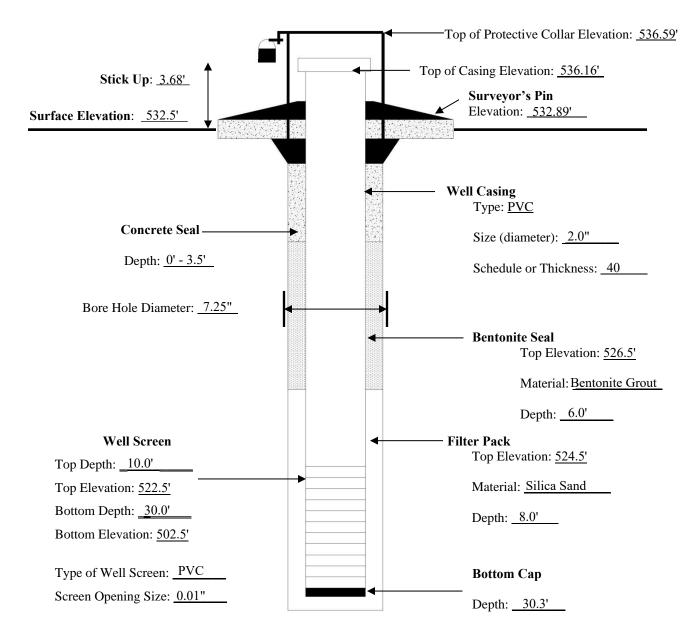
SCS Field Staff Supervising Installation: Valerie Wooters

Static Water Level after Well Development: _____

Name of Geologic Formation(s) in which Well is completed: Wolfe City Formation, Cretaceous

Type of Locking Device: Pad Lock Type of Case Protection: Aluminum

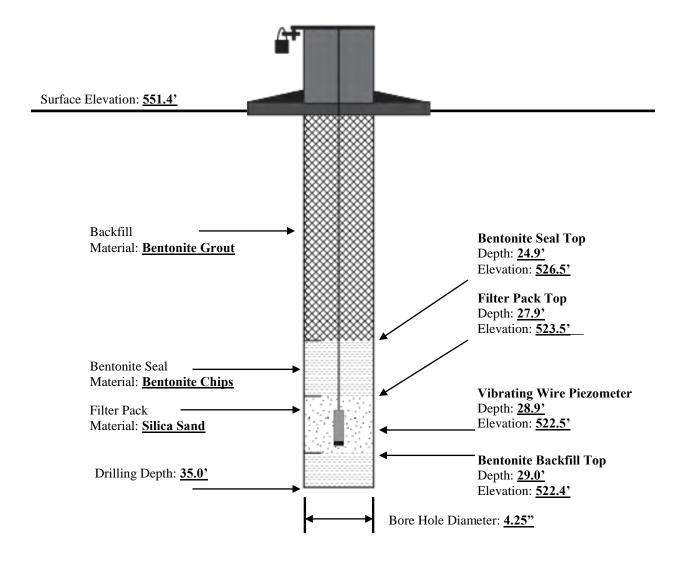
Type of Locking Device: Pad Lock Type of Case Protection: Aluminum Concrete Surface Pad (with steel reinforcement) Dimensions: 2.0' x 2.0'



APPENDIX III-4.I

VIBRATING WIRE PIEZOMETER COMPLETION DATA

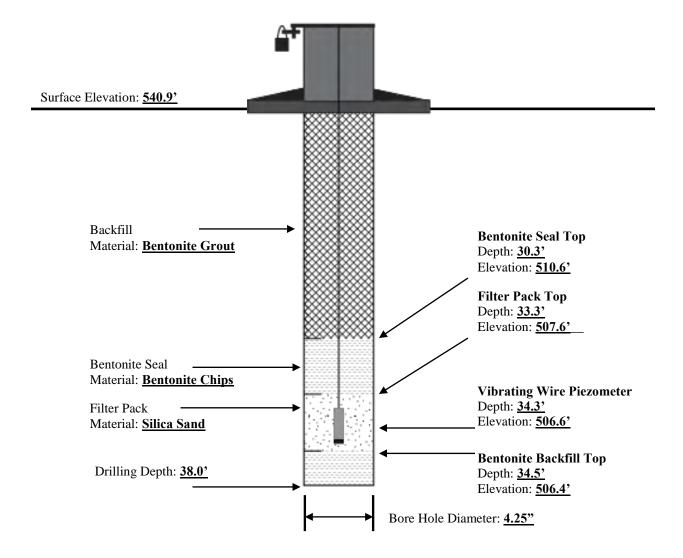




SCS ENGINEERS **WELL NUMBER B-1 (VWP-1)** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 **CLIENT** City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas **COMPLETED** 10/4/18 DATE STARTED 10/4/18 **GROUND ELEVATION** 551.7 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine **CHECKED BY** J. Lawrence AT END OF DRILLING _--- No Groundwater NOTES AFTER DRILLING 21.38 ft / Elev 530.32 ft WELL DIAGRAM GRAPHIC LOG NUMBER RECOVERY U.S.C.S. DEPTH (ft) **REMARKS** MATERIAL DESCRIPTION **VWP DIAGRAM** 0 Silty Clay, dark brown, slightly moist to moist, soft 1/ 1/1/ 2.0 549.7 (CL-ML) Silty Clay, red/orange to brown, slightly moist to moist, firm to stiff, with orange staining in joints 5 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C;USERS/PUBLIC/DOCUMENTS/BENTLEY/GINT/PROJECTS/SITE 50 WACO.GP. CL-ML 10 15 536.7 Silty Clay Shale, orange-brown mottled brown, slightly moist, stiff, non-calcareous, very weathered 20 Color change to orange-brown mottled tan to light gray and calcareous at 20 feet 25 28.0 523.7 Weathered to Silty Clay Shale, gray to dark gray, very stiff to hard, Unweathered slightly moist to dry, calcareous, unweathered zone 30 Slight orange staining in joints 30-39 feet. Revision 0 4-1-3 (Continued Next Page) May 2020

WELL NUMBER B-1 (VWP-1) PAGE 2 OF 2 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas GRAPHIC LOG NUMBER RECOVERY U.S.C.S. DEPTH (ft) **REMARKS** MATERIAL DESCRIPTION WELL DIAGRAM 35 Silty Clay Shale, gray to dark gray, very stiff to hard, slightly moist to dry, calcareous, unweathered Slight orange staining in joints 30-39 feet. (continued)

Bottom of borehole at 39.0 feet.



1901 Bedfo	Central Dord, Texas ohone: 81	rive ST 76021	E 550				WELL NUI	MBE	R B-	3 (VWP-3) PAGE 1 OF 2			
CLIE	NT City	of Wac	0				PROJECT NAME City of Waco Landfill MS	SW-240	00				
PRO	JECT NUI	MBER _	16216088.00										
DAT	E STARTE	D 10/	10/18	COMP	LETED	10/10/18	GROUND ELEVATION 541.1 ft He	OLE SI	ZE 8.25	inches			
DRIL	LING CO	NTRAC	TOR BEST Drill	ing			GROUND WATER LEVELS:						
DRIL	LING ME	THOD _	Continuous Fligh	nt Auge	r		AT TIME OF DRILLING No Groun	idwatei	ſ				
LOG	GED BY	T. Ders	stine	CHEC	KED B	J. Lawrence	AT END OF DRILLING No Ground	dwater					
NOT	ES						AFTER DRILLING No Groundwat	er					
O DEPTH	NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM	VWP DIAGRAM			
0						Blind Drill			Í				
GENERAL BH 7 P7 WELL - GINI SID US LABGOD - Z4719 15:00 - C: USERS/POBLIC/DOCOMEN SIDEN I FFYGUEL SISILE 50 WACO.GPJ - 2 P1						20.0 (SP-SC) Sa	nd, brown, soft, moist to wet, with traces of	521.1					
90 - C:UOER	-			SP- SC		clay, fine to	medium grained	518.5					
LAB.GDI - 2/4/19 15:	-			CL		(CL) Silty CI	ark brown, hard to stiff, moist ay, orange-brown mottled brown, hard, it, calcareous, with weathered shale	518.3					
Gini Sid Co	- - -					Silty Clay Sh	nale, gray with orange-brown staining, very woist, calcareous, with mineral desposits weathered	014.1					
30 30 30 30 30 30 30 30	-												
ńL	J									-VWP			
35						No mineral o	deposits 35-39 feet						

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

WELL NUMBER B-3 (VWP-3)

May 2020

PAGE 2 OF 2

CLIENT City of Waco

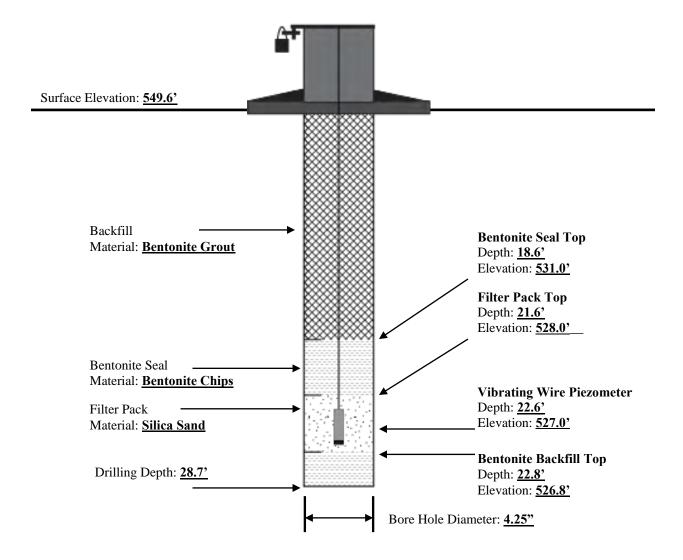
PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00

PROJECT LOCATION Waco, Texas

TESTS AND REMARKS OF DEPTH OF								
hard, slightly moist, calcareous, with mineral desposits in fractures, weathered PP = 4.5+ tsf Weathered to Unweathered zone 70 PP = 4.5+ tsf PP = 4.5+ tsf No mineral deposits 35-39 feet (continued) Silty Clay Shale, dark gray, very hard, slightly moist to dry, calcareous, unweathered		NUMBER	OVERY	AND	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	 VWP DIAGRAM
Dottom of harabala at 45 0 fact	40			Weathered to Unweathered zone	,		hard, slightly moist, calcareous, with mineral desposits in fractures, weathered No mineral deposits 35-39 feet (continued) Silty Clay Shale, dark gray, very hard, slightly moist to dry, calcareous, unweathered 45.0	

Bottom of borehole at 45.0 feet.



SCS ENGINEERS **BORING NUMBER A4 (VWP-4)** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas COMPLETED 1/23/18 DATE STARTED 1/23/18 **GROUND ELEVATION** 550.04 ft HOLE SIZE 7.25 inches **DRILLING CONTRACTOR** West Drilling **GROUND WATER LEVELS:** $\sqrt{2}$ AT TIME OF DRILLING <u>48.77 ft / Elev 501.27 ft</u> DRILLING METHOD Hollow stem auger/air rotary **AT END OF DRILLING** 96.59 ft / Elev 453.45 ft LOGGED BY T. Millbrand CHECKED BY J. Lawrence NOTES AFTER DRILLING _--- No Groundwater BLOW COUNTS (N VALUE) GRAPHIC LOG NUMBER RECOVERY DEPTH (ft) U.S.C.S. **VWP TESTS** MATERIAL DESCRIPTION Diagram (SC) Topsoil/Fill material SC 11/ Topsoil/Fill material, with dakr brown clay, soft, moist (CH) Clay, dark brown, hard, moist, calcareous 5 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C:\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ Color change to light brown at 8 feet. Pebbles 10 throughout 8-10 ft 15 Color change to mottled brown/grey at 16 feet Sand lenses throughout 18-20 feet 20 25 Clayey shale, dark grey, fissile, calcareous 30 30.0 Shale, dark grey to black, with limestone lenses, hard, calcareous Sand lenses throughout Fossil fragments throughout Revision 0 May 2020 4-1-9 (Continued Next Page)

BORING NUMBER A4 (VWP-4) 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas BLOW COUNTS (N VALUE) GRAPHIC LOG NUMBER RECOVERY U.S.C.S. DEPTH (ft) **TESTS** MATERIAL DESCRIPTION 35 Shale, dark grey to black, with limestone lenses, hard, calcareous Sand lenses throughout Fossil fragments throughout *(continued)* 40 45 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 24/19 15:50 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ ∇ 50 55 60 65 70

Revision 0

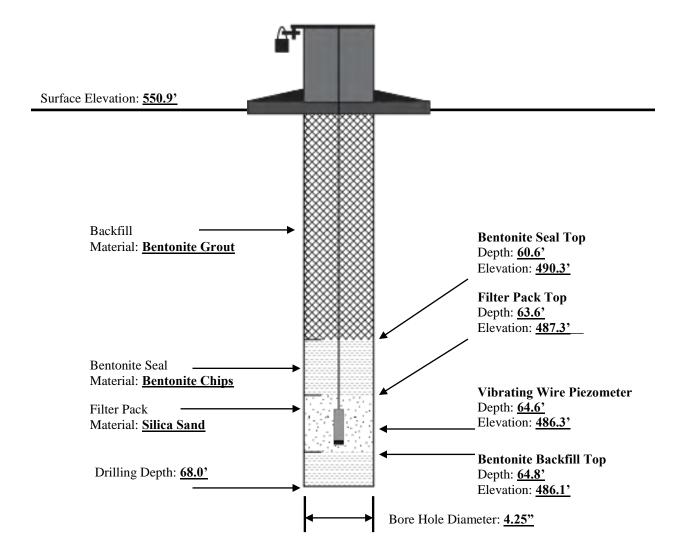
BORING NUMBER A4 (VWP-4) 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas BLOW COUNTS (N VALUE) GRAPHIC LOG NUMBER RECOVERY U.S.C.S. DEPTH (ft) **TESTS** MATERIAL DESCRIPTION 75 Shale, dark grey to black, with limestone lenses, hard, calcareous Sand lenses throughout Fossil fragments throughout *(continued)* 80 85 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C:\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 90 95 \blacksquare 100 449.0 Bottom of borehole at 101.0 feet.

4-1-11

May 2020

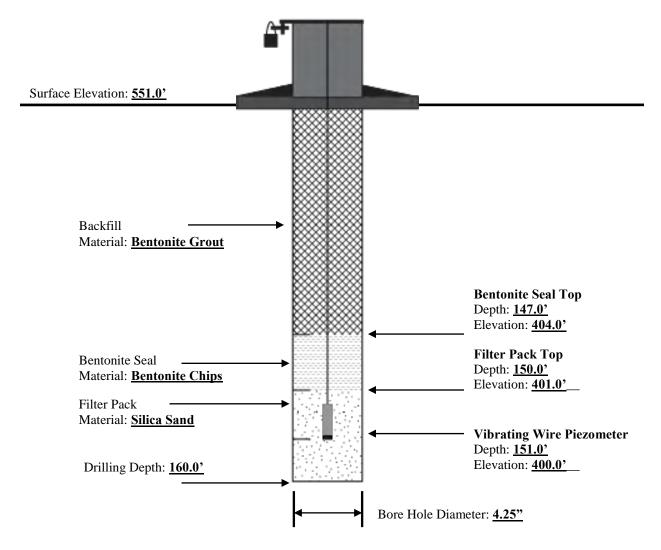
Revision 0

Site Name: Waco 2400 County: <u>Limestone</u> VWP I.D. No.: VWP-8 Date of Installation: 8/1/2019 Probe Serial No.: 1921442 Northing: _10599489.18_ 3357935.817 Easting:__ Well Driller Name and License Number West Drilling SCS Field Staff Supervising Installation: Doug Steen Static Water Level after Well Development: N/A Name of Geologic Formation(s) in which Well is completed: Wolfe City Formation Pad Lock Type of Case Protection: Aluminum Type of Locking Device:_____ Concrete Surface Pad (with steel reinforcement) Dimensions: 6'X6'

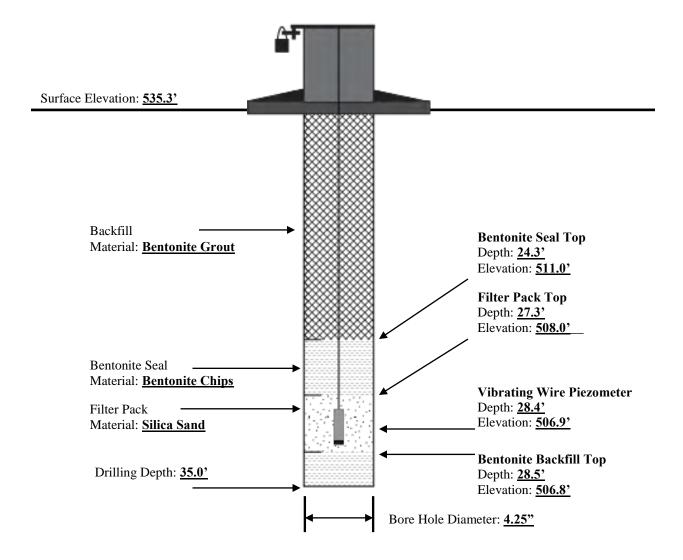


1901 (ENGII Central D rd, Texas	rive S	TE 550				WELL NUMBI	ER B-8 (VWP-8 PAGE 1 OF 2
	o, rexas none: 81							
CLIEN	IT City	of Wa	CO				PROJECT NAME City of Waco Landfill MSW-24	00
PROJ	ECT NUI	IBER	16216088	.00			PROJECT LOCATION Waco, Texas	
DATE	STARTE	D 11	1/27/18	COMPLET	ED _1	1/28/18	GROUND ELEVATION 550.34ft HOLE S	SIZE 8.25 inches
DRILL	ING CO	NTRAC	CTOR BES	ST Drilling			ft GROUND WATER LEVELS:	
DRILL	ING MET	THOD	Continuou	s Flight Auger			AT TIME OF DRILLING No Groundwate	er
LOGG	ED BY	T. Dei	rstine	CHECKED	BY J	. Lawren	ce AT END OF DRILLING No Groundwate	r
NOTE	s						AFTER DRILLING No Groundwater	
o DEPTH (ft)	NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM AMELL DIAGRAM
						7/1/2	Clayey Silt, dark brown, firm, moist, with roots and organics	
						4 4 1	(CL-ML) Silty Clay, gray to light gray, stiff to hard, moist to slightly moist, with white calcareous chalky material	
5			=				Trace of light gravel and orange-brown staining 6.5-10 feet	
	ST1	<u> </u>			CL- ML			
	SPT1							
10						1	0.0 540.8	
]] 	0.70						(CL-ML) Silty Clay, orange-brown stained gray and brown, stiff to hard, slighty moist,	
<u> </u>	ST2		_				calcareous, with white chalky material and silty gray interbeds	
- 1								
15					CL- ML			
	ST3							
	SPT2		-					
20			=			2	0.0 530.8	
	ST4						Silty Clay (Weathered Shale Marl), orange-brown mottled gray and brown, hard,	
<u>ن</u>	014		-				slighty moist, calcareous	
							White chalky material and silty gray interbeds 20-25 feet	
- 25								
5								
3	ST5							
) 	SPT3							
<u>-</u>								
30								
	ST6							
			-					
<u> </u>								
35		<u></u>					Crystalline material in joints/bedding 35-43.8 feet	
	Revision	on 0					feet 4-I-I3 (Continued Next Page)	May 2020

WELL NUMBER B-8 (VWP-8) 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 **CLIENT** City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas WELL DIAGRAM BLOW COUNTS (N VALUE) GRAPHIC LOG NUMBER RECOVERY U.S.C.S. DEPTH (ft) **TESTS** AND MATERIAL DESCRIPTION **VWP DIAGRAM REMARKS** 35 Silty Clay (Weathered Shale Marl), orange-brown mottled gray and brown, hard, ST7 slighty moist, calcareous SPT4 40 ST8 Weathered to 43.8 507.0 Unweathered Silty Clay Shale Marl, gray, hard, slightly moist, calcareous, with silty/micaceous zone 45 lenses and fossil remnants in interbeds, unweathered ST9 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C:/USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ Orange-brown staining 47-55 feet SPT5 50 ST10 55 ST11 60 -VWP 65 ST12 70 475.8 4-1-14 Bottom of borehole at 75.0 feet. Revision 0 May 2020



Site Name: Waco 2400 County: <u>Limestone</u> VWP I.D. No.: VWP-9 Date of Installation: 8/2/2019 Probe Serial No.: 1921447 Northing: 10599314.37 3355762.305 Easting:__ Well Driller Name and License Number West Drilling SCS Field Staff Supervising Installation: Doug Steen Static Water Level after Well Development: N/A Name of Geologic Formation(s) in which Well is completed: Wolfe City Formation Pad Lock Type of Case Protection: Aluminum Type of Locking Device:_____ Concrete Surface Pad (with steel reinforcement) Dimensions: 6'X6'

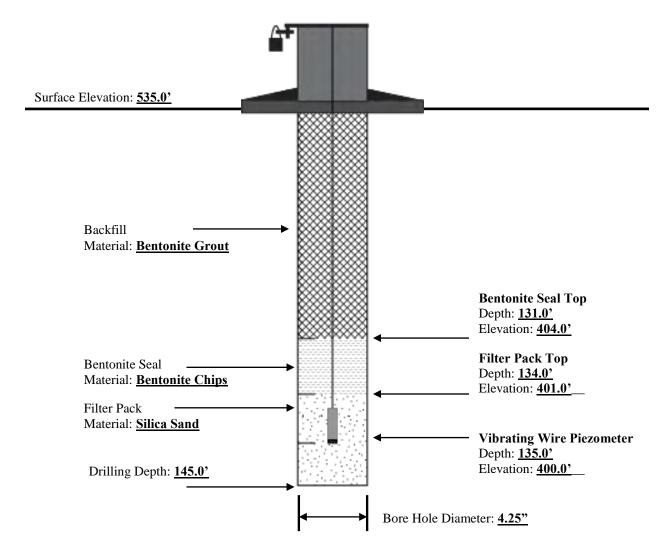


1901 Bedfo	Central Dr ord, Texas ohone: 817	ive STE 550 76021				WELL NUI	MBE	R B-	9 (VWP-9) PAGE 1 OF 2
CLIE	NT City o	f Waco				PROJECT NAME _City of Waco Landfill MS	SW-240	0	
- 1	-	IBER _16216088.00							
- 1		D 10/9/18							
- 1		TRACTOR BEST Dr							
		HOD Continuous Flig					ev 510.0)5 ft	
		T. Derstine							
						AFTER DRILLING			
DEPTH (ft)	NUMBER	% XY TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM	VWP DIAGRAM
0 	-		CL- ML		moist to mo and shells Color chang	ty Clay, dark brown to gray, stiff, slightly ist, organic rich, with limestone fragments ge to gray at 2.5 feet	530.2		
: 50 WACO.GPJ	- ST1		CL- ML		(CL-ML) Sili hard, slightl	ty Clay, light gray/tan mottled orange-brown, y moist, with minor sub-round gravel			
BENTLEYGINTPROJECTS\STE 50 WACO.GPJ	ST2				Silty Clay S yellow-brow with trace o	hale, gray and orange-brown mottled n, hard, slightly moist to dry, calcareous, f gravel	525.2		
OCUMENTS/BENTLEY/GI	- - ST3				Chalk/limes	stone in joints 15-20 feet			
C:\USERS\PUBLIC\DC	- - - - ST4					ge to orange-brown mottled gray at 20 feet enses in fractures 25-28.5 feet			
- 2/4/19 15:50 - 2/2/20 - 2/2/	-				<u>Ā</u>				
GINT STD US LAB.	ST5	Weathered to Unweathered zone				hale, very hard, dry, calcareous, with	506.7		-vwp
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:50 - C:USERSIPUBLIC/DOCUMENTS) 2	ST6					ich lenses in fractures wn staining in joints 28.5-30 feet			
GENERA - 35	Revisio	on 0			4-1	-17 (Continued Next Page)		May 2	2020

- 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME City of Waco Landfill MSW-2400

PROJ	ECT NUN	/IBER	16216088.00			PROJECT LOCATION Waco, Texas	PROJECT LOCATION Waco, Texas				
S DEPTH (ft)	NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION		WELL DIAGRAM	VWP DIAGRAM		
 40	ST7					Silty Clay Shale, very hard, dry, calcareous, with carbonate rich lenses in fractures	495.2				

Bottom of borehole at 40.0 feet.



SCHOOL SUPPLY STATES ST		ENGINI Enginee							WELL NUM	IBEF	R B-9	(VWP-9D)
Bedford, TX 76021 CUENT City of Wago PROJECT NAME City of Wago Landfill MSW-2400 PROJECT NAME City of Wago Landfill MSW-2400 PROJECT NAME City of Wago Landfill MSW-2400 PROJECT LOCATION Wago, Texas ONTESTATED 108/18 COMPLETED 12/13/19 DRILLING ONTRACTOR BEST Drilling: West Drilling UNITED MORNING STATES TO STATE COMPLETED 12/13/19 DRILLING METHOD Continuous Fight Auger LOGGED BY T Dersiline; A Boudreaux CHECKED BY J Lawrence NOTES ### Project Location Wago, Texas GROUND WATER LEVELS: VAIT TIME OF DRILLING 25.10 R / Elev 510.20 D. R. AT END OF DRILLING A TIME OF DRILLING A TEXAS OF DRILLING A TEXA	1901	Central										PAGE 1 OF 4
CLEMING CONTRACTOR BEST Drilling, West Drilling DRILLING CONTRACTOR BEST Drilling, West Drilling, Wes			6021									
DATE STARTED 109/18 COMPLETED 12/13/19 GROUND BETANTION 53.5 ft HOLE SIZE 8.25 inches DRILLING METHOD. Continuous Flight Auger DRILLING METHOD. Continuous Flight Auger LOGGED BY T. Deretine: A. Boudreaux CHECKED BY J. Lawrence NOTES AT TIME OF DRILLING				0					PROJECT NAME City of Waco Landfill M	SW-24	00	
DRILLING METHOD Continuous Flight Auger LOGGED 97 T. Derstine: A. Boudreaux CHECKED BY J. Lawrence NOTES ### AT TIME OF DRILLING 25.10 ft / Flev 510.20 ft AT END OF DRILLING ### AT TIME OF DRILLING AT FIND OF D	PRO	JECT NUN	/IBER	16216088.00					PROJECT LOCATION Waco, Texas			
DRILLING METHOD Continuous Flight Auger Destine, A. Boudreaux CHECKED BY J. Lawrence NOTES TESTS AND FREMARKS TESTS AND FR										HOLE S	IZE 8.25	inches
LOGGED BY T Dereitines: A Bouldreaux CHECKED BY J. Lawrence AT END OF DRILLING AFTER DRILLING WWP DIAGRAM WWP DIAGRAM O ST 1 CL. Mil. Silly Clay, light graytan mottled orange-brown mottled orange-brown hard, elightly moist, with minor sub-round grave at 2.5 feet Color change to gray at 2.5 feet Color change to gray at 2.5 feet Silly Clay Shale, gray and orange-brown mottled gray at 20 feet Chalk/limestone in joints 15-20 feet Color change to orange-brown mottled gray at 20 feet Limestone lenses in fractures 25-28.5 feet ST 3 ST 3 Weathered to Unweathered 2 Silly Clay Shale, very hard, dry, calcareous, with carbonate ich kinese in fractures 25-28.5 feet Silly Clay Shale, very hard, dry, calcareous, with carbonate ich kinese in fractures 25-28.5 feet Orange-brown staining in joints 28.5-20 feet Orange-brown staining in joints 28.5-20 feet	DRILL	ING CON	TRAC	TOR BEST Drillin	g; We	st Drill	ing		GROUND WATER LEVELS:			
NOTES AFTER DRILLING — AFTER DRILLING — Westbered to Universities of State of Sta	DRILI	LING MET	HOD	Continuous Flight	Auge	r			$\sqrt{2}$ AT TIME OF DRILLING 25.10 ft / E	lev 510	.20 ft	
TESTS AND COMMENTARY SET AND COM	LOGO	SED BY	T. Der	stine; A. Boudreau	× CH	ECKE	DBY J	. Lawrence	AT END OF DRILLING			
CL-ML Sitry Clay, dark brown to gray, stiff, slightly moist to most, organic rich, with limestone fragments and shells Color change to gray at 2.5 feet 5.0 ST1 CL-ML Sitry Clay, light gray/tan mottled orange-brown, hard, slightly moist, with minor sub-round gravel 5.0 Sitry Clay Shale, gray and orange-brown mottled yellow-brown, hard, slightly moist to dry, calcareous, with race of gravei Chalk/limestone in joints 15-20 feet Color change to orange-brown mottled gray at 20 feet Limestone lenses in fractures 25-28.5 feet ST3 Weathered to Unweathered 20. ST6 ST6 ST7 ST6 C-ALL Sitry Clay, light gray/tan mottled orange-brown, mottled gray at 20 feet Color change to orange-brown mottled gray at 20 feet Limestone lenses in fractures 25-28.5 feet ST6 ST7 ST7 Orange-brown staining in joints 28.5-20 feet	NOTE	ES							AFTER DRILLING			
CL ML ST1 CL ML ST2 ST2 Meathered to Unweathered zone ST4 ST6 ST6 Meathered to Unweathered to Carbonate rich lenses in fractures 25-28.5 feet ST6 ST6 ME ST6 ST6 ST6 ST6 ST6 ST6 ST6 ST		SAMPLE TYPE NUMBER		AND	U.S.C.S.	GRAPHIC LOG					WELL DIAGRAM	VWP DIAGRAM
ST1 CL-ML 10 10.0 Sity Clay, light gray/tan mottled orange-brown, hard, slightly moist, with minor sub-round gravel 525.3 yellow-brown, hard, slightly moist to dry, calcareous, with trace of gravel Chalk/limestone in joints 15-20 feet Color change to orange-brown mottled gray at 20 feet Limestone lenses in fractures 25-28.5 feet ST3 ST4 ST5 Weathered to Unweathered zone ST8 ST8 ST8 ST8 ST8 ST8 ST8 ST		-						moist to mois and shells	st, organic rich, with limestone fragments			
ST1 CL-ML) Slity Clay, light gray/tan mottled orange-brown, hard, slightly moist, with minor sub-round gravel 10 10.0 Sity Clay Shale, gray and orange-brown mottled yellow-brown, hard, slightly moist to dry, calcareous, with trace of gravel Chalk/limestone in joints 15-20 feet Color change to orange-brown mottled gray at 20 feet Limestone lenses in fractures 25-28.5 feet ST3 ST4 ST5 Weathered to Unweathered 2 28.5 Sity Clay Shale, very hard, dry, calcareous, with carbonate rich lenses in fractures Orange-brown staining in joints 28.5-20 feet Orange-brown staining in joints 28.5-20 feet	-	-			ML			Color change	to gray at 2.5 feet			
ST1 CL-ML) Slity Clay, lightly moist, with minor sub-round gravel 10 10.0 Sity Clay Shale, gray and orange-brown mottled yellow-brown, hard, slightly moist to dry, calcareous, with trace of gravel Chalk/limestone in joints 15-20 feet Color change to orange-brown mottled gray at 20 feet Limestone lenses in fractures 25-28.5 feet ST3 ST4 ST5 Weathered to Unweathered 2 28.5 Sity Clay Shale, very hard, dry, calcareous, with carbonate rich lenses in fractures Orange-brown stairing in joints 28.5-20 feet Orange-brown stairing in joints 28.5-20 feet	十 _ ·	-								=00.0		
Sitty Clay Shale, gray and orange-brown mottled yellow-brown, hard, slightly moist to dry, calcareous, with trace of gravel Chalk/limestone in joints 15-20 feet Color change to orange-brown mottled gray at 20 feet Limestone lenses in fractures 25-28.5 feet ST3 ST4 Weathered to Unweathered zone Weathered to Unweathered zone Orange-brown staining in joints 28.5-20 feet Orange-brown staining in joints 28.5-20 feet	_ 5	ST1						(CL-ML) Silty hard, slightly	Clay, light gray/tan mottled orange-brown, moist, with minor sub-round gravel	530.3		
Sity Clay Shale, gray and orange-brown mottled yellow-brown, hard, slightly moist to dry, calcareous, with trace of gravel Chalk/limestone in joints 15-20 feet Color change to orange-brown mottled gray at 20 feet Limestone lenses in fractures 25-28.5 feet ST3 Weathered to Unweathered zone Weathered to Unweathered zone Orange-brown staining in joints 28.5-20 feet	'	311										
ST2 ST2 ST3 ST3 ST3 ST4 ST5 ST5 ST5 ST6 ST6 SSIty Clay Shale, very hard, dry, calcareous, with carbonate rich lenses in fractures Orange-brown staining in joints 28.5-20 feet SST6 SST7 SST6 SST7 SST6 SST7 SST8 SST8]			IVIL							
yellow-brown, hard, slightly moist to dry, calcareous, with trace of gravel Chalk/limestone in joints 15-20 feet Color change to orange-brown mottled gray at 20 feet Limestone lenses in fractures 25-28.5 feet ST3 ST4 ST5 ST5 Weathered to Unweathered zone ST6 Orange-brown staining in joints 28.5-20 feet Orange-brown staining in joints 28.5-20 feet	10]					10.0			525.3		
Limestone lenses in fractures 25-28.5 feet ST3 Limestone lenses in fractures 25-28.5 feet ST4 ST5 Weathered to Unweathered zone Silty Clay Shale, very hard, dry, calcareous, with carbonate rich lenses in fractures Orange-brown staining in joints 28.5-20 feet	ACO.GPJ	ST2						yellow-brown	, hard, slightly moist to dry, calcareous,			
Limestone lenses in fractures 25-28.5 feet ST3 Limestone lenses in fractures 25-28.5 feet ST4 ST5 Weathered to Unweathered zone Silty Clay Shale, very hard, dry, calcareous, with carbonate rich lenses in fractures Orange-brown staining in joints 28.5-20 feet	NSITE 50 W							Chalk/limesto	one in joints 15-20 feet			
Davision () May 2020	15							Color change	to orange-brown mottled gray at 20 feet			
Davisian A 100	SINT/PRO.	ST3						Limestone le	nses in fractures 25-28.5 feet			
Davisian A 100	SENTLEY(-										
Davisian A 100	置 20											
Davisian A 100		-										
Davisian A 100		S14										
Davisian A 100	- - - -	1										
Davisian A 100	25	1										
Davisian A 100	100						¥					
Davisian A 100	LAB.											
Davisian A 100	50 C			Marthur								
Davisian A 100	INT ST							Silty Clav Sha	ale, very hard, dry, calcareous, with	506.8		
Devision 0 May 2020	<u>0</u> 30			zone								
Devision 0 May 2020	ME .							Orange-brow	n staining in joints 28.5-20 feet			
Devision 0 May 2020	<u>}</u> .	ST6										
Devision 0 May 2020	<u>.</u>											
Devision 0 May 2020	¥ 											
TO VIGIOUS TO THE TOTAL TOTAL TO THE TOTAL T	B <u>35</u>	Revision	n O					4-1-	20 (2)		May 20	120

SCS ENGINEERS WELL NUMBER B-9 (VWP-9D) SCS Engineers 1901 Central Dr Ste. 550 Bedford, TX 76021 CLIENT City of Waco PROJECT NAME _City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas SAMPLE TYPE NUMBER WELL DIAGRAM GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS VWP DIAGRAM** AND MATERIAL DESCRIPTION **REMARKS** 35 Silty Clay Shale, very hard, dry, calcareous, with carbonate rich lenses in fractures ST7 40 40.0 495.3 40-45' no sample recovery 45 45.0 490.3 Shale with minor, very fine sand. Dark gray, hard to very hard, damp to moist, well laminated 50 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/5/20 11:23 - L:\VALERIE\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 55 60 Shale with minor, very fine sand. Dark gray, hard to very hard, damp to moist, laminated 65 70

4-1-21 (Continued Next Page)

Revision 0

May 2020

SCS ENGINEERS

SCS Engineers 1901 Central Dr Ste. 550 Bedford, TX 76021

WELL NUMBER B-9 (VWP-9D) PAGE 3 OF 4

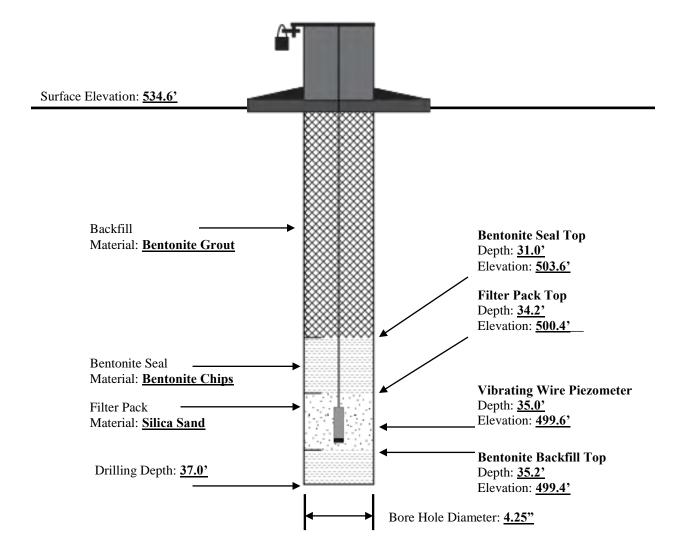
CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

	CT NUM		16216088.00			PROJECT LOCATION Waco, Texas	PROJECT LOCATION Waco, Texas				
DEPTH (#)	SAMPLE TYPE NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM	VWP DIAGRAM			
						75-80' small fossils present					
						Becoming harder with depth					
85											
90						Fewer laminations with depth					
95											
				_							
 105											
. –											
						Shale with minor, very fine sand. Dark gray, very hard, moist, trace lamination					
115	Revisio	n O				4-1-22 (Continued Next Page)	May 2				

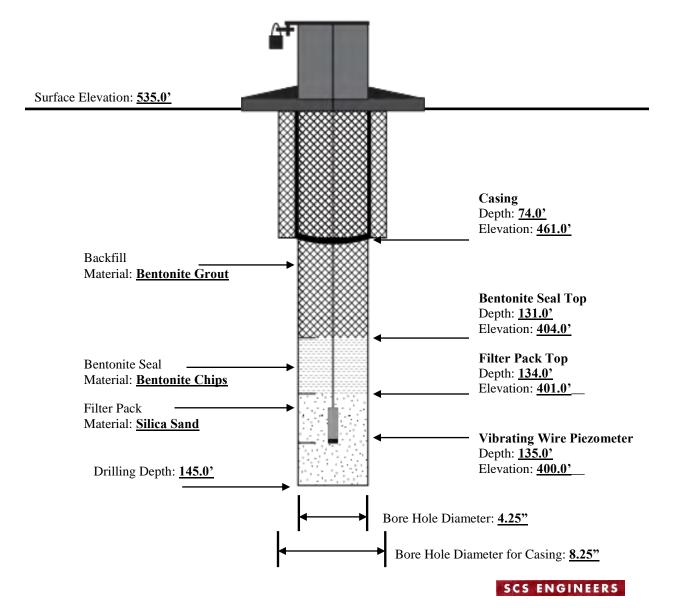
SCS ENGINEERS WELL NUMBER B-9 (VWP-9D) SCS Engineers 1901 Central Dr Ste. 550 Bedford, TX 76021 CLIENT City of Waco PROJECT NAME _City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas SAMPLE TYPE NUMBER WELL DIAGRAM GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS** AND MATERIAL DESCRIPTION **VWP DIAGRAM REMARKS** 115 120 Becoming harder with depth 125 Fewer laminations with depth 130 Shale with minor, very fine sand. Dark gray, very hard, GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/5/20 11:23 - L:\VALER!E\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ moist, scarce lamination 135 400.3 -VWP Bottom of borehole at 135.0 feet.

Site Name: Waco 2400 County: <u>Limestone</u> VWP I.D. No.: VWP-18 Date of Installation: 7/25/2019 Probe Serial No.: 1921452 Northing: __10601254.04__ 3356694.758 Easting: Well Driller Name and License Number West Drilling SCS Field Staff Supervising Installation: Doug Steen Static Water Level after Well Development: N/A Name of Geologic Formation(s) in which Well is completed: Wolfe City Formation Pad Lock Type of Case Protection: Aluminum Type of Locking Device:_____ Concrete Surface Pad (with steel reinforcement) Dimensions: 6'X6'

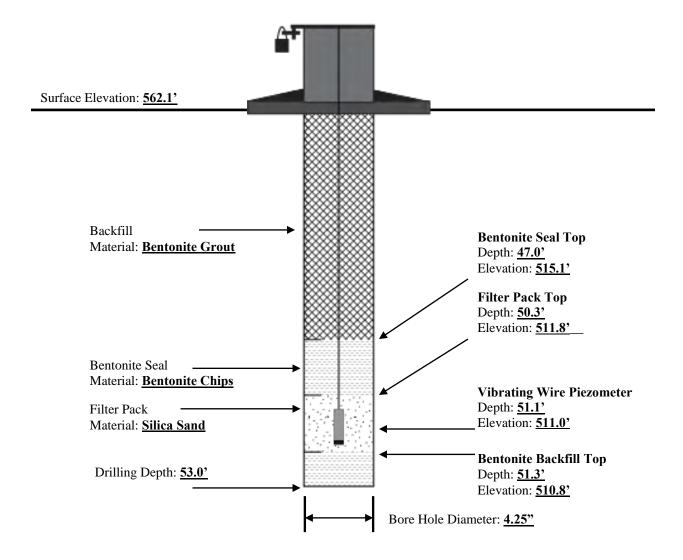


1901	Central D	rive S7	ΓE 550				WELL NUM	IBER	B-18	(VWP-18) PAGE 1 OF 2
	rd, Texas hone: 81									
CLIEN	NT City	of Wad	0				PROJECT NAME City of Waco Landfill	MSW-24	00	
1	_									
1							GROUND ELEVATION 534.75 ft	HOLE S	I ZE 8.25	inches
DRILI	LING CO	NTRAC	TOR BEST Drill	ling			GROUND WATER LEVELS:			
DRILI	LING ME	THOD	Continuous Fligh	nt Auge	r		AT TIME OF DRILLING No Gro	oundwate	er	
LOGG	GED BY	T. Der	stine	CHEC	KED B	Y J. Lawrence	AT END OF DRILLING No Gro	undwate	r	
NOTE	ES						AFTER DRILLING No Grounds	vater		
O DEPTH (ft)	NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM	VWP Diagram
	-			CL- ML		(CL-ML) Sili moist, orgai	ty Clay Topsoil, dark brown, soft to firm, nic			
5	-			CL- ML		2.7 (CL-ML) Silt of small to r	ty Clay, brown, firm to stiff, moist, with trace nedium gravel and chalk in fractures/joints	532.1 es		
; 	ST ²	1					ty Clay, orange-brown mottled gray, hard,	528.0		
]					slightly mois	st, calcareous			
10				CL-		Silty lenses	in bedding 10-14.5 feet			
-	OT/			ML						
-	ST2	2								
15			Weathered to Unweathered			14.5 Silty Shale	gray, hard, slightly moist, calcareous,	520.3		
			\zone	1		unweathere				
20	ST	3					ge-brown staining 14.5-30 feet			
-	-					Trace of sho	ells 30-56 feet			
20	-									
1 20										
	ST4	4								
- - 										
-										
25				_						
	ST	5								
-										
30										
						Silty lenses	in bedding 30-35 feet			
-						S.1., 1011003				
- -										
	-									-VWP
35	Revisi	on 0				4-1	-25 (Continued Next Page)		May 2	

WELL NUMBER B-18 (VWP-18)
PAGE 2 OF 2 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas WELL DIAGRAM GRAPHIC LOG NUMBER RECOVERY U.S.C.S. DEPTH (ft) **TESTS** AND REMARKS MATERIAL DESCRIPTION **VWP** Diagram 35 Silty Shale, gray, hard, slightly moist, calcareous, unweathered ST6 40 45 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 24/19 15:51 - C.\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ ST7 50 55 478.8 Bottom of borehole at 56.0 feet.



M:\Projects\Waco\16216088.00 New LF\Site 50\Site 50 Phase II DDD, Well Completion, Field Logs, drilling started Oct 4 2018\Files for Permit Figures



SCS ENGINEERS

M:\Projects\Waco\16216088.00 New LF\Site 50\Site 50 Phase II DDD, Well Completion, Field Logs, drilling started Oct 4 2018\Files for Permit Figures

SCS ENGINEERS **BORING NUMBER B-19 (VWP-19)** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas **COMPLETED** 10/30/18 DATE STARTED 10/30/18 **GROUND ELEVATION** 562.05 ft HOLE SIZE 7.25 inches **DRILLING CONTRACTOR** West Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY V. Wooters CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater GRAPHIC LOG RECOVERY NUMBER U.S.C.S. DEPTH (ft) **TESTS VWP** AND MATERIAL DESCRIPTION Diagram **REMARKS** 0 (CL-ML) Silty Clay, dark brown, soft, moist, calcareous CL-ML (CL-ML) Silty Clay, gray/tan mottled orange, hard, slightly moist, calcareous 5 Chalk in fractures/joints 4-20 feet ST1 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C:\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 10 ST2 15 Very weathered zones 15-20 feet ST3 CL-ML ST4 25 ST5 30 ST6 May 2020 Revision 0 4-1-29 (Continued Next Page)

BORING NUMBER B-19 (VWP-19) 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 **CLIENT** City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas GRAPHIC LOG NUMBER RECOVERY U.S.C.S. DEPTH (ft) **TESTS** VWP AND MATERIAL DESCRIPTION Diagram **REMARKS** 35 (CL-ML) Silty Clay, gray/tan mottled orange, hard, slightly moist, calcareous ST7 CL-ML 40 (CL) Clay, dark gray with orange to tan mottling, dry, hard, calcareous, with soft weathered shale zones ST8 CL 45 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C:\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 49.0 513.1 Silty Clay Shale, dark gray, hard, dry, calcareous, with chalk in 50 joints/fractures, weathered ST9 509. Weathered to Silty Clay Shale, dark gray, hard, dry, calcareous, unweathered Unweathered zone Chalk in fractures/joints 53-65 feet 55 Intermittent weathered zones from 50-87 feet 60 ST10 65 70 ST11 May 2020 Revision 0

4-1-30

(Continued Next Page)

BORING NUMBER B-19 1901 Central Drive STE 550 PAGE 3 OF 3 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas GRAPHIC LOG NUMBER RECOVERY U.S.C.S. DEPTH (ft) **TESTS** AND REMARKS MATERIAL DESCRIPTION 75 Silty Clay Shale, dark gray, hard, dry, calcareous, unweathered Chalk in fractures/joints 53-65 feet Intermittent weathered zones from 50-87 feet (continued)

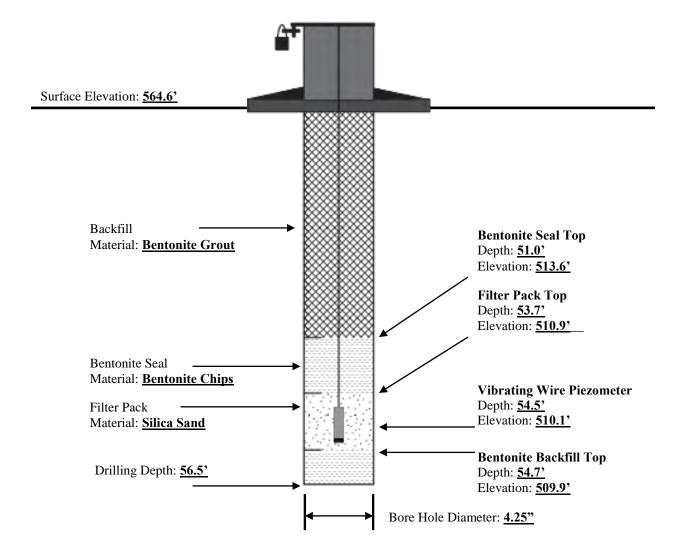
Bottom of borehole at 87.0 feet.

475.1

80

85

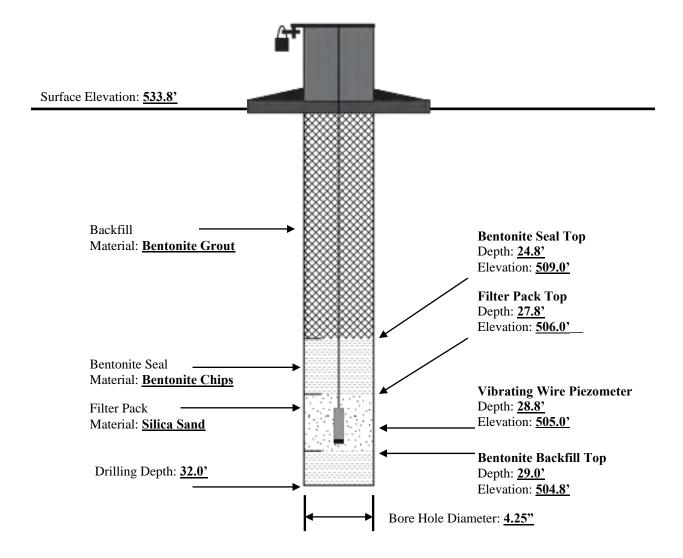
ST12



	ENGI Central D						WELL NUM	1BER	B-20	(VWP-20)
Bedfor	rd, Texas	7602	1							PAGE 1 OF 2
	IT City						PROJECT NAME _City of Waco Landfill	MSW 240	00	
1			_16216088.00					101000-240	<i>.</i>	
				COMP	LETE		GROUND ELEVATION 564.1 ft	HOLE SI	ZE 7.25	inches
1			CTOR West Drill							
DRILL	ING ME	THOD	Continuous Flig	ht Auge	r		AT TIME OF DRILLING No Gro	oundwate	r	
LOGG	ED BY	V. Wo	ooters	CHEC	KED E	J. Lawrence	AT END OF DRILLING No Gro	undwater		
NOTE	s						AFTER DRILLING 7.90 ft / Elev 5	56.20 ft		
o DEPTH (ft)	NUMBER	RECOVERY %	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM	VWP DIAGRAN
				CL- ML		<1/8" pebb	lty Clay, gray mottled tan, hard, dry, with les and chalk in fractures/joints, calcareous			
5						5.0 (CL-ML) Si	Ity Clay, tan/gray mottled orange, hard, dry,	559.1		
	ST1					calcareous				
	311	-				√ <1/8" pebb	les 5-10 feet			
						Chalk in joi	nts/fractures 5-10 feet			
10										
2 _		-								
	ST2	2								
<u>-</u> 		1								
<u>-</u> 										
15						Very uncor	nsolidated/weathered 15-35 feet			
- -										
	ST3	3								
		1								
20_				CL- ML						
J										
-	ST4									
<u>-</u>										
25						Minoral do	posits 24-25 feet			
<u> </u>						Milleral de	JUSIUS 24-23 1661			
<u>-</u>	ST5									
3 -	313	<u>'</u>								
- -										
30										
=	ST6	6								
		-								
<u> </u>										
35	Dovisi	00.0				35.0	1 23	529.1	Maxia	
	Revision	UIIU				4-	I-33 (Continued Next Page)		May 2	020

WELL NUMBER B-20 (VWP-20) 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 **CLIENT** City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas WELL DIAGRAM GRAPHIC LOG NUMBER RECOVERY U.S.C.S. DEPTH (ft) **TESTS** AND MATERIAL DESCRIPTION **VWP DIAGRAM REMARKS** 35 (CL) Clay, dark gray with orange/tan mottling, hard, dry, calcareous, with weathered shale ST7 Mineral deposits in fractures 25-35 feet CL 40 ST8 43.0 521.1 Silty Clay Shale, dark gray, hard, dry, calcareous, weathered 45 Weathered to GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C:\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ ST9 47.0 517.1 Unweathered Silty Clay Shale, dark gray, hard, dry, calcareous, zone unweathered Orange-brown oxidation staining 50-55 feet 50 Chalk/limestone in fractures 50-55 feet 55 No oxidation staining beginning at 57.5 feet ST10 65 ST11 70 491.1 Bottom of borehole at 73.0 feet.

Site Name: Waco 2400 VWP I.D. No.: <u>VWP-25</u> County: <u>Limestone</u> Date of Installation: 8/2/2019 Probe Serial No.: 1921450 Northing: _10599102.9_ Easting:___ 3356251.06 Well Driller Name and License Number __West Drilling SCS Field Staff Supervising Installation: Doug Steen Static Water Level after Well Development: N/A Name of Geologic Formation(s) in which Well is completed: Wolfe City Formation Type of Case Protection: Aluminum Type of Locking Device:_____ Pad Lock Concrete Surface Pad (with steel reinforcement) Dimensions: 6'X6'



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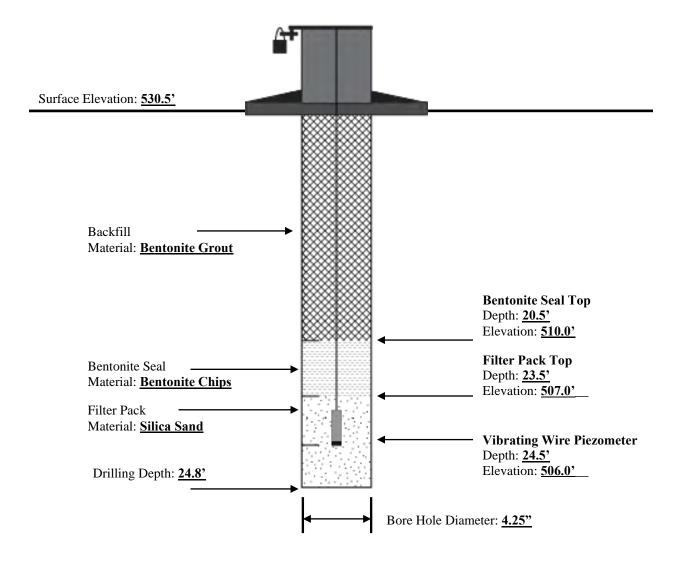
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C:USERS/PUBLIC/DOCUMENTS/BENTLEY/GINT/PROJECTS/SITE 50 WACO.GP J

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

BORING NUMBER B-25 (VWP-25)

PAGE 1 OF

Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas **COMPLETED** 10/11/18 DATE STARTED 10/11/18 **GROUND ELEVATION** 533.25 ft HOLE SIZE 7.25 inches **DRILLING CONTRACTOR** West Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY V. Wooters CHECKED BY J. Lawrence AT END OF DRILLING _-- No Groundwater NOTES AFTER DRILLING _--- No Groundwater GRAPHIC LOG NUMBER RECOVERY U.S.C.S. DEPTH (ft) **TESTS** AND MATERIAL DESCRIPTION **VWP** REMARKS Diagram 0 (CL-ML) Silty Clay, dark gray, soft to hard, slightly moist to dry, calcareous, with chalk in joints CL-Color change to light gray 4-5 feet ML 5 528.3 (CL-ML) Silty Clay, orange/gray/tan mottled, hard, slightly moist to dry, calcareous, with chalk in joints and sub-rounded pebbles 1/8" ST₁ 10 ST2 CL-ML 15 No pebbles 15-20 feet ST3 Silty Sand lenses in fractures 15-23 feet 20 ST4 510.3 (CL) Shaley Clay, dark gray, medium hard to soft, dry, calcareous, CL weathered 25 25.0 508.3 Silty Clay Shale, dark gray, hard, dry, calcareous, unweathered Intermittent weathered zones 25-33 feet ST5 Weathered to Unweathered zone 30 ST6 500.3 Bottom of borehole at 33.0 feet.



SCS ENGINEERS **BORING NUMBER B-26 (VWP-26)** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 11/18/18 **COMPLETED** 11/18/18 **GROUND ELEVATION** 530.45 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Millbrand CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater NOTES AFTER DRILLING _--- No Groundwater BLOW COUNTS (N VALUE) GRAPHIC LOG NUMBER RECOVERY DEPTH (ft) U.S.C.S. **TESTS** AND MATERIAL DESCRIPTION **VWP REMARKS** Diagram 0 Top Soil, black, soft, moist, with roots and small gravel 529 (CL-ML) Silty Clay, llight brown, hard, slightly moist, with small round to CLsub-rounded gravel up to 1/4", slightly calcareous ML 5 5.0 525.5 (CL-ML) Silty Clay, tan to light brown mottled orange and gray, very hard, dry, slightly calcareous ST1 SPT 10 CL Orange staining 10-15 feet ML ST2 15 15.0 515.5 (CL-ML) Silty Clay, tan/brown with orange staining, hard to very hard, calcareous ST3 CL-SPT2 ML Color change to dark gray at 20 feet 20 20.0 (CL-ML) Silty Clay, dark gray to gray with orange staining, very soft to very hard, dry, slightly to moderately calcareous ST4 Transition zone into weathered shale CL-ML 25 Weathered to 504.5 Unweathered Clay (Shale), dark gray, very soft to very hard, dry, zone with fossil remnants, slightly calcareous, unweathered SPT3 Trace of orange staining 25-30 feet 30 ST6

GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C:USERS/PUBLIC/DOCUMENTS/BENTLEY/GINT/PROJECTS/SITE 50 WACO.GP J

Revision 0

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BORING NUMBER B-26 (VWP-26)

PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

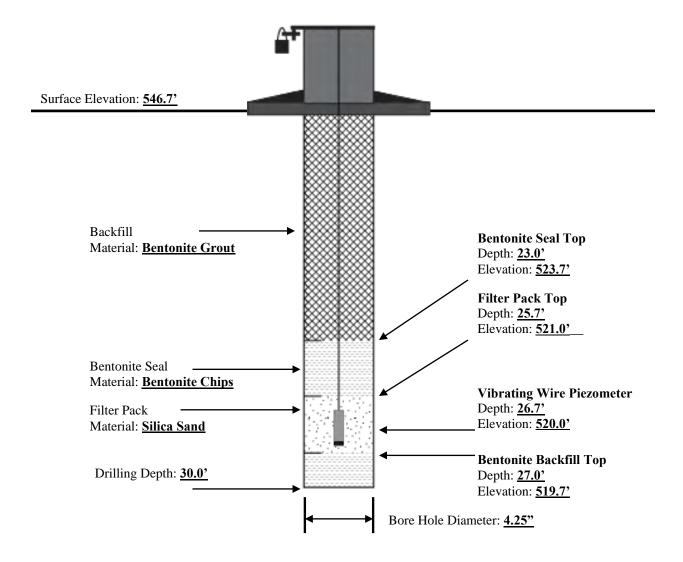
CLIENT City of Waco PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00 PROJECT LOCATION Waco, Texas

35 DEPTH (ft)	NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
							36.0 494.5

Bottom of borehole at 36.0 feet.

Site Name: Waco 2400 VWP I.D. No.: _VWP-27_ County: <u>Limestone</u> Date of Installation: 7/26/2019 Probe Serial No.: 1921446 Northing: 10600427.7 Easting:___ 3358308.89 Well Driller Name and License Number __West Drilling SCS Field Staff Supervising Installation: Doug Steen Static Water Level after Well Development: N/A Name of Geologic Formation(s) in which Well is completed: Wolfe City Formation Type of Case Protection: Aluminum Type of Locking Device:_____ Pad Lock Concrete Surface Pad (with steel reinforcement) Dimensions: 6'X6'



SCS ENGINEERS **BORING NUMBER B-27 (VWP-27)** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 **CLIENT** City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas DATE STARTED 11/14/18 **COMPLETED** 11/14/18 **GROUND ELEVATION** 546.65 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater NOTES AFTER DRILLING _--- No Groundwater BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY NUMBER DEPTH (ft) U.S.C.S. **TESTS** VWP AND MATERIAL DESCRIPTION **REMARKS** Diagram 0 (MH) Clayey Silt, dark brown, soft to firm, very moist, organic MH (MH) Clayey Silt, brown, stiff to hard, moist to slightly moist, with white chalk and fossil fragments, calcareous 5 MH ST1 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C:\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 10 536.7 (CL-ML) Silty Clay, orange-brown mottled brown and gray, hard, slightly moist, calcareous CL-SPT ML 15 15.0 531.7 Silty Shale, orange-brown mottled brown and light gray, hard, slightly moist, calcareous, weathered ST3 White crystalline lenses in interbeds 17.7-21.4 feet 20 ST4 SPT3 Orange-brown and crystalline in interbeds 25-29 feet 25 SPT4 Weathered to 517.7 29.0 Unweathered Silty Shale, gray, hard, slightly moist, calcareous, micaceous, 30 Orange-brown staining in joints/bedding 29-40 feet SS5 Occasional fossil fragments 33-38 feet ST6 Fossil fragments 40.8-53 feet Revision 0 May 2020 4-1-41 (Continued Next Page)

BORING NUMBER B-27 (VWP-27) PAGE 2 OF 2

1901 Central Drive STE 550 Bedford, Texas 76021

Telephone: 817-571-2288

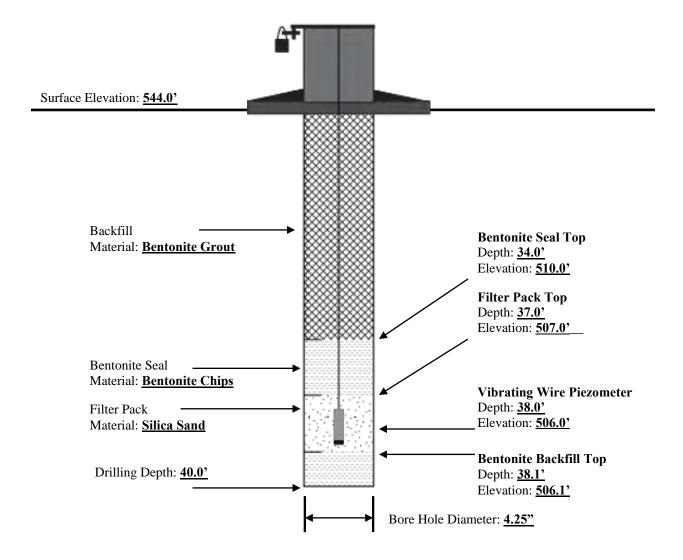
CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00 PROJECT LOCATION Waco, Texas

1 103	LCT NON	IDLIX	102 10000	.00			FROJECT LOCATION _Waco, Texas			
HT GEPTH (#) 35	NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION			
40 45	ST7 SPT6 ST8						Silty Shale, gray, hard, slightly moist, calcareous, micaceous, unweathered Orange-brown staining in joints/bedding 29-40 feet Occasional fossil fragments 33-38 feet Fossil fragments 40.8-53 feet (continued)			
2	Bottom of borehole at 53.0 feet.									

Site Name: Waco 2400 VWP I.D. No.: VWP-30 County: <u>Limestone</u> Date of Installation: 7/26/2019 Probe Serial No.: 1921451 Northing: _10598886.4_ Easting:___ 3357828.13 Well Driller Name and License Number __West Drilling SCS Field Staff Supervising Installation: Doug Steen Static Water Level after Well Development: N/A Name of Geologic Formation(s) in which Well is completed: Wolfe City Formation Type of Case Protection: Aluminum Type of Locking Device:_____ Pad Lock Concrete Surface Pad (with steel reinforcement) Dimensions: 6'X6'



SCS ENGINEERS **BORING NUMBER B-30 (VWP-30)** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas **COMPLETED** 11/18/18 DATE STARTED 11/17/18 **GROUND ELEVATION** 543.05 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater BLOW COUNTS (N VALUE) GRAPHIC LOG NUMBER RECOVERY U.S.C.S. DEPTH (ft) **TESTS** MATERIAL DESCRIPTION VWP Diagram 0 Top Soil, dark brown to black, very soft, with organic material and silt 1.1/ 541 (CL-ML) Silty Clay, gray, medium to very hard, slightly moist, with some round to sub-rounded pebles and chalky white material ML 5 538. (CL-ML) Silty Clay, gray mottled orange and brown, ST1 moderately hard, slightly moist, with some round to GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C:\USERS\PUBLIC\DOCUMENTS\BENTLEY\G\NT\PROJECTS\S\ITE 50 WACO.GPJ sub-rounded pebbles up to 1/2" and CLwhite chalky material, calcareous ML 57.6 10 10.0 (CL-ML) Silty Clay, orange-brown mottled gray and orange, medium soft, slightly moist, with white chalky material, calcareous ST2 31.8 Minor pebbles less than 1/8" 10-15 feet 15 No pebbles or chalky white material 15-20 feet ST3 Turning gray 15-20 feet CL-SPT2 ML 20 Crystalline deposits and very hard 20-25 feet ST4 25 518. (CL-ML) Silty Clay, light brown/orange to gray, medium hard to very hard, dry, calcareous, weathered ST5 Red-brown staining along fractures, medium soft to hard, SPT3 and crystalline deposits 30-35 feet

CL-ML

30

ST6

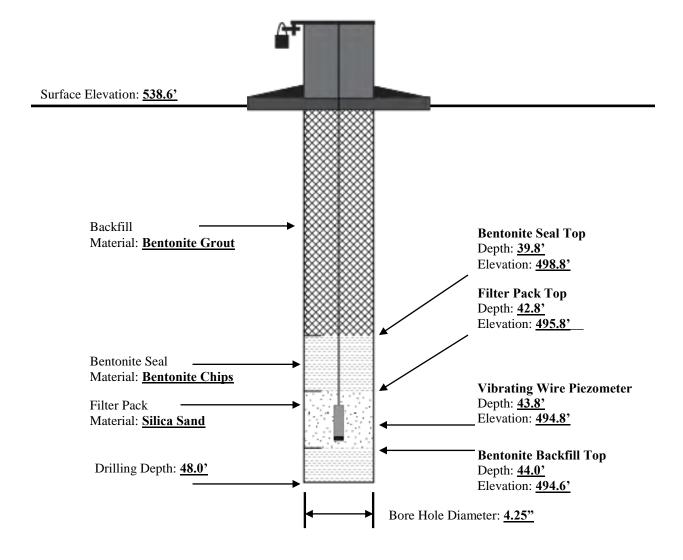
Revision 0

BORING NUMBER B-30 (VWP-30) 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME City of Waco Landfill MSW-2400 PROJECT NUMBER _ 16216088.00 PROJECT LOCATION Waco, Texas

HTG DEPTH (ft)	NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	VWP Diagram
	ST7				CL- ML		37.3 505.8 Silty Clay Shale Marl, gray to dark gray, very hard, dry, with orange-brown staining, calcareous unweathered	-vwp
40							Less orange staining 40-45 feet	
	ST8							
45							Some orange mottling and hard to very hard 45-48 feet	
	ST9						, ,	
VACO. GP	SPT5	\/					48.0 495.1	

Bottom of borehole at 48.0 feet.

PAGE 2 OF 2



1901 (Bedfo	ENGII Central D rd, Texas hone: 81	rive S7 76021	TE 550 1					WELL NUME	BER B-33	(VWP-33) PAGE 1 OF 2		
CLIEN	NT City o	of Wad	00					PROJECT NAME _City of Waco Landfill MS	SW-2400			
1				.00								
1								GROUND ELEVATION 539.4 ft H	OLE SIZE 8.25	5 inches		
1			TOR BES					GROUND WATER LEVELS:				
1				s Flight Auger				AT TIME OF DRILLING No Groun	ndwater			
LOGG	SED BY	T. Der	rstine	CHECKED	BY J	. Lawr	ence	AT END OF DRILLING No Groun	dwater			
NOTE	S							AFTER DRILLING No Groundwat	ter			
O DEPTH (ft)	NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION	WELL DIAGRAM	VWP DIAGRAM		
						1/ 1/1/		Clayey Silt Topsoil, dark brown, soft to firm, moist, with roots and organics	507.0			
	-						1.5	(CL-ML) Silty Clay, orange-brown mottled brown/tan, hard, moist to slightly moist, with white chalky material, calcareous	537.9			
5								Silty/micaceous interbeds 5-15 feet				
_ -												
- -	ST1											
¥ 	SPT1				CL-							
6 	-				ML							
10					+							
급 -	ST2											
<u> </u>	SPT2											
15	1						15.0		524.4			
0,00								(CL-ML) Silty Clay, orange-brown mottled brown and light gray, hard, slightly moist,				
	ST3							with black iron staining, fossil remnants, and				
3								silty/micaceous interbeds, calcareous				
집 								Weathered shale marl transition zone and mostly gray color at 25 feet				
20					4							
	ST4				CL-							
ِ - - ا	314				ML							
	1											
25 -												
5 23					1							
- LAB	ST5											
	SPT3			10/			28.0		511.4			
<u> </u>				Weathered to Unweathered	CL-			(CL-ML) Silty Clay Shale Marl, gray, hard, slightly moist, calcareous, unweathered				
30_				zone	ML		30.0	Orange-brown staining at 28.2 and 29.7 feet /	509.4			
 								Shale Marl, gray, very hard, slightly moist,				
	ST6							with fossil remnants, calcareous, unweathered				
	-											
2 -	-											
35	Revision	on 0			1		Z	(Continued Next Page)	May 2	1020 2020		

WELL NUMBER B-33 (VWP-33) PAGE 2 OF 2 1901 Central Drive STE 550 Bedford, Texas 76021

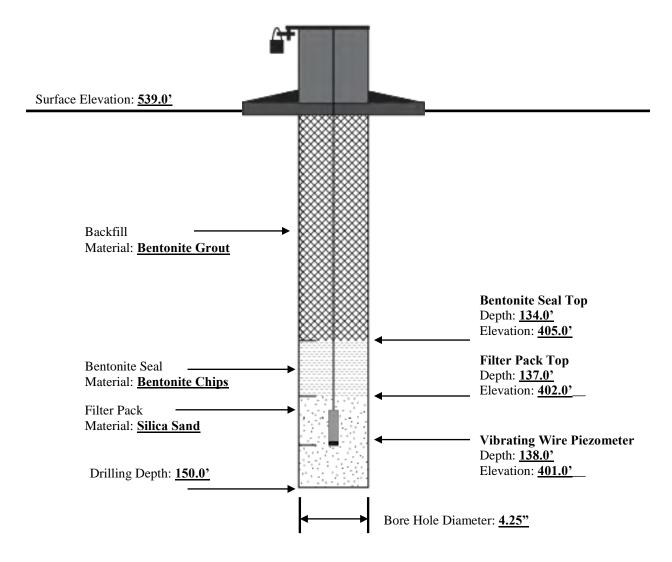
Telephone: 817-571-2288

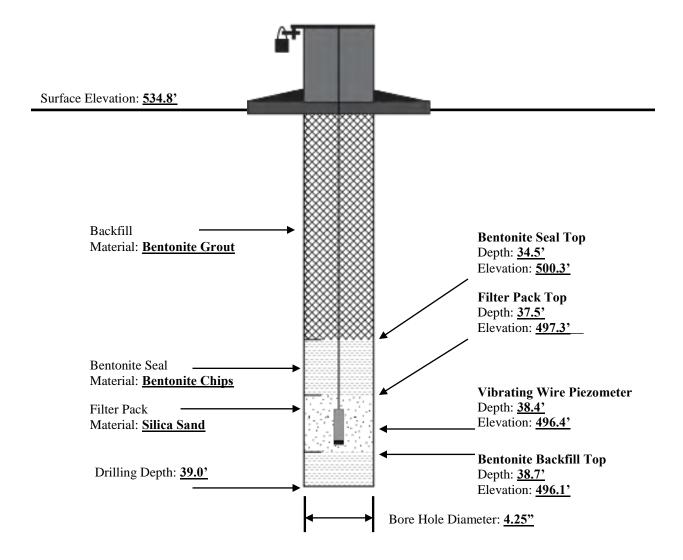
CLIENT City of Waco PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER 16216088.00 PROJECT LOCATION Waco, Texas

•	DEPTH (ft)	NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM	VWP DIAGRAM
-	40	ST7						Shale Marl, gray, very hard, slightly moist, with fossil remnants, calcareous, unweathered (continued)		
TE 50 WACO.GPJ	45 	ST8								-vwp
TS/BENTLEY/GINT/PROJECTS/SIT	50 55	-						55.0 484.4 Bottom of borehole at 55.0 feet.		
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C:USERSIPUBLICIDOCUMENTSIBENTLEYIGINTIPROJECTSISITE 50 WACO.GPJ										
SINT STD US LAB.GDT - 2/4/19 15:										
GENERAL BH / TP / WELL - G		Revisio	in O					4-1-48	May 2	020

Site Name: Waco 2400 County: <u>Limestone</u> VWP I.D. No.: VWP-33D Date of Installation: 12/4/2019 Probe Serial No.: 1943866 Northing: _10598320.64 3357774.619 Easting: Well Driller Name and License Number West Drilling SCS Field Staff Supervising Installation: Asher Boudreaux Static Water Level after Well Development: N/A Name of Geologic Formation(s) in which Well is completed: Wolfe City Formation Pad Lock Type of Case Protection: Aluminum Type of Locking Device:___ Concrete Surface Pad (with steel reinforcement) Dimensions: 6'X6'





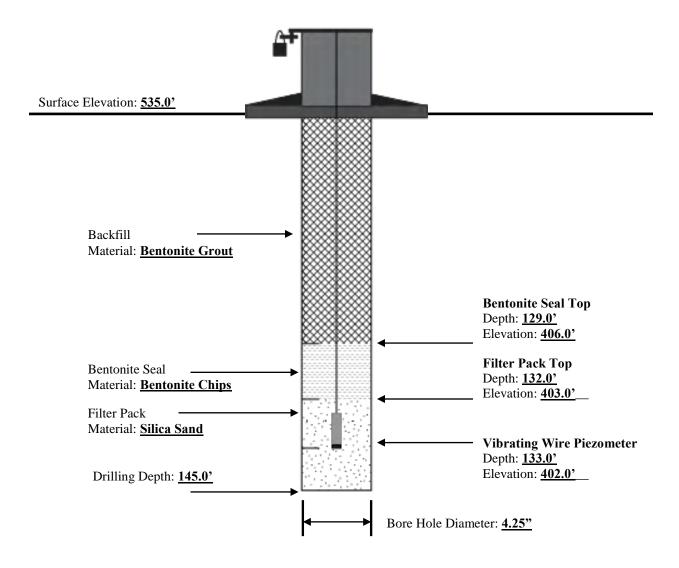
SCS ENGINEERS **WELL NUMBER B-41 (VWP-41)** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas COMPLETED _12/18/18 DATE STARTED 12/17/18 GROUND ELEVATION 535 ft HOLE SIZE 8.25 inches **DRILLING CONTRACTOR** BEST Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY T. Derstine CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater **NOTES** AFTER DRILLING _--- No Groundwater WELL DIAGRAM GRAPHIC LOG NUMBER RECOVERY U.S.C.S. **TESTS AND** MATERIAL DESCRIPTION **VWP DIAGRAM** REMARKS (CL-ML) Silty Clay, dark brown to gray, soft to stiff, moist to very moist, with a trace of gravel and roots/organics CL-ML 5 530.0 (CL-ML) Silty Clay, gray grading to brown and orange-brown stained, stiff, moist, with trace of small to GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:51 - C.;USERS/PUBLIC/DOCUMENTS/BENTLEY/GINT/PROJECTS/SITE 50 WACO.GP. large sub-rounded gravel and white chalky material Color change to orange-brown stained brown at 10 feet CL-ML 10 523.0 (CL-ML) Silty Clay Shale Marl, orange-brown stained brown and gray, stiff to hard, moist, with white crystalline lenses in bedding, calcareous 15 20 CL-ML 25 506.0 Shale Marl, dark gray with orange-brown stainining in 30 joints, hard, slightly moist to moist, calcareous, unweathered Trace of crystalline areas 29-30 feet 4-1-51 (Continued Next Page) May 2020 Revision 0

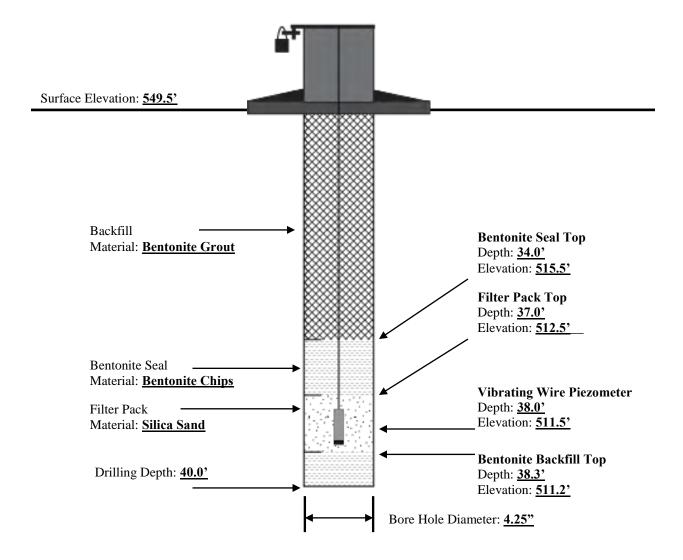
WELL NUMBER B-41 (VWP-41) 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas WELL DIAGRAM GRAPHIC LOG NUMBER RECOVERY U.S.C.S. DEPTH (ft) **TESTS** AND MATERIAL DESCRIPTION **VWP DIAGRAM REMARKS** 35 Shale Marl, dark gray with orange-brown stainining in joints, hard, slightly moist to moist, calcareous, unweathered Trace of crystalline areas 29-30 feet (continued) -VWP 40 43.0 492.0 Weathered to Shale Marl, gray to dark gray, hard, slightly moist, with lighter limey/silty lenses, fossil remnants, and crystalline areas, unweathered Unweathered zone 45

475.0

50

55





ST ST ST ST ST ST ST ST	1901 (ENGIN Central Dr rd, Texas	rive ST	E 550					WELL NUMBE	ER B-4	3 (VWP-43) PAGE 1 OF 2
PROJECT NUMBER 1621-608-00 PROJECT NUMBER 1621-6											
DATE STARTED 11/18/18 COMPLETED 11/16/18 CRUND GONTRACTOR BEST Drilling DRILLING GONTRACTOR BEST Drilling CORDUND STARTED Confinences Flight Auger CHECKED BY J. Lawrence OHECKED BY J. Lawrence NOTES TESTS AND ODE MAY MAY TESTS AND ODE MAY TESTS AND ODE MAY TESTS AND ODE MAY MAY MAY MAY MAY MAY MAY MA	CLIEN	IT City o	of Wac	0					PROJECT NAME _City of Waco Landfill MSV	/-2400	
DRILLING CONTRACTOR BEST Drilling DRILLING METHOD Continuous Flight Auger LOGGED BY _T_Densine	1		_								
DRILLING METHOD Continuous Flight Auger LOGGED BY T. Durstline CHECKED BY J. Lawrence NOTES AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — AT END OF DRILLING — No Groundwater AT END OF DRILLING — AT END OF DRILLING — NOTES AT END OF DRILLING — No Groundwater AT END OF DRILLING — AT END OF DRILLING — NO GROUNDWATER AT END OF DRILLING — AT END OF DRILLING — NO GROUNDWATER AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — No Groundwater AT END OF DRILLING — NO GROUNDWATER AT END OF DRILLING — NO GROUN	DATE	STARTE	D 11/	15/18	COMPLETE	ED _1	1/16/1	8	GROUND ELEVATION 549.65 ft HOI	E SIZE 8.	25 inches
LOGGED BY T. Dersitine CHECKED BY J. Lawrence AFTER DRILLING — REAL STATES AND DESCRIPTION SALES AND DESCRIPT	DRILL	ING CON	ITRAC	TOR BES	T Drilling				GROUND WATER LEVELS:		
NOTES AFTER DRILLING Weathered to Unweathered transition at 25 feet 255.0 ST6 ST6 ST7 ST7 ST7 ST7 ST7 ST7	DRILL	ING MET	HOD	Continuou	s Flight Auger				AT TIME OF DRILLING No Ground	water	
STE STS	LOGG	ED BY	T. Ders	stine	CHECKED	BY _J	. Lawr	ence	AT END OF DRILLING No Groundy	vater	
MH CL CL ML ST1 ST1 CL ML SPT3 ST2 ST2 ST3 ST3 ST3 ST3 ST3 ST5 ST5 ST6	NOTE	s					1		AFTER DRILLING		
MH CL CL-ML ST1 CL-ML ST1 CL-ML ST1 CL-ML ST1 CL-ML ST2 ST2 ST2 ST3 CL-ML ST3 ST3 ST3 ST4 ST5 ST5 ST5 ST5 ST6 ST6 Weathered to Unweathered transition at 25 feet ST6 ST7		NUMBER		BLOW COUNTS (N VALUE)	AND	U.S.C.S.	GRAPHIC		MATERIAL DESCRIPTION	WELL DIAGRAM	VWP DIAGRAM
CL ML Silty Clay, dark brown, hard, moist, with trace of gravel and organics ST1						МН		1.0	(MH) Clayey Silt, dark brown, soft, very		
CL-ML) Sitty Clay, crange-brown mottled gray and brown, sith or hard, slightly moist to moist, with white chalky material in interbeds, calcareous ST2 10.0 S39.7 CL-ML) Sitty Clay (weathered shale/mart), crange-brown stained light gray and brown, stiff to hard, slightly moist, calcareous, weathered White chalky material in interbeds 10-16 feet White chalky material in interbeds 10-16 feet White chalky material in interbeds 20-24 feet ST3 SPT2 Black iron staining in joints/interbeds 20-24 feet Weathered to unweathered transition at 25 feet CL-ML Sitty Clay, (shale/mart) gray with some orange-brown staining, hard, calcareous, with white fossil remnants CL-ML ML Weathered to Unweathered transition at 25 feet ST5 ST6 Weathered to Unweathered transition at 25 feet CL-ML Sitty Clay, (shale/mart) gray with some orange-brown staining, hard, calcareous, with white fossil remnants	 								(CL-ML) Silty Clay, dark brown, hard, moist,		
moist, with white chalky material in interbeds, calcareous 10.0 539.7	5							5.0	(CL-ML) Silty Clay, orange-brown mottled	44.7	
SPT3 ST2 ST2 ST3 CL-ML Silty Clay (weathered shale/mart), orange-brown stained light gray and brown, stiff to hard, slightly moist, calcareous, weathered White chalky material in interbeds 10-16 feet White chalky material in interbeds 20-24 feet Weathered to unweathered transition at 25 feet ST4 Weathered to unweathered transition at 25 feet ST5 SPT3 ST6 Weathered to Unweathered transiting, hard, calcareous, with white fossil remnants SPT3 ST6 Weathered to Unweathered to Unweathered transition at 25 feet ST7.7 ST7.7 ST8 Weathered to Unweathered to Unweathered transition at 25 feet SPT3 ST7.7 ST8 SPT3 ST8 Weathered to Unweathered to Unweathered transition at 25 feet SPT3 ST7 ST8 SPT3 ST8 ST8 SPT3 ST8 ST8 SPT3 SPT		ST1							moist, with white chalky material in		
ST2 ST2 ST3 SPT2 20 ST4 ST5 SPT2 20 ST6 Weathered to Unweathered 31-20 (CL-ML) Silty Clay weathered shaller gray and brown, stiff to hard, slightly moist, calcareous, weathered White chalky material in interbeds 10-16 feet White chalky material in interbeds 10-16 feet White chalky material in interbeds 20-24 feet Black iron staining in joints/interbeds 20-24 feet Weathered to unweathered transition at 25 feet ST5 ST5 SPT3 CL-ML Weathered to unweathered transition at 25 feet orange-brown staining, hard, calcareous, with white fossil remnants CL-ML ML 32.0 ST6 Weathered to Unweathered to Unweathered transition at 25 feet orange-brown staining, hard, calcareous, with white fossil remnants ST7.7 ST7.7 ST7.7		SPT1							interbeds, calcareous		
ST2 ST2 ST3 SPT2 20 ST4 ST5 SPT2 ST5 SPT3 ST6 Weathered to Unweathered 32.0											
ST3 SPT2 Black iron staining in joints/interbeds 20-24 feet Weathered to unweathered transition at 25 feet ST5 ST5 ST5 SPT3 SPT3 SPT3 SPT3 SPT3 SPT3 SPT3 SPT3	_ 10 _							10.0		39.7	
ST3 SPT2 ST4 ST4 Black iron staining in joints/interbeds 20-24 feet Weathered to unweathered transition at 25 feet ST5 ST5 ST5 ST5 ST6 Weathered to Unweathered transition at 25 feet CL-ML Sitty Clay, (shale/mart) gray with some orange-brown staining, hard, calcareous, with white fossil remnants SPT3 ST6 Weathered to Unweathered to Unweathered transition at 25 feet ST6 ST7 ST7 ST8 ST8 ST8 ST8 Weathered to Unweathered to Unweathered to Unweathered transition at 25 feet ST8 ST8 ST8 ST8 ST8 ST8 ST8 ST	 	ST2							orange-brown stained light gray and brown, stiff to hard, slightly moist, calcareous,		
ST3 SPT2 Black iron staining in joints/interbeds 20-24 feet Weathered to unweathered transition at 25 feet ST5 ST5 ST5 ST6 Weathered to Unweathered	- 								White chalky material in interbeds 10-16 feet		
	15										
ML Black iron staining in joints/interbeds 20-24 feet Weathered to unweathered transition at 25 feet 524.7 ST5 ST5 ST6 Weathered to Unweathered zone 32.0 ST6 Weathered to Unweathered to Unweathered to Unweathered to Unweathered to Unweathered zone		ST3									
ST4 ST4 Black iron staining in joints/interbeds 20-24 feet Weathered to unweathered transition at 25 feet ST5 ST5 ST6 Weathered to Unweathered transition at 25 feet (CL-ML) Silty Clay, (shale/marl) gray with some orange-brown staining, hard, calcareous, with white fossil remnants CL-ML Weathered to Unweathered zone ST6 Weathered to Unweathered zone		SPT2									
Black iron staining in joints/interbeds 20-24 feet ST4 Weathered to unweathered transition at 25 feet ST5 ST5 ST6 Weathered to Unweathered transition at 25 some orange-brown staining, hard, calcareous, with white fossil remnants CL-ML Weathered to Unweathered to Unweathered to Unweathered zone	L _										
ST4 25 Weathered to unweathered transition at 25 feet ST5 ST5 ST5 ST6 Weathered to Unweathered transition at 25 feet (CL-ML) Silty Clay, (shale/marl) gray with some orange-brown staining, hard, calcareous, with white fossil remnants CL-ML Weathered to Unweathered zone 32.0 ST6 ST6 ST7 ST7 ST7 ST7 ST7 ST8 ST8 ST8	20										
ST4 Weathered to unweathered transition at 25 feet ST5 ST5 ST6 Weathered to Unweathered Weathered to Unweathered ST6 Weathered to Unweathered ST7 ST7 ST7 ST7 ST7 ST7 ST7 ST	L _								_ ,		
25 ST5 ST5 ST6 Weathered to Unweathered zone St6 St7	L -	ST4									
25 ST5 ST5 SPT3 ST6 Weathered to Unweathered zone ST6 ST7 ST7											
ST5 ST5 ST6 Weathered to Unweathered zone ST6 Weathered to Unweathered zone ST6 ST7 ST7 ST7 ST7 ST7 ST7 ST7	 								Weathered to unweathered transition at 25		
ST5 SPT3 SPT3 Weathered to Unweathered zone ST6 ST6 SPT3 Some orange-brown staining, hard, calcareous, with white fossil remnants ST7 ST7 ST7 SOME OF A ST8 SOM	25							25.0	5	24.7	
ST5 SPT3 SPT3 ST6 Weathered to Unweathered zone ST6 ST6 ST7 ST7 ST7 ST7 SPT3 SPT3 SPT3 SPT3 SPT3 SPT3 SPT3 SPT3	 										
ST6 Weathered to Unweathered zone 35 Double De la company de la compa	L -	ST5									
ST6 Weathered to Unweathered zone 35	<u> </u>	SPT3				C					
ST6 Weathered to Unweathered zone 32.0 517.7											
Unweathered zone 517.7	30					-					
	<u> </u>										
	ļ -	ST6						32.0	5	17.7	
	ļ -										
Dovición O Moy 2020											
	35	Dovicio)n (<u> </u>	4-1-55 (Continued Next Page)	May	2020

WELL NUMBER B-43 (VWP-43) 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 **CLIENT** City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas WELL DIAGRAM BLOW COUNTS (N VALUE) GRAPHIC LOG NUMBER RECOVERY DEPTH (ft) U.S.C.S. **TESTS** VWP DIAGRAM AND MATERIAL DESCRIPTION **REMARKS** 35 Silty Shale Marl, gray, hard, slightly moist, calcareous, unweathered ST7 VWP Occasional orange-brown staining and fossil remnants in beds 32-43 feet White crystalline material in bedding/joints at 40 35 feet ST8 45 Micaceous interbeds and traces of fossil remnants 45-70 feet (continued) ST9 GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:52 - C:/USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ SPT4 50 55 ST10 SPT5 60 65 ST11 70

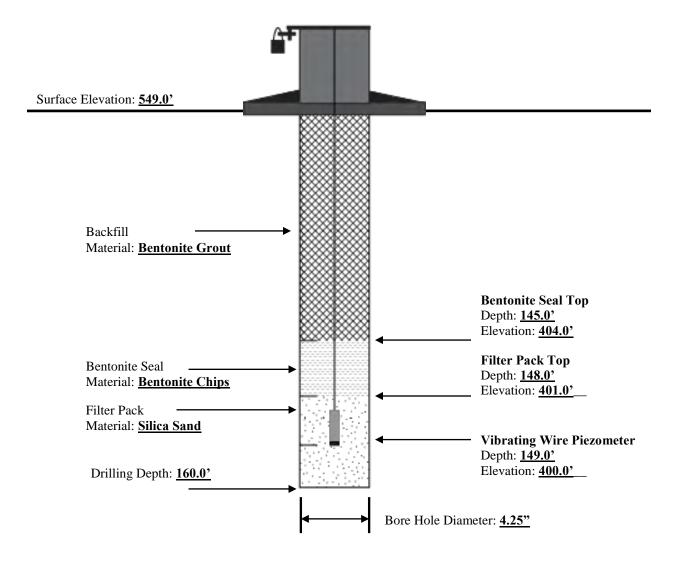
474.7

May 2020

75

Revision 0

Site Name: Waco 2400 VWP I.D. No.: VWP-43D County: <u>Limestone</u> Date of Installation: 12/3/2019 Probe Serial No.: 1943859 Northing: _10600433.69 3358875.537 Easting: Well Driller Name and License Number West Drilling SCS Field Staff Supervising Installation: __Asher Boudreaux Static Water Level after Well Development: N/A Name of Geologic Formation(s) in which Well is completed: Wolfe City Formation Pad Lock Type of Case Protection: Aluminum Type of Locking Device:__ Concrete Surface Pad (with steel reinforcement) Dimensions: 6'X6'



	ENGIN							WELL NUMBE	ER B	3-43 (VWP-43D)
	Enginee Central										PAGE 1 OF 4
Ste. 5	50										
	rd, TX 7 I T _City o		00					PROJECT NAME City of Waco Landfill M	SW-240	00	
				.00							
								GROUND ELEVATION 548.86 ft H	IOLE S	IZE 8.2	5 inches
				T Drilling; West Dr							
DRILL	ING ME	THOD	Continuo	us Flight Auger				AT TIME OF DRILLING No Grou	ndwate	r	
LOGG	ED BY	T. De	rstine; A. B	oudreaux CHECK	(EDB	Y J. l	_awrence	AT END OF DRILLING No Groun	ndwater		
NOTE	s							AFTER DRILLING			
	Ш	%								Σ	
	SAMPLE TYPE NUMBER		ZS JE JE	TESTS	S.	₽				WELL DIAGRAM	
DEPTH (ft)	LE '	RECOVERY	BLOW COUNTS (N VALUE)	AND	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		OIAC	VWP DIAGRAM
	MM		BO√ NOB	REMARKS	⊃	GR.				=	
0	8	2 2								WE	
					МН		1.0	(MH) Clayey Silt, dark brown, soft, very moist, with trace of gravel and organics	547.9		
								(CL-ML) Silty Clay, dark brown, hard, moist,			
					CL-			with trace of gravel and organics			
					ML						
5					1		5.0		543.9		
		\vdash					1	(CL-ML) Silty Clay, orange-brown mottled gray and brown, stiff to hard, slightly moist to			
	ST1				CL-		1	moist, with white chalky material in interbeds, calcareous			
	SPT1				ML			interbeds, calcureous			
_ 10							10.0	(OLANI) Other Olary (weather and a half (weath)	538.9		
5							1	(CL-ML) Silty Clay (weathered shale/marl), orange-brown stained light gray and brown,			
S 	ST2						1	stiff to hard, slightly moist, calcareous, weathered			
S											
								White chalky material in interbeds 10-16 feet			
15					4			Black iron staining in joints/interbeds 20-24 feet			
3 -	ST3							Weathered to unweathered transition at 25			
4rekelben - - - - - - - - -					CL-		4	feet			
	SPT2				ML						
20					+						
	ST4										
<u>+</u>											
7/9/7							05.0		500.0		
25			-					(CL-ML) Silty Clay, (shale/marl) gray with	523.9		
SID OS LAB.GD	ST5							some orange-brown staining, hard, calcareous, with white fossil remnants			
	SPT3							,			
	01 19				CL- ML						
30					IVIL						
					1						
<u>-</u> -	ST6			Weathered to			32.0		516.9		
			-	Unweathered zone		rvvn	, 02.0		3.0.0		
ENEKAL BH											
35											
	Revision	on 0					4-	I-58 (Continued Next Page)		May 2	2020

SCS ENGINEERS WELL NUMBER B-43 (VWP-43D) SCS Engineers 1901 Central Dr PAGE 2 OF 4 Ste. 550 Bedford, TX 76021 CLIENT City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas SAMPLE TYPE NUMBER WELL DIAGRAM BLOW COUNTS (N VALUE) GRAPHIC LOG RECOVERY U.S.C.S. DEPTH (ft) **TESTS** AND MATERIAL DESCRIPTION VWP DIAGRAM **REMARKS** 35 Silty Shale Marl, gray, hard, slightly moist, calcareous, unweathered ST7 Occasional orange-brown staining and fossil remnants in beds 32-43 feet White crystalline material in bedding/joints at 40 35 feet Micaceous interbeds and traces of fossil ST8 remnants 45-70 feet 45 ST9 SPT4 50 GENERAL BH / TP / WELL - GINT STD US LAB. GDT - 2/5/20 12:11 - L:\VALERIE\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 55 ST10 SPT5 60 65 ST11 70 4-1-59

Revision 0

May 2020

(Continued Next Page)

SCS ENGINEERS

SCS Engineers 1901 Central Dr Ste. 550 Bedford, TX 76021

WELL NUMBER B-43 (VWP-43D)

PAGE 3 OF 4

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

PROJE	CT NUN	IBER	16216088	.00			PROJECT LOCATION Waco, Texas		
DEPTH (#) 75	SAMPLE TYPE NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM	VWP DIAGRAM
 							Shale with minor, very fine sand to silt. Dark gray, very hard, moist, laminated Few, small fossils		
80 							Becoming harder with depth Fewer laminations with depth		
85							80-85' very small mica flakes 85-95' some fossils		
 90									
95									
 _ 110 							Large bivalve fossil @ 110'		
 _115	Revisio	on 0					Shale with minor, very fine sand. Dark gray, very hard, moist, trace lamination 4-1-60 (Continued Next Page)	May 2	2020

SCS ENGINEERS

SCS Engineers 1901 Central Dr Ste. 550 Bedford, TX 76021

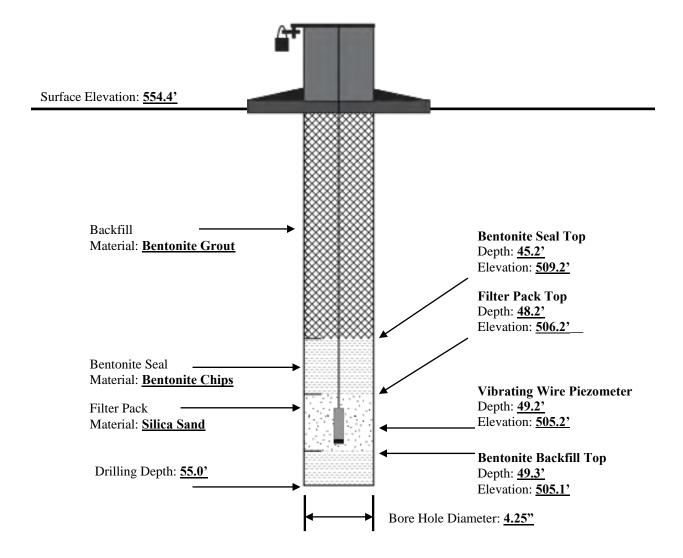
WELL NUMBER B-43 (VWP-43D) PAGE 4 OF 4

CLIENT City of Waco

PROJECT NAME City of Waco Landfill MSW-2400

			16216088	.00	1		PROJECT NAME _City of Waco Landfill MSW-2400 PROJECT LOCATION _Waco, Texas		
(ft) (ft)	SAMPLE TYPE NUMBER	RECOVERY %	BLOW COUNTS (N VALUE)	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM	VWP DIAGRAM
 							Shale with minor, very fine sand to silt. Dark gray, very hard, moist, laminated		
 120 					-		Becoming harder with depth		
 125							Trace sands transitioning to no sands		
 130							below 125'		
 							Scarce laminations		
 _135 _ 					-		Featureless		
 140 					_				
 145									
 							Shale. Dark gray, very hard, moist, no lamination		• -vwi
150		<u> </u>			<u> </u>		Bottom of borehole at 150.0 feet.		<u> </u>
	Revisio	n ()					4-1-61	May 20	20

Vibrating Wire Piezometer Data Sheet



SCS ENGINEERS

M:\Projects\Waco\16216088.00 New LF\Site 50\Site 50 Phase II DDD, Well Completion, Field Logs, drilling started Oct 4 2018\Files for Permit Figures

SCS ENGINEERS **BORING NUMBER B-44 (VWP-44)** 1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288 **CLIENT** City of Waco PROJECT NAME _ City of Waco Landfill MSW-2400 **PROJECT NUMBER** 16216088.00 PROJECT LOCATION Waco, Texas **COMPLETED** 10/10/18 **DATE STARTED** 10/10/18 **GROUND ELEVATION** 551.2 ft HOLE SIZE 7.25 inches **DRILLING CONTRACTOR** West Drilling **GROUND WATER LEVELS:** DRILLING METHOD Continuous Flight Auger AT TIME OF DRILLING _--- No Groundwater LOGGED BY V. Wooters CHECKED BY J. Lawrence AT END OF DRILLING _--- No Groundwater NOTES AFTER DRILLING _--- No Groundwater GRAPHIC LOG NUMBER RECOVERY U.S.C.S. **TESTS** AND MATERIAL DESCRIPTION **VWP REMARKS** Diagram (CL) Clay, dark brown to black, hard, moist, non-calcareous Calcareous 4-5 feet. CL 5 5.0 546.2 (CL-ML) Silty Clay, orange-tan mottled gray, hard, slightly moist, with ST1 chalk/limestone deposits in joints and fractures, calcareous GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:52 - C:\USERS\PUBLIC\DOCUMENTS\BENTLEY\GINT\PROJECTS\SITE 50 WACO.GPJ 10 ST2 15 No chalk/limestone in fractures 15-25 feet ST3 Minor sand and silt in fractures (gray) 15-39.5 feet 20 ML ST4 25 ST5 30 ST6

Revision 0

BORING NUMBER B-44 (VWP-44) PAGE 2 OF 3

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

	City c		16216088.00			PROJECT NAME _City of Waco Landfill MSW-2400 PROJECT LOCATION _Waco, Texas	
		%					
(ft) (ft) 35	NUMBER	RECOVERY	TESTS AND REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	VWP Diagram
	ST7					(CL-ML) Silty Clay, orange-tan mottled gray, hard, slightly moist, with chalk/limestone deposits in joints and fractures, calcareous	
				CL- ML		No chalk/limestone in fractures 15-25 feet	
			Weathered to		39.5	Minor sand and silt in fractures (gray) 15-39.5 feet (continued) 511.7	
40	0.70		Unweathered zone		41.0	Shaley Clay, dark gray, hard, dry, slightly calcareous, weathered 510.2	
	ST8				41.0	Silty Clay Shale, dark gray, hard, dry, calcareous, with limestone intrusions in fractures	
45							
	ST9						
: =							
50							- -V
	ST10						
	0110						
55						No limestone intrusions in fractures 55-76 feet	
60							
	ST11						
65							
						Interbedded heavily weathered zones 65-76 feet	
70	OTIC						
-]	ST12						
75	Revisio					4-1-64 (Continued Next Page) May 202	

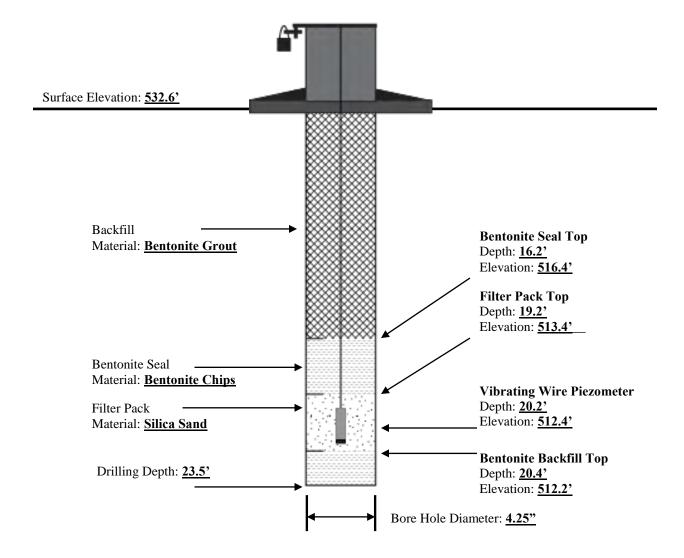
(Continued Next Page)

BORING NUMBER B-44 (VWP-44) 1901 Central Drive STE 550 PAGE 3 OF 3 Bedford, Texas 76021 Telephone: 817-571-2288 CLIENT City of Waco PROJECT NAME _City of Waco Landfill MSW-2400 PROJECT LOCATION Waco, Texas **PROJECT NUMBER** 16216088.00 GRAPHIC LOG NUMBER RECOVERY U.S.C.S. DEPTH (ft) **TESTS** AND REMARKS MATERIAL DESCRIPTION 75 76.0 475.2 Bottom of borehole at 76.0 feet.

ST13

Vibrating Wire Piezometer Data Sheet

Site Name: Waco 2400 County: <u>Limestone</u> VWP I.D. No.: <u>VWP-47</u> Date of Installation: 8/2/2019 Probe Serial No.: 1921449 Northing: _10598701.96_ 3356561.53 Easting:__ Well Driller Name and License Number West Drilling SCS Field Staff Supervising Installation: Doug Steen Static Water Level after Well Development: N/A Name of Geologic Formation(s) in which Well is completed: Wolfe City Formation Pad Lock Type of Case Protection: ___Aluminum Type of Locking Device:_____ Concrete Surface Pad (with steel reinforcement) Dimensions: 6'X6'



SCS ENGINEERS

	ENGIN						WELL NUM	/IBER	B-47	(VWP-47)
Bedfor	Central Dr d, Texas ione: 817	76021	1							PAGE 1 OF 2
CLIEN	IT City o	of Wac	00				PROJECT NAME _City of Waco Landfill	MSW-240	00	
							PROJECT LOCATION Waco, Texas			
							GROUND ELEVATION 532.4 ft	HOLE S	IZE 7.25	inches
			TOR West Drilling				GROUND WATER LEVELS:			
								oundwate	r	
1						Y J. Lawrence				
							AFTER DRILLING No Ground			
O DEPTH	NUMBER	RECOVERY %	REMARKS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		WELL DIAGRAM	VWP DIAGRAM
0				ML		(), -	ark brown, soft, moist	531.9		
 5				CL			ght gray, hard, dry, calcareous, with chalk	in		
	ST1					7.0		525.4		
S S						(CL-ML) Sil	ty Clay, orange-tan mottled gray, hard, dry, with chalk in fractures/joints			
00							-			
<u> </u> 10						Trace of su	ıb-angular gravel 1/8" at 7-10 feet			
SIS										
GENERAL BH / IP/ WELL - GINI SID US LAB. GD 2.24-19 15:25 - C: USERSNPUBLIC/DOCOMEN IS/BEN ILEY/GINI PROJECT 50 WACO GPJ 10 10 10 10 10 10 10 1	ST2									
15										
-	ST3			CL- ML						
<u> </u>				IVIL						
}										
20	_									-VWP
<u></u>										
<u>;</u>	ST4									
-										
25										
						07.0		===		
	ST5						gray with orange-brown mottling, hard, sligh	505.4 ity		
							, calcareous, with weathered shale,			ļ
						weathered				
30				CL						
<u> </u>										
<u>-</u>			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			33.0		400.4		
<u> </u>			Weathered to Unweathered		<i>/////</i>	33.0		499.4		
5 35			zone							
<u>ا 35 ا</u>	Revisio	n 0	<u> </u>			4-1	-67 (Continued Next Page)		May 2	b20

WELL NUMBER B-47 (VWP-47)

1901 Central Drive STE 550 Bedford, Texas 76021 Telephone: 817-571-2288

PAGE 2 OF 2

CLIENT City of Waco

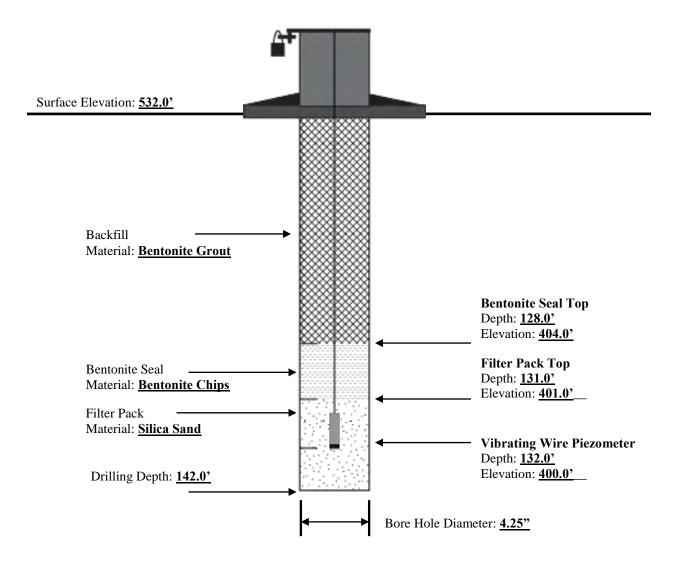
PROJECT NAME City of Waco Landfill MSW-2400

PROJECT NUMBER _16216088.00

PROJECT LOCATION Waco, Texas

DEPTH (ff)	NUMBER	RECOVERY %	REMARKS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	WELL DIAGRAM	VWP DIAGRAM
						Silty Clay Shale, dark gray, hard, dry, calcareous, unweathered		
						Limestone lenses in fractures 38-57 (continued)		
40								
45								
ACO.GPJ	ST6							
SITE 50 W								
OJECTS/8								
AGINTIPR								
BENTLE -								
UMENTS	ST7					57.0 475.4 Bottom of borehole at 57.0 feet.	1	
BLIC\DOC						Bottom of boreflole at 37.0 leet.		
SERS/PU								
:52 - C:\U:								
2/4/19 15								
AB.GDT -								
STD US L								
L - GINT								
TP / WEL								
GENERAL BH / TP / WELL - GINT STD US LAB.GDT - 2/4/19 15:52 - C:\USERS\PUBLIC\DOCUMENTS\BENTLE\G\G\NT\PROJECTS\SITE 50 WACO.GPJ								
GEN	Revisio	n O				4-1-68	May	2020

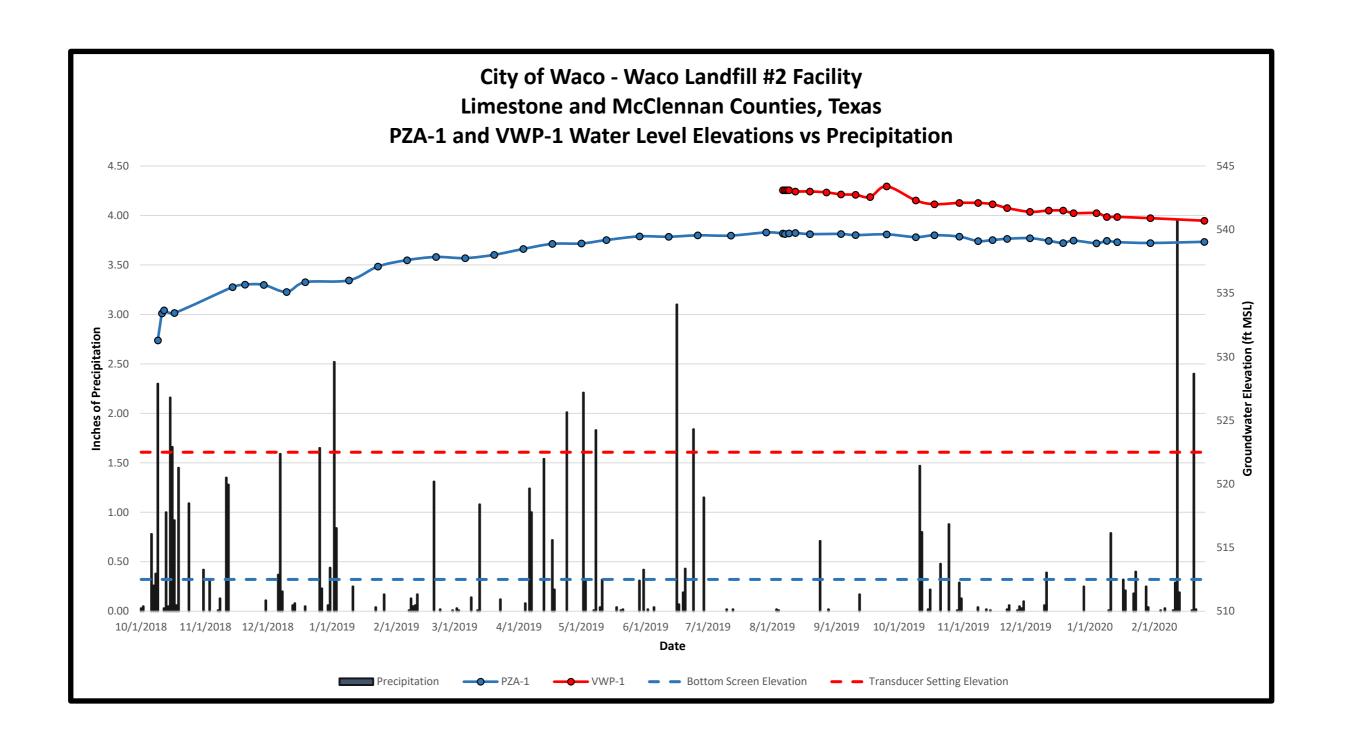
Vibrating Wire Piezometer Data Sheet

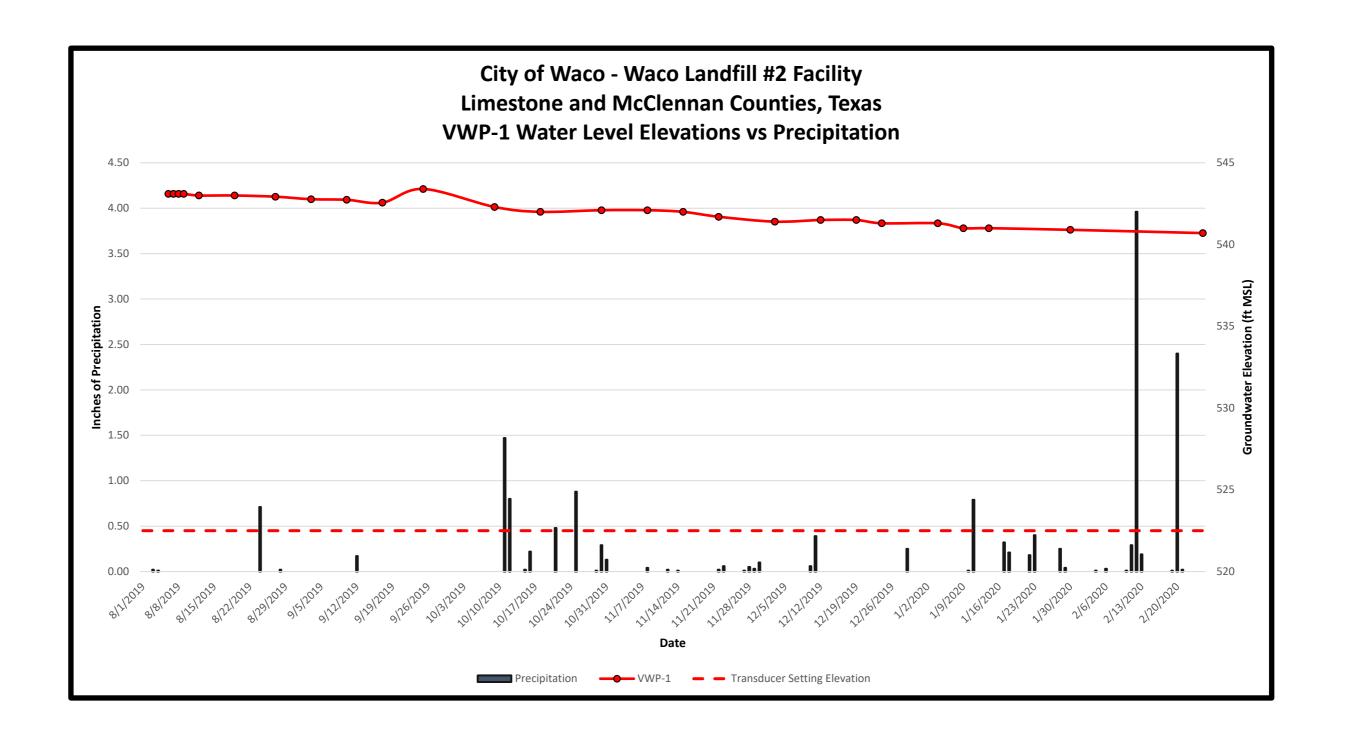


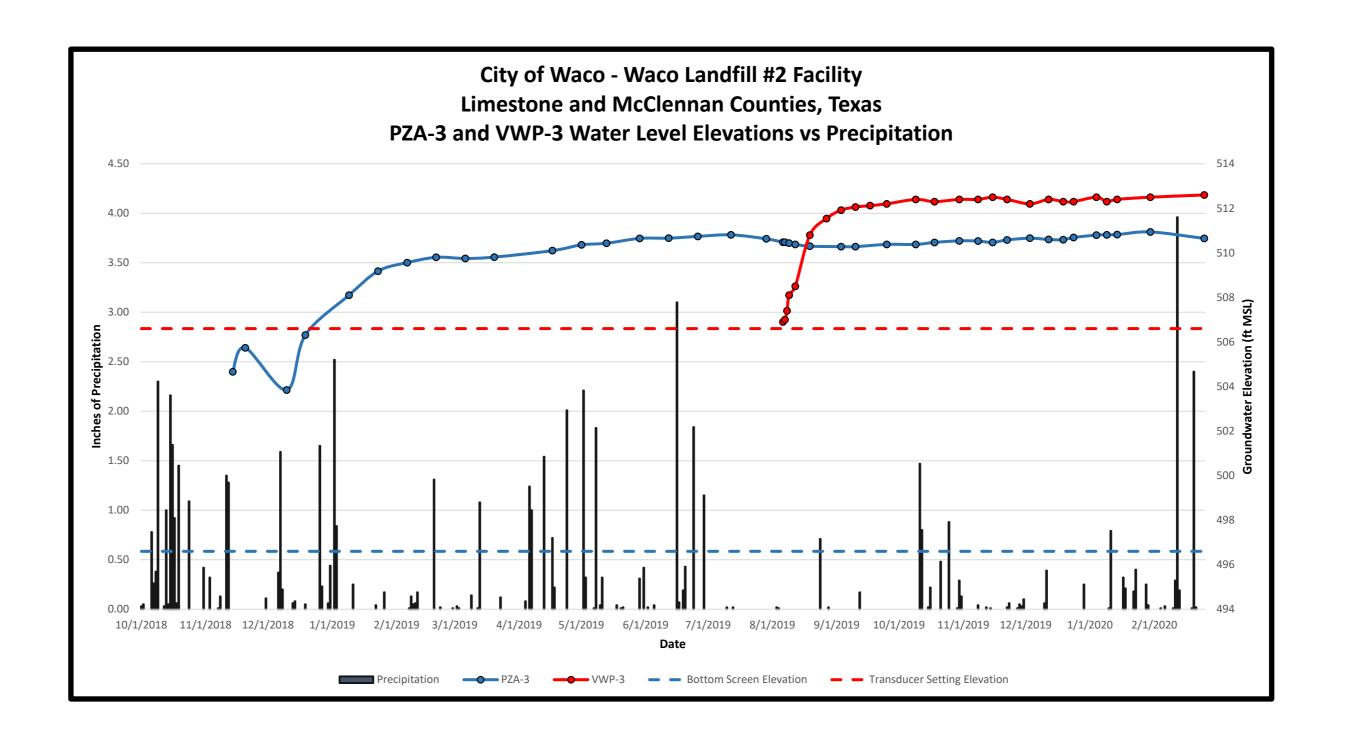
SCS ENGINEERS

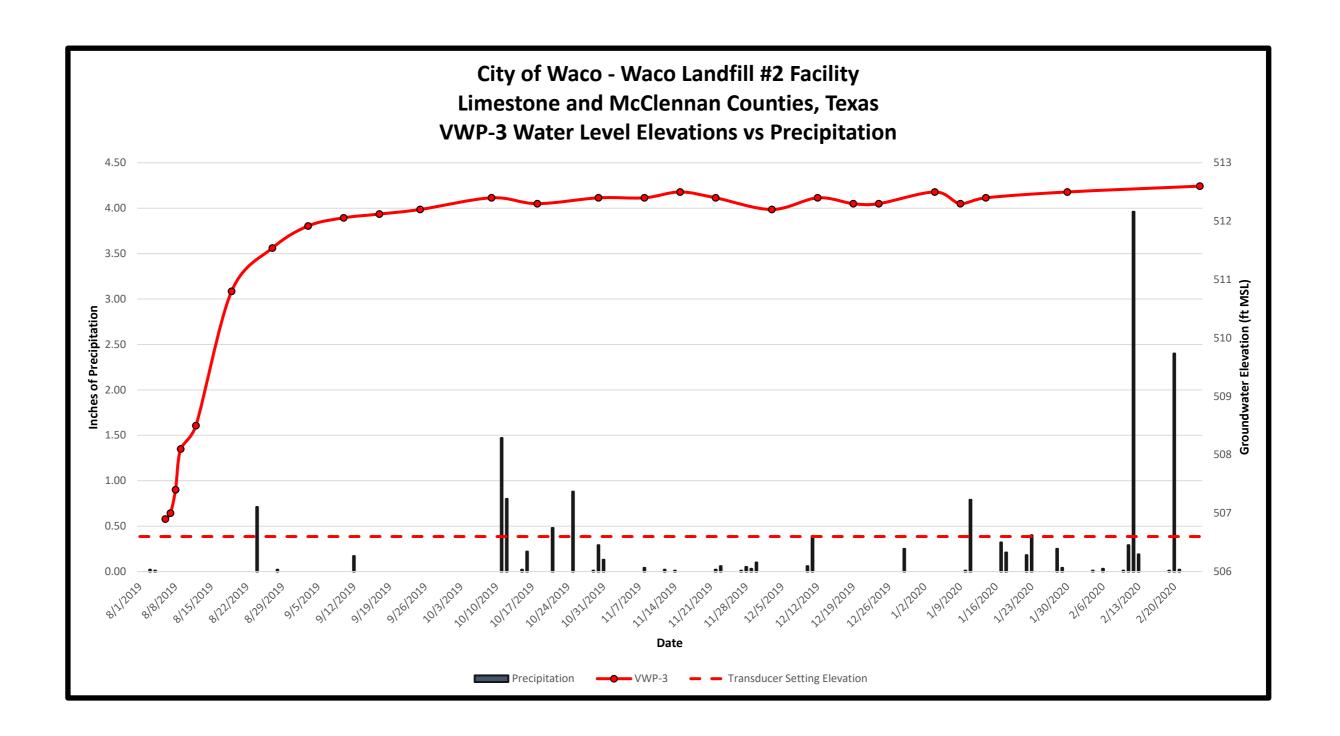
APPENDIX III-4.J PRECIPITATION AND GROUNDWATER ELEVATION DATA

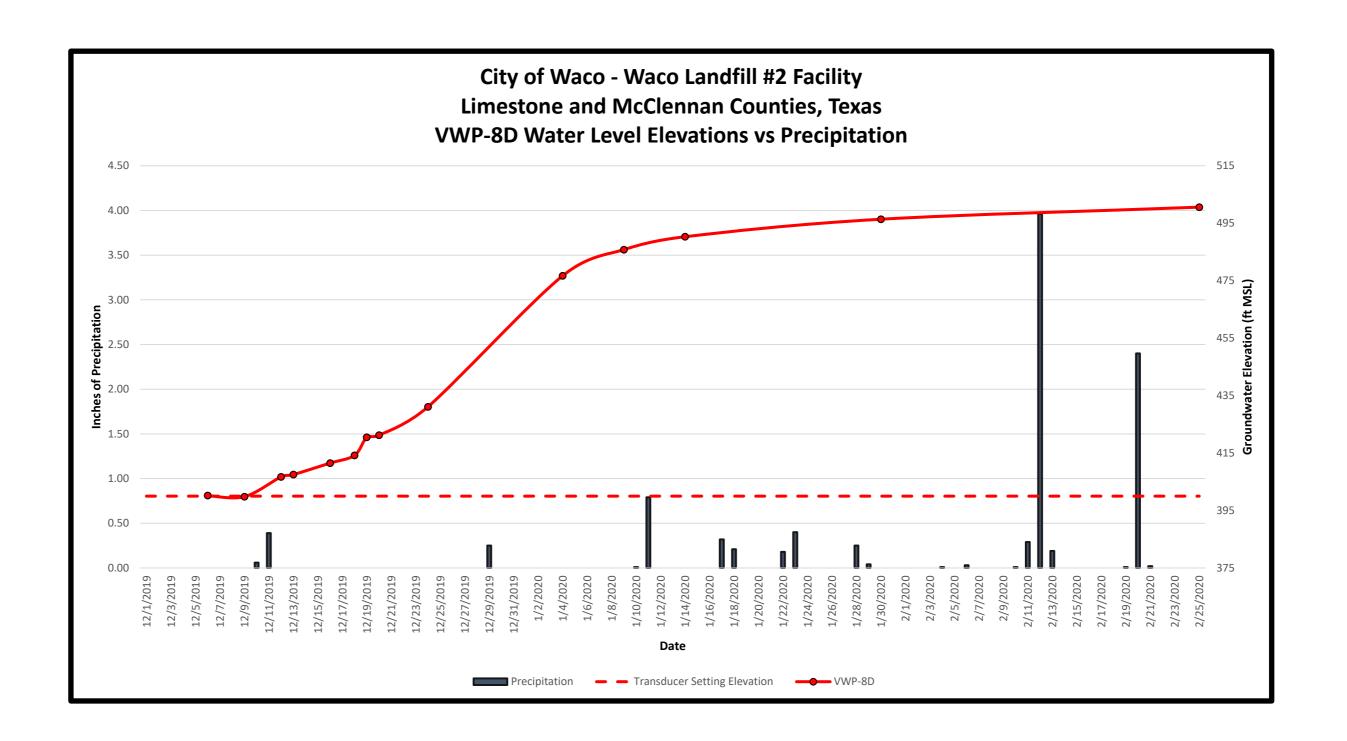


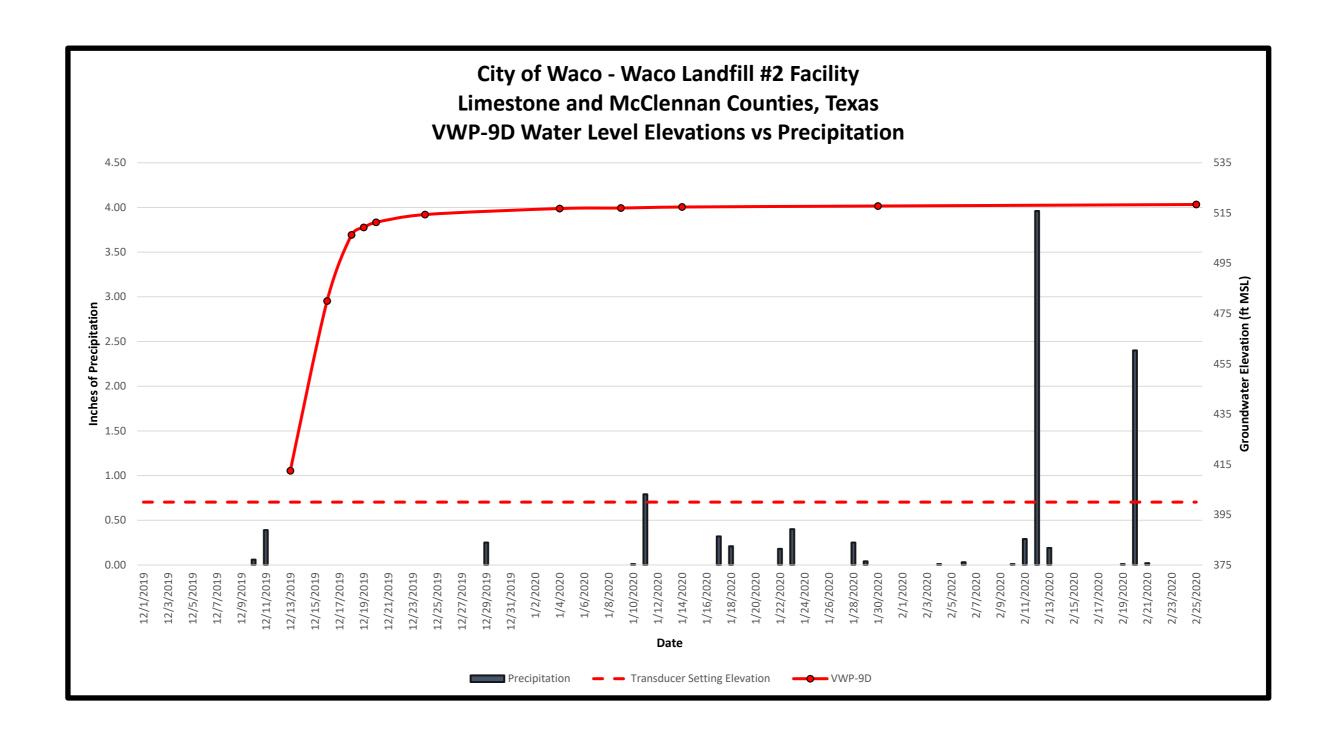


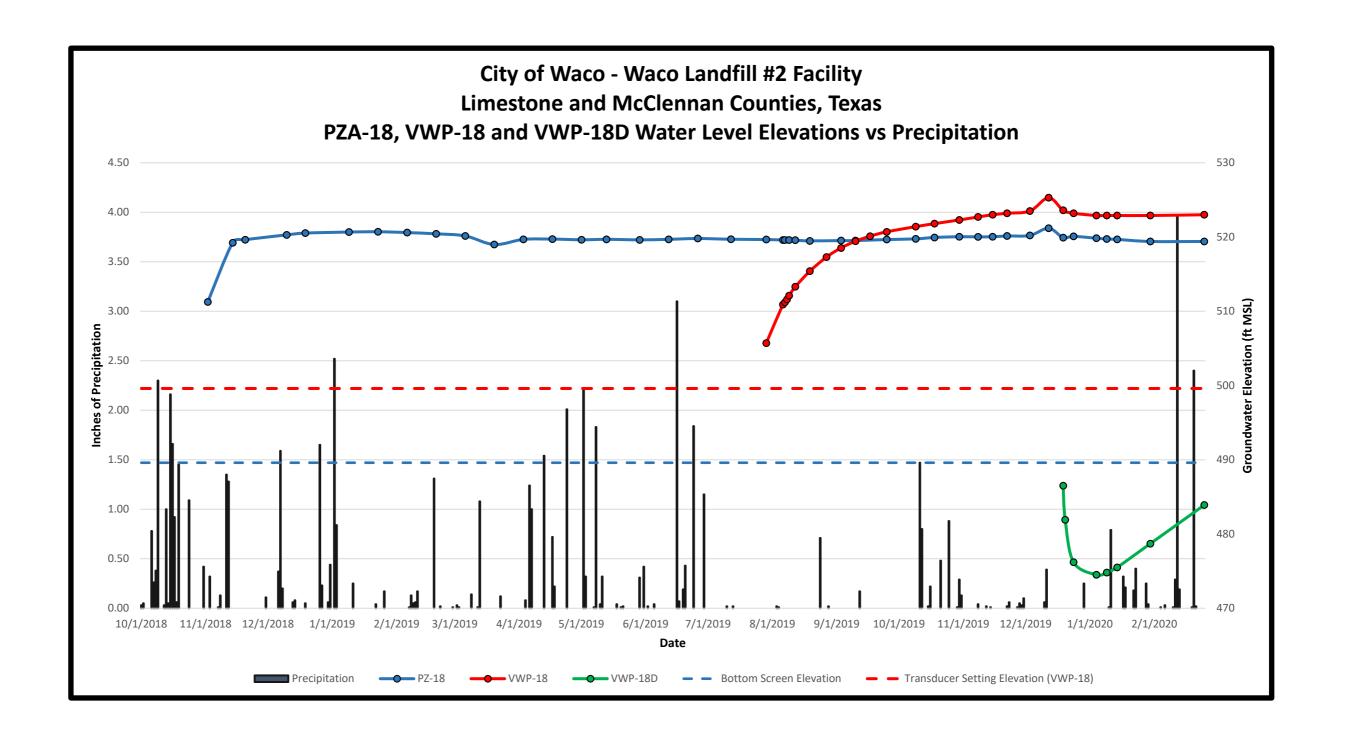


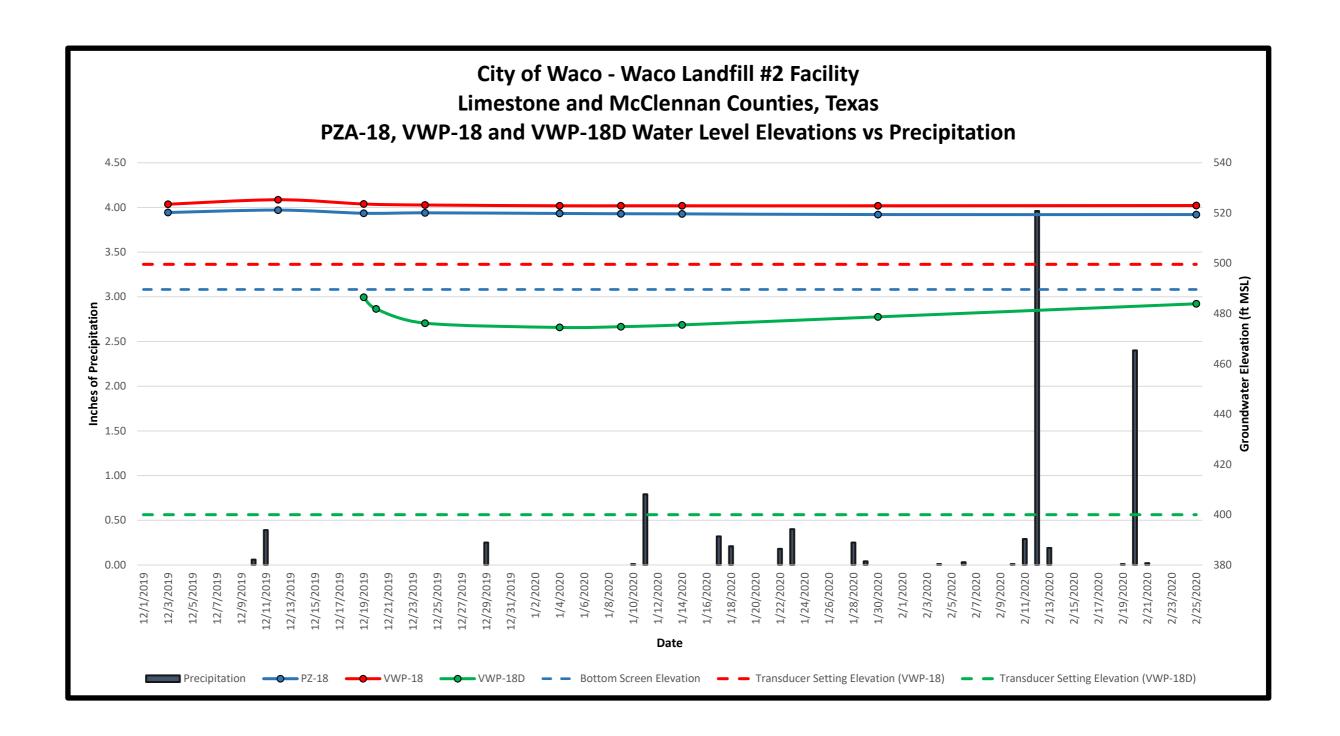


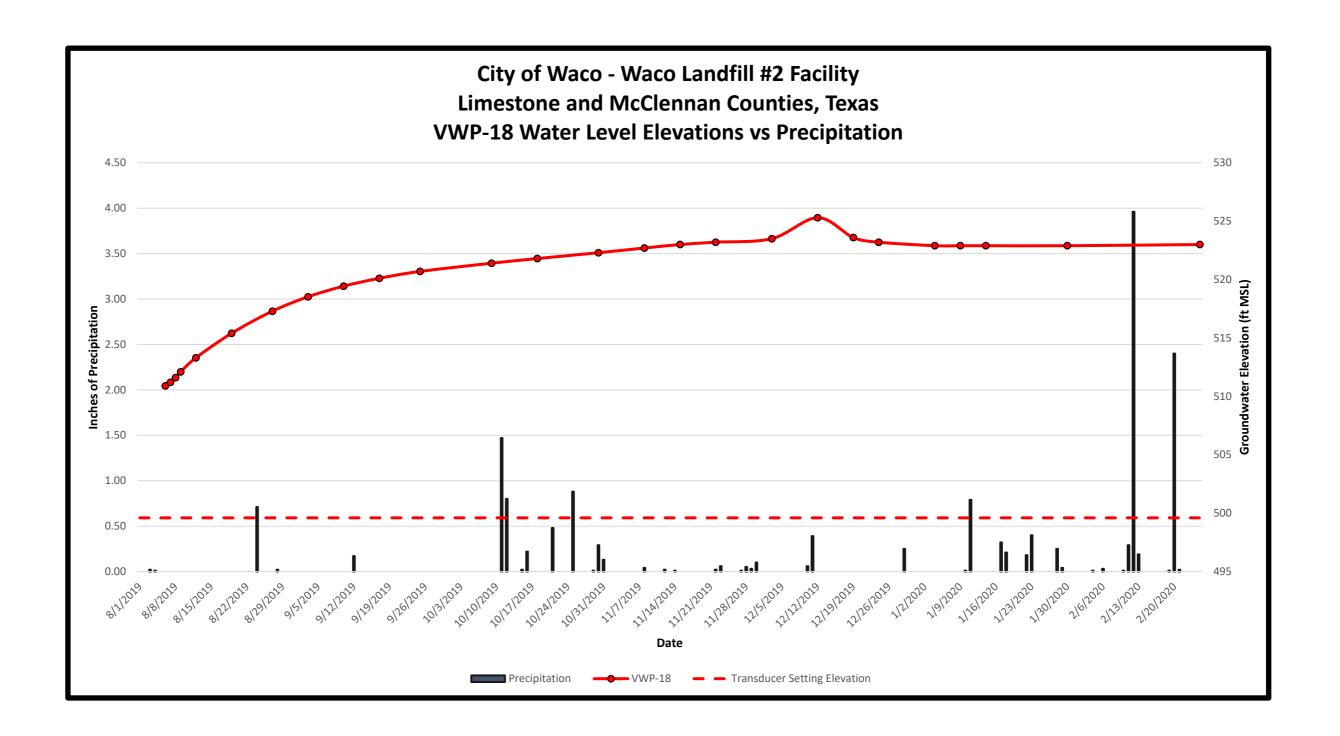


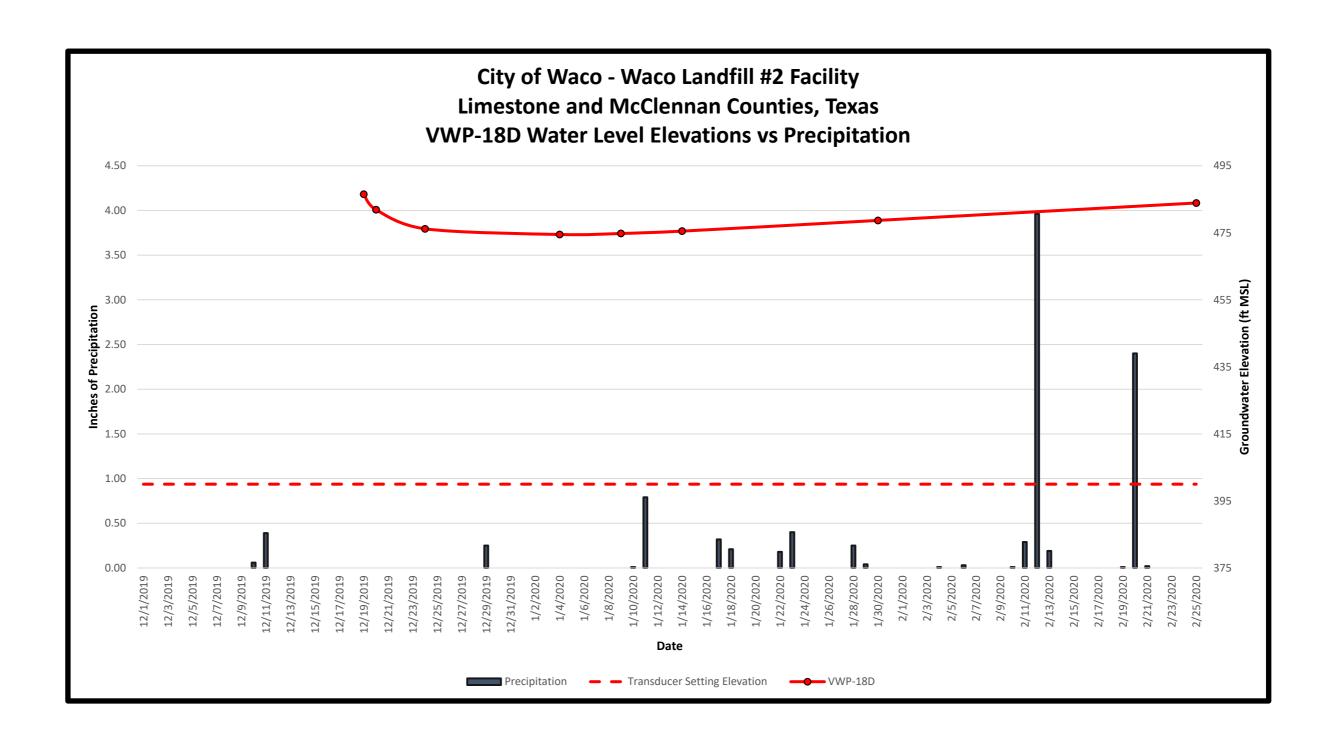


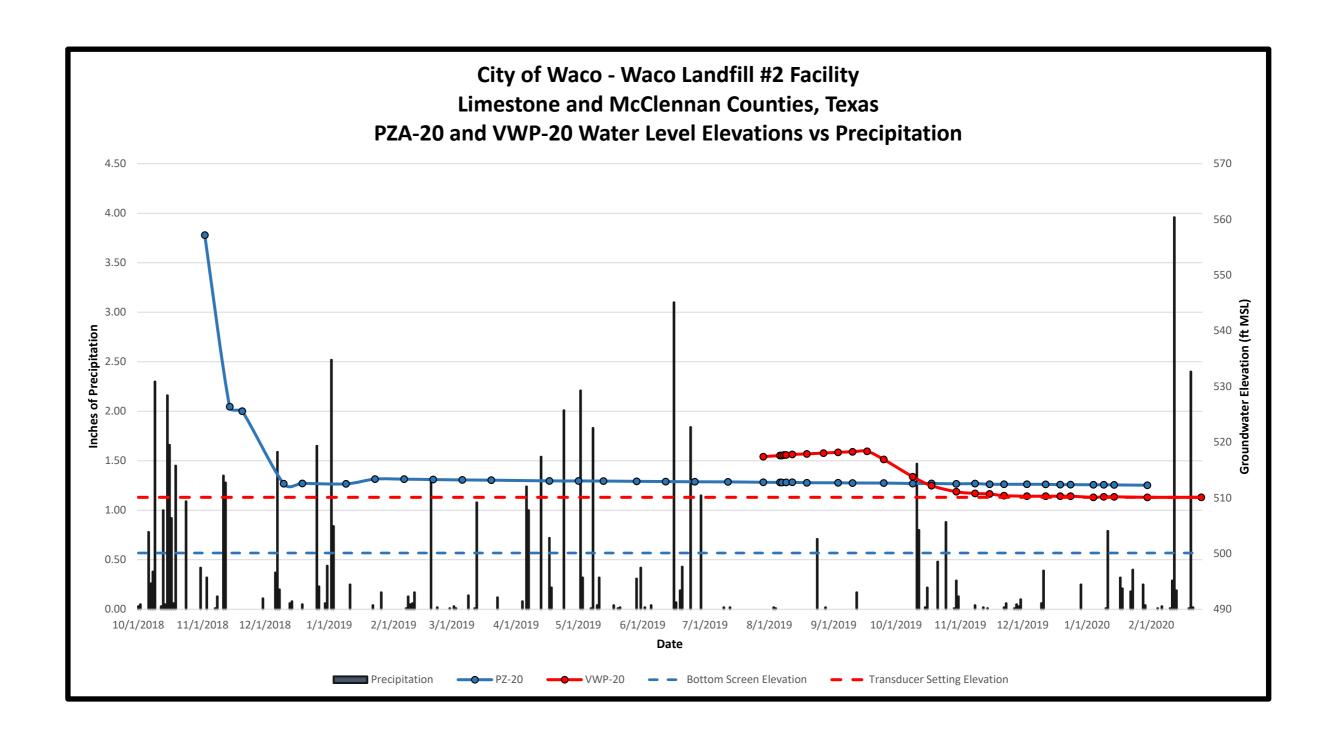


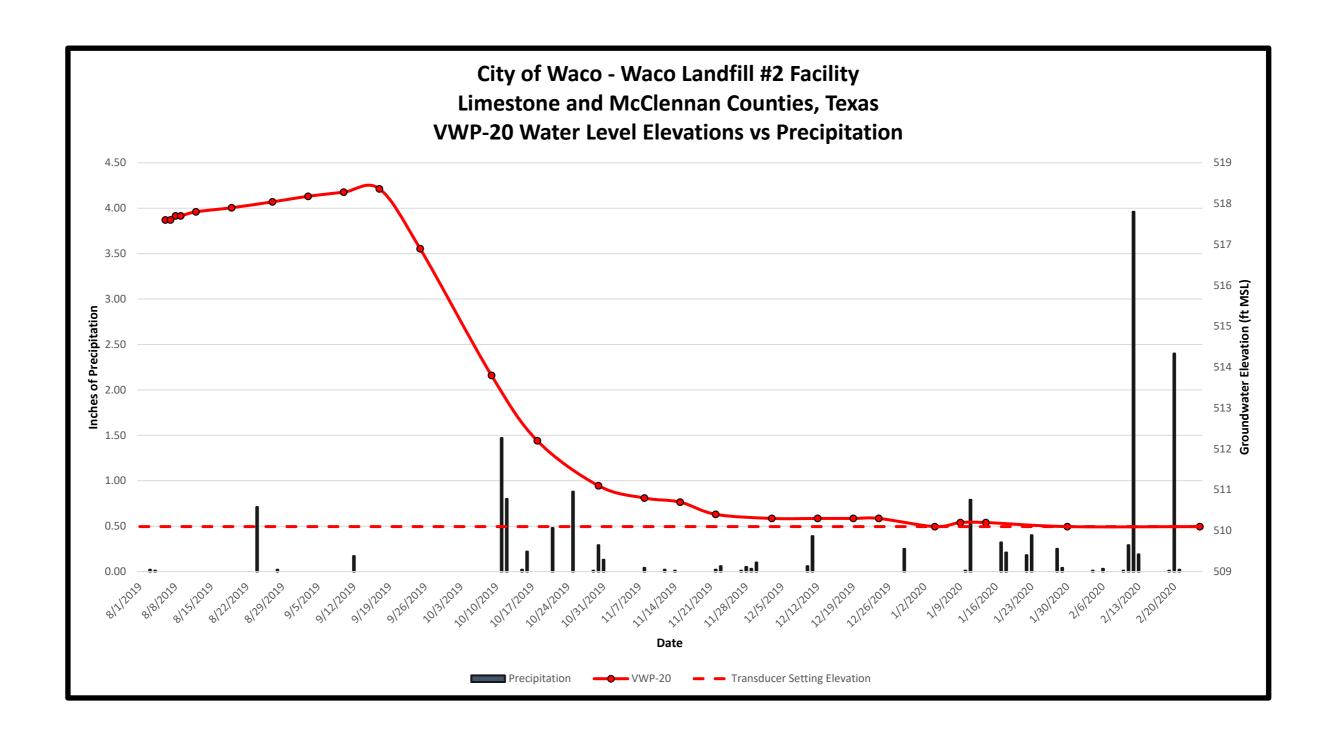


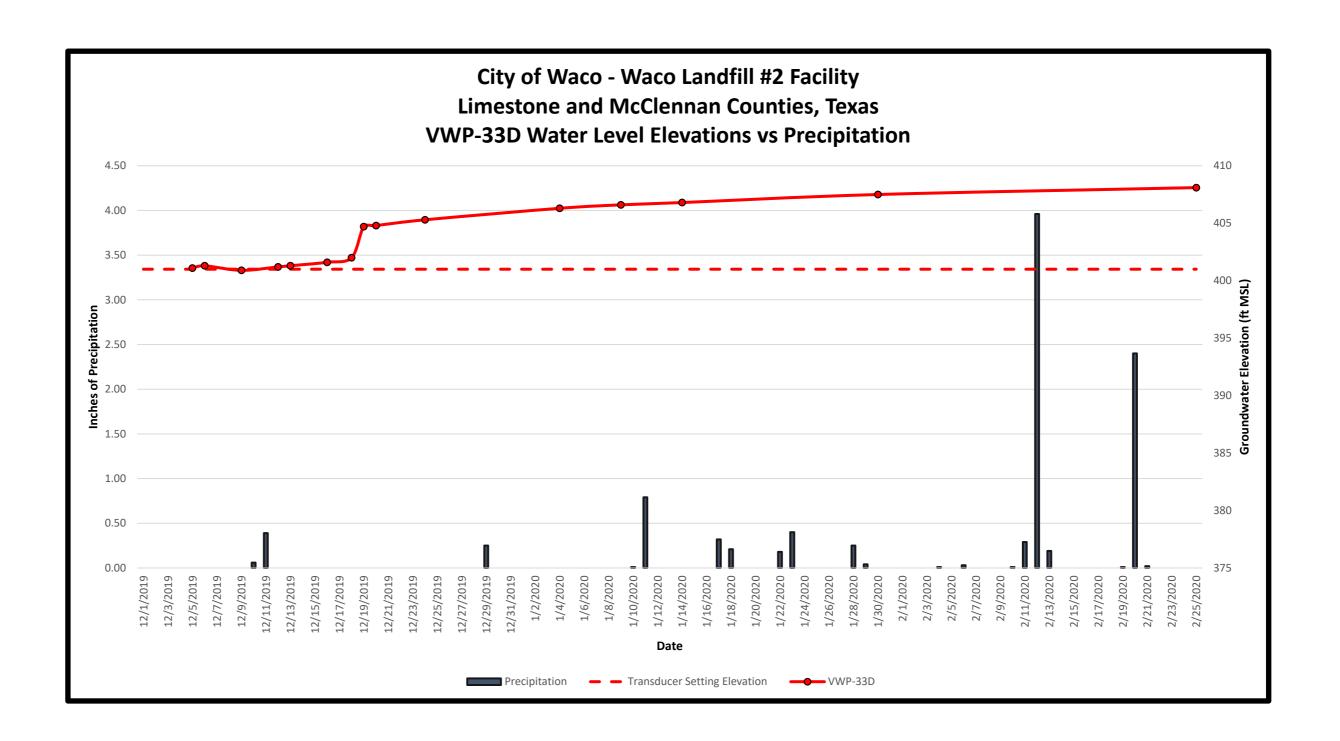


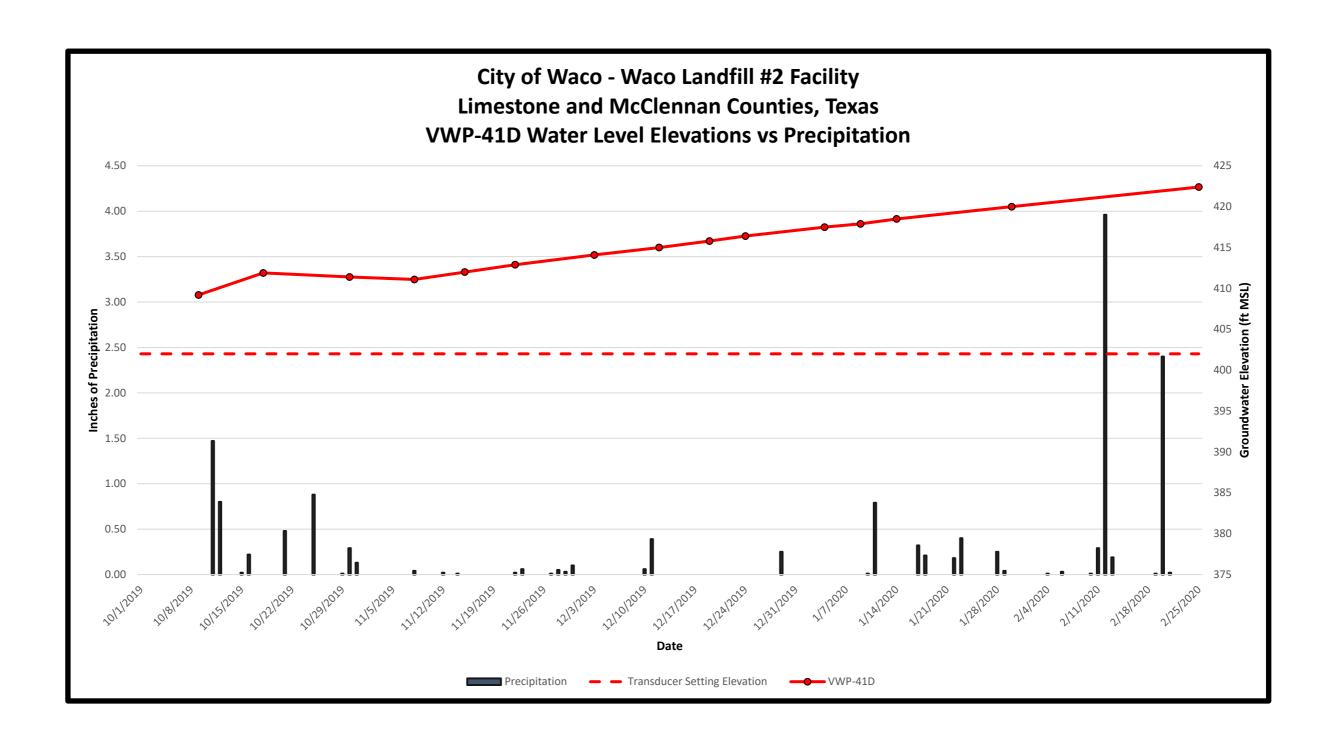


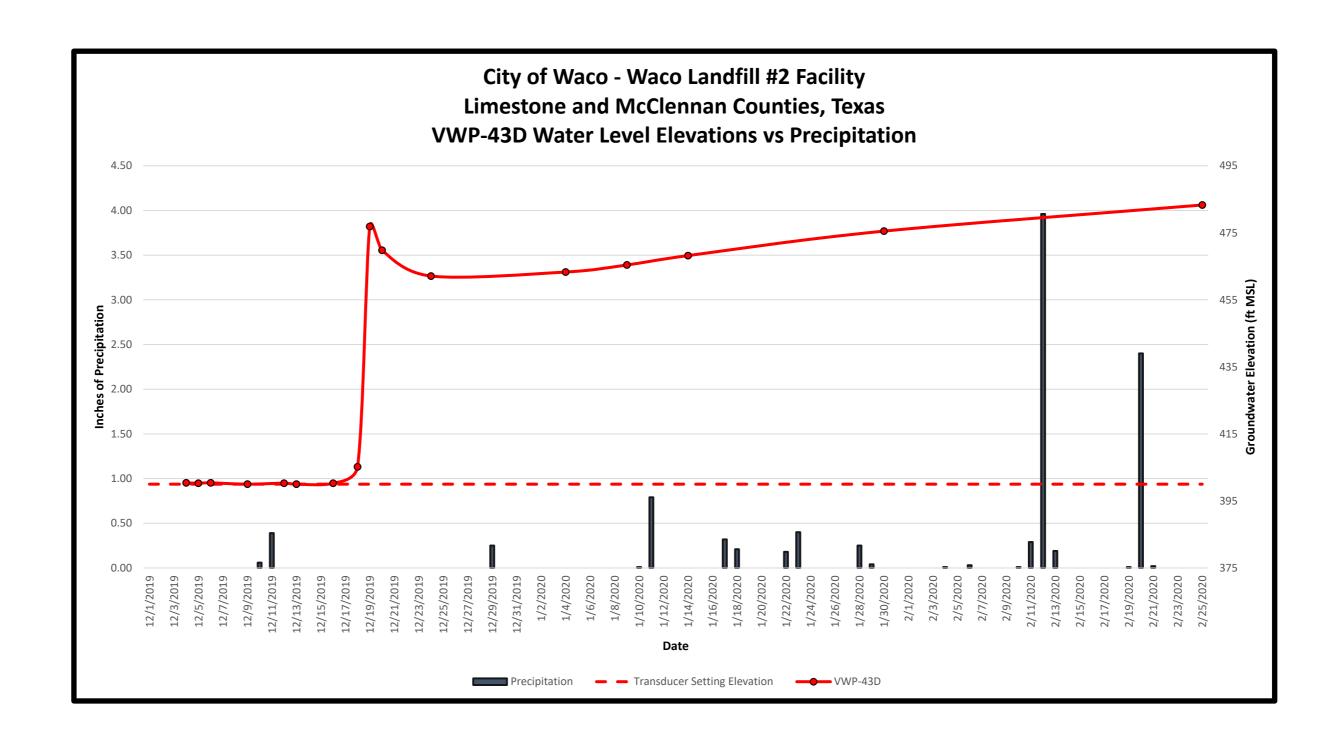


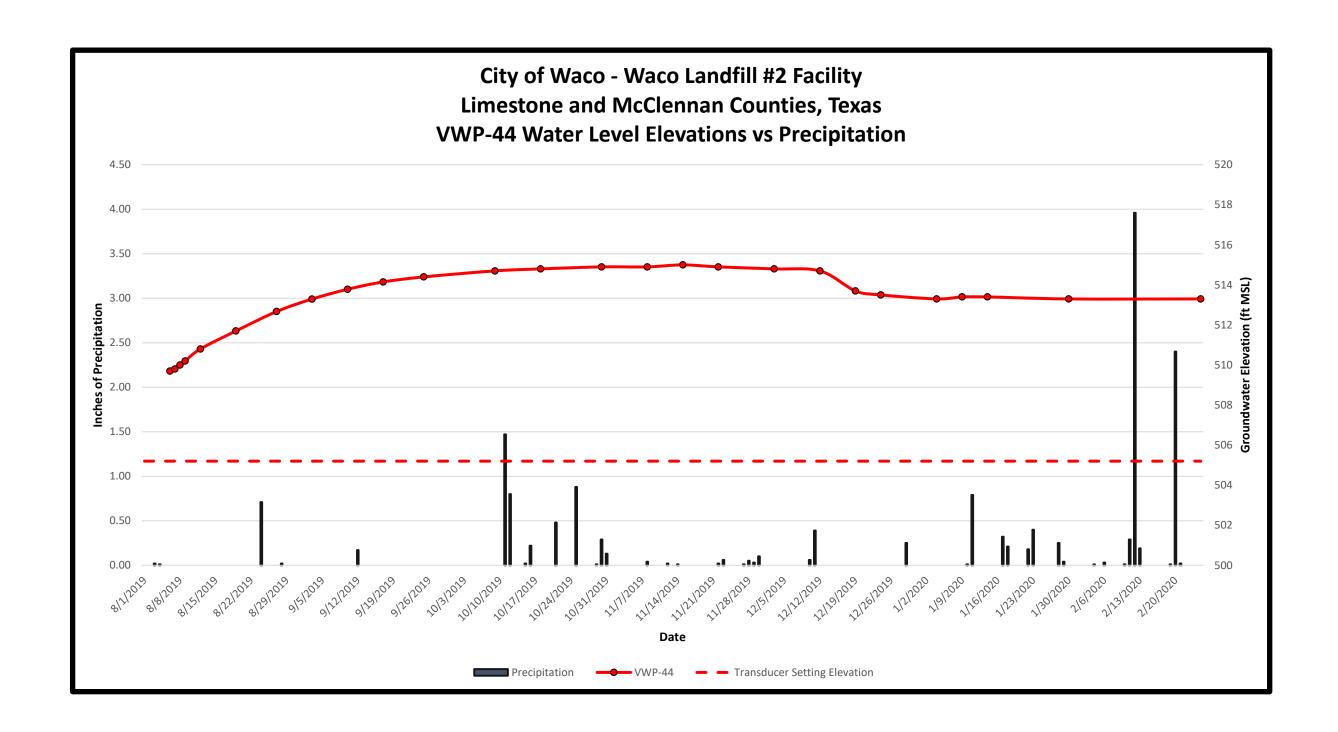


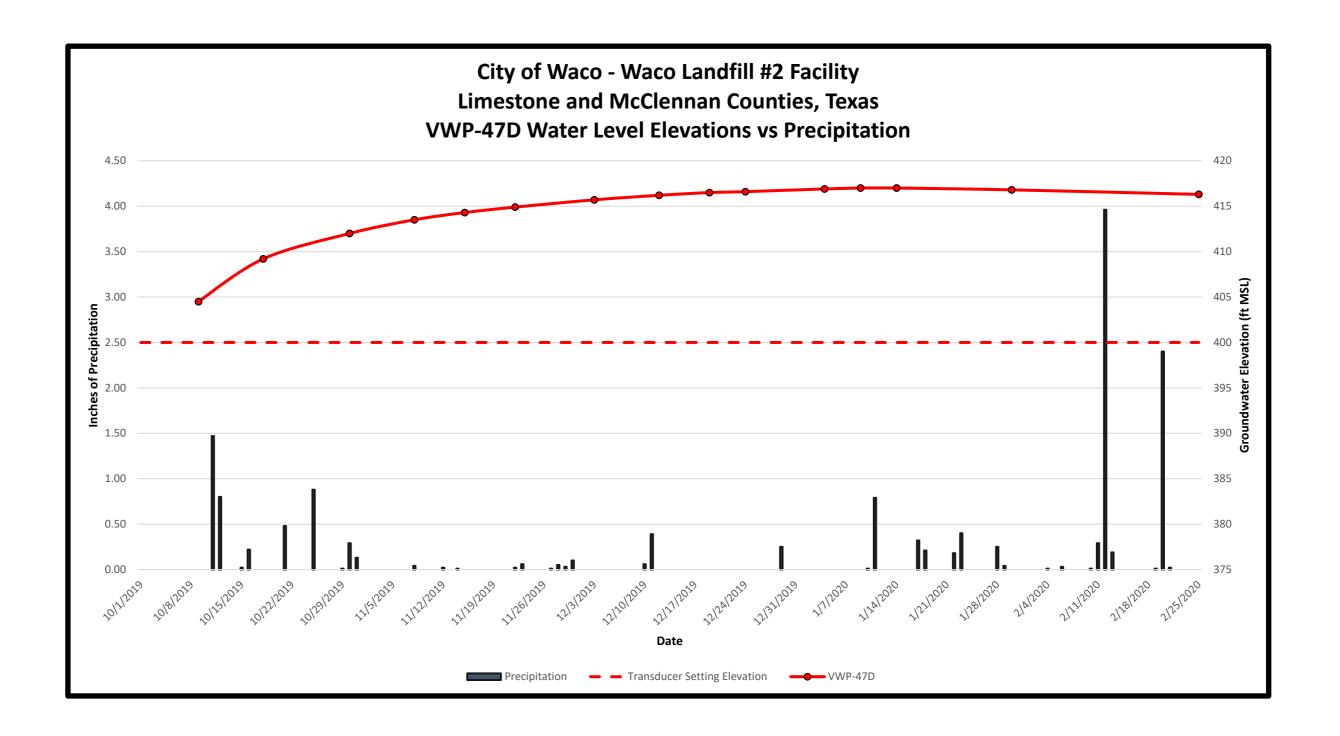












APPENDIX III-4.K

STANDPIPE PIEZOMETER HISTORIC WATER LEVEL DATA



															Append	dix III-	4.K: Sta	ndpipe	Piezomet	er Histo	ric Water	Level Da	ıta														
																		Dept	h to water (ft,	тос)																	
Well I.D.	1/23/2019	2/6/2019	2/20/2019	3/6/2019	3/20/2019	9 4/3/2019	4/17/2019	5/1/2019	5/13/2019	5/29/2019	6/12/2019	6/26/2019	7/12/2019	7/29/2019	8/6/2019	8/7/2019	8/9/2019	8/12/2019	8/19/2019	9/3/2019	9/10/2019	9/25/2019	10/9/2019	10/18/2019	10/30/2019	11/8/2019	11/15/2019	11/22/2019	12/3/2019	12/12/2019	12/19/2019	12/24/2019	1/4/2020	1/9/2020 1	1/14/2020	1/30/2020	2/25/2020
PZ-1	18.02	17.52	17.27	17.36	17.10	16.64	16.24	16.21	15.94	15.65	15.68	15.57	15.59	15.34	15.42	15.46	15.41	15.38	15.47	15.46	15.55	15.49	15.71	15.56	15.67	16.02	15.94	15.84	15.79	16	16.17	15.98	16.19	16	16.1	16.17	16.08
PZ-3	35.03	34.65	34.41	34.46	34.40	n/a	34.11	33.85	33.78	33.56	33.55	33.47	33.40	33.58	33.73	33.73	33.77	33.83	33.91	33.93	33.93	33.83	33.83	33.74	33.67	33.68	33.74	33.63	13.55	33.61	33.62	33.52	33.41	33.4	33.39	33.27	33.56
PZ-8	DRY	77.17	77.19	77.56	77.57	DRY	DRY	77.53	77.54	DRY	77.55	77.54	77.57	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	77.55	77.58	77.56	77.57	77.58	77.57	77.56	77.57	77.57	DRY	DRY	DRY
PZ-9	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
PZ-18	17.09	17.20	17.37	17.65	18.81	18.12	18.08	18.17	18.11	18.18	18.11	18.00	18.10	18.14	18.20	18.21	18.21	18.23	18.32	18.28	18.28	18.14	18.05	17.86	17.76	17.78	17.76	17.66	17.59	16.61	17.88	17.71	17.96	18.07	18.12	18.4	18.4
PZ-20	54.40	54.41	54.48	54.55	54.59	n/a	54.72	54.73	54.75	54.80	54.84	54.88	54.90	54.97	55.00	55.01	54.99	54.97	55.05	55.06	55.10	55.11	55.19	55.18	55.25	55.21	55.32	55.33	55.33	55.34	55.4	55.39	55.42	55.41	55.44	55.5	N/A
PZ-33	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
PZ-41	DRY	DRY	51.64	51.75	DRY	DRY	51.63	51.64	51.64	51.65	51.63	51.65	51.64	DRY	DRY	DRY	DRY	DRY	DRY	51.63	51.63	DRY	DRY	DRY	DRY	51.63	DRY	51.64	51.65	51.63	51.64	51.64	51.62	51.63	DRY	DRY	DRY
PZ-43	DRY	50.41	50.41	50.44	DRY	DRY	DRY	DRY	50.44	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	50.46	50.46	50.46	50.46	50.45	50.43	50.45	DRY	DRY	DRY
PZ-47	33.50	33.49	33.44	33.89	DRY	DRY	DRY	DRY	33.93	DRY	DRY	33.92	33.90	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
																	١	Water Level E	levation (ft ms	sl, from T.O.C																	
Well I.D.	1/22/2010	2/6/2019	2/20/2019	3/6/2019	2/20/2010	9 4/3/2019	4/17/2019	5/1/2019	5/13/2019	E/20/2010	6/12/2019	6/26/2019	7/12/2010	7/29/2019	9/6/2010	9/7/2010	8/9/2019	9/12/2010	8/19/2019	9/3/2019	9/10/2019	9/25/2019	10/9/2019	10/18/2019	10/30/2019	11/9/2010	11/15/2010	11/22/2010	12/2/2010	12/12/2010	12/19/2019	12/24/2010	1/4/2020	1/0/2020 1	1/14/2020	1/20/2020	2/25/2020
PZ-1	537.10	537.60	537.85	537.76	538.02	538.48	538.88	538.91	539.18	539.47	539.44	539.55	539.53	539.78	539.70	539.66	539.71	539.74	539.65	539.66	539.57	539.63	539.41	539.56	539.45	539.1	539.18	539.28	539.33	539.12	538.95	539.14	+		539.02	538.95	539.04
PZ-3	509.18	509.56	509.80	509.75	509.81	n/a	510.10	510.36	510.43	510.65	510.66	510.74	510.81	510.63	510.48	510.48	510.44	510.38	510.30	510.28	510.28	510.38	510.38	510.47	510.54	510.53	510.47	510.58	510.66	510.60	510.59	510.69	+		510.82	510.94	510.65
PZ-8	DRY	476.22	476.20	475.83	475.82	DRY	DRY	475.86	475.85	DRY	475.84	475.85	475.82	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	475.84	475.81	475.83	475.82	475.81	475.82	475.83		475.82	DRY	DRY	DRY
PZ-9	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
PZ-18	520.71	520.60	520.43	520.15	518.99	519.68	519.72	519.63	519.69	519.62	519.69	519.80	519.70	519.66	519.60	519.59	519.59	519.57	519.48	519.52	519.52	519.66	519.75	519.94	520.04	520.02	520.04	520.14	520.21	521.19	519.92	520.09	519.84		519.68	519.4	519.4
PZ-20	513.37	513.36	513.29	513.22	513.18	n/a	513.05	513.04	513.02	512.97	512.93	512.89	512.87	512.80	512.77	512.76	512.78	512.80	512.72	512.71	512.67	512.66	512.58	512.59	512.52	512.56	512.45	512.44	512.44	512.43	512.37	512.38	+ +		512.33	512.27	N/A
PZ-33	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
PZ-41	DRY	DRY	486.40	486.29	DRY	DRY	486.41	486.40	486.40	486.39	486.41	486.39	486.40	DRY	DRY	DRY	DRY	DRY	DRY	486.41	486.41	DRY	DRY	DRY	DRY	486.41	DRY	486.4	486.39	486.41	486.4	486.4	486.42	486.41	DRY	DRY	DRY
PZ-43	DRY	500.90	500.90	500.87	DRY	DRY	DRY	DRY	500.87	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	500.85	500.85	500.85	500.85	500.86	500.88	500.86	DRY	DRY	DRY
PZ-47	502.66	502.67	502.72	502.27	DRY	DRY	DRY	DRY	502.23	DRY	DRY	502.24	502.26	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
Well I.D.	1/22/2010	2/5/2010	2/20/2010	2/6/2010	2/20/2016	2 4/2/2010	4/17/2010	F /1 /2010	5/13/2019	F /20 /2010	6/12/2010	6/26/2010	7/12/2010	7/20/2010	9/6/2010	9/7/2010	8/0/2010		of Water Colu	` ,	0/10/2010	0/25/2010	10/9/2019	10/19/2010	10/20/2010	11/9/2010	11/15/2010	11/22/2010	12/2/2010	12/12/2010	12/10/2010	12/24/2010	1/4/2020	1/0/2020 1	1/14/2020	1/20/2020	2/25/2020
PZ-1	24.92	25.42	25.67	25.58	25.84	26.30	26.70	26.73	27.00	27.29	27.26	27.37	27.35	27.60	27.52	27.48	27.53	27.56	27.47	27.48	27.39	27.45	27.23	27.38	27.27	26.92	27	27.1	27.15	26.94	26.77	26.96	26.75	26.94	26.84	26.77	26.86
PZ-1 PZ-3	12.97	13.35	13.59	13.54	13.60	N/A	13.89	14.15	14.22	14.44	14.45	14.53	14.60	14.42	14.27	14.27	14.23	14.17	14.09	14.07	14.07	14.17	14.17	14.26	14.33	14.32	14.26	14.37	34.45	14.39	14.38	14.48	14.59	14.6	14.61	14.73	14.44
PZ-3 PZ-8	DRY	0.59	0.57	0.20	0.19	DRY	DRY	0.23	0.22	DRY	0.21	0.22	0.19	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	0.21	0.18	0.2	0.19	0.18	0.19	0.2	0.19	0.19	DRY	DRY	DRY
PZ-8	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
PZ-9 PZ-18	31.72	31.61	31.44	31.16	30.00	30.69	30.73	30.64	30.70	30.63	30.70	30.81	30.71	30.67	30.61	30.60	30.60	30.58	30.49	30.53	30.53	30.67	30.76	30.95	31.05	31.03	31.05	31.15	31.22	32.23	30.93	31.1	30.85	30.74	30.69	30.41	30.41
PZ-18	12.64	12.63	12.56	12.49	12.45	DRY	12.32	12.31	12.29	12.24	12.20	12.16	12.14	12.07	12.04	12.03	12.05	12.07	11.99	11.98	11.94	11.93	11.85	11.86	11.79	11.83	11.72	11.71	11.71	11.7	11.64	11.65	+	11.63	11.6	11.54	N/A
PZ-20	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
PZ-41	DRY	DRY	0.16	0.05	DRY	DRY	0.17	0.16	0.16	0.15	0.17	0.15	0.16	DRY	DRY	DRY	DRY	DRY	DRY	0.17	0.17	DRY	DRY	DRY	DRY	0.17	DRY	0.16	0.15	0.17	0.16	0.16	0.18	0.17	DRY	DRY	DRY
PZ-43	DRY	0.16	0.16	0.13	DRY	DRY	DRY	DRY	0.13	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	0.11	0.13	0.11	0.11	0.12	0.14	0.12	DRY	DRY	DRY
PZ-47	0.47	0.48	0.53	0.08	DRY	DRY	DRY	DRY	0.04	DRY	DRY	0.05	0.07	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY	DRY
1 = 7/	J. 77	0.40	0.55	3.00	5111	אכו		1 2111	0.07		DIVI	0.00	0.07	ווע	וועם	וווט	ואט	וווים	DIVI	DIVI	DIVI	DIVI	1 21/1	ווט	ווט	ווע	ואט	וווט	וועם	וווט	ווע	וווט	וווט	וווע	ואט	וווט	D.111

Revision 0

Well I.D.	Latitude	Longitude	Ground Surface Elevation (ft msl)	Concrete Slab Elevation (ft msl)	Top of PVC Pipe (ft msl)	Top of Steel Casing Elevation (ft msl)	Total Well Depth (ft below TOC)
PZ-1	31° 42′ 16.86706″ N	96° 55' 59.13570" W	551.74	552.12	555.12	555.49	42.94
PZ-3	31° 41′ 54.27334″ N	96° 55' 43.84234" W	541.20	541.58	544.21	545.05	48.00
PZ-8	31° 42' 11.59335" N	96° 55' 12.20821" W	550.34	550.89	553.39	553.74	77.76
PZ-9	31° 42′ 10.45884″ N	96° 55' 37.43147" W	535.30	535.58	539.44	539.94	37.45
PZ-18	31° 42′ 28.96389″ N	96° 55' 26.98650" W	534.84	535.23	537.80	538.26	48.81
PZ-20	31° 42′ 34.92848″ N	96° 55' 14.44772" W	564.68	565.05	567.77	568.35	67.04
PZ-33	31° 42' 00.00182" N	96° 55' 14.53975" W	539.20	539.57	542.49	542.89	57.59
PZ-41	31° 42' 10.66572" N	96° 54' 59.07613" W	534.62	535.03	538.04	538.39	51.80
PZ-43	31° 42′ 20.55019″ N	96° 55' 01.03302" W	548.86	549.20	551.31	552.07	50.57
PZ-47	31° 42' 04.14903" N	96° 55' 28.39274" W	532.48	532.89	536.16	536.59	33.97

APPENDIX III-4.L

VIBRATING WIRE PIEZOMETER HISTORIC WATER LEVEL DATA



														Арр	endix III-4	l.L: Vibratin	g Wire Pie	ezometer	Historic W	ater Leve	el Data														
VWP ID	7/29/2019	8/6/2019	8/7/2019 8/	/8/2019 8/	/9/2019	8/12/2019	8/19/2019	8/27/2019	9/3/2019	9/10/2019	9/17/2019	9/25/2019	10/9/2019	10/18/2019	10/30/2019	11/8/2019	Readii 11/15/2019		12/3/2019	12/4/2019	12/5/2019	12/6/2019	12/9/2019	12/12/2019	12/13/2019	12/16/2019	12/18/2019	12/19/2019	12/20/2019	12/24/201	9 1/4/2020	1/9/2020	1/14/2020	1/30/2020	2/25/2020
VWP-1 VWP-3		7948.2 8684.3			7950.2 8652.7	7952.6 8642.8	7952.7 8583.1	7954.5 8562.5	7959.1 8552.5	7960.2 8548.8	7965.5 8547.2	7941.4 8545.2	7973.3 8539.6	7981.3 8541.9	7980.2 8539.0	7978.7 8540.1	7982.5 8538.3	7990.5 8540.4	7999.3 8543.8					7998.3 8538.7				7996.6 8541.3		8004.3 8542.3	8003.8 8537.1	8011.9 8541.3	8011.7 8539.9	8016.0 8537.6	8020.7 8535.5
VWP-4 VWP-8		8716.0 8690.2	8717.2	8717.8	8718.8 8692.6	8720.7 8694.8	8717.0 8689.9	8718.1 8691.3	8717.5 8690.0	8715.1 8687.3	8718.6 8690.7	8720.3 8693.3	8713.6 8686.8	8723 8696.6	8716.2 8688.4	8708.5 8681.2	8708.8 8681.9	8717 8689.2	8717.5 8690.4					8714.4 8687.6		 		8708 8681.4		8714.9 8689.1	8709.9 8682.5	8719.1 8693.2	8716.7 8690.1	8716.7 8689.2	8719.3 8692.4
VWP-8D						-																8929.3	8942.3	8762.4	8739.4	8637	8563.8	8399.3	8380.9	8121.1	6927.9	6688.5	6570.0	6411.4	6299.4
VWP-9 VWP-9D		8599.6 ——	8600.6		8601.7 ——	8603.9 ——	8600.8	8599.5 ——	8600.4	8598.3 ——	8600.9	8603.2	8597.4 ——	8605.5 ——	8599.2 ——	8591.1 ——	8591.9 ——	8600.3	8600.3					8592.7 ——	 8712.3	6743.6	 5978.5	8590.7 5890.9	5830.6	8598.2 5739.9	8593.2 5669.8	8601.1 5664.2	8599.0 5654.6	8599.5 5642.3	8601.5 5625.6
VWP-18 VWP-18D	8599.2 ——	8467.5	8458.0		8435.3	8404.8	8351.2	8303.2	8271.7	8248.4	8231.2	8217	8199.5 ——	8187.3 ——	8174.3	8163.9	8157.1 ——	8152.1 ——	8144.3					8098.2 ——				8143.3 6433.5	 6572.6	8151.6 6743.7	8160.2 6796.6	8160.4 6784.6	8160.9 6764.6	8160.2 6669.5	8157.1 6514.2
VWP-19 VWP-20	8812.8	8814.8 8570.1	8815.0 8569.5		8815.5	8815.8	8816.2	8816.9	8815.5	8815.3	8814.8	8815.8	8815.1	8815.6 8715.2	8815.6	8811.7	8809.9	8813.7	8814					8811.1				8809.3		8812.2 8764.8	8812.2 8770.7	8813.8	8813.7	8814.2	8816.8 8769.4
VWP-25	8576.4 ——	8766.4	8767.7	8768.4	8568.2 8768.5	8566.3 8770.5	8561.8 8766.6	8558.6 8765.5	8555.0 8766.7	8552.3 8764.3	8550.1 8767.4	8587.9 8769.5	8672.3 8762.9	8771.3	8743.6 8765.0	8751.9 8757.5	8754.9 8758.2	8763.4 8765.6	8766.3 8765.8					8765.3 8758.3				8765.9 8756.2		8763.7	8758.5	8767.4 8767.6	8768.5 8764.5	8769.5 8764.8	8766.6
VWP-26 VWP-27	8645.4 8618.6	8648.0 8620.8			8649.7 8622.6	8651.7 8624.6	8647.0 8619.4	8648.0 8620.7	8646.8 8619.8	8644.3 8617.5	8646.8 8620.5	8649.4 8622.5	8643.0 8616.5	8652.7 8625.7	8644.4 8618.4	8637.4 8610.7	8637.9 8611.2	8645.1 8619.1	8646 8619.8					8642.8 8617.2				8637.1 8610.7		8644.1 8617.8	8637.8 8611.6	8647.8 8621.4	8644.9 8618.9	8644.6 8618.8	8647.4 8621.4
VWP-30 VWP-33	8779.3 ——	8692.9 8625.2			8689.6 8629.9	8689.8 8633.5	8689.9 8630.3	8688.8 8634.2	8688.6 8634.6	8686.6 8633.5	8689.5 8638.6	8691.2 8639.5	8684.8 8620.7	8692.9 8631.7	8688.4 8622.5	8679.3 8614.3	8679.8 8614.6	8686.8 8624.1	8687.5 8624.6		 			8684.6 8621.6	 			8679.2 8614.3		8686 8622.9	8680.8 8616.4	8689.7 8627.5	8687.5 8624.8	8685.2 8624.3	8599.3 8627.3
VWP-33D																					8958	8953.7	8965.7	8957	8955.5	8945	8935.6	8860.3	8856.3	8844.5	8817.3	8808.1	8801.7	8783.2	8765.6
VWP-41 VWP-41D	8628.6	8631.7 ——	8632.7 8 ——		8633.8 ——	8636.3 ——	8631.5	8632.6	8631.8	8629.4	8632.9	8635.3	8629.0 8788.2	8638.4 8717.3	8630.8 8730.9	8623.8 8739.7	8624.3 8715.6	8631.7 8692.4	8632.7 8660.7					8629.5 8634.7				8624.1 8613.9		8630.8 8599.5	8625.6 8570.7	8634.9 8558.2	8632.4 8544.1	8632.1 8504.1	8635.2 8441.0
VWP-43 VWP-43D	8641.7	8643.8	8644.3	8645.2	8645.4	8647.1 ——	8643.8	8644.0	8643.8	8641.8	8644.6	8646.3	8640.6 ——	8648.4	8642.4	8634.7	8635.4 ——	8643.5	8644.1	—— 8871.2	 8874.3	—— 8870.9	 8881.9	8641.1 8872.7	 8883.1	—— 8874.7	—— 8736.7	8635.1 6716.3	—— 6916.7	8642.5 7132.4	8636.3 7099.7	8645.4 7039.9	8643.8 6961.8	8643.3 6755.9	8645.5 6534.9
VWP-44		8661.3			8646.3	8633.6	8609.6	8585.6	8569.9	8557.7	8548.5	8542.1	8535.2	8532.3	8529.8	8528.5	8528.4	8529	8531.6					8534.5				8560.7		8565.9	8569.3	8566.3	8567.1	8569.3	8568.7
VWP-47 VWP-47D		8718.1 ——	8718.9 ——		8719.9 ——	8722.8 ——	8718.9 ——	8718.8	8718.7 ——	8716.3 ——	8719.2 ——	8721.1	8715.4 8801.7	8723 8673.1	8716.7 8596.5	8709 8556.3	8709.3 8534.6	8717.2 8517.5	8717.5 8495.5					8709.6 8482.8	 			8708.2 8474		8715.7 8470.2	8710.3 8463.2	8719.4 8461.7	8716.5 8461.5	8717.5 8466.1	8719.6 8479.8
																	Tempera	ature (°C)																	
VWP ID	7/29/2019	8/6/2019 21.5	8/7/2019 8/	/ 8/2019 8 /	/9/2019	8/12/2019 21.5	8/19/2019 21.4	8/27/2019	9/3/2019	9/10/2019	9/17/2019 21.4	9/25/2019	10/9/2019 21.4	10/18/2019	10/30/2019 21.3	11/8/2019 21.3	11/15/2019 21.4	11/22/2019 21.4	12/3/2019	12/4/2019 ——	12/5/2019	12/6/2019 ——	12/9/2019	12/12/2019	12/13/2019	12/16/2019	12/18/2019	12/19/2019 21.4	12/20/2019	12/24/201 21.4	1/4/2020 21.5	1/9/2020 21.4	1/14/2020 21.4	1/30/2020 21.5	2/25/2020 21.5
VWP-3		21.5	21.6	21.5	21.5	21.5	21.5	21.5	21.5	21.5	21.4	21.4	21.4	21.4	21.4	21.4	21.4	21.5	21.4					21.4				21.4		21.5	21.5	21.5	21.5	21.4	21.5
VWP-4 VWP-8		20.8	20.8	20.8	20.8	20.7 20.0	20.8	20.8	20.8	20.8	20.8	20.9	21.0 20.0	21	21.1	21.2	21.2 20.0	21.3 20	21.3					21.3 20				21.4 20		21.4	21.5	21.4	21.4	21.4 20.0	21.4
VWP-8D VWP-9		 21.2	 21.1	 21.2	 21.1	 21.1	21.1	21.1	 21.1	21.1	21.1	21.1	 21.1	 21.1	 21.2	21.2	 21.1	21.2	21.4		 	22.7	22	21.9 21.2	21.9	21.8	21.8	21.8 21.3	21.8	21.8 21.3	21.8 21.3	21.8 21.3	21.8 21.3	21.7 21.4	21.8 21.5
VWP-9D			—— 20.8																						22.4	22.5	22.4	22.5	22.5	22.4	22.5	22.5	22.5	22.5	22.5
VWP-18 VWP-18D	20.8	20.8	20.8		20.7	20.8	20.8	20.7	20.7	20.7	20.7	20.7	20.7	20.7	20.7	20.7	20.6	20.7	20.7					20.7				20.7 22.7	22.4	20.7	20.7	20.7	20.8	20.8	20.8
VWP-19 VWP-20	21.7 21.7	21.6 21.7	21.7 21.7	21.7	21.7 21.7	21.7 21.7	21.6 21.7	21.7	21.6 21.7	21.6 21.7	21.6 21.7	21.6 21.7	21.6 21.7	21.6 21.7	21.6 21.7	21.6 21.7	21.6 21.7	21.6 21.7	21.6 21.7					21.6 21.8			<u></u>	21.6 21.7		21.6 21.7	21.6 21.7	21.5 21.7	21.7 21.7	21.6 21.7	21.6 21.7
VWP-25 VWP-26		19.5	19.4	19.5 19.7	19.4 19.7	19.4 19.7	19.4 19.7	19.4 19.7	19.4 19.7	19.4	19.4 19.7	19.4	19.4 19.9	19.4	19.4	19.4	19.5	19.5	19.6					19.5				19.5		19.6	19.6	20.2	19.7	19.6 20.5	19.7
VWP-27	19.7	19.7 20.8	20.8	20.8	20.8	20.7	20.8	20.7	20.8	20.8	20.8	20.8	20.8	20.9	20.0	20.1	20.1	20.1	21.1					21.2				20.3		20.3	20.4	20.4	20.5	21.4	21.4
VWP-30 VWP-33	20.3	20.2	20.2 21.6	20.2	20.2	20.2 21.5	20.2	20.2	20.2	20.2	20.2	20.2	20.2 21.4	20.1 21.4	20.1	20.1	20.2 21.4	20.1	20.1					20.1 21.4				20.1 21.5		20.1	20.1	20.2	20.2 21.5	20.2 21.4	20.2 21.5
VWP-33D VWP-41	 19.7	 19.7	 19.7		 19.7	 19.7	 19.7	 19.7	 19.6	 19.6	 19.6	 19.6	 19.6	 19.6	 19.6	 19.7	 19.6	 19.6	 19.6		23.5	22.7	22.4	22.3	22.3	22.2	22.3	22.2 19.6	22.2	22.2	22.1 19.7	22.2 19.6	22.2 19.6	22.1 19.6	22.1 19.7
VWP-41D	19.7	19.7	——		——		19.7				19.6	19.6	21.7	21.4	21.4	21.3	21.3	21.4	21.4					21.3				21.2		21.3	21.3	21.3	21.3	21.3	21.3
VWP-43 VWP-43D	20.4	20.4	20.3	20.3	20.3	20.3	20.3	20.2	20.2	20.3	20.2	20.2	20.2	20.2	20.2	20.2	20.2	20.2	20.2	22.4	22.1	22	21.9	20.2 21.9	21.9	21.8	21.9	20.2 21.8	21.9	20.2	20.2	20.2	20.2	20.3 21.8	20.3
VWP-44 VWP-47		22.1 19.4	22.1 19.4	22.1 19.4	22.1 19.4	22.1 19.4	22.1 19.5	22.1 19.6	22.1 19.6	22.0 19.9	22.1 20.0	22.1 20.2	22.1 20.5	22.1 20.7	22.1 20.9	22 21.1	22.0 21.1	22.1 21.3	22.0 21.3					22.1				22 21.3		22 21.3	22 21.2	22.0 21.2	22.0 21.0	22.0 20.8	22.0 20.5
VWP-47D													22.1	21.3	21.2	21.2	21.2	21.2	21.1					21.2				21.1		21.2	21.1	21.2	21.2	21.1	21.1
																	Pressu	ro (DSI)																	
	1					- 4 4	T - 4:- 4:		T - 4- 4	T - 4 - 4		T - 4 4						<u> </u>	T										T	T	-				
VWP ID VWP-1	7/29/2019	- 	8/7/2019 8/ 8.922337 8.		•		+	8/27/2019 8.8394912		+		9/25/2019 9.0280002		10/18/2019 8.4544554		11/8/2019 8.4918694	11/15/2019	<u> </u>		12/4/2019 ——	12/5/2019	12/6/2019	12/9/2019	12/12/2019 8.2092092	12/13/2019 ——	12/16/2019	12/18/2019 ——	12/19/2019 8.2336722	12/20/2019	12/24/201 8.1228692	1/4/2020 2 8.129448		1/14/2020 8.0163832		2/25/2020 7.886257
	+	- 	8.922337 8.	.915142 8.	•		+			+		 				+ 	11/15/2019 8.4365712 2.53484	11/22/2019 8.3214512 2.498774					' ' ' 		<u> </u>	 		8.2336722 2.48585	+		2 8.129448 2 2.552663		8.0163832		7.886257 2.578791
VWP-1 VWP-3 VWP-4 VWP-8		8.929532 0.148887 -0.033429 0.027982	8.922337 8.	.915142 8. .331783 0. .063075 -0 .010437 -0	.900752 .664915 .079545 .010298	8.866216 0.826582 -0.109845 -0.045388	8.8653932 1.801483 -0.049899 0.032767		8.7732972 2.301181 -0.058134 0.031172	2.361602 -0.018606 0.074237	8.6812012 2.389503 -0.076251 0.020007	9.0280002 2.422163 -0.105243 -0.021463	8.5689592 2.513611 0.004113 0.082212	8.4544554 2.476052 -0.150705 -0.074098	8.4702844 2.523409 -0.039702 0.056692	8.4918694 2.505446 0.086124 0.171532	11/15/2019 8.4365712 2.53484 0.081183 0.160367	11/22/2019 8.3214512 2.498774 -0.054864 0.043932	8.194203 2.445025 -0.063099 0.024792	 		 	 	8.2092092 2.528308 -0.012042 0.069452			 	8.2336722 2.48585 0.092373 0.168342		8.1228692 2.467747 -0.02127 0.045527	2 8.129448 2 2.552663 0.060087 0.150797	8.0135052 2.484077 -0.090444 -0.019868	8.0163832 2.506939 -0.050916 0.029577	7.95389 2.546271 -0.050916 0.043932	7.886257 2.578791 -0.093738 -0.007108
VWP-1 VWP-3 VWP-4		8.929532 0.148887 -0.033429	8.922337 8. 0.176508 0. -0.053193 -0 0.013627 0. ——	.915142 8. .331783 0. .063075 -0 .010437 -0	.900752 .664915 .079545	8.866216 0.826582 -0.109845	8.8653932 1.801483 -0.049899	8.8394912 2.137881 -0.068016	8.7732972 2.301181 -0.058134	8.7574682 2.361602 -0.018606 0.074237	8.6812012 2.389503 -0.076251 0.020007 ——	9.0280002 2.422163 -0.105243	8.5689592 2.513611 0.004113	8.4544554 2.476052 -0.150705	8.4702844 2.523409 -0.039702	8.4918694 2.505446 0.086124	11/15/2019 8.4365712 2.53484 0.081183	11/22/2019 8.3214512 2.498774 -0.054864	8.194203 2.445025 -0.063099			 	 	8.2092092 2.528308 -0.012042	 	 4.956661	 6.165193	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455		8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025	2 8.129448 2.552663 0.060087 0.150797 33.173902 0.091375	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394
VWP-1 VWP-3 VWP-4 VWP-8 VWP-8D	 	8.929532 0.148887 -0.033429 0.027982	8.922337 8. 0.176508 0. -0.053193 -0 0.013627 0. -0.033995 -0	915142 8. 331783 0. .063075 -0 .010437 -0 .049025 -0	.900752 .664915 .079545 .010298	8.866216 0.826582 -0.109845 -0.045388 ——	8.8653932 1.801483 -0.049899 0.032767 ——	8.8394912 2.137881 -0.068016 0.010437	8.7732972 2.301181 -0.058134 0.031172 ——	8.7574682 2.361602 -0.018606 0.074237	8.6812012 2.389503 -0.076251 0.020007 -0.039176	9.0280002 2.422163 -0.105243 -0.021463 ——	8.5689592 2.513611 0.004113 0.082212 ——	8.4544554 2.476052 -0.150705 -0.074098	8.4702844 2.523409 -0.039702 0.056692	8.4918694 2.505446 0.086124 0.171532 ——	11/15/2019 8.4365712 2.53484 0.081183 0.160367 ——	11/22/2019 8.3214512 2.498774 -0.054864 0.043932	8.194203 2.445025 -0.063099 0.024792	 		 0.108153	 -0.088872	8.2092092 2.528308 -0.012042 0.069452 2.883792	 3.263522	 4.956661	 6.165193	8.2336722 2.48585 0.092373 0.168342 8.881088	 9.184872	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 50.562496	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424
VWP-1 VWP-3 VWP-4 VWP-8 VWP-8D VWP-9 VWP-9D VWP-18	2.640668	8.929532 0.148887 -0.033429 0.027982 -0.017939 4.871666 	8.922337 8. 0.176508 00.053193 -0 0.013627 00.033995 -0 5.032596 5.	915142 8. 331783 0063075 -0 .010437 -0	.900752 .664915 .079545 .010298 .052992 .418397	8.866216 0.826582 -0.109845 -0.045388 -0.090986 5.933804 	8.8653932 1.801483 -0.049899 0.032767 -0.037449 6.841788	8.8394912 2.137881 -0.068016 0.010437 -0.014998 7.656171	8.7732972 2.301181 -0.058134 0.0311720.030541 8.189781	2 8.7574682 2.361602 -0.018606 0.074237 0.005726 8.584483	8.6812012 2.389503 -0.076251 0.020007 -0.039176 8.875851	9.0280002 2.422163 -0.105243 -0.021463 -0.078897 9.116399	8.5689592 2.513611 0.004113 0.082212 0.021269 9.412849	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.619517	8.4702844 2.523409 -0.039702 0.056692 -0.011031 9.839737	8.4918694 2.505446 0.086124 0.171532 —— 0.128856 —— 10.015913	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 ——	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.215805	8.194203 2.445025 -0.063099 0.024792 -0.032456 10.347937 	 	 	 0.108153 	 -0.088872 	8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 —— 11.128871 ——	 3.263522 5.41438 	 4.956661 34.627304 	 6.165193 45.983972 	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382	9.184872 —— 48.176224 —— 35.451316	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224275 32.978922	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 6 50.562496 5 10.078591 1 32.21951	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019
VWP-1 VWP-3 VWP-4 VWP-8 VWP-8D VWP-9 VWP-18 VWP-18 VWP-18D VWP-19 VWP-20		8.929532 0.148887 -0.033429 0.027982 -0.017939 4.871666 -0.42593 3.25128	8.922337 8. 0.176508 00.053193 -0 0.013627 00.033995 -0 5.032596 50.430932 -0 3.261012 3.	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0186319 5434274 -0 .272366 3.	.900752 .664915 .079545 .010298 .052992 .418397 .439287 .282098	8.866216 0.826582 -0.109845 -0.045388 -0.090986 5.933804 -0.4443 3.312916	8.8653932 1.801483 -0.049899 0.032767 -0.037449 6.841788 -0.449324 3.385906	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202	2.361602 2.361602 -0.018606 0.074237 0.005726 8.584483 -0.434285 3.539996	8.6812012 2.389503 -0.076251 0.020007 -0.039176 8.875851 -0.42593 3.57568	9.0280002 2.422163 -0.105243 -0.021463 -0.078897 9.116399 -0.44264 2.962564	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954	8.194203 2.445025 -0.063099 0.024792 -0.032456 10.347937			 0.108153 	 -0.088872 	8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 11.1288710.364103 0.083276	 3.263522 5.41438 	 4.956661 34.627304 	 6.165193 45.983972 	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404	9.184872 —— 48.176224 —— 35.451316 ——	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224279 32.978922 -0.382484 0.093246	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 6. 50.562496 10.078591 1 32.21951 4 -0.382484 6 -0.002452	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634
VWP-1 VWP-3 VWP-4 VWP-8 VWP-8D VWP-9 VWP-9D VWP-18 VWP-18D VWP-19		8.929532 0.148887 -0.033429 0.027982 -0.017939 4.871666 -0.42593 3.25128 -0.041373	8.922337 8. 0.176508 00.053193 -0 0.013627 00.033995 -0 5.032596 50.430932 -0 3.261012 3.	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0	.900752 .664915 .079545 .010298 	8.866216 0.826582 -0.109845 -0.045388 -0.090986 5.933804 -0.4443	8.8653932 1.801483 -0.049899 0.032767 -0.037449 6.841788 -0.449324 3.385906 -0.043939	8.8394912 2.137881 -0.068016 0.010437 -0.014998 7.656171 -0.462681	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627	2 8.7574682 2.361602 -0.018606 0.074237 0.005726 8.584483 -0.434285 3.539996 -0.00431	8.6812012 2.389503 -0.076251 0.020007 -0.039176 8.875851 -0.42593 3.57568 -0.057723	9.0280002 2.422163 -0.105243 -0.021463 -0.078897 9.116399 -0.44264	8.5689592 2.513611 0.004113 0.082212 0.021269 9.4128490.430943	8.4544554 2.476052 -0.150705 -0.074098 -0.118618 9.619517 -0.439298	8.4702844 2.523409 -0.039702 0.056692 -0.011031 9.839737 -0.439298	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549	8.194203 2.445025 -0.063099 0.024792 -0.032456 10.347937 -0.412562	 		 0.108153 	 -0.088872 	8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 —— 11.128871 —— -0.364103	 3.263522 5.41438 	 4.956661 34.627304 	 6.165193 45.983972 	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025	9.184872 —— 48.176224 —— 35.451316	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224272 32.978922 -0.382484	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 6 50.562496 5 10.078591 1 32.21951 1 -0.382484 6 -0.002452 8 0.093864	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579
VWP-1 VWP-3 VWP-4 VWP-8 VWP-8 VWP-9 VWP-9 VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-27		8.929532 0.148887 -0.033429 0.027982 -0.017939 4.871666 -0.42593 3.25128 -0.041373 -0.123938 -0.133506	8.922337 8. 0.176508 00.053193 -0 0.013627 00.033995 -0 5.032596 50.430932 -0 3.261012 30.062892 -0 -0.130313 -0 -0.143388 -0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0	.900752 .664915 .079545 .010298 .052992 .418397 .439287 .282098 .076676 .152974 .163152	8.866216 0.826582 -0.109845 -0.045388 -0.090986 5.933804 -0.4443 3.312916 -0.111136 -0.1871344 -0.194625	8.8653932 1.801483 -0.049899 0.032767 -0.037449 6.841788 -0.449324 3.385906 -0.043939 -0.1068584 -0.110448	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.130392	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662	8.7574682 2.361602 -0.018606 0.074237 0.005726 8.584483 -0.434285 3.539996 -0.00431 -0.0607424 -0.079155	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424	9.0280002 2.422163 -0.105243 -0.021463 -0.078897 9.116399 -0.44264 2.962564 -0.093906 -0.148308 -0.161505	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.0394536 -0.062685	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908	8.194203 2.445025 -0.063099 0.024792 -0.032456 10.347937 -0.412562 0.068916 -0.031915 -0.0920664 -0.121437			 0.108153 	 -0.088872 	8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 11.1288710.364103 0.083276 0.09819 -0.037868 -0.080082	 3.263522 5.41438 	 4.956661 34.627304 	 6.165193 45.983972 	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973	9.184872 —— 48.176224 —— 35.451316 ——	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224275 32.978922 -0.382484 0.093246 0.004268 -0.060072 -0.091431	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 6 50.562496 10.078591 1 32.21951 1 -0.382484 -0.002452 0.093864 0.0470744 0.009216	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219
VWP-1 VWP-3 VWP-4 VWP-8 VWP-8 VWP-9 VWP-9 VWP-18 VWP-18 VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33	2.6406680.39417 3.149094 -0.0795304 -0.097272 -1.67265	8.929532 0.148887 -0.033429 0.027982 -0.017939 4.871666 -0.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 0.15327 -0 .121095 -0 .087352 -0	.900752 .664915 .079545 .010298 .052992 .418397 .439287 .282098 .076676 .152974 .163152 .105381	8.866216 0.826582 -0.109845 -0.045388 -0.090986 5.933804 -0.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.1784412	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 -0.1068584 -0.110619 -0.1310172	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.130392 -0.091413 -0.1880208	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743	8.7574682 2.361602 -0.018606 0.074237 0.005726 8.584483 -0.434285 3.539996 -0.00431 -0.0607424 -0.079155 -0.053001 -0.1784412	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232	9.0280002 2.422163 -0.105243 -0.021463 -0.078897 9.116399 -0.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.2673612	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.021573 0.0120492	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.1509708	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332	8.194203 2.445025 -0.063099 0.024792 -0.032456 10.347937 -0.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488			0.108153	0.088872	8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 11.1288710.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888	3.263522 5.41438	4.956661 34.627304	6.165193 45.983972	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028	9.184872 9.184872 48.176224 35.451316 	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224272 32.978922 -0.382484 0.093246 0.004268 -0.060072 -0.091431 -0.041418	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 6. 50.562496 5. 10.078591 1. 32.21951 10.382484 60.002452 8. 0.093864 1. 0.093864 1. 0.009216 1. 0.009216 1. 0.009216 1. 0.009384 2. 0.049374 2. 0.0749808	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-41		8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .121095 -0 .087352 -0	.900752 .664915 .079545 .010298 .052992 .418397 .439287 .282098 .076676 .152974 .163152 .105381 .125089 	8.866216 0.826582 -0.109845 -0.045388 -0.090986 5.933804 -0.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873	8.8653932 1.801483 -0.049899 0.032767 -0.037449 6.841788 -0.449324 3.385906 -0.043939 -0.1068584 -0.110448 -0.110619	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.130392 -0.091413 -0.1880208	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743	8.7574682 2.361602 -0.018606 0.074237 0.005726 8.584483 -0.434285 3.539996 -0.00431 -0.0607424 -0.079155 -0.053001	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232	9.0280002 2.422163 -0.105243 -0.021463 -0.078897 9.116399 -0.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317	8.5689592 2.513611 0.004113 0.082212 0.021269 9.4128490.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.062685 -0.021573 0.0120492 0.081978	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023	8.194203 2.445025 -0.063099 0.024792 -0.032456 10.347937 -0.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373			0.108153		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 —— 11.128871 —— -0.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974	3.263522 5.41438	4.956661 34.627304	 6.165193 45.983972 	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731	9.184872 9.184872 48.176224 35.451316 	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224272 32.978922 -0.382484 0.093246 0.004268 -0.060072 -0.091431 -0.041418 -0.021349 1.849597 0.052008	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 6 50.562496 10.078591 1 32.21951 4 -0.382484 6 -0.002452 0.093864 0.0470744 1 0.009216 0.049374 2 0.0749808 2 2.275262 0.137199	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-33D	2.6406680.39417 3.149094 -0.0795304 -0.097272 -1.67265	8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623	8.922337 8. 0.176508 00.053193 -0 0.013627 00.033995 -0 5.032596 50.430932 -0 3.261012 30.062892 -0 -0.130313 -0 -0.143388 -0 -0.131571 -0 -0.07105 -0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .121095 -0 .087352 -0 .017043 0.	.900752 .664915 .079545 .010298 .052992 .418397 .439287 .282098 .076676 .152974 .163152 .105381 .125089 	8.866216 0.826582 -0.109845 -0.045388 -0.090986 5.933804 -0.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.1784412 	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 -0.1068584 -0.110448 -0.110619 -0.1310172	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.130392 -0.091413 -0.1880208	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743	8.7574682 2.361602 -0.018606 0.074237 0.005726 8.584483 -0.434285 3.539996 -0.00431 -0.0607424 -0.079155 -0.053001 -0.1784412 0.075318	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.017043	9.0280002 2.422163 -0.105243 -0.021463 -0.078897 9.116399 -0.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.2673612 	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.021573 0.0120492 ——	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.1509708	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 ——	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332	8.194203 2.445025 -0.063099 0.024792 -0.032456 10.347937 -0.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488			0.108153		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 —— 11.128871 —— -0.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399	3.263522 5.41438 0.115814	4.956661 34.627304 0.280792	6.165193 45.983972 0.426453	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959	9.184872 48.176224 35.451316 1.665399	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224279 32.978922 -0.382484 0.093246 0.004268 -0.060072 -0.091431 -0.041418 -0.021349 1.849597	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 6.50.562496 5.10.078591 1.32.21951 1.4-0.382484 1.0002452 1.009216	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368 7.131106	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-33 VWP-41 VWP-41D VWP-43 VWP-43	2.6406680.39417 3.149094 -0.0795304 -0.097272 -1.67265 0.0872490.001269	8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.0356340.036486	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .121095 -0 .087352 -0 .017043 0058413 -0	.900752 .664915 .079545 .010298 	8.866216 0.826582 -0.109845 -0.0453880.090986 5.9338040.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.17844120.0409560.090276	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 -0.1068584 -0.110619 -0.1310172 0.0389640.034935	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.130392 -0.091413 -0.1880208 0.0206490.036738	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743 0.0353580.033384	8.7574682 2.361602 -0.018606 0.074237 8.584483 8.584483 -0.434285 3.539996 -0.00431 -0.0607424 -0.079155 -0.0753001 -0.1784412 0.075318 	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.0170430.0468	9.0280002 2.422163 -0.105243 -0.0214630.078897 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.0229170.075309	8.5689592 2.513611 0.004113 0.082212 0.021269 9.4128490.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.021573 0.0120492 0.081978 3.121894 0.02028	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233 4.318506 0.107484 ——	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023 4.697493 -0.028353	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373 5.217373 -0.038415			0.108153 0.13962 0.169716		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 —— 11.128871 —— -0.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735	3.263522 5.41438 0.115814	4.956661 34.627304 0.280792 0.116682	6.165193 45.983972 0.426453 2.233695	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706	9.184872 9.184872 48.176224 35.451316 1.665399 30.188895	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224272 32.978922 -0.382484 0.093246 0.004268 -0.060072 -0.091431 -0.021349 1.849597 0.052008 6.222546 -0.011583 26.87841	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 6.50.562496 5.10.078591 1.32.21951 1.40.382484 60.002452 8.0.093864 1.0.093864 1.0.09216 1.0.009216 1.0.0749808 1.0.0749808 1.0.0749808 1.0.0749808 1.0.0749808 1.0.0749808 1.0.0749808 1.0.0749808 1.0.0749808 1.0.092391 1.0.092391 1.0.092391 1.0.092391 1.0.092391	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257 6.899866 -0.060216 28.29921	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368 7.131106 -0.033384 29.498826	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363 7.787106 -0.02655 32.66145	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-33 VWP-41 VWP-41D VWP-43 VWP-43 VWP-44 VWP-47	2.6406680.39417 3.149094 -0.0795304 -0.097272 -1.67265 0.0872490.001269	8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.035634 1.9263516 -0.017259	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .087352 -0 .017043 0058413 -0 .0781516 2034289 -0	.900752 .664915 .079545 .010298 	8.866216 0.826582 -0.109845 -0.0453880.090986 5.9338040.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.17844120.0409560.090276 2.4041766 -0.0973	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 -0.1068584 -0.110619 -0.1310172 0.0389640.034935 2.8181766 -0.032353	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.130392 -0.091413 -0.1880208 0.0206490.036738 3.2321766 -0.03212	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743 0.0353580.033384 3.5030016 -0.030417	8.7574682 2.361602 -0.018606 0.074237 0.005726 8.584483 -0.434285 3.539996 -0.00431 -0.0607424 -0.079155 -0.053001 -0.1784412 0.075318 3.7140882 0.006045	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.0170430.0468 3.8721516 -0.044812	9.0280002 2.422163 -0.105243 -0.0214630.078897 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.0229170.075309 3.9825516 -0.080109	8.5689592 2.513611 0.004113 0.082212 0.021269 9.4128490.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.021573 0.0120492 0.081978 3.121894 0.02028 4.1015766 0.012552	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016 -0.119816	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882 0.112724	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 0.107615	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023 4.697493 -0.028353 4.2085266 -0.029862	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373 5.217373 -0.038415 4.1643132 -0.034971			0.108153 0.13962 0.169716		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 —— 11.128871 —— -0.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735 4.1136516 0.099566	3.263522 5.41438 0.115814	4.956661 34.627304 0.280792 0.116682	6.165193 45.983972 0.426453 2.233695	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706 3.6623382 0.123408	9.184872 48.176224 35.451316 1.665399 30.188895	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224279 32.978922 -0.382484 0.093246 0.004268 -0.060072 -0.091431 -0.041418 -0.021349 1.849597 0.052008 6.222546 -0.011583 26.87841 3.5726382 -0.004317	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 6 50.562496 5 10.078591 1 32.21951 1 -0.382484 6 -0.002452 0.093864 0.0470744 1 0.009216 3 0.049374 2 0.0749808 2 2.275262 3 0.137199 6 6.694866 8 0.092391 2 7.380682 2 3.5139882 7 0.089115	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257 6.899866 -0.060216 28.29921 3.5657382 -0.065858	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368 7.131106 -0.033384 29.498826 3.5519382 -0.013531	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363 7.787106 -0.02655 32.66145 3.5139882 -0.027621	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601 3.5243382 -0.058974
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-33 VWP-41 VWP-41D VWP-43 VWP-43 VWP-44	2.6406680.39417 3.149094 -0.0795304 -0.097272 -1.67265 0.0872490.001269	8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.0356340.036486 1.9263516	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .087352 -0 .017043 0058413 -0 .0781516 2034289 -0	.900752 .664915 .079545 .010298 	8.866216 0.826582 -0.109845 -0.0453880.090986 5.9338040.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.17844120.0409560.090276 2.4041766	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 -0.1068584 -0.110619 -0.1310172 0.0389640.034935 2.8181766	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.130392 -0.091413 -0.1880208 0.0206490.036738 3.2321766	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743 0.0353580.033384 3.5030016	8.7574682 2.361602 -0.018606 0.074237 8.584483 -0.434285 3.539996 -0.00431 -0.0607424 -0.079155 -0.053001 -0.1784412 0.075318 3.7140882	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.0170430.0468 3.8721516	9.0280002 2.422163 -0.105243 -0.0214630.078897 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.0229170.075309 3.9825516	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.021573 0.0120492 —— 0.081978 3.121894 0.02028 —— 4.1015766	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 0.107615 6.181586	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023 4.697493 -0.028353 4.2085266 -0.029862 6.452279	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373 5.217373 -0.038415 4.1643132 -0.034971			0.108153		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 —— 11.128871 —— -0.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735 4.1136516	3.263522 5.41438 0.115814 0.015009	4.956661 34.627304 0.280792 0.116682	6.165193 45.983972 0.426453 2.233695	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706 3.6623382	9.184872 48.176224 35.451316 1.665399 30.188895	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224279 32.978922 -0.382484 0.093246 0.004268 -0.060072 -0.091431 -0.041418 -0.021349 1.849597 0.052008 6.222546 -0.011583 26.87841 3.5726382 -0.004317	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 6.50.562496 5.10.078591 1.32.21951 1.4-0.382484 1.0-0.002452 1.0.092452 1.0.093864 1.0.09216 1.0.09216 1.0.09216 1.0.0749808 1.0	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257 6.899866 -0.060216 28.29921 3.5657382 -0.065858	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368 7.131106 -0.033384 29.498826 3.5519382 -0.013531	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363 7.787106 -0.02655 32.66145 3.5139882 -0.027621	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601 3.5243382 -0.058974
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-33 VWP-41 VWP-41D VWP-43 VWP-43 VWP-44 VWP-47	2.6406680.39417 3.149094 -0.0795304 -0.097272 -1.67265 0.0872490.001269	8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.035634 1.9263516 -0.017259	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .121095 -0 .087352 -0 .017043 0058413 -00781516 2.3 .034289 -0	.900752 .664915 .079545 .010298 	8.866216 0.826582 -0.109845 -0.0453880.090986 5.9338040.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.17844120.040956 2.4041766 -0.0973	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 -0.1068584 -0.110619 -0.1310172 0.0389640.034935 2.8181766 -0.032353	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.130392 -0.091413 -0.1880208 0.0206490.036738 3.2321766 -0.03212	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743 0.0353580.033384 3.5030016 -0.030417	8.7574682 2.361602 -0.018606 0.074237 0.005726 8.584483 -0.434285 3.539996 -0.00431 -0.0607424 -0.079155 -0.053001 -0.1784412 0.075318 3.7140882 0.006045 	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.017043 3.8721516 -0.044812	9.0280002 2.422163 -0.105243 -0.0214630.078897 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.0229170.075309 3.9825516 -0.080109	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.021573 0.0120492 —— 0.081978 3.121894 0.02028 —— 4.1015766 0.012552 1.938147	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016 -0.119816	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882 0.112724 5.838075	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 0.107615 6.181586	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023 4.697493 -0.028353 4.2085266 -0.029862 6.452279	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373 5.217373 -0.038415 4.1643132 -0.034971			0.108153 0.13962 0.169716		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 11.1288710.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735 4.1136516 0.099566 7.00158	3.263522 5.41438 0.115814	4.956661 34.627304 0.280792 0.116682	6.165193 45.983972 0.426453 2.233695	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706 3.6623382 0.123408	9.184872 48.176224 35.451316 1.665399 30.188895	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224272 32.978922 -0.382484 0.093246 0.0042682 -0.0600722 -0.0914312 -0.021349 1.849597 0.052008 6.222546 -0.011583 26.87841 3.5726382 -0.004317 7.201038	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 6 50.562496 5 10.078591 1 32.21951 1 -0.382484 6 -0.002452 0.093864 0.0470744 1 0.009216 3 0.049374 2 0.0749808 2 2.275262 3 0.137199 6 6.694866 8 0.092391 2 7.380682 2 3.5139882 7 0.089115	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257 6.899866 -0.060216 28.29921 3.5657382 -0.065858 7.335593	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368 7.131106 -0.033384 29.498826 3.5519382 -0.013531 7.338759	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363 7.787106 -0.02655 32.66145 3.5139882 -0.027621 7.267635	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601 3.5243382 -0.058974 7.050764
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-33 VWP-41 VWP-41D VWP-43 VWP-47 VWP-47 VWP-47 VWP-47D	2.6406680.39417 3.149094 -0.0795304 -0.097272 -1.67265 0.087249 0.001269	8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.035634 1.9263516 -0.017259 8/6/2019 20.63	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .121095 -0 .087352 -0 .017043 0058413 -0 .0781516 2034289 -0034289 -0034289 -0034289 -0034289 -0034289 -0	.900752 .664915 .079545 .010298 	8.866216 0.826582 -0.109845 -0.0453880.090986 5.9338040.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.17844120.040956 2.4041766 -0.0973 2.4041766 -0.0973 2.4049	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 -0.1068584 -0.110619 -0.1310172 0.0389640.034935 2.8181766 -0.032353 8/19/2019 20.49	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.1239384 -0.130392 -0.091413 -0.1880208 0.0206490.036738 3.2321766 -0.03212 8/27/2019 20.43	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743 0.0353580.033384 3.5030016 -0.030417 9/3/2019 20.27	8.7574682 2.361602 -0.018606 0.074237 0.005726 8.5844830.434285 3.539996 -0.00431 -0.0607424 -0.079155 -0.053001 -0.1784412 0.075318 3.7140882 0.006045 9/10/2019 20.24	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.017043 3.8721516 -0.044812 9/17/2019 20.06	9.0280002 2.422163 -0.105243 -0.0214630.078897 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.075309 3.9825516 -0.080109 9/25/2019 20.86	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.062685 -0.021573 0.0120492 —— 0.081978 3.121894 0.02028 —— 4.1015766 0.012552 1.938147	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016 -0.119816 3.987437	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467 5.201709	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882 0.112724 5.838075	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 0.107615 6.181586 Pressure Heither Pressur	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023 4.697493 -0.028353 4.2085266 -0.029862 6.452279 ad (feet H ₂ O) 11/22/2019 19.23	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373 5.217373 -0.038415 4.1643132 -0.034971 6.802233			0.108153 0.13962 0.169716 0.169716 12/6/2019		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 11.1288710.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735 4.1136516 0.099566 7.00158	3.263522 5.41438 0.115814 12/13/2019	4.956661 34.627304 0.280792 0.116682 12/16/2019	6.165193 45.983972 0.426453 2.233695 12/18/2019	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706 3.6623382 0.123408 7.142578	9.184872 9.184872 35.451316 1.665399 30.188895 30.188895 31.2/20/2019	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224272 32.978922 -0.382484 0.093246 0.0042682 -0.0600722 -0.0914312 -0.0213499 1.849597 0.052008 6.2225462 -0.0115832 26.87841 3.5726382 -0.004317 7.201038	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 6.50.562496 5.10.078591 1.32.21951 1.4-0.382484 60.002452 8.0.093864 1.0.093864 1.0.009216 1.0.009216 1.0.0749808 1.0.0749808 1.0.0749808 1.0.0749808 1.0.092391 1.0.092391 1.0.092391 1.0.089115 1.0.089115 1.0.089115 1.0.089115 1.0.089115 1.0.089115 1.0.089115 1.0.089115 1.0.089115 1.0.089115	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257 6.899866 -0.060216 28.29921 3.5657382 -0.065858 7.335593	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368 7.131106 -0.033384 29.498826 3.5519382 -0.013531 7.338759	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363 7.787106 -0.02655 32.66145 3.5139882 -0.027621 7.267635	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601 3.5243382 -0.058974 7.050764
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-33 VWP-41 VWP-41D VWP-43 VWP-47 VWP-47 VWP-47 VWP-47 VWP-47 VWP-1 VWP-1 VWP-1 VWP-3 VWP-1	2.6406680.39417 3.149094 -0.0795304 -0.097272 -1.67265 0.0872490.001269 7/29/2019	8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.035634 1.9263516 -0.017259 8/6/2019 20.63 0.34 -0.08	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .017043 0058413 -0 .0781516 2.3 .034289 -0034289 -00781516 2.3 .034289 -0077 -0.15	.900752 .664915 .079545 .010298 .—	8.866216 0.826582 -0.109845 -0.0453880.090986 5.9338040.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.17844120.040956 2.4041766 -0.0973 8/12/2019 20.49 1.91 -0.25	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 -0.1068584 -0.110448 -0.110619 -0.1310172 0.0389640.034935 2.8181766 -0.032353 8/19/2019 20.49 4.16 -0.12	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.130392 -0.091413 -0.1880208 0.0206490.036738 3.2321766 -0.03212 8/27/2019 20.43 4.94 -0.16	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743 0.0353580.033384 3.5030016 -0.030417 9/3/2019 20.27 5.32 -0.13	8.7574682 2.361602 -0.018606 0.074237 0.005726 8.5844830.434285 3.539996 -0.0607424 -0.079155 -0.053001 -0.1784412 0.075318 0.075318 3.7140882 0.006045 9/10/2019 20.24 5.46 -0.04	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.017043 3.8721516 -0.044812 9/17/2019 20.06 5.52 -0.18	9.0280002 2.422163 -0.105243 -0.0214630.078897 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.075309 3.9825516 -0.080109	8.5689592 2.513611 0.004113 0.082212 0.021269 9.4128490.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.021573 0.0120492 0.081978 3.121894 0.02028 4.1015766 0.012552 1.938147	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016 -0.119816 3.987437	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467 5.201709 10/30/2019 19.57 5.83 -0.09	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882 0.112724 5.838075	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 0.107615 6.181586 Pressure Head In 1950 5.86 0.19	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023 4.697493 -0.028353 4.2085266 -0.029862 6.452279 ad (feet H ₂ O) 11/22/2019 19.23 5.77 -0.13	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373 5.217373 -0.038415 4.1643132 -0.034971 6.802233			0.108153 0.13962 0.169716 0.169716		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 —— 11.128871 —— -0.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735 4.1136516 0.099566 7.00158	3.263522 5.41438 0.115814	4.956661 34.627304 0.280792 0.116682 12/16/2019	6.165193 45.983972 0.426453 2.233695 12/18/2019	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706 3.6623382 0.123408 7.142578	9.184872 48.176224 35.451316 1.665399 30.188895 1 12/20/2019	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224272 32.978922 -0.382484 0.093246 0.004268 -0.060072 -0.091431 -0.021349 1.849597 0.052008 6.222546 -0.011583 26.87841 3.5726382 -0.004317 7.201038	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 50.562496 10.078591 1 32.21951 1 -0.382484 6 -0.002452 0.093864 0.0470744 1 0.009216 3 0.049374 2 0.0749808 2 2.275262 3 0.137199 6 6.694866 8 0.092391 27.380682 2 3.5139882 7 0.089115 7 7.313542	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257 6.899866 -0.060216 28.29921 3.5657382 -0.065858 7.335593	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368 7.131106 -0.033384 29.498826 3.5519382 -0.013531 7.338759 1/14/2020 18.52 5.79 -0.12	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363 7.787106 -0.02655 32.66145 3.5139882 -0.027621 7.267635 1/30/2020 18.38 5.88 -0.12	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601 3.5243382 -0.058974 7.050764 2/25/2020 18.22 5.96 -0.22
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-33 VWP-41 VWP-41 VWP-41D VWP-43 VWP-47 VWP-47 VWP-47 VWP-47 VWP-47		8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.035634 1.9263516 -0.017259 8/6/2019 20.63 0.34	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .017043 0058413 -0 .0781516 2.3 .034289 -0034289 -00781516 2.3 .034289 -0077 -0.15	.900752 .664915 .079545 .079545 .010298 	8.866216 0.826582 -0.109845 -0.0453880.090986 5.9338040.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.17844120.040956 2.4041766 -0.0973 2.4041766 -0.0973 8/12/2019 20.49 1.91	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 -0.1068584 -0.110619 -0.1310172 0.0389640.034935 2.8181766 -0.032353 8/19/2019 20.49 4.16	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.130392 -0.091413 -0.1880208 0.0206490.036738 3.2321766 -0.03212 8/27/2019 20.43 4.94	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743 0.0353580.033384 3.5030016 -0.030417 9/3/2019 20.27 5.32	8.7574682 2.361602 -0.018606 0.074237 8.584483 8.584483 -0.434285 3.539996 -0.00431 -0.0607424 -0.079155 -0.053001 -0.1784412 0.075318 3.37140882 0.006045 9/10/2019 20.24 5.46	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.017043 3.8721516 -0.044812 9/17/2019 20.06 5.52	9.0280002 2.422163 -0.105243 -0.0214630.078897 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.075309 3.9825516 -0.080109 9/25/2019 20.86 5.60	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.021573 0.0120492 —— 0.081978 3.121894 0.02028 —— 4.1015766 0.012552 1.938147	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016 -0.119816 3.987437	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467 5.201709	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882 0.112724 5.838075	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 0.107615 6.181586 Pressure Head I1/15/2019 19.50 5.86	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023 4.697493 -0.028353 4.2085266 -0.029862 6.452279 ad (feet H ₂ O) 11/22/2019 19.23 5.77	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373 5.217373 -0.038415 4.1643132 -0.034971 6.802233			0.108153 0.13962 0.169716 12/6/2019		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 11.1288710.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735 4.1136516 0.099566 7.00158	3.263522 5.41438 0.115814 12/13/2019	4.956661 34.627304 0.280792 0.116682 12/16/2019	6.165193 45.983972 0.426453 2.233695 2.233695 2.23895	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706 3.6623382 0.123408 7.142578	9.184872 9.184872 35.451316 1.665399 30.188895 12/20/2019	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224272 32.978922 -0.382484 0.093246 0.004268 -0.060072 -0.091431 -0.021349 1.849597 0.052008 6.222546 -0.011583 26.87841 3.5726382 -0.004317 7.201038	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 6.50.562496 5.10.078591 1.32.21951 1.4-0.382484 1.5-0.002452 1.5-0.002452 1.5-0.009216 1.5-0.009216 1.5-0.009216 1.5-0.009216 1.5-0.009216 1.5-0.009216 1.5-0.0092391 1.5-0.092391 1.5-0.092391 1.5-0.089115 1.5-0.089115 1.5-0.089115 1.5-0.092391 1.5-0.089115 1.5-0.089115 1.5-0.089115 1.5-0.089115 1.5-0.089115 1.5-0.089115 1.5-0.089115 1.5-0.089115 1.5-0.089115 1.5-0.089115 1.5-0.089115 1.5-0.089115 1.5-0.089115	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257 6.899866 -0.060216 28.29921 3.5657382 -0.065858 7.335593	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368 7.131106 -0.033384 29.498826 3.5519382 -0.013531 7.338759	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363 7.787106 -0.02655 32.66145 3.5139882 -0.027621 7.267635	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601 3.5243382 -0.058974 7.050764
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-33 VWP-41 VWP-41D VWP-43 VWP-47 VWP-47 VWP-47 VWP-47 VWP-47 VWP-47 VWP-4 VWP-8 VWP-8 VWP-9	2.6406680.39417 3.149094 -0.0795304 -0.097272 -1.67265 0.087249 0.001269	8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.035634 1.9263516 -0.017259 8/6/2019 20.63 0.34 -0.08 0.060.04	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .121095 -0 .087352 -0 .017043 0058413 -0 .0781516 2034289 -0 .0781516 2034289 -0 .077 -0.15 .0020.11	.900752 .664915 .079545 .010298 	8.866216 0.826582 -0.109845 -0.0453880.090986 5.9338040.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.17844120.040956 2.4041766 -0.0973 2.4041766 -0.0973 2.4049 1.91 -0.25 -0.100.21	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 -0.1068584 -0.110619 -0.1310172 0.0389640.034935 2.8181766 -0.032353 8/19/2019 20.49 4.16 -0.12 0.080.09	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.1239384 -0.130392 -0.091413 -0.1880208 0.036738 3.2321766 -0.03212 8/27/2019 20.43 4.94 -0.16 0.020.03	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743 0.0353580.033384 3.5030016 -0.030417 9/3/2019 20.27 5.32 -0.13 0.070.07	8.7574682 2.361602 -0.018606 0.074237 0.005726 8.5844830.434285 3.539996 -0.00431 -0.0607424 -0.079155 -0.053001 -0.1784412 0.075318 3.7140882 0.006045 9/10/2019 20.24 5.46 -0.04 0.17 0.01	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.017043 3.8721516 -0.044812 9/17/2019 20.06 5.52 -0.18 0.050.09	9.0280002 2.422163 -0.105243 -0.0214630.078897 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.075309 3.9825516 -0.080109 9/25/2019 20.86 5.60 -0.24 -0.050.18	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.062685 -0.021573 0.0120492 —— 0.081978 3.121894 0.02028 —— 4.1015766 0.012552 1.938147	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016 -0.119816 3.987437 10/18/2019 19.54 5.72 -0.35 -0.170.27	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467 5.201709 10/30/2019 19.57 5.83 -0.09 0.130.03	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882 0.112724 5.838075 11/8/2019 19.62 5.79 0.20 0.40 0.30	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 0.107615 6.181586 Pressure Heading States of the states	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023 4.697493 -0.028353 4.2085266 -0.029862 6.452279 ad (feet H ₂ O) 11/22/2019 19.23 5.77 -0.13 0.100.07	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373 5.217373 -0.038415 4.1643132 -0.034971 6.802233 12/3/2019 18.94 5.65 -0.15 0.060.07			0.108153		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 11.1288710.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735 4.1136516 0.099566 7.00158 12/12/2019 18.97 5.84 -0.03 0.16 6.66 0.23	3.263522 5.41438 0.115814	4.956661 34.627304 0.280792 0.116682 11.45 11.45	6.165193 45.983972 0.426453 2.233695 2.233695 14.25 14.25	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706 3.6623382 0.123408 7.142578 12/19/2019 19.03 5.74 0.21 0.39 20.52 0.31	9.184872 48.176224 35.451316 1.665399 30.188895 30.188895 21.22	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224273 32.978922 -0.382484 0.093246 0.004268 -0.060072 -0.091431 -0.021349 1.849597 0.052008 6.222546 -0.011583 26.87841 3.5726383 -0.004317 7.201038	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 50.562496 10.078591 1 32.21951 1 -0.382484 2 -0.002452 0.093864 0.009216 0.0092391	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257 6.899866 -0.060216 28.29921 3.5657382 -0.065858 7.335593 1/9/2020 18.52 5.74 -0.21 -0.05 85.79 -0.10	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368 7.131106 -0.033384 29.498826 3.5519382 -0.013531 7.338759 1/14/2020 18.52 5.79 -0.12 0.07 90.31 -0.02	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363 7.787106 -0.02655 32.66145 3.5139882 -0.027621 7.267635 1/30/2020 18.38 5.88 -0.12 0.10 96.37 -0.04	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601 3.5243382 -0.058974 7.050764 2/25/2020 18.22 5.96 -0.22 -0.02 100.64 -0.13
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-33 VWP-41 VWP-41 VWP-41 VWP-47 VWP-47 VWP-47 VWP-47 VWP-47 VWP-47 VWP-4 VWP-8 VWP-8		8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.035634 1.9263516 -0.017259 8/6/2019 20.63 0.34 -0.08 0.06	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .049025 -0 .186319 5	.900752 .664915 .079545 .010298 	8.866216 0.826582 -0.109845 -0.0453880.090986 5.9338040.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.17844120.040956 2.4041766 -0.0973 2.4041766 -0.0973 2.49 1.91 -0.25 -0.10	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 -0.1068584 -0.110619 -0.1310172 0.0389640.034935 2.8181766 -0.032353 8/19/2019 20.49 4.16 -0.12 0.08	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.130392 -0.091413 -0.1880208 0.0206490.036738 3.2321766 -0.03212 8/27/2019 20.43 4.94 -0.16 0.02	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743 0.0353580.033384 3.5030016 -0.030417 9/3/2019 20.27 5.32 -0.13 0.07	8.7574682 2.361602 -0.018606 0.074237 8.584483 8.584483 -0.0431 -0.0607424 -0.079155 -0.053001 -0.1784412 0.075318 3.3.7140882 0.006045 9/10/2019 20.24 5.46 -0.04 0.17	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.017043 3.8721516 -0.0468 3.8721516 -0.044812 9/17/2019 20.06 5.52 -0.18 0.05	9.0280002 2.422163 -0.105243 -0.105243 -0.021463 9.116399 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.075309 3.9825516 -0.080109 9/25/2019 20.86 5.60 -0.24 -0.05	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.021573 0.0120492 —— 0.081978 3.121894 0.02028 —— 4.1015766 0.012552 1.938147 10/9/2019 19.80 5.81 0.01 0.19 ——	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016 -0.119816 3.987437 10/18/2019 19.54 5.72 -0.35 -0.17	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467 5.201709 10/30/2019 19.57 5.83 -0.09 0.13	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882 0.112724 5.838075 11/8/2019 19.62 5.79 0.20 0.40	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 0.107615 6.181586 Pressure Head I1/15/2019 19.50 5.86 0.19 0.37 ——	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023 4.697493 -0.028353 4.2085266 -0.029862 6.452279 ad (feet H ₂ O) 11/22/2019 19.23 5.77 -0.13 0.10	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373 5.217373 -0.038415 4.1643132 -0.034971 6.802233 12/3/2019 18.94 5.65 -0.15 0.06			0.108153		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 11.1288710.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735 4.1136516 0.099566 7.00158 12/12/2019 18.97 5.84 -0.03 0.16 6.66	3.263522 5.41438 0.115814 12/13/2019 7.54	4.956661 34.627304 0.280792 0.116682 11.45	6.165193 45.983972 0.426453 2.233695 2.233695 1 14.25	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706 3.6623382 0.123408 7.142578 12/19/2019 19.03 5.74 0.21 0.39 20.52	9.184872 48.176224 35.451316 1.665399 30.188895 30.188895 21.22	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224273 32.978922 -0.382484 0.093246 0.004268 -0.060072 -0.091431 -0.021349 1.849597 0.052008 6.222546 -0.011583 26.87841 3.5726382 -0.004317 7.201038	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 5.50.562496 1.0.078591 1.32.21951 1.4-0.382484 1.5-0.002452 1.5-0.002452 1.5-0.009216 1.5-0.009216 1.5-0.009216 1.5-0.009216 1.5-0.009216 1.5-0.0092391	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257 6.899866 -0.060216 28.29921 3.5657382 -0.065858 7.335593 1/9/2020 18.52 5.74 -0.21 -0.05	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368 7.131106 -0.033384 29.498826 3.5519382 -0.013531 7.338759 1/14/2020 18.52 5.79 -0.12 0.07 90.31	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363 7.787106 -0.02655 32.66145 3.5139882 -0.027621 7.267635 1/30/2020 18.38 5.88 -0.12 0.10 96.37	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601 3.5243382 -0.058974 7.050764 2/25/2020 18.22 -0.02 100.64 -0.13 118.36 23.41
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-33 VWP-41 VWP-41 VWP-41D VWP-47 VWP-47 VWP-47 VWP-47 VWP-47 VWP-47 VWP-8 VWP-8 VWP-9 VWP-9D	2.6406680.39417 3.149094 -0.0795304 -0.097272 -1.67265 0.087249 0.001269	8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.035634 1.9263516 -0.017259 8/6/2019 20.63 0.34 -0.08 0.060.04	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .087352 -0 .017043 0058413 -0 .0781516 2.: .034289 -0034289 -0034289 -00155 0.02	.900752 .664915 .079545 .010298 	8.866216 0.826582 -0.109845 -0.0453880.090986 5.9338040.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.17844120.040956 2.4041766 -0.0973 2.4041766 -0.0973 2.4049 1.91 -0.25 -0.100.21	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 -0.1068584 -0.110619 -0.1310172 0.0389640.034935 2.8181766 -0.032353 8/19/2019 20.49 4.16 -0.12 0.080.09	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.130392 -0.091413 -0.1880208 0.0206490.036738 3.2321766 -0.03212 8/27/2019 20.43 4.94 -0.16 0.020.030.03	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743 0.0353580.033384 3.5030016 -0.030417 9/3/2019 20.27 5.32 -0.13 0.070.070.07	8.7574682 2.361602 -0.018606 0.074237 0.005726 8.5844830.434285 3.539996 -0.00431 -0.0607424 -0.079155 -0.053001 -0.1784412 3.7140882 0.006045 9/10/2019 20.24 5.46 -0.04 0.17 0.01 0.01	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.017043 3.8721516 -0.044812 9/17/2019 20.06 5.52 -0.18 0.050.09	9.0280002 2.422163 -0.105243 -0.0214630.078897 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.075309 3.9825516 -0.080109 9/25/2019 20.86 5.60 -0.24 -0.050.18	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.021573 0.0120492 —— 0.081978 3.121894 0.02028 —— 4.1015766 0.012552 1.938147 10/9/2019 19.80 5.81 0.01 0.19 —— 0.05 ——	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016 -0.119816 3.987437 10/18/2019 19.54 5.72 -0.35 -0.170.270.27	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467 5.201709 10/30/2019 19.57 5.83 -0.09 0.130.03	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882 0.112724 5.838075 11/8/2019 19.62 5.79 0.20 0.40 0.30	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 0.107615 6.181586 Pressure Heither He	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023 4.697493 -0.028353 4.2085266 -0.029862 6.452279 ad (feet H ₂ O) 11/22/2019 19.23 5.77 -0.13 0.100.07	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373 5.217373 -0.038415 4.1643132 -0.034971 6.802233 12/3/2019 18.94 5.65 -0.15 0.060.07			0.108153		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 11.1288710.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735 4.1136516 0.099566 7.00158 12/12/2019 18.97 5.84 -0.03 0.16 6.66 0.23	3.263522 5.41438 0.115814 12/13/2019 7.54 12.51	4.956661 34.627304 0.280792 0.116682 0.116682 11.45 80.02	6.165193 45.983972 0.426453 2.233695 2.233695 1 14.25 106.26	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706 3.6623382 0.123408 7.142578 12/19/2019 19.03 5.74 0.21 0.39 20.52 0.31 109.26	9.184872 48.176224 35.451316 1.665399 30.188895 30.188895 21.22 111.33	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224272 32.978922 -0.382484 0.093246 0.004268 -0.060072 -0.091431 -0.041418 -0.021349 1.849597 0.052008 6.222546 -0.011583 26.87841 3.5726382 -0.004317 7.201038	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 50.562496 510.078591 132.21951 1-0.382484 -0.002452 0.093864 0.0470744 0.009216 0.0470744 0.009216 0.0749808 2.275262 0.137199 6.6694866 3 0.092391 27.380682 2.375262 3.5139882 7 0.089115 7.313542 19 1/4/2020 18.79 5.90 0.14 0.35 76.66 0.21 116.84	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257 6.899866 -0.060216 28.29921 3.5657382 -0.065858 7.335593 1/9/2020 18.52 5.74 -0.21 -0.05 85.79 -0.10 117.03	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368 7.131106 -0.033384 29.498826 3.5519382 -0.013531 7.338759 1/14/2020 18.52 5.79 -0.12 0.07 90.31 -0.02 117.36	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363 7.787106 -0.02655 32.66145 3.5139882 -0.027621 7.267635 1/30/2020 18.38 5.88 -0.12 0.10 96.37 -0.04 117.78	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601 3.5243382 -0.058974 7.050764 2/25/2020 18.22 5.96 -0.22 -0.02 100.64 -0.13 118.36
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-33 VWP-41 VWP-41 VWP-41 VWP-47 VWP-47 VWP-47 VWP-47 VWP-47 VWP-48 VWP-8 VWP-8 VWP-9 VWP-9 VWP-18 VWP-19 VWP-19 VWP-19 VWP-19		8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.035634 1.9263516 -0.017259 8/6/2019 20.63 0.34 -0.08 0.060.041.260.98 7.51	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .121095 -0 .017043 0017043 0058413 -00781516 2.: .034289 -0077 -0.15 .0.02		8.866216 0.826582 -0.109845 -0.0453880.090986 5.9338040.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.17844120.040956 2.4041766 -0.0973 2.4041766 -0.0973 2.4041766 -0.0973 1.91 -0.25 -0.100.21 13.711.03 7.66	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 -0.1068584 -0.110619 -0.1310172 0.0389640.034935 2.8181766 -0.032353 8/19/2019 20.49 4.16 -0.12 0.080.09 15.811.04 7.82	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.130392 -0.091413 -0.1880208 0.0206490.036738 3.2321766 -0.03212 8/27/2019 20.43 4.94 -0.16 0.020.031.07 7.94	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743 0.0353580.033384 3.5030016 -0.030417 9/3/2019 20.27 5.32 -0.13 0.070.071.01 8.08	8.7574682 2.361602 -0.018606 0.074237 0.005726 8.5844830.434285 3.539996 -0.00431 -0.0607424 -0.079155 -0.053001 -0.1784412 0.075318 3.7140882 0.006045 9/10/2019 20.24 5.46 -0.04 0.17 0.01 19.84 1.00 8.18	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.017043 3.8721516 -0.0468 3.8721516 -0.044812 9/17/2019 20.06 5.52 -0.18 0.050.090.09 20.510.98 8.26	9.0280002 2.422163 -0.105243 -0.105243 -0.021463 9.116399 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.075309 3.9825516 -0.080109 9/25/2019 20.86 5.60 -0.24 -0.050.181.02 6.85	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.062685 -0.021573 0.0120492 —— 0.081978 3.121894 0.02028 —— 4.1015766 0.012552 1.938147 10/9/2019 19.80 5.81 0.01 0.19 —— 0.05 —— 21.75 —— -1.00 3.68	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016 -0.119816 3.987437 10/18/2019 19.54 5.72 -0.35 -0.170.27 22.231.02 2.07	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467 5.201709 10/30/2019 19.57 5.83 -0.09 0.130.03 22.741.02 1.01	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882 0.112724 5.838075 11/8/2019 19.62 5.79 0.20 0.40 0.30 0.30 23.140.86 0.70	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 0.107615 6.181586 Pressure Head of the state of th	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023 4.697493 -0.028353 4.2085266 -0.029862 6.452279 ad (feet H ₂ O) 11/22/2019 19.23 5.77 -0.13 0.100.07 23.610.94 0.27	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373 5.217373 -0.038415 4.1643132 -0.034971 6.802233 12/3/2019 18.94 5.65 -0.15 0.060.07 23.910.95 0.16			0.108153 0.13962 0.169716 0.169716 0.169716 0.169716 0.169716		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 11.1288710.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735 4.1136516 0.099566 7.00158 12/12/2019 18.97 5.84 -0.03 0.16 6.66 0.23 25.720.84 0.19	3.263522 5.41438 0.115814 12/13/2019 7.54 12.51	4.956661 34.627304 0.280792 0.116682 11.45 80.02 80.02	6.165193 45.983972 0.426453 2.233695 2.233695 106.26 106.26	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706 3.6623382 0.123408 7.142578 12/19/2019 19.03 5.74 0.21 0.39 20.52 0.31 109.26 23.95 86.55 -0.77 0.17	9.184872 48.176224 35.451316 1.665399 30.188895 30.188895 21.22 111.33 81.92	8.1228693 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524796 10.224273 32.978923 -0.382484 0.093246 0.004268 -0.060072 -0.091431 -0.041418 -0.021349 1.849597 0.052008 6.222546 -0.011583 26.87841 3.5726383 -0.004317 7.201038	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 5.50.562496 1.0.078591 1.32.21951 1.4-0.382484 2.0.093864 2.0.0470744 1.0.009216 3.0.049374 2.0.0749808 2.275262 3.0.137199 3.6.694866 3.0.092391 27.380682 3.5139882 7.0.089115 7.313542 2.9 1/4/2020 18.79 5.90 0.14 0.35 76.66 0.21 116.84 23.29 74.45 -0.88 -0.01	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257 6.899866 -0.060216 28.29921 3.5657382 -0.065858 7.335593 1/9/2020 18.52 5.74 -0.21 -0.05 85.79 -0.10 117.03 23.28 74.85 -0.94 0.12	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368 7.131106 -0.033384 29.498826 3.5519382 -0.013531 7.338759 1/14/2020 18.52 5.79 -0.12 0.07 90.31 -0.02 117.36 23.26 75.52 -0.95 0.08	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363 7.787106 -0.02655 32.66145 3.5139882 -0.027621 7.267635 1/30/2020 18.38 5.88 -0.12 0.10 96.37 -0.04 117.78 23.29 78.70 -0.96 0.04	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601 3.5243382 -0.058974 7.050764 2/25/2020 18.22 5.96 -0.22 -0.02 100.64 -0.13 118.36 23.41 83.88 -1.06 0.04
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-33 VWP-33 VWP-33D VWP-41 VWP-41 VWP-41D VWP-43 VWP-47 VWP-47 VWP-47 VWP-47 VWP-48 VWP-48 VWP-8 VWP-9 VWP-9 VWP-9 VWP-18 VWP-18 VWP-19 VWP-19 VWP-20 VWP-25 VWP-26	2.6406680.39417 3.149094 -0.0795304 -0.097272 -1.67265 0.087249 0.001269	8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.035634 1.9263516 -0.017259 8/6/2019 20.63 0.34 -0.08 0.060.04 11.260.98 7.51 -0.10 -0.29	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .121095 -0 .087352 -0 .017043 0058413 -00781516 2.3 .034289 -0034289 -00111011981.00 .7.56 .0.31	.900752 .664915 .079545 .010298 	8.866216 0.826582 -0.109845 -0.0453880.090986 5.9338040.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.17844120.040956 2.4041766 -0.0973 2.4041766 -0.0973 2.4041766 -0.0973 1.0100.21 13.711.03 7.66 -0.26 -0.43	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 -0.1068584 -0.110619 -0.1310172 0.0389640.034935 2.8181766 -0.032353 8/19/2019 20.49 4.16 -0.12 0.080.09 15.811.04 7.82 -0.10 -0.25	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.130392 -0.091413 -0.1880208 0.0206490.036738 3.2321766 -0.03212 8/27/2019 20.43 4.94 -0.16 0.020.03 17.691.07 7.94 -0.06 -0.29	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743 3.5030016 -0.030417 9/3/2019 20.27 5.32 -0.13 0.07 18.92 1.01 8.08 -0.11 -0.24	8.7574682 2.361602 -0.018606 0.074237 0.005726 8.584483 8.5844830.434285 3.539996 -0.00431 -0.0607424 -0.079155 -0.053001 -0.1784412 0.075318 3.7140882 0.006045 9/10/2019 20.24 5.46 -0.04 0.17 19.84 19.84 19.84 19.84 100 8.18 -0.01 -0.14	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.017043 3.8721516 -0.044812 3.8721516 -0.044812 20.06 5.52 -0.18 0.050.09 20.510.98 8.26 -0.13 -0.24	9.0280002 2.422163 -0.105243 -0.0214630.078897 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.075309 3.9825516 -0.080109 9/25/2019 20.86 5.60 -0.24 -0.050.18 21.071.02 6.85 -0.22 -0.34	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.021573 0.0120492 —— 0.081978 3.121894 0.02028 —— 4.1015766 0.012552 1.938147 10/9/2019 19.80 5.81 0.01 0.19 —— 0.05 —— 21.75 —— 21.75 —— -1.00 3.68 0.05 -0.09	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016 -0.119816 3.987437 10/18/2019 19.54 5.72 -0.35 -0.17 20.27 22.231.02 2.07 -0.29 -0.48	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467 5.201709 10/30/2019 19.57 5.83 -0.09 0.13 22.741.02 1.01 -0.04 -0.15	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882 0.112724 5.838075 11/8/2019 19.62 5.79 0.20 0.40 0.30 23.140.86 0.70 0.26 0.13	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 0.107615 6.181586 Pressure Head State of the state of	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023 4.697493 -0.028353 4.2085266 -0.029862 6.452279 ad (feet H ₂ O) 11/22/2019 19.23 5.77 -0.13 0.100.07 23.610.94 0.27 -0.06 -0.18	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 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7.338759 1/14/2020 18.52 5.79 -0.12 0.07 90.31 -0.02 117.36 23.26 75.52 -0.95 0.08 -0.02 -0.17	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363 7.787106 -0.02655 32.66145 3.5139882 -0.027621 7.267635 1/30/2020 18.38 5.88 -0.12 0.10 96.37 -0.04 117.78 23.29 78.70 -0.96 0.04 -0.03 -0.16	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601 3.5243382 -0.058974 7.050764 2/25/2020 18.22 5.96 -0.22 -0.02 100.64 -0.13 118.36 23.41 83.88 -1.06 0.04 -0.11 -0.27
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-33 VWP-41 VWP-41D VWP-43 VWP-47 VWP-47 VWP-47 VWP-47 VWP-47 VWP-48 VWP-8 VWP-9 VWP-9 VWP-18 VWP-18 VWP-18 VWP-19 VWP-19 VWP-19 VWP-20 VWP-20 VWP-20 VWP-20 VWP-20 VWP-20	2.6406680.39417 3.149094 -0.0795304 -0.097272 -1.67265 0.087249 0.001269	8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.036486 1.9263516 -0.017259 8/6/2019 20.63 0.34 -0.08 0.060.04 11.260.98 7.51 -0.10	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .087352 -0 .017043 0058413 -0 .0781516 2034289 -0 .077 -0.15 .034289 -0 .077 -0.15 .0020111.981.981.00 .7.567.567.56	.900752 .664915 .079545 .010298 	8.866216 0.826582 -0.109845 -0.0453880.090986 5.9338040.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.17844120.040956 2.4041766 -0.0973 2.4041766 -0.0973 2.4041766 -0.0973 1.01 1.021 13.711.03 7.66 -0.26	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 -0.1068584 -0.110619 -0.1310172 0.0389640.034935 2.8181766 -0.032353 8/19/2019 20.49 4.16 -0.12 0.080.09 15.811.04 7.82 -0.10	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.130392 -0.091413 -0.1880208 0.036738 3.2321766 -0.03212 8/27/2019 20.43 4.94 -0.16 0.020.03 17.691.07 7.94 -0.06	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743 0.0353580.033384 3.5030016 -0.030417 9/3/2019 20.27 5.32 -0.13 0.07 18.92 1.01 8.08 -0.11	8.7574682 2.361602 -0.018606 0.074237 0.005726 8.5844830.434285 3.539996 -0.00431 -0.0607424 -0.079155 -0.053001 -0.1784412 0.075318 3.7140882 0.006045 9/10/2019 20.24 5.46 -0.04 0.17 19.84 19.84 1.00 8.180.01	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.017043 3.8721516 -0.044812 3.8721516 -0.044812 20.06 5.52 -0.18 0.050.09 20.510.98 8.26 -0.13	9.0280002 2.422163 -0.105243 -0.0214630.078897 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.075309 3.9825516 -0.080109 9/25/2019 20.86 5.60 -0.24 -0.050.18 21.071.02 6.85 -0.22	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.021573 0.0120492 —— 0.081978 3.121894 0.02028 —— 4.1015766 0.012552 1.938147 10/9/2019 19.80 5.81 0.01 0.19 —— 0.05 —— 21.75 —— -1.00 3.68 0.05	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016 -0.119816 3.987437 10/18/2019 19.54 5.72 -0.35 -0.170.27 22.231.02 2.07 -0.29	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467 5.201709 10/30/2019 19.57 5.83 -0.09 0.13 22.741.02 1.01 -0.04	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882 0.112724 5.838075 11/8/2019 19.62 5.79 0.20 0.40 0.30 23.140.86 0.70 0.26	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 0.107615 6.181586 Pressure Heading States of the states	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023 4.697493 -0.028353 4.2085266 -0.029862 6.452279 ad (feet H ₂ O) 11/22/2019 19.23 5.77 -0.13 0.100.07 23.610.94 0.27 -0.06	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373 5.217373 -0.038415 4.1643132 -0.034971 6.802233 12/3/2019 18.94 5.65 -0.15 0.06 23.91 23.910.95 0.16 -0.07			0.108153		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 —— 11.128871 —— -0.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735 4.1136516 0.099566 7.00158 12/12/2019 18.97 5.84 -0.03 0.16 6.66 0.23 —— 25.72 —— -0.84 0.19 0.23	3.263522 5.41438 0.115814 12/13/2019 7.54 12.51	4.956661 34.627304 0.280792 0.116682 11.45 11.45 80.02 80.02		8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706 3.6623382 0.123408 7.142578 12/19/2019 19.03 5.74 0.21 0.39 20.52 0.31 109.26 23.95 86.55 -0.77 0.17 0.31	12/20/2019 30.188895 30.188895 21.22 21.22 21.22 21.22 21.22 21.22 21.22 21.22	8.1228692 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224273 32.978922 -0.382484 0.093246 -0.060072 -0.0914312 -0.021349 1.849597 0.052008 6.222546 -0.011583 26.87841 3.5726382 -0.004317 7.201038	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 50.562496 10.078591 32.21951 4 -0.382484 6 -0.002452 8 0.093864 0.0470744 1 0.009216 8 0.049374 2 0.0749808 2 2.275262 3 0.137199 6 6.694866 8 0.092391 27.380682 2 3.5139882 7 0.089115 7.313542 19 1/4/2020 18.79 5.90 0.14 0.35 76.66 0.21 116.84 23.29 74.45 -0.88 -0.01 0.22	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257 6.899866 -0.060216 28.29921 3.5657382 -0.065858 7.335593 1/9/2020 18.52 5.74 -0.21 -0.05 85.79 -0.10 117.03 23.28 74.85 -0.94 0.12 -0.16	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368 7.131106 -0.033384 29.498826 3.5519382 -0.013531 7.338759 1/14/2020 18.52 5.79 -0.12 0.07 90.31 -0.02 117.36 23.26 75.52 -0.95 0.08 -0.02	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.028557 -0.0413028 2.807563 0.030363 7.787106 -0.02655 32.66145 3.5139882 -0.027621 7.267635 1/30/2020 18.38 5.88 -0.12 0.10 96.37 -0.04 117.78 23.29 78.70 -0.96 0.04 -0.03	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601 3.5243382 -0.058974 7.050764 2/25/2020 18.22 -0.02 100.64 -0.13 118.36 23.41 83.88 -1.06 0.04 -0.11
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-33 VWP-41 VWP-41 VWP-41D VWP-43 VWP-47 VWP-47 VWP-47 VWP-47 VWP-47 VWP-48 VWP-48 VWP-8 VWP-9 VWP-9 VWP-9 VWP-9 VWP-18 VWP-18 VWP-18 VWP-19 VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-26 VWP-27 VWP-30 VWP-30 VWP-30 VWP-30 VWP-30 VWP-30 VWP-30 VWP-30		8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.0356340.036486 1.9263516 -0.017259 8/6/2019 20.63 0.34 -0.08 0.060.040.09 -0.040.09 -0.98 7.51 -0.10 -0.29 -0.31	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .121095 -0 .087352 -0 .017043 0058413 -00781516 2.3 .034289 -00781516 2.3 .034289 -0017043 0058413 -00781516 2.3 .034289 -0017043 0058413 -00781516 2.3 .034289 -0077 -0.15 .002011011011011011011011011011011011011011011011011011012011011011011012011012013035028028020		8.866216 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-0.053001 -0.1784412 0.075318 3.7140882 0.006045 9/10/2019 20.24 5.46 -0.04 0.17 0.01 19.84 1.00 8.180.01 -0.18	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.0170430.0468 3.8721516 -0.044812 9/17/2019 20.06 5.52 -0.18 0.050.09 20.510.98 8.26 -0.13 -0.24 -0.30	9.0280002 2.422163 -0.105243 -0.105243 -0.021463 9.116399 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.075309 3.9825516 -0.080109 3.9825516 -0.080109 9/25/2019 20.86 5.60 -0.24 -0.050.181.02 6.85 -0.22 -0.34 -0.37	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.062685 -0.062685 -0.021573 0.0120492 —— 0.081978 3.121894 0.02028 —— 4.1015766 0.012552 1.938147 10/9/2019 19.80 5.81 0.01 0.19 —— 0.05 —— 21.75 —— -1.00 3.68 0.05 -0.09 -0.14	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016 -0.119816 3.987437 10/18/2019 19.54 5.72 -0.35 -0.170.27 22.231.02 2.07 -0.29 -0.48 -0.50	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467 5.201709 10/30/2019 19.57 5.83 -0.09 0.130.03 22.741.02 1.01 -0.04 -0.15 -0.22	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882 0.112724 5.838075 11/8/2019 19.62 5.79 0.20 0.40 0.30 0.30 23.140.86 0.70 0.26 0.13 0.07	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 0.107615 6.181586 Pressure Heiler 11/15/2019 19.50 5.86 0.19 0.37 —— 23.41 —— 23.41 —— -0.80 0.59 0.23 0.11 0.05	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023 4.697493 -0.028353 4.2085266 -0.029862 6.452279 ad (feet H ₂ O) 11/22/2019 19.23 5.77 -0.13 0.100.07 23.610.94 0.27 -0.06 -0.18 -0.25	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373 5.217373 -0.038415 4.1643132 -0.034971 6.802233 12/3/2019 18.94 5.65 -0.15 0.060.07 23.910.95 0.16 -0.07 -0.21 -0.28			0.108153		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 11.1288710.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735 4.1136516 0.099566 7.00158 12/12/2019 18.97 5.84 -0.03 0.16 6.66 0.23 25.720.84 0.19 0.23 -0.09 -0.19 -0.04 0.00	3.263522 5.41438 0.115814	12/16/2019 0.116682 0.116682 11.45 11.45 80.02	6.165193 45.983972 0.426453 2.233695 2.233695 106.26 14.25 106.26	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 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-0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601 3.5243382 -0.058974 7.050764 2/25/2020 18.22 5.96 -0.22 -0.02 100.64 -0.13 118.36 23.41 83.88 -1.06 0.04 -0.11 -0.27 -0.35 3.40 -0.20
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-33 VWP-33 VWP-41 VWP-41D VWP-43 VWP-47 VWP-47 VWP-47 VWP-47 VWP-47 VWP-48 VWP-8 VWP-9 VWP-9 VWP-9 VWP-9 VWP-18 VWP-18 VWP-18 VWP-18 VWP-19 VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-33 VWP-33 VWP-33 VWP-30 VWP-30 VWP-30 VWP-31	2.6406680.39417 3.149094 -0.0795304 -0.097272 -1.67265 0.087249 0.001269	8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.035634 1.9263516 -0.017259 8/6/2019 20.63 0.34 -0.08 0.06 1.1.260.04 11.260.98 7.51 -0.10 -0.29 -0.31 -0.38 -0.13 -0.38 -0.13 0.08	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .121095 -0 .087352 -0 .017043 0058413 -00781516 2.3 .034289 -00781516 2.3 .034289 -0017043 0058413 -00781516 2.3 .034289 -0 .077 -0.15 .00201111.981.00 .7.56 .0.18 .0.31 .0.35 .0.28 .0.200.04	.000752 .664915 .079545 .010298 	8.866216 0.826582 -0.109845 -0.0453880.090986 5.9338040.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.17844120.040956 2.4041766 -0.0973 2.4041766 -0.0973 2.4041766 -0.0973 13.71 13.71 1.03 7.66 -0.26 -0.43 -0.45 -0.25 -0.410.09	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 -0.1068584 -0.110619 -0.1310172 0.0389640.034935 2.8181766 -0.032353 8/19/2019 20.49 4.16 -0.12 0.080.09 15.811.04 7.82 -0.10 -0.25 -0.26 -0.30 0.09	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.130392 -0.091413 -0.1880208 0.0206490.036738 3.2321766 -0.03212 8/27/2019 20.43 4.94 -0.16 0.020.03 17.691.07 7.94 -0.06 -0.29 -0.30 -0.21 -0.43 0.05	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743 3.5030016 -0.030417 9/3/2019 20.27 5.32 -0.13 0.07 18.92 1.01 8.08 -0.11 -0.24 -0.27 -0.20 -0.45 0.08	8.7574682 2.361602 -0.018606 0.074237 0.005726 8.584483 8.5844830.0431 -0.0607424 -0.079155 -0.053001 -0.1784412 0.075318 3.7140882 0.006045 9/10/2019 20.24 5.46 -0.04 0.17 19.84 1.00 8.18 -0.01 -0.18 -0.12 -0.41 0.17	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.017043 3.8721516 -0.044812 3.8721516 -0.044812 9/17/2019 20.06 5.52 -0.18 0.050.09 20.510.98 8.26 -0.13 -0.24 -0.30 -0.24 -0.59 0.04	9.0280002 2.422163 -0.105243 -0.021463 9.116399 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.075309 3.9825516 -0.080109 9/25/2019 20.86 5.60 -0.24 -0.050.18 21.071.02 6.85 -0.22 -0.34 -0.37 -0.31 -0.620.05	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.021573 0.0120492 —— 0.081978 3.121894 0.02028 —— 4.1015766 0.012552 1.938147 10/9/2019 19.80 5.81 0.01 0.19 —— 0.05 —— 21.75 —— 21.75 —— -1.00 3.68 0.05 -0.09 -0.14 -0.05 0.03 —— 0.19	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016 -0.119816 3.987437 10/18/2019 19.54 5.72 -0.35 -0.17 22.23 22.23 22.231.02 2.07 -0.29 -0.48 -0.50 -0.37 -0.350.17	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467 5.201709 10/30/2019 19.57 5.83 -0.09 0.13 22.741.02 1.01 -0.04 -0.15 -0.22 -0.19 -0.04 -0.12	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882 0.112724 5.838075 11/8/2019 19.62 5.79 0.20 0.40 23.14 23.140.86 0.70 0.26 0.13 0.07 0.17 0.25 0.39	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 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-0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257 6.899866 -0.060216 28.29921 3.5657382 -0.065858 7.335593 1/9/2020 18.52 5.74 -0.21 -0.05 85.79 -0.10 117.03 23.28 74.85 -0.94 0.12 -0.16 -0.29 -0.35 -0.25 -0.21 5.59 -0.04	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368 7.131106 -0.033384 29.498826 3.5519382 -0.013531 7.338759 1/14/2020 18.52 5.79 -0.12 0.07 90.31 -0.02 117.36 23.26 75.52 -0.95 0.08 -0.02 -0.17 -0.25 -0.16 -0.11 5.82 0.06	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363 7.787106 -0.02655 32.66145 3.5139882 -0.027621 7.267635 1/30/2020 18.38 5.88 -0.12 0.10 96.37 -0.04 117.78 23.29 78.70 -0.96 0.04 -0.03 -0.96 0.04 -0.03 -0.16 -0.25 -0.07 -0.10 6.49 0.07	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601 3.5243382 -0.058974 7.050764 2/25/2020 18.22 -0.02 100.64 -0.13 118.36 23.41 83.88 -1.06 0.04 -0.11 -0.27 -0.35 3.40 -0.20 7.12 -0.05
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-33 VWP-33 VWP-41 VWP-41 VWP-41 VWP-47 VWP-47 VWP-47 VWP-47 VWP-47 VWP-48 VWP-48 VWP-49 VWP-9 VWP-9 VWP-9 VWP-9 VWP-18 VWP-18 VWP-19 VWP-19 VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-26 VWP-27 VWP-30 VWP-33 VWP-33 VWP-33 VWP-33 VWP-33 VWP-33 VWP-33 VWP-33 VWP-30 VWP-30 VWP-33 VWP-33 VWP-33		8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.035634 1.9263516 -0.017259 8/6/2019 20.63 0.34 -0.08 0.060.040.09 -0.040.09 -0.31 -0.38 -0.13 -0.38 -0.13 -0.38 -0.13	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .121095 -0 .087352 -0 .017043 0058413 -00781516 2.3 .034289 -00781516 2.3 .034289 -0017043 0058413 -00781516 2.3 .034289 -0 .077 -0.15 .00201111.981.00 .7.56 .0.18 .0.31 .0.35 .0.28 .0.200.04		8.866216 0.826582 -0.109845 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-0.19 -0.04 0.00 0.21	3.263522 5.41438 0.115814			8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706 3.6623382 0.123408 7.142578 12/19/2019 19.03 5.74 0.21 0.39 20.52 0.31 109.26 23.95 86.55 -0.77 0.17 0.31 0.14 0.06 0.18 0.25 3.70	12/20/2019 30.188895 30.188895 21.22 111.33 21.22 3.85	8.1228693 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524796 10.224273 32.978923 -0.382484 0.093246 0.004268 -0.060072 -0.091431 -0.041418 -0.021349 1.849597 0.052008 6.222546 -0.011583 26.87841 3.5726383 -0.004317 7.201038	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 5.50.562496 1.0.078591 1.32.21951 1.4-0.382484 2.0.093864 2.0.0470744 1.0.009216 3.0.049374 2.0.0749808 2.275262 3.0.137199 6.694866 3.0.092391 27.380682 2.3.5139882 7.0.089115 7.313542 2.9 1/4/2020 18.79 5.90 0.14 0.35 76.66 0.21 116.84 23.29 74.45 -0.88 -0.01 0.02 0.11 0.02 0.11 0.07 5.26	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257 6.899866 -0.060216 28.29921 3.5657382 -0.065858 7.335593 1/9/2020 18.52 5.74 -0.21 -0.05 85.79 -0.10 117.03 23.28 74.85 -0.94 0.12 -0.16 -0.29 -0.35 -0.25 -0.21 5.59	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368 7.131106 -0.033384 29.498826 3.5519382 -0.013531 7.338759 1/14/2020 18.52 5.79 -0.12 0.07 90.31 -0.02 117.36 23.26 75.52 -0.95 0.08 -0.02 -0.17 -0.25 -0.16 -0.11 5.82	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363 7.787106 -0.02655 32.66145 3.5139882 -0.027621 7.267635 1/30/2020 18.38 5.88 -0.12 0.10 96.37 -0.04 117.78 23.29 78.70 -0.96 0.04 -0.03 -0.96 0.04 -0.03 -0.16 -0.25 -0.10 6.49	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601 3.5243382 -0.058974 7.050764 2/25/2020 18.22 -0.02 100.64 -0.13 118.36 23.41 83.88 -1.06 0.04 -0.11 -0.27 -0.35 3.40 -0.20 7.12
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-33 VWP-33 VWP-41 VWP-41D VWP-47 VWP-47 VWP-47 VWP-47 VWP-8 VWP-8 VWP-9 VWP-9 VWP-9 VWP-9 VWP-9 VWP-1 VWP-1 VWP-1 VWP-1 VWP-1 VWP-1 VWP-1 VWP-1 VWP-2 VWP-1	2.6406680.39417 3.149094 -0.0795304 -0.097272 -1.67265 0.087249 0.001269	8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.035634 1.9263516 -0.017259 8/6/2019 20.63 0.34 -0.08 0.060.04 11.260.98 7.51 -0.10 -0.29 -0.31 -0.38 -0.13 -0.38 -0.13 0.08	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .186319 5	1900752 1900	8.866216 0.826582 -0.109845 -0.0453880.090986 5.9338040.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.17844120.040956 2.4041766 -0.0973 2.4041766 -0.0973 13.71 13.71 13.71 1.03 7.66 -0.26 -0.43 -0.45 -0.25 -0.410.090.210.090.210.09	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 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-0.119816 3.987437 10/18/2019 19.54 5.72 -0.35 -0.17 22.231.02 2.07 -0.29 -0.48 -0.50 -0.37 -0.350.17 9.91 -0.26	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467 5.201709 10/30/2019 19.57 5.83 -0.09 0.13 22.741.02 1.01 -0.04 -0.15 -0.22 -0.19 -0.04 0.12 9.40 -0.02 0.12	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882 0.112724 5.838075 11/8/2019 19.62 5.79 0.20 0.40 23.140.86 0.70 0.26 0.13 0.07 0.17 0.25 0.39 9.07 0.28 0.39 9.07 0.28	8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 0.107615 6.181586 Pressure Head State of the state o	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 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VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-30 VWP-33 VWP-33 VWP-41 VWP-41 VWP-41 VWP-47 VWP-47 VWP-47 VWP-8 VWP-9 VWP-9 VWP-9 VWP-9 VWP-9 VWP-9 VWP-1 VWP-1 VWP-1 VWP-1 VWP-1 VWP-1 VWP-1 VWP-20 VWP-1 VWP-20 VWP-25 VWP-26 VWP-27 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-44 VWP-47 VWP-47 VWP-47 VWP-47 VWP-40 VWP-40 VWP-41 VWP-41 VWP-41 VWP-41 VWP-41 VWP-43 VWP-43 VWP-43 VWP-43 VWP-43 VWP-44 VWP-44		8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.035634 1.9263516 -0.017259 8/6/2019 20.63 0.34 -0.08 0.06 1.1.26 11.260.98 7.51 -0.10 -0.29 -0.31 -0.38 -0.13 -0.38 -0.13 -0.080.080.080.080.080.080.080.080.080.080.09 -0.31 -0.38 -0.130.080.080.09 -0.040.09 -0.31 -0.38 -0.080.0080.0080.0080.0080.0080.0080.0080.0080.0080.0080.0080.008	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .186319 5		8.866216 0.826582 -0.109845 -0.0453880.090986 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0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.021573 0.0120492 —— 0.081978 3.121894 0.02028 —— 4.1015766 0.012552 1.938147 10/9/2019 19.80 5.81 0.01 0.19 —— 0.05 —— 21.75 —— -1.00 3.68 0.05 -0.09 -0.14 -0.05 0.03 —— 0.19 7.21 0.05 —— 9.48 0.03	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016 -0.119816 3.987437 10/18/2019 19.54 5.72 -0.35 -0.170.27 22.231.02 2.07 -0.29 -0.48 -0.50 -0.37 -0.350.17 9.91 -0.26 9.59 -0.28	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467 5.201709 10/30/2019 19.57 5.83 -0.09 0.130.03 22.741.02 1.01 -0.04 -0.15 -0.22 -0.19 -0.04 0.12 9.40 0.12 9.40 0.12 9.40 0.12 9.40 0.02 9.69 9.69 9.69 9.69 9.69	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 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-0.09 9.62 -0.08		12/5/2019 0.114825 0.114825 0.115 0.27 0.27	0.108153		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 11.1288710.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735 4.1136516 0.099566 7.00158 12/12/2019 18.97 5.84 -0.03 0.16 6.66 0.23 25.720.84 0.19 0.23 -0.09 -0.19 -0.04 0.00 0.21 0.17 13.05 0.03 0.33 9.51 0.23	3.263522 5.41438 0.115814	12/16/2019	6.165193 45.983972 0.426453 2.233695 14.25 106.26 14.25 106.26 10.99 0.99 5.16	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706 3.6623382 0.123408 7.142578 12/19/2019 19.03 5.74 0.21 0.39 20.52 0.31 109.26 23.95 86.55 -0.77 0.17 0.31 0.14 0.06 0.18 0.25 3.70 0.38 13.84 0.26 76.88 8.46 0.29	12/20/2019 30.188895 31.133 21.22 21.22 31.8895 21.22 31.33 21.22 33.85 33.85	8.1228693 2.467747 -0.02127 0.045527 13.47417 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-0.27 -0.35 3.40 -0.20 7.12 -0.05 20.39 -0.15 83.32 83.14 -0.14
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-33 VWP-33 VWP-33D VWP-41 VWP-41 VWP-41D VWP-47 VWP-47 VWP-47 VWP-47 VWP-8 VWP-8 VWP-9 VWP-9 VWP-9 VWP-9 VWP-18 VWP-18 VWP-18 VWP-19 VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-30 VWP-40 VWP-10 VW		8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.035634 1.9263516 -0.017259 8/6/2019 20.63 0.34 -0.08 0.060.041.260.98 7.51 -0.10 -0.29 -0.31 -0.38 -0.13 -0.38 -0.13 -0.38 -0.13 -0.38 -0.13 -0.38 -0.13 -0.38 -0.08	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .186319 5	.000752 .664915 .079545 .010298 	8.866216 0.826582 -0.109845 -0.0453880.090986 5.9338040.4443 3.312916 -0.111136 -0.1871344 -0.194625 -0.108873 -0.17844120.040956 2.4041766 -0.0973 2.4041766 -0.0973 2.4041766 -0.0973 13.711.03 7.66 -0.25 -0.101.03 7.66 -0.26 -0.43 -0.45 -0.25 -0.410.090.210.210.210.25 -0.410.090.210.25 -0.410.09	8.8653932 1.801483 -0.049899 0.0327670.037449 6.8417880.449324 3.385906 -0.043939 -0.1068584 -0.110619 -0.1310172 0.0389640.034935 2.8181766 -0.032353 8/19/2019 20.49 4.16 -0.12 0.080.09 15.811.04 7.82 -0.10 -0.25 -0.26 -0.26 -0.30 0.090.090.090.090.090.090.25 -0.26 -0.300.090.090.090.090.090.090.090.080.08	8.8394912 2.137881 -0.068016 0.0104370.014998 7.6561710.462681 3.43781 -0.024986 -0.1239384 -0.130392 -0.091413 -0.1880208 0.0206490.036738 3.2321766 -0.03212 8/27/2019 20.43 4.94 -0.16 0.020.031.07 7.94 -0.06 -0.29 -0.30 -0.21 -0.43 0.050.080.08	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743 0.035358 3.5030016 -0.030417 9/3/2019 20.27 5.32 -0.13 0.07 18.92 1.01 8.08 -0.11 -0.24 -0.27 -0.20 -0.45 0.08 0.08 0.08 0.08 0.08 0.08	8.7574682 2.361602 -0.018606 0.074237 	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.017043 3.8721516 -0.044812 3.8721516 -0.044812 20.06 5.52 -0.18 0.050.09 20.510.98 8.26 -0.13 -0.24 -0.30 -0.24 -0.59 0.04 1.004	9.0280002 2.422163 -0.105243 -0.0214630.078897 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.075309 3.9825516 -0.080109 9/25/2019 20.86 5.60 -0.24 -0.050.18 21.071.02 6.85 -0.22 -0.34 -0.37 -0.31 -0.620.050.0770.0770.0770.0770.0770.0770.0770.0770.0770.077	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.021573 0.0120492 —— 0.081978 3.121894 0.02028 —— 4.1015766 0.012552 1.938147 10/9/2019 19.80 5.81 0.01 0.19 —— 0.05 —— 21.75 —— 21.75 —— -1.00 3.68 0.05 -0.09 -0.14 -0.05 0.03 —— 0.19 7.21 0.05 —— 9.48	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016 -0.119816 3.987437 10/18/2019 19.54 5.72 -0.35 -0.170.27 22.231.02 2.07 -0.29 -0.48 -0.50 -0.37 -0.350.17 9.91 -0.26 9.59	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467 5.201709 10/30/2019 19.57 5.83 -0.09 0.130.03 22.741.02 1.01 -0.04 -0.15 -0.02 -0.12 9.69	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882 0.112724 5.838075 11/8/2019 19.62 5.79 0.20 0.40 0.30 23.140.86 0.70 0.26 0.13 0.07 0.17 0.25 0.39 9.07 0.28 0.39 9.07 0.28 0.39 9.07 0.28 0.39 9.07	11/15/2019 8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 0.107615 6.181586 Pressure Heat 1/15/2019 19.50 5.86 0.19 0.37 —— 0.27 —— 23.41 —— -0.80 0.59 0.23 0.11 0.05 0.15 0.24 —— 0.37 9.98 0.25 —— 9.75 0.25 14.28	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023 4.697493 -0.028353 4.2085266 -0.029862 6.452279 ad (feet H ₂ O) 11/22/2019 19.23 5.77 -0.13 0.10 23.61 23.610.94 0.27 -0.06 -0.18 -0.25 -0.13 -0.09 23.610.94 0.27 -0.06 -0.18 -0.25 -0.13 -0.09 23.610.94 0.27 -0.06 -0.18 -0.25 -0.13 -0.09 0.09 10.85 -0.07 9.73 -0.07 14.91	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373 5.217373 -0.038415 4.1643132 -0.034971 6.802233 12/3/2019 18.94 5.65 -0.15 0.06 23.91 23.91 23.910.95 0.16 -0.07 -0.21 -0.28 -0.16 -0.07 -0.21 -0.28 -0.16 -0.07 -0.21 -0.28 -0.16 -0.07 -0.21 -0.28 -0.16 -0.09 9.62 -0.08 15.72			0.108153 0.13962 0.169716 0.169716 0.25 0.25 0.32 0.32 0.39		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 11.1288710.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735 4.1136516 0.099566 7.00158 12/12/2019 18.97 5.84 -0.03 0.16 6.66 0.23 25.720.84 0.19 0.23 -0.09 -0.19 -0.04 0.00 0.21 0.17 13.05 0.03 0.33 9.51	3.263522 5.41438	12/16/2019 0.116682 0.116682 1.45		8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706 3.6623382 0.123408 7.142578 12/19/2019 19.03 5.74 0.21 0.39 20.52 0.31 109.26 23.95 86.55 -0.77 0.17 0.31 0.14 0.06 0.18 0.25 3.70 0.38 13.84 0.26 76.88 8.46	12/20/2019	8.1228693 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224273 32.978923 -0.382484 0.093246 0.004268 -0.060072 -0.091431 -0.021349 1.849597 0.052008 6.222546 -0.011583 26.87841 3.5726383 -0.004317 7.201038 12/24/201 18.77 5.70 -0.05 0.11 31.14 0.01 114.44 23.63 76.21 -0.88 0.22 0.01 -0.14 -0.21 -0.10 -0.05 4.27 0.12 14.38 -0.03 62.11 8.26	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 5.50.562496 1.0.078591 1.32.21951 1.40.382484 2.0.093864 2.0.0470744 1.0.009216 3.0.049374 2.0.0749808 2.275262 3.0.137199 3.6.694866 3.0.092391 27.380682 2.3.5139882 7.0.089115 7.313542 2.9.74.45 2.9.74.45 2.0.21 2.0.11 2.0.02 2.11 2.0.02 2.11 2.0.02 2.11 2.0.02 2.11 2.0.02 2.11 2.0.02 2.11 2.0.02 2.11 2.0.02 2.11 2.0.02 2.11 2.0.02 2.11 2.0.02 2.11 2.0.02 2.11 2.0.02 2.11 2.12 3.29 3.21 3.21 3.21 3.21 3.21 3.21 3.22 3.23 3.21 3.23 3.21 3.23 3.21 3.23 3.21 3.23 3.23	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257 6.899866 -0.060216 28.29921 3.5657382 -0.065858 7.335593 1/9/2020 18.52 5.74 -0.21 -0.05 85.79 -0.10 117.03 23.28 74.85 -0.94 0.12 -0.16 -0.29 -0.35 -0.25 -0.21 5.59 -0.04 15.94 -0.14 65.39 8.24	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368 7.131106 -0.033384 29.498826 3.5519382 -0.013531 7.338759 1/14/2020 18.52 5.79 -0.12 0.07 90.31 -0.02 117.36 23.26 75.52 -0.95 0.08 -0.02 -0.17 -0.25 -0.16 -0.11 5.82 0.06 16.48 -0.08 68.17 8.21	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363 7.787106 -0.02655 32.66145 3.5139882 -0.027621 7.267635 1/30/2020 18.38 5.88 -0.12 0.10 96.37 -0.04 117.78 23.29 78.70 -0.96 0.04 -0.03 -0.16 -0.25 -0.07 -0.10 6.49 0.07 17.99 -0.06 75.47 8.12	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601 3.5243382 -0.058974 7.050764 2/25/2020 18.22 5.96 -0.22 -0.02 100.64 -0.13 118.36 23.41 83.88 -1.06 0.04 -0.11 -0.27 -0.35 3.40 -0.20 7.12 -0.05 20.39 -0.15 83.32 8.14
VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-30 VWP-33 VWP-33 VWP-41 VWP-41 VWP-41 VWP-47 VWP-47 VWP-47 VWP-8 VWP-9 VWP-9 VWP-9 VWP-9 VWP-9 VWP-9 VWP-1 VWP-1 VWP-1 VWP-1 VWP-1 VWP-1 VWP-1 VWP-20 VWP-1 VWP-20 VWP-25 VWP-26 VWP-27 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-44 VWP-47 VWP-47 VWP-47 VWP-47 VWP-40 VWP-40 VWP-41 VWP-41 VWP-41 VWP-41 VWP-41 VWP-43 VWP-43 VWP-43 VWP-43 VWP-43 VWP-44 VWP-44		8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.0356340.036486 1.9263516 -0.017259 8/6/2019 20.63 0.34 -0.08 0.060.040.08 0.060.09 -0.31 -0.38 -0.13 -0.38 -0.13 -0.38 -0.13 -0.38 -0.13 0.080.080.09 -0.31 -0.38 -0.130.080.080.09 -0.31 -0.38 -0.130.080.09 -0.31 -0.38 -0.130.080.080.080.09 -0.130.080.09 -0.10 -0.29 -0.31 -0.38 -0.130.080.080.09	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0 .186319 5434274 -0 .272366 3075833 -0 .121095 -0 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-0.03212 8/27/2019 20.43 4.94 -0.16 0.020.031.07 7.94 -0.06 -0.29 -0.30 -0.21 -0.431.07 7.94 -0.06 -0.29 -0.30 -0.21 -0.430.050.080.08	8.7732972 2.301181 -0.058134 0.0311720.030541 8.1897810.437627 3.496202 -0.045662 -0.103442 -0.117036 -0.087921 -0.194743 0.0353580.033384 3.5030016 -0.030417 9/3/2019 20.27 5.32 -0.13 0.07 18.921.01 8.08 -0.11 -0.24 -0.27 -0.20 -0.45 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.09	8.7574682 2.361602 -0.018606 0.074237 0.005726 8.5844830.434285 3.539996 -0.00431 -0.0607424 -0.079155 -0.053001 -0.1784412 0.075318 3.7140882 0.006045 9/10/2019 20.24 5.46 -0.04 0.17 0.01 19.84 0.01 19.84 0.01 0.01 0.01 19.84 0.01	8.6812012 2.389503 -0.076251 0.0200070.039176 8.8758510.42593 3.57568 -0.057723 -0.1034424 -0.128565 -0.103635 -0.2540232 0.017043 3.8721516 -0.0468 3.8721516 -0.044812 9/17/2019 20.06 5.52 -0.18 0.050.09 20.510.98 8.26 -0.13 -0.24 -0.30 -0.24 -0.59 0.04 0.04 0.09 20.510.98 8.26 -0.13 -0.24 -0.590.09	9.0280002 2.422163 -0.105243 -0.021463 9.116399 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.075309 3.9825516 -0.080109 9/25/2019 20.86 5.60 -0.24 -0.050.181.02 6.85 -0.22 -0.34 -0.37 -0.31 -0.620.050.050.17 9.20 -0.19	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.021573 0.0120492 —— 0.081978 3.121894 0.02028 —— 4.1015766 0.012552 1.938147 10/9/2019 19.80 5.81 0.01 0.19 —— 0.05 —— 21.75 —— -1.00 3.68 0.05 -0.09 -0.14 -0.05 0.03 —— 0.19 7.21 0.05 —— 0.19 7.21 0.05 —— 9.48 0.03 4.48	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016 -0.119816 3.987437 10/18/2019 19.54 5.72 -0.35 -0.170.27 22.231.02 2.07 -0.29 -0.48 -0.50 -0.37 -0.350.17 9.91 -0.26 9.59 -0.28 9.21	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 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10.85 -0.07 9.73 -0.09 14.91	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373 5.217373 -0.038415 4.1643132 -0.034971 6.802233 12/3/2019 18.94 5.65 -0.15 0.06 23.91 23.91 23.910.95 0.16 -0.07 -0.21 -0.28 -0.16 -0.11 0.05 12.06 -0.09 9.62 -0.08 15.72		12/5/2019	0.108153 0.13962 0.169716 0.25 0.25 0.32 0.32 0.39 0.39		8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 11.1288710.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735 4.1136516 0.099566 7.00158 12/12/2019 18.97 5.84 -0.03 0.16 6.66 0.23 25.720.84 0.19 0.23 -0.09 -0.19 -0.04 0.00 0.21 0.17 13.05 0.03 0.33 9.51 0.23 16.18	3.263522 5.41438	12/16/2019 0.116682 0.1145 11.45 11.45 0.65 0.27 0.27 0.27 0.27 0.27 0.27 0.27 0.27 0.27 0.27 0.27 0.27 0.27		8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706 3.6623382 0.123408 7.142578 12/19/2019 19.03 5.74 0.21 0.39 20.52 0.31 109.26 23.95 86.55 -0.77 0.17 0.31 0.14 0.06 0.18 0.25 3.70 0.38 13.84 0.26 76.88 8.46 0.29 16.51	12/20/2019	8.1228693 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524796 10.224273 32.978923 -0.382484 0.093246 0.004268 -0.060072 -0.091431 -0.041418 -0.021349 1.849597 0.05208 6.222546 -0.011583 26.87841 3.5726383 -0.004317 7.201038 12/24/201 18.77 5.70 -0.05 0.11 31.14 0.01 114.44 23.63 76.21 -0.88 0.22 0.01 -0.14 -0.21 -0.10 -0.05 4.27 0.12 14.38 -0.03 62.11 8.26 -0.01 16.64	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 5.50.562496 5.10.078591 1.32.21951 1.4-0.382484 6.0.093864 1.0.009216 1.0.0749808 1.0.092391 1.0.092391 1.0.092391 1.0.089115 1.0.17 1.0.17 1.0.17 1.0.17 1.0.17 1.0.22 1.0.11 1.0.17 1.0.21	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 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VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-33 VWP-41 VWP-41 VWP-41 VWP-47 VWP-47 VWP-8 VWP-9 VWP-9 VWP-9 VWP-9 VWP-9 VWP-1 VWP-1 VWP-1 VWP-1 VWP-1 VWP-1 VWP-1 VWP-1 VWP-20 VWP-1 VWP-20 VWP-25 VWP-26 VWP-27 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-19 VWP-19 VWP-19 VWP-19 VWP-20 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-41 VWP-41 VWP-41 VWP-41 VWP-41 VWP-47 VWP-47 VWP-47 VWP-47		8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.035634 1.9263516 -0.017259 8/6/2019 20.63 0.34 -0.08 0.06 1.1.260.98 7.51 -0.10 -0.29 -0.31 -0.38 -0.13 -0.38 -0.38 -0.13 -0.38 -	8.922337 8. 0.176508 00.053193 -0 0.013627 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .121095 -0 .087352 -0 .017043 0058413 -00781516 2.: .034289 -00781516 2.: .034289 -0017043 0058413 -00781516 2.: .034289 -00781516 2.: .034289 -00781516 2.: 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0.040.11 8.95 -0.100.11 8.95 -0.100.11 8.95 -0.100.110.110.110.110.110.110.110.11	9.0280002 2.422163 -0.105243 -0.105243 -0.021463 9.116399 9.1163990.44264 2.962564 -0.093906 -0.148308 -0.161505 -0.133317 -0.26736120.075309 3.9825516 -0.080109 9/25/2019 20.86 5.60 -0.24 -0.050.181.02 6.85 -0.22 -0.34 -0.37 -0.31 -0.620.050.050.050.171.02 6.85 -0.22 -0.34 -0.37 -0.31 -0.620.050.050.170.050.170.050.170.050.170.050.17	8.5689592 2.513611 0.004113 0.082212 —— 0.021269 —— 9.412849 —— -0.430943 1.593596 0.019812 -0.0394536 -0.062685 -0.021573 0.0120492 —— 0.081978 3.121894 0.02028 —— 4.1015766 0.012552 1.938147 10/9/2019 19.80 5.81 0.01 0.19 —— 0.05 —— 21.75 —— -1.00 3.68 0.05 -0.09 -0.14 -0.05 0.03 —— 0.19 7.21 0.05 —— 9.48 0.03 4.48	8.4544554 2.476052 -0.150705 -0.0740980.118618 9.6195170.439298 0.897758 -0.12492 -0.2055872 -0.215676 -0.161892 -0.15097080.074532 4.289133 -0.110526 4.1516016 -0.119816 3.987437 10/18/2019 19.54 5.72 -0.35 -0.170.27 22.231.02 2.07 -0.29 -0.48 -0.50 -0.37 -0.350.17 9.91 -0.26 9.59 -0.28 9.21	8.4702844 2.523409 -0.039702 0.0566920.011031 9.8397370.439298 0.43711 -0.016371 -0.0638232 -0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467 5.201709 10/30/2019 19.57 5.83 -0.09 0.130.03 22.741.02 1.01 -0.04 -0.15 -0.22 -0.19 -0.04 -0.15 -0.22 -0.19 -0.04 0.12 9.40 0.12 9.40 0.12 9.40 0.12 9.40 0.12 9.40 0.12 9.40 0.12 9.40 0.12 9.40 0.12	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882 0.112724 5.838075 11/8/2019 19.62 5.79 0.20 0.40 0.30 23.140.86 0.70 0.26 0.13 0.07 0.17 0.25 0.39 9.07 0.17 0.25 0.39 9.07 0.17 0.25 0.39 9.07 0.17 0.25 0.39 9.07 0.17 0.25 0.39 9.07 0.17 0.25 0.39 9.07 0.28 9.75 0.26 13.49	8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 0.107615 6.181586 Pressure Head State of Control of Contr	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023 4.697493 -0.028353 4.2085266 -0.029862 6.452279 ad (feet H ₂ O) 11/22/2019 19.23 5.77 -0.13 0.100.07 23.610.94 0.27 -0.06 -0.18 -0.25 -0.13 -0.09 0.09 10.85 -0.07 9.73 -0.09 0.09 10.85 -0.07 9.73 -0.07 14.91 ser Elevation (final part of the part of	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373 5.217373 -0.038415 4.1643132 -0.034971 6.802233 12/3/2019 18.94 5.65 -0.15 0.06 23.91 20.05 12.06 -0.07 -0.21 -0.28 -0.16 -0.07 -0.21 -0.28 -0.16 -0.09 9.62 -0.08 15.72		12/5/2019	12/6/2019 0.32 0.39 0.30	12/9/2019	8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 11.1288710.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735 4.1136516 0.099566 7.00158 12/12/2019 18.97 5.84 -0.03 0.16 6.66 0.23 25.720.84 0.19 0.23 -0.09 -0.19 -0.04 0.00 0.21 0.17 13.05 0.03 0.33 9.51 0.23 16.18	3.263522 5.41438	12/16/2019	6.165193 45.983972 0.426453 2.233695 2.233695 106.26 14.25 106.26 14.25 106.26 14.25 106.26 14.25 106.26 14.25 106.26 106.26	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706 3.6623382 0.123408 7.142578 12/19/2019 19.03 5.74 0.21 0.39 20.52 0.31 109.26 23.95 86.55 -0.77 0.17 0.31 0.14 0.06 0.18 0.25 3.70 0.38 13.84 0.26 76.88 8.46 0.29 16.51	12/20/2019	8.1228693 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224273 32.978923 -0.382484 0.093246 0.004268 -0.060072 -0.091431 -0.041418 -0.021349 1.849597 0.052008 6.222546 -0.011583 26.87841 3.5726383 -0.004317 7.201038 0 12/24/201 18.77 5.70 -0.05 0.11 31.14 0.01 114.44 23.63 76.21 -0.88 0.22 0.01 -0.14 -0.21 -0.10 -0.05 4.27 0.12 14.38 -0.03 62.11 8.26 -0.01 16.64	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 5.50.562496 5.10.078591 1.32.21951 1.4.0.382484 6.0.093864 1.0.009216 1.0.009216 1.0.0749808 1.0.092391 1.0.092391 1.0.089115 1.0.089115 1.0.089115 1.0.089115 1.0.089115 1.0.089115 1.0.089115 1.0.092 1.0.14 1.0.35 1.0.66 1.0.21 1.0.17 1.0.17 1.0.17 1.0.22 1.0.11 1.0.17 1.0.22 1.0.11 1.0.17 1.0.22 1.0.11 1.0.17 1.0.22 1.0.11 1.0.17 1.0.22 1.0.11 1.0.17 1.0.22 1.0.11 1.0.17 1.0.22 1.0.11 1.0.17 1.0.22 1.0.11 1.0.17 1.0.22 1.0.11 1.0.17 1.0.22 1.0.11 1.0.22 1.0.21 1.0.	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257 6.899866 -0.060216 28.29921 3.5657382 -0.065858 7.335593 1/9/2020 18.52 5.74 -0.21 -0.05 85.79 -0.10 117.03 23.28 74.85 -0.94 0.12 -0.16 -0.29 -0.35 -0.25 -0.21 5.59 -0.04 15.94 -0.14 65.39 8.24 -0.15 16.95	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 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VWP-1 VWP-8 VWP-8 VWP-9 VWP-9D VWP-18 VWP-18D VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-33 VWP-33D VWP-41 VWP-41D VWP-43 VWP-47 VWP-47 VWP-47 VWP-8 VWP-9 VWP-9 VWP-9 VWP-9 VWP-9 VWP-18 VWP-18 VWP-18 VWP-18 VWP-19 VWP-20 VWP-25 VWP-26 VWP-27 VWP-30 VWP-10		8.929532 0.148887 -0.033429 0.0279820.017939 4.8716660.42593 3.25128 -0.041373 -0.123938 -0.133506 -0.162999 -0.05623 0.035634 1.9263516 -0.017259 8/6/2019 20.63 0.34 -0.08 0.06 1.1.260.98 7.51 -0.10 -0.29 -0.31 -0.38 -0.13 -0.38 -0.13 -0.38 -0.13 -0.38 -0.13 -0.38 -0.13 -0.38 -0.13 -0.38 -0.13 -0.38 -0.13 -0.38 -0.08	8.922337 8. 0.176508 0. 0.013627 0. 0.013627 00.033995 -0 5.032596 50.430932 -0 3.261012 30.062892 -0 -0.130313 -0 -0.143388 -0 -0.131571 -0 -0.07105 -0 0.018984 0	915142 8. 331783 0063075 -0 .010437 -0 .049025 -0186319 5434274 -0 .272366 3075833 -0 .134186 -0 .15327 -0 .121095 -0 .087352 -0 .017043 0058413 -00781516 2.3 .034289 -00781516 2.3 .034289 -0017043 0058413 -00781516 2.3 .034289 -0017043 0034289 -0017043 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-0.095445 -0.083322 -0.0154212 0.052008 4.066093 -0.009906 4.1947266 -0.015467 5.201709 10/30/2019 19.57 5.83 -0.09 0.13 22.741.02 1.01 -0.04 -0.15 -0.02 -0.04 -0.15 -0.22 -0.19 -0.04 0.12 9.40 -0.02 9.69 -0.04 12.02	8.4918694 2.505446 0.086124 0.171532 0.128856 10.0159130.374129 0.302484 0.112854 0.0552792 0.029907 0.075564 0.1061028 0.167169 3.923266 0.119223 4.2177882 0.112724 5.838075 11/8/2019 19.62 5.79 0.20 0.40 0.30 23.140.86 0.70 0.26 0.13 0.07 0.17 0.25 0.39 9.07 0.28 0.39 9.07 0.28 0.39 9.07 0.28 0.39 9.07 0.28 0.39 9.07 0.28 0.39 9.07 0.28 0.39 9.07 0.28 0.39 9.07 0.28 0.39 9.07 0.28 0.39 9.07 0.28 0.39 9.07 0.28 0.39 9.07	8.4365712 2.53484 0.081183 0.160367 —— 0.116254 —— 10.132368 —— -0.344051 0.253824 0.099913 0.0467392 0.021672 0.065727 0.1024512 —— 0.160233 4.318506 0.107484 —— 4.2195132 0.107615 6.181586 Pressure Heat 1/15/2019 19.50 5.86 0.19 0.37 —— 23.41 —— 23.41 —— -0.80 0.59 0.23 0.11 0.05 0.15 0.24 —— 0.37 9.98 0.25 —— 10.37 9.98 0.25 —— 0.37 9.98 0.25 —— 0.37 9.98 0.25 —— 0.37 9.98 0.25 —— 0.37 9.98 0.25 —— 0.37 9.98 0.25 —— 0.27 —— 0.37 9.98 0.25 —— 0.37	11/22/2019 8.3214512 2.498774 -0.054864 0.0439320.030028 10.2158050.407549 0.115954 -0.027589 -0.0762368 -0.109908 -0.055386 -0.0391332 0.037023 4.697493 -0.028353 4.2085266 -0.029862 6.452279 ad (feet H ₂ O) 11/22/2019 19.23 5.77 -0.13 0.10 23.61 23.61 23.61 20.94 0.27 -0.06 -0.18 -0.94 0.27 -0.06 -0.18 -0.25 -0.13 -0.09 23.61 23.61 20.94 0.27 -0.06 -0.18 -0.25 -0.13 -0.09 23.61 23.61 20.94 0.27 -0.06 -0.18 -0.25 -0.13 -0.09 23.61 23.61 20.94 0.27 -0.06 -0.18 -0.25 -0.13 -0.09 23.61 23.61 20.94 0.27 -0.06 -0.18 -0.25 -0.13 -0.09 23.610.94 0.27 -0.06 -0.18 -0.25 -0.13 -0.09 0.09 10.85 -0.07 9.73 -0.07	8.194203 2.445025 -0.063099 0.0247920.032456 10.3479370.412562 0.068916 -0.031915 -0.0920664 -0.121437 -0.067608 -0.0457488 0.020373 5.217373 -0.038415 4.1643132 -0.034971 6.802233 12/3/2019 18.94 5.65 -0.15 0.06 23.91 23.91 23.910.95 0.16 -0.07 -0.21 -0.28 -0.16 -0.07 -0.21 -0.28 -0.16 -0.07 -0.21 -0.28 -0.16 -0.07 -0.21 -0.28 -0.16 -0.07 -0.21 -0.28 -0.16 -0.07 -0.21 -0.28 -0.16 -0.07 -0.21 -0.28 -0.16 -0.07 -0.21 -0.28 -0.16 -0.07 -0.21 -0.28 -0.16 -0.07 -0.21 -0.28 -0.16 -0.07 -0.21 -0.28 -0.16 -0.07 -0.21 -0.28 -0.16 -0.11	12/4/2019 12/4/2019 12/4/2019	12/5/2019 12/5/2019 12/5/2019	12/6/2019 12/6/2019 12/6/2019	12/9/2019 12/9/2019 12/9/2019	8.2092092 2.528308 -0.012042 0.069452 2.883792 0.101224 11.1288710.364103 0.083276 0.09819 -0.037868 -0.080082 -0.016974 -0.0012888 0.092399 0.073653 5.645266 0.011895 0.144735 4.1136516 0.099566 7.00158 12/12/2019 18.97 5.84 -0.03 0.16 6.66 0.23 25.720.84 0.19 0.23 -0.09 -0.19 -0.04 0.00 0.21 0.17 13.05 0.03 0.33 9.51 0.23 16.18	3.263522 5.41438	12/16/2019 12/16/2019 12/16/2019	6.165193 45.983972 0.426453 2.233695 2.233695 106.26 14.25 106.26 14.25 106.26 14.25 106.26 106.26 106.26 106.26	8.2336722 2.48585 0.092373 0.168342 8.881088 0.13455 47.281372 10.364877 37.45382 -0.334025 0.075404 0.134373 0.059488 0.026973 0.07731 0.1061028 1.602959 0.163563 5.987879 0.112515 33.269706 3.6623382 0.123408 7.142578 12/19/2019 19.03 5.74 0.21 0.39 20.52 0.31 109.26 23.95 86.55 -0.77 0.17 0.31 0.14 0.06 0.18 0.25 3.70 0.38 13.84 0.26 76.88 8.46 0.29 16.51	12/20/2019 12/20/2019 12/20/2019	8.1228693 2.467747 -0.02127 0.045527 13.47417 0.005025 49.524790 10.224273 32.978923 -0.382484 0.093246 0.004268 -0.060072 -0.091431 -0.021349 1.849597 0.052008 6.222546 -0.011583 26.87841 3.5726383 -0.004317 7.201038 12/24/201 18.77 5.70 -0.05 0.11 31.14 0.01 114.44 23.63 76.21 -0.88 0.22 0.01 -0.14 -0.21 -0.10 -0.05 4.27 0.12 14.38 -0.03 62.11 8.26 -0.01 16.64	8.129448 2.552663 0.060087 0.150797 33.173902 0.091375 5.50.562496 1.0.078591 1.32.21951 1.4.0.382484 2.0.093864 2.0.0470744 1.0.009216 3.0.049374 2.0.0749808 2.275262 3.0.137199 3.6.694866 3.0.092391 27.380682 2.3.5139882 7.0.089115 7.313542 2.9.74,45 2.0.74 2.0.1 2.0.2 2.0.11 2.0.2	8.0135052 2.484077 -0.090444 -0.019868 37.126396 -0.045058 50.6456 10.075203 32.390413 -0.40756 0.051074 -0.068209 -0.123726 -0.150723 -0.107127 -0.089521 2.417801 -0.016257 6.899866 -0.060216 28.29921 3.5657382 -0.065858 7.335593 1/9/2020 18.52 5.74 -0.21 -0.05 85.79 -0.10 117.03 23.28 74.85 -0.94 0.12 -0.16 -0.29 -0.35 -0.25 -0.25 -0.21 5.59 -0.04 15.94 -0.14 65.39 8.24 -0.15 16.95	8.0163832 2.506939 -0.050916 0.029577 39.082831 -0.008791 50.788064 10.06547 32.679413 -0.409209 0.033232 -0.010396 -0.0746512 -0.109548 -0.068715 -0.0495072 2.517705 0.025368 7.131106 -0.033384 29.498826 3.5519382 -0.013531 7.338759 1/14/2020 18.52 5.79 -0.12 0.07 90.31 -0.02 117.36 23.26 75.52 -0.95 0.08 -0.02 -0.17 -0.25 -0.16 -0.11 5.82 0.06 16.48 -0.08 68.17 8.21 -0.03 16.96	7.95389 2.546271 -0.050916 0.043932 41.703832 -0.01864 50.970596 10.077328 34.056105 -0.415904 0.017012 -0.014685 -0.0695272 -0.109368 -0.028557 -0.0413028 2.807563 0.030363 7.787106 -0.02655 32.66145 3.5139882 -0.027621 7.267635 1/30/2020 18.38 5.88 -0.12 0.10 96.37 -0.04 117.78 23.29 78.70 -0.96 0.04 -0.03 -0.16 -0.055 -0.07 -0.10 6.49 0.07 17.99 -0.06 75.47 8.12 -0.06 16.79	7.886257 2.578791 -0.093738 -0.007108 43.550437 -0.054394 51.218424 10.129842 36.30019 -0.45935 0.018634 -0.046579 -0.1173512 -0.15219 1.471257 -0.0865572 3.082299 -0.022641 8.821946 -0.063444 36.05601 3.5243382 -0.058974 7.050764 2/25/2020 18.22 5.96 -0.22 -0.02 100.64 -0.13 118.36 23.41 83.88 -1.06 0.04 -0.11 -0.27 -0.35 3.40 -0.27 -0.35 3.40 -0.20 7.12 -0.05 20.39 -0.15 83.32 8.14 -0.14 16.29

 VWP-9D
 - <th

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506.9

507.1 506.8 506.9 506.9

VWP-9 VWP-9D

506.9 506.8

506.8

506.9

| VWP-18D | | | | | | | | | | | | | | | | | | | | | | | | | | | | 486.5 | 481.9 | 476.2 | 474.5 | 474.8 | 475.5 | 478.7 | 483.9 |
|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| VWP-19 | 510.1 | 510.0 | 510.0 | 510.0 | 510.0 | 510.0 | 510.0 | 509.9 | 510.0 | 510.0 | 510.0 | 510.0 | 510.0 | 510.0 | 510.0 | 510.1 | 510.2 | 510.1 | 510.0 | | | | | 510.2 | | | | 510.2 | | 510.1 | 510.1 | 510.1 | 510.1 | 510.0 | 509.9 |
| VWP-20 | 517.4 | 517.6 | 517.6 | 517.7 | 517.7 | 517.8 | 517.9 | 518.0 | 518.2 | 518.3 | 518.4 | 516.9 | 513.8 | 512.2 | 511.1 | 510.8 | 510.7 | 510.4 | 510.3 | | | | | 510.3 | | | | 510.3 | | 510.3 | 510.1 | 510.2 | 510.2 | 510.1 | 510.1 |
| VWP-25 | | 504.9 | 504.9 | 504.8 | 504.8 | 504.7 | 504.9 | 504.9 | 504.9 | 505.0 | 504.9 | 504.8 | 505.0 | 504.7 | 505.0 | 505.3 | 505.2 | 504.9 | 504.9 | | | | | 505.2 | | | | 505.3 | | 505.0 | 505.2 | 504.8 | 505.0 | 505.0 | 504.9 |
| VWP-26 | 505.8 | 505.7 | 505.7 | 505.7 | 505.6 | 505.6 | 505.8 | 505.7 | 505.8 | 505.9 | 505.8 | 505.7 | 505.9 | 505.5 | 505.9 | 506.1 | 506.1 | 505.8 | 505.8 | | | | | 505.9 | | | | 506.1 | | 505.9 | 506.1 | 505.7 | 505.8 | 505.8 | 505.7 |
| VWP-27 | 519.8 | 519.7 | 519.7 | 519.6 | 519.6 | 519.6 | 519.7 | 519.7 | 519.7 | 519.8 | 519.7 | 519.6 | 519.9 | 519.5 | 519.8 | 520.1 | 520.1 | 519.7 | 519.7 | | | | | 519.8 | | | | 520.1 | | 519.8 | 520.0 | 519.7 | 519.7 | 519.7 | 519.6 |
| VWP-30 | 502.1 | 505.6 | 505.7 | 505.7 | 505.8 | 505.7 | 505.7 | 505.8 | 505.8 | 505.9 | 505.8 | 505.7 | 506.0 | 505.6 | 505.8 | 506.2 | 506.2 | 505.9 | 505.8 | | | | | 506.0 | | | | 506.2 | | 505.9 | 506.1 | 505.8 | 505.8 | 505.9 | 509.4 |
| VWP-33 | | 494.7 | 494.6 | 494.6 | 494.5 | 494.4 | 494.5 | 494.4 | 494.3 | 494.4 | 494.2 | 494.2 | 494.8 | 494.5 | 494.8 | 495.0 | 495.0 | 494.7 | 494.7 | | | | | 494.8 | | | | 495.0 | | 494.8 | 495.0 | 494.6 | 494.7 | 494.7 | 494.6 |
| VWP-33D | | | | | | | | | | | | | | | | | | | | | 401.1 | 401.3 | 400.9 | 401.2 | 401.3 | 401.6 | 402.0 | 404.7 | 404.8 | 405.3 | 406.3 | 406.6 | 406.8 | 407.5 | 408.1 |
| VWP-41 | 496.6 | 496.5 | 496.4 | 496.4 | 496.4 | 496.3 | 496.5 | 496.4 | 496.5 | 496.6 | 496.4 | 496.3 | 496.6 | 496.2 | 496.5 | 496.8 | 496.8 | 496.5 | 496.4 | | | | | 496.6 | | | | 496.8 | | 496.5 | 496.7 | 496.4 | 496.5 | 496.5 | 496.3 |
| VWP-41D | | | | | | | | | | | | | 409.2 | 411.9 | 411.4 | 411.1 | 412.0 | 412.9 | 414.1 | | | | | 415.0 | | | | 415.8 | | 416.4 | 417.5 | 417.9 | 418.5 | 420.0 | 422.4 |
| VWP-43 | 511.5 | 511.4 | 511.4 | 511.4 | 511.4 | 511.3 | 511.4 | 511.4 | 511.4 | 511.5 | 511.4 | 511.3 | 511.5 | 511.2 | 511.5 | 511.8 | 511.7 | 511.4 | 511.4 | | | | | 511.5 | | | | 511.8 | | 511.5 | 511.7 | 511.4 | 511.4 | 511.4 | 511.4 |
| VWP-43D | | | | | | | | | | | | | | | | | | | | 400.4 | 400.3 | 400.4 | 400.0 | 400.3 | 400.0 | 400.3 | 405.2 | 476.9 | 469.8 | 462.1 | 463.3 | 465.4 | 468.2 | 475.5 | 483.3 |
| VWP-44 | | 509.7 | 509.8 | 510.0 | 510.2 | 510.8 | 511.7 | 512.7 | 513.3 | 513.8 | 514.1 | 514.4 | 514.7 | 514.8 | 514.9 | 514.9 | 515.0 | 514.9 | 514.8 | | | | | 514.7 | | | | 513.7 | | 513.5 | 513.3 | 513.4 | 513.4 | 513.3 | 513.3 |
| VWP-47 | | 512.4 | 512.3 | 512.3 | 512.3 | 512.2 | 512.3 | 512.3 | 512.3 | 512.4 | 512.3 | 512.2 | 512.4 | 512.1 | 512.4 | 512.7 | 512.6 | 512.3 | 512.3 | | | | | 512.6 | | | | 512.7 | | 512.4 | 512.6 | 512.2 | 512.4 | 512.3 | 512.3 |
| VWP-47D | | | | | | | | | | | | | 404.5 | 409.2 | 412.0 | 413.5 | 414.3 | 414.9 | 415.7 | | | | | 416.2 | | | | 416.5 | | 416.6 | 416.9 | 417.0 | 417.0 | 416.8 | 416.3 |

* Pressure (P, in psi) calculated using the following linear equation provided by Geokon:

 $P = G(R_1 - R_0) + K(T_1 - T_0) - (S_1 - S_0)$

G = Linear Gauge Factor (psi/digit)

R₁ = Instrument Reading (digits) R₀ = Initial Zero Instrument Reading (digits)

 $T_1 = Temperature Reading (°C)$

T₀ = Initial Zero Temperature Reading (°C)

K = Thermal Factor (psi/°C) S_1 = Measured Barometric pressure (psi)

 S_0 = Intiial Zero Barometric pressure (psi)

Note: Barometric corrections not performed as VWPs are installed in sealed boreholes, per Geokon Model 4500 Series Instruction Manual, p. 6.

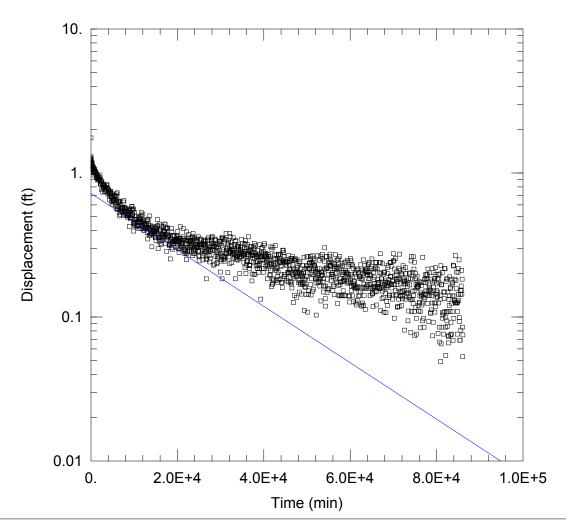
*Note: Values in red represent a zero pressure head. Elevation values in red are associated with the subsurface location of the transducer and should not be considered an inferred groundwater elevation.

May 2020 4-L-3 Revision 0

| | | | | MSW-2400 V | /ibrating Wire Pie | zometer (VWP) Refe | erence Information | n | | |
|---------|----------------------------------|------------------------------|-----------|---------------|----------------------------------|----------------------------------|--------------------------------|-----------------------------------|--------------------------------------|------------------------------|
| VWP ID | Surface
Elevation (ft
MSL) | VWP
Elevation
(ft MSL) | VWP Depth | Serial Number | Factory Zero
Reading (digits) | Factory Zero
Temperature (°C) | Field Zero
Reading (digits) | Field Zero
Temperature
(°C) | Linear Gauge
Factor G (psi/digit) | Thermal Factor K
(psi/°C) |
| VWP-1 | 551.40 | 522.50 | 28.90 | 1921455 | 8572 | 21.2 | 8562.1 | 37.0 | -0.01439 | -0.006162 |
| VWP-3 | 540.90 | 506.60 | 34.30 | 1921444 | 8695 | 22.2 | 8678.0 | 35.7 | -0.01633 | -0.01773 |
| VWP-4 | 549.59 | 527.00 | 22.59 | 1921438 | 8717 | 22.2 | 8707.7 | 31.2 | -0.01647 | -0.00993 |
| VWP-8 | 550.90 | 486.30 | 64.60 | 1921442 | 8691 | 21.9 | 8679.2 | 31.8 | -0.01595 | -0.01724 |
| VWP-8D | 551.00 | 400.00 | 151.00 | 1943860 | 8928 | 21.6 | 8945.6 | 16.3 | -0.01651 | -0.02515 |
| VWP-9 | 535.25 | 506.90 | 28.35 | 1921447 | 8599 | 22.2 | 8593.5 | 28.4 | -0.01727 | -0.01214 |
| VWP-9D | 535.00 | 400.00 | 135.00 | 1943862 | 9086 | 21.9 | 9082.2 | 19.5 | -0.01484 | -0.02584 |
| VWP-18 | 534.60 | 499.60 | 35.00 | 1921452 | 8748 | 21.6 | 8743.9 | 35.8 | -0.01694 | -0.01263 |
| VWP-18D | 535.00 | 400.00 | 135.00 | 1943861 | 9040 | 21.6 | 9034.1 | 17.7 | -0.01445 | -0.02497 |
| VWP-19 | 562.10 | 511.00 | 51.10 | 1921454 | 8816 | 21.7 | 8775.8 | 35.2 | -0.01671 | -0.01660 |
| VWP-20 | 564.55 | 510.10 | 54.45 | 1921440 | 8772 | 21.7 | 8756.1 | 34.3 | -0.01622 | -0.01860 |
| VWP-25 | 533.80 | 505.00 | 28.80 | 1921450 | 8766 | 21.4 | 8759.3 | 28.7 | -0.01723 | -0.00880 |
| VWP-26 | 530.50 | 506.00 | 24.50 | 1921453 | 8649 | 21.5 | 8637.1 | 33.3 | -0.01708 | -0.004576 |
| VWP-27 | 546.70 | 520.00 | 26.70 | 1921446 | 8632 | 22.0 | 8610.2 | 23.6 | -0.01647 | -0.01467 |
| VWP-30 | 544.05 | 506.00 | 38.05 | 1921451 | 8690 | 22.5 | 8676.4 | 31.5 | -0.01746 | -0.01107 |
| VWP-33 | 538.60 | 494.80 | 43.80 | 1921439 | 8627 | 21.9 | 8617.6 | 28.7 | -0.01482 | -0.00794 |
| VWP-33D | 539.00 | 401.00 | 138.00 | 1943866 | 8963 | 21.9 | 8965.6 | 18.4 | -0.01561 | -0.01073 |
| VWP-41 | 534.80 | 496.40 | 38.40 | 1921443 | 8631 | 22.0 | 8627.5 | 27.3 | -0.01665 | -0.01389 |
| VWP-41D | 535.00 | 402.00 | 133.00 | 1933662 | 8996 | 23.2 | 8975.1 | 25.5 | -0.01640 | -0.01493 |
| VWP-43 | 549.50 | 511.50 | 38.00 | 1921441 | 8642 | 21.9 | 8637.0 | 25.4 | -0.01677 | -0.01551 |
| VWP-43D | 549.00 | 400.00 | 149.00 | 1943859 | 8879 | 22.0 | 8888.2 | 18.4 | -0.01536 | -0.02667 |
| VWP-44 | 554.35 | 505.20 | 49.15 | 1921448 | 8781 | 21.4 | 8767.4 | 37.2 | -0.01725 | -0.006366 |
| VWP-47 | 532.60 | 512.40 | 20.20 | 1921449 | 8718 | 21.6 | 8708.8 | 29.0 | -0.01703 | -0.0147 |
| VWP-47D | 532.00 | 400.00 | 132.00 | 1933663 | 8931 | 23.2 | 8923.6 | 22.6 | -0.01583 | -0.01694 |

APPENDIX III-4.M SLUG TEST DATA





PZ-1 SLUG IN TEST

Data Set: M:\Projects\Waco\16216088.00 New LF\Site 50\Aquifer Testing\PZ-1\PZ-1 Slug In Test.aqt

Date: 05/09/19 Time: 15:20:07

PROJECT INFORMATION

Company: SCS Engineers

Client: City of Waco
Project: 16216088.00
Location: Waco, TX
Test Well: PZ-1 Slug In
Test Date: 3/18/2019

AQUIFER DATA

Saturated Thickness: 25.84 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (PZ-1)

Initial Displacement: 1.753 ft

Total Well Penetration Depth: 42.58 ft

Casing Radius: 0.089 ft

Static Water Column Height: 25.84 ft

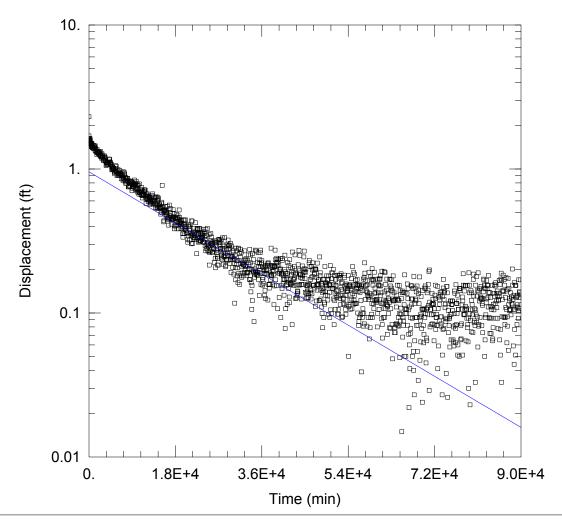
Screen Length: 20. ft
Well Radius: 0.089 ft
Gravel Pack Porosity: 0.

SOLUTION

Aguifer Model: Unconfined

K = Revision 0 2.03E-8 cm/sec Solution Method: Bouwer-Rice

 $^{4-M-2}$ v0 = 0.<u>7208</u> ft



PZ-1 SLUG OUT

Data Set: M:\Projects\Waco\16216088.00 New LF\Site 50\Aquifer Testing\PZ-1\PZ-1 slug out.aqt

Date: 05/09/19 Time: 15:20:58

PROJECT INFORMATION

Company: SCS Engineers

Client: City of Waco
Project: 16216088.00
Location: Waco, TX
Test Well: PZ-1 out
Test Date: 3/20/2019

AQUIFER DATA

Saturated Thickness: 25.84 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (PZ-1 slug out)

Initial Displacement: 2.303 ft Static Water Column Height: 25.84 ft

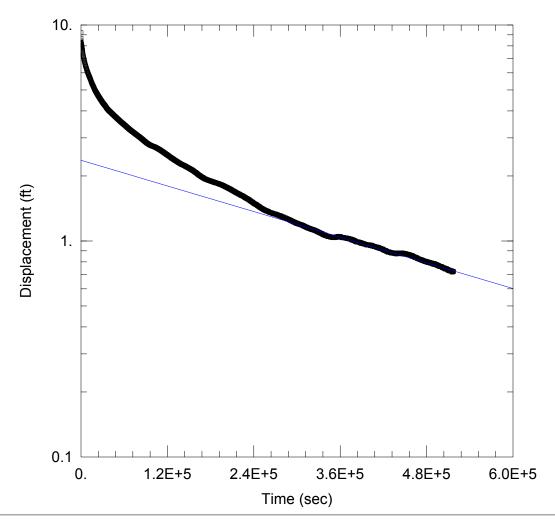
Total Well Penetration Depth: 42.57 ft Screen Length: 20. ft Casing Radius: 0.089 ft Well Radius: 0.089 ft

Gravel Pack Porosity: 0.

SOLUTION

Aquifer Model: <u>Unconfined</u> Solution Method: <u>Bouwer-Rice</u>

K = 2.043E-8 cm/sec 4-M-3 y 0 = 0.955 ftMay 2020



PZ-3 SLUG IN 3.2.2020

Data Set: M:\...\PZ-3 Slug in 3.2.2020.aqt

Date: 03/03/20 Time: 13:12:50

PROJECT INFORMATION

Company: SCS Engineers

Client: City of Waco
Project: 16216088.00
Location: Waco, TX
Test Well: PZ-3 Slug In
Test Date: 2/25/2020

AQUIFER DATA

Saturated Thickness: 14.44 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (PZ-3)

Initial Displacement: 10.51 ft

Total Well Penetration Depth: 47.54 ft

Casing Radius: 0.089 ft

Static Water Column Height: 14.44 ft

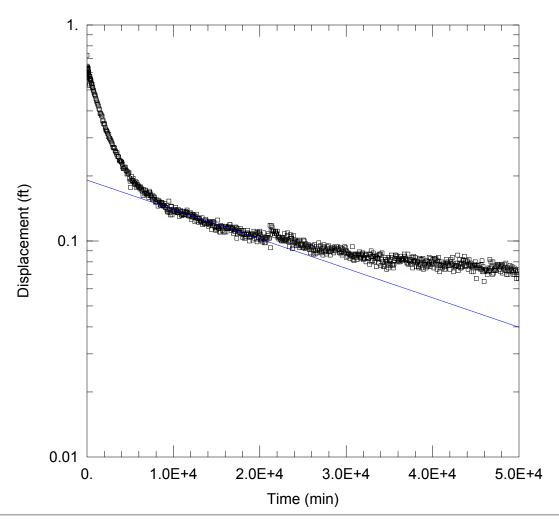
Screen Length: 20. ft
Well Radius: 0.089 ft
Gravel Pack Porosity: 0.

SOLUTION

Aguifer Model: Unconfined

K = Revision 0 K = 6.967E-8 cm/sec Solution Method: Bouwer-Rice

 $^{4-M-4}y0 = 2.363$ ft



PZ-18 SLUG IN TEST

Data Set: M:\Projects\Waco\16216088.00 New LF\Site 50\Aquifer Testing\PZ-18\PZ-18 Slug In.aqt

Date: 05/09/19 Time: 15:58:12

PROJECT INFORMATION

Company: SCS Engineers

Client: City of Waco
Project: 16216088.00
Location: Waco, TX
Test Well: PZ-18
Test Date: 3/18/2019

AQUIFER DATA

Saturated Thickness: 30. ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (PZ-18)

Initial Displacement: 1.016 ft

Total Well Penetration Depth: 48.14 ft

Casing Radius: 0.089 ft

Static Water Column Height: 30. ft

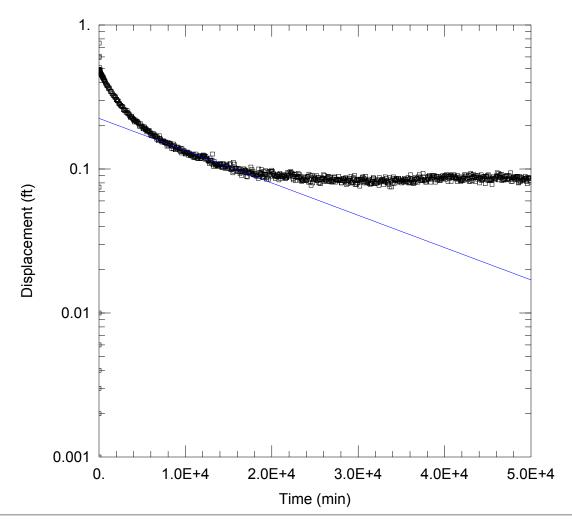
Screen Length: 20. ft
Well Radius: 0.089 ft
Gravel Pack Porosity: 0.

SOLUTION

Aguifer Model: Unconfined

K = Revision 0 K = 1.435E-8 cm/sec Solution Method: Bouwer-Rice

 $^{4-M-5}$ v0 = 0.1914 ft



PZ-18 SLUG OUT

Data Set: M:\Projects\Waco\16216088.00 New LF\Site 50\Aquifer Testing\PZ-18\PZ-18 out.aqt

Date: 05/09/19 Time: 16:00:06

PROJECT INFORMATION

Company: SCS Engineers

Client: City of Waco
Project: 16216088.00
Location: Waco, TX
Test Well: PZ-18
Test Date: 3/20/2019

AQUIFER DATA

Saturated Thickness: 30. ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (PZ-18)

Initial Displacement: 0.0748 ft

Total Well Penetration Depth: 48.14 ft

Static Water Column Height: 30. ft

Casing Radius: 0.089 ft

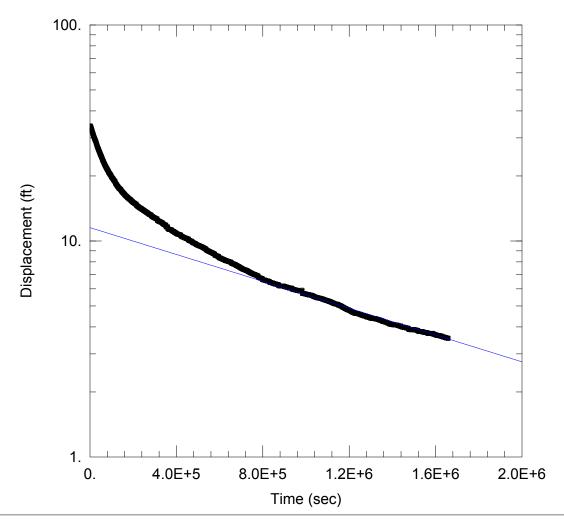
Screen Length: 20. ft
Well Radius: 0.089 ft
Gravel Pack Porosity: 0.

SOLUTION

Aquifer Model: Unconfined

K = Revision 0 E = 2.363E-8 cm/sec Solution Method: Bouwer-Rice

 $^{4-M-6}$ v0 = 0.2245 ft



PZ-20 SLUG IN 3.2.2020

Data Set: M:\...\PZ-20 Slug In 3.2.2020.aqt

Date: 03/03/20 Time: 13:27:52

PROJECT INFORMATION

Company: SCS Engineers

Client: City of Waco
Project: 16216088.00
Location: Waco, TX
Test Well: PZ-20
Test Date: 2/11/2020

AQUIFER DATA

Saturated Thickness: 22.8 ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (PZ-20 Feb 2020)

Initial Displacement: 34.11 ft

Static Water Column Height: 44.2 ft

Total Well Penetration Depth: 67.09 ft Casing Radius: 0.089 ft

Screen Length: 20. ft Well Radius: 0.089 ft

Gravel Pack Porosity: 0.

SOLUTION

Aguifer Model: Unconfined

 $K = \overset{\text{Revision 0}}{2.05E-8} \text{ cm/sec}$

Solution Method: Bouwer-Rice

 $^{4-M-7}$ y0 = 11.53 ft